

A COMPLAT  
T R E A T I S E  
OF PRACTICAL  
NAVIGATION  
Demonstrated from its First  
P R I N C I P L E S  
Together with all the Necessary TABLES.

To which are added,

The Useful Theorems of MENSURATION, SURVEYING and GAUING; with their Application to Navigation, &c.

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Written for the Use of the ACADEMY in  
Tower-Street.

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By ARCHIBALD PATOUN,  
Fellow of the Royal-Society.

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In this Third Edition is added a large Supplement by SAMUEL FULLER.

CONTAINING

dry New Methods of Sailing and Correcting the Errors and Defects in  
several Nautical INSTRUMENTS, &c.

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TO

WILLIAM CLELAND, Esq;

Of Rayhouse *in the County of Essex.*

SIR,

HAVING had the Honour of your Acquaintance for some Time, and considering your Qualifications in this Subject, together with the Obligations I lie under to you, I could not find a more proper Person to patronize this Work:

A 2 Where-

Wherefore, as a grateful Acknowledgment of the many Favours received, I humbly beg leave to dedicate this Piece to you; and am with the greatest Regard

SIR,

*Your most Obliged*

*and*

*most Humble Servant*

ARCHIBALD PATOUN.



# THE P R E F A C E

**H**Ere are so many Books of Nation alre y sent, that it may seem impertinent to trouble the World with a new one; especially since some good Mathematicians both at home and abroad, and many who were perfect Masters of the Practice, have written on this Subject. The former of these being fond of ingenious Speculations, have generally been too prolix on the Theory, and too short on the practical Part. Whereas the latter have in a great Measure neglected the Theory, and not being very solicitous about Language or Method, have delivered the practical Rules in such a Manner, as they cannot be easily comprehended, and much less remembred, especially since there is seldom mention made of the Reasons on which they depend.

But I am very far from finding Fault with all the Books on this Subject; for there are some very full both on Theory and Practice, against which, I have no other Objection, but that they are too tedious to be taught, and too dear to be purchased by most People.

## The P R E F A C E.

Youth ought to learn the Elements from shorter Treatises, and afterwards at their Leisure should read general Systems in order to perfect them.

For these Reasons, I have ventured to publish this small Treatise; wherein I have made it my chief Business to keep a due Medium betwix the two Extremes, into which the speculative Writers on the one Hand, and the practical ones on the other are apt to run. I have laid down all useful Rules, and troubled the Reader with no more of the Theory than is necessary to explain them. I have also explained the principles of ~~Ad~~ensuration, Surveying and Gauging, and shewed how they are applied to Practice, in order that my Book might better answer the particular End for which it is designed, namely, the Instruction of the Gentlemen of Mr. WATTS's Academy.

As for the particular Rules of each Section, the Reader will find them at the End of the Book, and therefore they need not be repeated. ~~I~~ shall only observe, that I have designedly omitted Great Circle-Sailing, as being only speculative, and depending on Spherical Trigonometry, which would require a particular Volum to explain it. There are indeed two or three Problems necessary in Practice, which depend on the Resolution of Spherical Triangles; but for the Solution of these, I have laid down such clear and short Rules that no body can mistake the Manner of applying them.

I know, some are of Opinion, that the Demonstrations are not to be easily learnt by every Capacity, on which account they teach the Practice only. This Book is therefore so written as to serve for their Purpose likewise, because they may take the Rules alone without their Reasons. It is true indeed, that there may be great Difficulty in finding out a proper Demonstration; but after it is found, it is easier to be understood than that of which it is the Reason: and therefore

therefore they who are not capable of understanding the Demonstrations, are much less capable of understanding the Practical Rules which depend on them. And I am inclin'd to believe, that what is commonly attributed to want of Genius in the Scholar, is often owing to want of Method and Perspicuity in the Master.

In preparing this Treatise for the Press, I own myself obliged to Mr. STIRLING, F R. S. (of the Academy in Tower-Street) who on his first seeing my Papers, so far approved both of the matter they contained and of the Order in which they were put together, as to think them fit to be made publick with very little Alteration.

I acknowledge myself also obliged to that most excellent Book of Mr. HODGSON, entituled a System of Mathematics, which I hold to be by far the most compleat Treatise on this Subject, both as to Theory and Practice. And on this Occasion I cannot but take notice of a late Writer, who has accused him and all Writers on Navigation of being guilty of a very gross Error; which is, that they took their Departure and Meridional Distance to be the same. Indeed in Plain-Sailing he took them to be the same; and is still of the same Opinion, notwithstanding what has been said to the contrary. But that he did not in other Cases take them to be the same will appear by the following Passage of his Book at the End of Mercator's-Sailing.

" To give the Learner all the Helps necessary to a  
" right Understanding of this most useful Part of  
" Sailing, I shall endeavour (before I conclude  
" this Part) to set his Notions right, concerning  
" Difference of Longitude, Meridional Distance,  
" and Departure; and let him see, that tho' these  
" are synonymous Terms in Plain-Sailing, constant-  
" ly signifying the same thing, and in every Ques-  
" tion are represented by the same Right Line, yet  
" in

" in the true Sailing they are essentially different  
 " one from another; and in the same Problem, are,  
 " as they really should be, represented or expressed  
 " by different Lines, and are of different Values."

*Now after reading this Passage, I shall leave it to  
 the Public to judge as they think fit, of the Writer,  
 who owns that he has seen Mr. HODGSON's System  
 of Mathematics by his quoting it, and at the same  
 time affirms that he never had any Author who  
 made any Distinction between Departure and Meri-  
 dional Distance.*

*And I hope I may be excused for vindicating the  
 Author to whom I have professed myself so much ob-  
 liged, lest, from my Silence on this Head, it should be  
 suspected that I were guilty of the same Error, which  
 is unjustly laid to his Charge.*



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*The Supplement, containing the easie Construction  
of the Tables of Sines, &c. Sailing by Common Arith-  
metick, New and Full Moons, with the Visible Eclipses  
to the Year 1657. Also the sundry Errors and Defects  
in Charts, Compasses, Quadrant, &c. with proper  
Helps proposed.*

*To which are added the Tables necessary in Navi-  
gation.*



THE



THE  
PRINCIPLES  
OF  
NAVIGATION.  
DEFINITION.



NAVIGATION is that Art whereby we are enabled to carry a Ship from one Port to another.

This Science depends upon some Parts of the Mathematicks, which must be known before we can treat of it; therefore we shall first lay down the Principles of *Geometry*.

## S E C T. I.

Of such Geometrical Propositions as are absolutely necessary for NAVIGATION.

ART. I. GEOMETRY is that Science where-in we consider the Properties of Magnitude.

2. A Point is that which is not made up of Parts, or which is of it self indivisible, as A.

3. A Line is a Length without Breadth, as B—

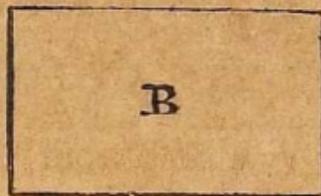
4. The Extremities of a Line are Points; as the Extremities of the Line AB, are the Points A and B.



5. If the Line A B be the nearest Distance between its Extremes A and B, then it is call'd a strait Line, as A B in the former Figure; but if it be not the nearest Distance, then it is called a curve Line, as A B.



6. A Surface is that which is considered as having only Length and Breadth, but no Thickness, as B.



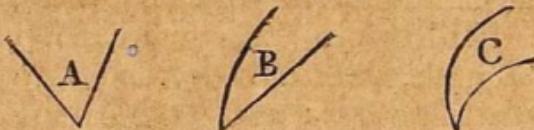
7. The Terms of a Surface are Lines.

8. A plain Surface is that which lies equally between its Extremes.

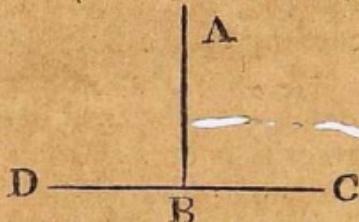
9. The Inclination between two Lines meeting one another, (provided they do not make one continued

tinued Line) or the Opening between them, is called an Angle; thus the Inclination of the Line A B to the Line C B, meeting one another at B, or the Opening between the two Lines A P and C B, is called an Angle.

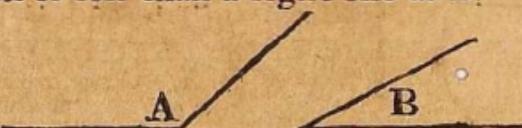
10. When the Lines forming the Angle are right Lines, then it is called a right lin'd Angle, as A; if one of them be right and the other curv'd, it is called a mix'd Angle, as B; if both of them be curv'd, it is called a curve-lin'd Angle, as C.



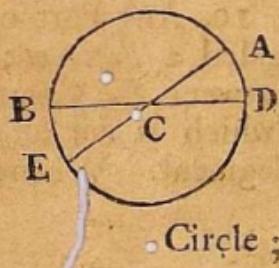
11. If a right Line A B fall upon another DC, so as to incline neither to the one side nor to the other, but make the Angles A BD, A BC on each side equal to one another, then the Line A B is said to be perpendicular to the Line DC; and the two Angles are called right Angles.



12. An obtuse Angle is that which is greater than a right one, as A; and an acute Angle, that which is less than a right one as B.



13. If a right Line DC be fastened at one of its Ends C, and the other End D, be carried quite round, then the Space comprehended is called a Circle; the curve Line described by the Point D, is called the Perifery or Circumference of the



## Geometrical Propositions.

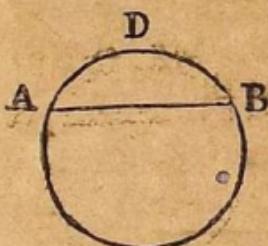
Circle; the fix'd Point C, is called the Center of it.

14. The describing Line CD, is called the Radius, *viz.* any Line drawn from the Center to the Circumference; whence all Radii of the same or equal Circles are equal.

15. Any Line drawn through the Center, and terminated bothWays by the Circumference, is called a *Diameter*, as BD is a Diameter of the Circle BADE. And the Diameter divides the Circle and Circumference into two equal Parts, and is double the Radius.

16. The Circumference of every Circle is supposed to be divided into 360 equal Parts, called *Degrees*; and each Degree is divided into 60 equal Parts, called *Minutes*; and each Minute into 60 equal Parts, called *Seconds*; and these into *Thirds*, *Fourths*, &c. these Parts being greater or less according as the Radius is.

17. Any Part of the Circumference is called an *Arc*, or *arc*; and is called an *Arc* of as many Degrees as it contains Parts of the 360, into which the Circumference was divided: Thus if AD (in the former Figure) be the  $\frac{1}{4}$  of the Circumference, then the Arc AD is an Arc of 90 Degrees.



18. A Line drawn from one End of an *Arc* to the other, is called a *Chord*, and is the Measure of the *Arc*; thus the right Line AB is the Chord of the Arc ADB.

19. Any Part of a Circle cut off by a Chord, is called a *Segment*; thus the Space comprehended between the Chord AB and Circumference ADB (which is cut off by the Chord AB) is called a Segment. Whence it is plain,

# Geometrical Propositions.

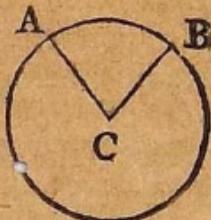
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1st, That all Chords divide the Circle into two Segments.

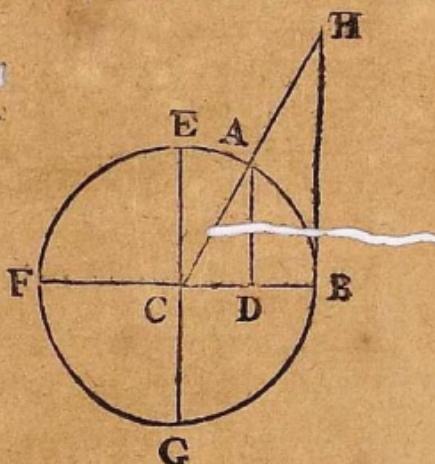
2dly, The less the Chord is the more unequal are the Segments, &c e contra.

3dly, When the Chord is greatest, viz. when it is a Diameter, then the Segments are equal, viz. each a Semicircle.

20. Any Part of a Circle (less than a Semicircle) contained between two Radii and an Arc, is called a Sector; thus the Space contained between the two Radii, AC, BC, and the Arch AB, is called a Sector.



21. The right Sine of any Arc, is a Line drawn perpendicular from one End of the Arc, to a Diameter drawn through the other End of the same Arc: thus AD is the right Sine of the Arc AB, it being a Line drawn from A, the one End of the Arc AB, perpendicular to CB, a Diameter passing through B, the other End of the Arc AB.



Now the Sines standing on the same Diameter still encrease till they come to the Center, and then becoming the Radius, it is plain that the Radius EC is the greatest possible Sine, and for that Reason is called the whole-Sine.

Since the whole Sine EC must be perpendicular to the Diameter FB (by Def. 21.) therefore producing the Diameter EG, the two Diameters, FB, EG, must cross one another at right Angles, and so the Circumference of the Circle must be divided by them into four parts EB, BG, GF, and FE, and these

these four parts are equal to one another (by Def. 11.) and so  $\angle B$  a Quadrant, or fourth Part of the Circumference; therefore the Radius  $E C$  is always the Sine of the Quadrant, or fourth Part of the Circle  $E B$ .

Sines are said to be of so many Degrees, as the Arch contains Parts of the 360, into which the Circumference is supposed to be divided; so the Radius being the Sine of a Quadrant, or fourth Part of the Circumference which contains 90 Degrees; (the fourth part of 360) therefore the Radius must be the Sine of 90 Degrees.

22. That Part of the Radius comprehended between the Extremity of the right Sine and the lower End of the Arch, viz.  $D B$ , is called the versed Sine of the Arch  $A B$ .

23. If to any Point in the Circumference, viz.  $B$ , there be drawn a Diameter  $F C B$ , and from the point  $B$  perpendicular to that Diameter, there be drawn the Line  $B H$ ; that Line is called a Tangent to the Circle in the Point  $B$ , which Tangent can touch the Circle only in one point  $B$ , else if it touch'd it in more, it would go within it, and so not be a Tangent but a Chord (by Art. 18.)

24. The Tangent of any Arch  $A B$ , is a right Line drawn perpendicular to a Diameter through the one End of the Arch  $B$ , and terminated by a Line  $C A H$ , drawn from the Center through the other End  $A$ ; thus  $B H$  is the Tangent of the Arch  $A B$ .

25. And the Line which terminates the Tangent, viz.  $C H$ , is called the Secant of the Arch  $A B$ .

26. What an Arch wants of a Quadrant is called the Complement of that Arch; thus  $A E$  being what the Arch  $A B$  wants of the Quadrant  $E B$ ; is called the Complement of the Arch  $A B$ .

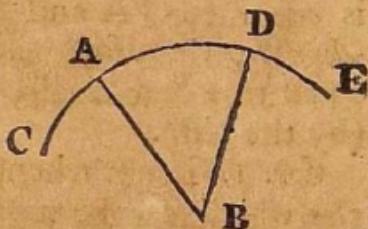
27. And what an Arch wants of a Semicircle is called the Supplement of that Arch; thus since  $A F$  is

is what the Arch A B wants of the Semicircle BAF, it is called the Supplement of the Arch A B.

28. The Sine, Tangent, &c. of the Complement of any Arch, is called the Co-Sine, Co-Tangent, &c. of that Arch; thus the Sine, Tangent, &c. of the Arch A E is called the Co-Sine, Co-Tangent, &c. of the Arc A B.

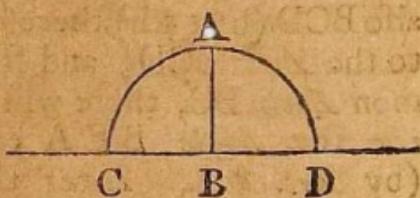
29. The Sine of the Supplement of an Arch is the same with the Sine of the Arch itself, for drawing them according to the Definitions, there results the self same Line.

30. A right lin'd Angle is measured by an Arch of a Circle described upon the angular Point as a Center is comprehended between the two Legs that form the Angle; thus the Angle A B D is measured by the Arch A D of the Circle C A D E that is described upon the Point B as a Center; and the Angle is said to be of as many Degrees as the Arch is; so if the Arch A D be 45 Degrees, then the Angle A B D is said to be an Angle of 45 Degrees.



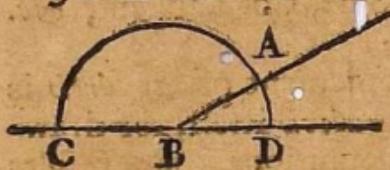
Hence Angles are greater or less according as the Arch described about the angular Point, and terminated by the two Legs, contain a greater or less Number of Degrees.

31. When one Line falls perpendicularly on another, (as A B on C D) then the Angles are right; (by the 11th) and describing a Circle on the Center B, since the Angles A B C, A B D are equal, their Measures must be so too, i. e. the Arches A C, A D must be equal; but the whole C A D is a Semicircle



micircle, since  $C D$ , a Line passing through the Center  $B$ , is a Diameter, therefore each of the Parts  $A C$ ,  $A D$  is a Quadrant, i.e. 90 Degrees; so the Measure of a right Angle is always 90 Degrees.

32. If one Line  $A B$  fall any way upon another,



$C D$  then the Sum of the two Angles  $A B C$ ,  $A B D$  is always equal to the Sum of two right Angles.

For on the

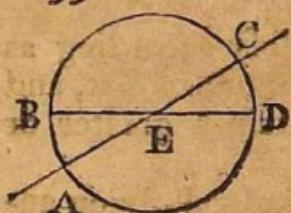
point  $B$ , describing the Circle  $C A D$ , it is plain, that  $C A D$  is a Semicircle, (by 15th); but  $C A D$  is equal to  $C A$  and  $A D$  the Measures of the two Angles; therefore the Sum of the two Angles is equal to a Semicircle, that is, to two right Angles (by the last).

Cor. 1. From whence it is plain, that all the Angles which can be made from a point in any Line, towards one side of the Line, are equal to two right Angles.

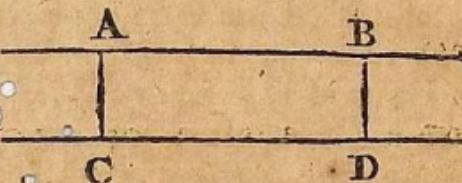
2. And that all the Angles which can be made about a Point, are equal to four right ones.

33. If one Line  $A C$  crosses another  $B D$  in the

Point  $E$ , then the opposite Angles are equal, viz.  $B E A$  to  $C E D$ , and  $B E C$  equal to  $A E D$ . For upon the point  $E$ , as a Center, describing the Circle  $A B C D$ , it is plain  $A B C$  is a Semicircle, as also  $B C D$  (by 15th) therefore the Arch  $A B C$  is equal to the Arch  $B C D$ ; and from both taking the common Arch  $B C$ , there will remain  $A B$  equal to  $C D$ , i.e. the Angle  $B E A$  equal to the Angle  $C E D$  (by Art. 30). After the same Manner we may prove, that the Angle  $B E C$  is equal to the Angle  $A E D$ .

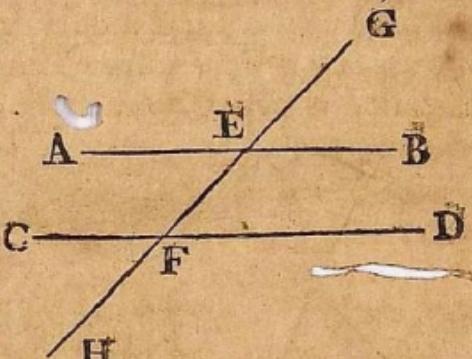


34. Lines which are equally distant from one another are called *Parallel Lines*; as AB, CD.



35. If a Line GH crosses two Parallels AB, CD, then the external Angles are equal, viz. GEB equal to CFH and AEG equal HFD. For since AB and CD are parallel to one another, they may be considered as one broad Line, and GH crossing it; then the vertical or opposite Angles GEB, CFH are equal (by the 33d) as also AEG and HFD by the same.

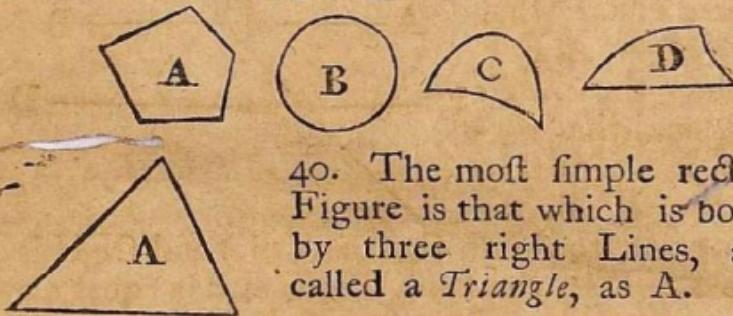
36. If a Line GH cross two Parallels AB, CD then the alternate Angles, viz. AEF and EFD, or CFE and FEB are equal; that is, the Angle AEF is equal to the Angle EFD, and the Angle CFE is equal to the Angle FEB, for GEB is equal to AEF (by the 33d.) and CFH is equal to EFD by the same, but GEB is equal to CFH by the last. Therefore AEF is equal to EFD; the same way we prove FEB equal to FEC.



37. If a Line GH cross two parallel Lines AB, CD, then the external Angle GEB is equal to the internal opposite one EFD, or GEA equal to CFE. For the Angle AEF is equal to the Angle EFD by the last; but AEF is equal to GEB (by the 33d) therefore GEB is equal to EFD; the same Way we may prove AEG equal to CFE.

38. If a Line GH cross two parallel Lines A B, C D, then the Sum of the two internal Angles, viz. B E F and D F E, or A E F and C F E are equal to two right Angles; for since the Angle G E B is equal to the Angle E F D (by the last) to both add the Angle F E B, then G E B and B E F are equal to B E F and D F E; but G E B and B E F are equal to two right Angles (by the 32d) therefore B E F and D F E are also equal to two right Angles. The same Way we may prove that A E F and C F E are equal to two right Angles.

39. A Figure is any part of Space bounded, by Lines or a Line. If the bounding Lines be strait, it is called a *Rectilineal Figure* as A; if they be curved, it is called a *curvilinear Figure* as B or C; if they be partly curve Lines and partly strait, it is called a *mixt Figure* as D.



40. The most simple rectilineal Figure is that which is bounded by three right Lines, and is called a *Triangle*, as A.

41. Triangles are divided into different Kinds, both with Respect to their Sides and Angles: with Respect to their Sides they are commonly divided into three Kinds, viz.

42. A Triangle having all it's three Sides equal to one another, is called an *Equilateral Triangle*, as A.

43. A Triangle having two of it's Sides equal to one another, and the third Side not equal to either of them, is called an *Isosceles Triangle*, as B.

44. A Triangle having none of it's Sides equal to one another, is called a *Scalene Triangle*, as C.

containing the Right Ascensions, Declinations, Longitudes and Latitudes of above Sixty Eminent Stars  
from the Flamsteidian Observations, and fitted to the Year 1726.

of the Fixed Stars.	Right Ascension.		Declination.		Longitude. D. M. S.	Latitude. D. M. S.	Decomposition D. M. S.	Magnitude N. S.	Right Ascension.		Declination.		Denomination D. M. S.
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the Scheher	-	-	-	6 18 14	5 02 03	N	4 00 00 46 35 54	N	2 3	The Virgin's Spike	197 42 07	09 43 23	S
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the Two Fifies	-	-	-	26 59 42	25 20 55	N	25 32 33 09 57 12	S	3	The last but one in the Tail of Hydra	196 02 04	21 43 20	S
the Libellula	-	-	-	6 7 56	17 23 05	S	03 49 18 09 57 12	N	2	The last of the three in the Tail of the Great Bear	194 11 35	50 41 04	S
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the Aldebaran	-	-	-	6 02 52	1 57 23	N	05 57 00 05 29 49	S	1	The Bright Star in the Southern Balance	218 57 37	14 52 52	S
Rigel	-	-	-	7 07 14	4 19 19	N	18 01 41 23 51 47	N	1	The Bright Star in the Northern Crown	210 46 40	27 39 08	S
	-	-	-	26 20 46	0 33 00	S	13 00 00 31 10 11	S	1	The Bright Star in the Neck of the Serpent	234 41 37	07 18 12	S
the Bull	-	-	-	17 13 40	20 33	N	19 43 56 05 21 34	N	2	The Head of the Scorpion Antares	243 10 25	47 22	S
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the Bull	-	-	-	0 19 12	21 56 20	S	10 57 28 04 14 24	S	3	The Head of Hercules	232 58 14	43 16	N
Belt of Orion	-	-	-	0 34 23	0 24 49	S	19 37 44 24 53 23	S	2	The Head of Serpentarius	260 32 35	12 46 49	N
of Orion	-	-	-	81 44 34	0 07 01	S	20 51 45 25 46 17	S	1	The following Shoulder of Serpentarius	265 29 01	04 42 23	S
of Orion	-	-	-	85 04 33	0 19 15	N	24 55 28 16 06 46	S	1	In the Head of the Dragon, a Bright Star	207 35 29	51 32 16	N
	-	-	-	98 16 32	20 59	S	10 19 01 39 33 08	S	1	The Bright Star in the Head of the Serpent	276 54 03	38 33 02	N
the Northernmost Twin	-	-	-	109 15 44	27 09	N	16 25 20 10 03 48	S	1				
far	-	-	-	111 14 01	0 54 26	N	22 02 21 15 57 55	S	2	The middlemost of the three in the Head of Sagittary	285 04 37	22 06 12	S
the Southernmost Twin	-	-	-	118 07 34	2 39 25	N	19 26 09 06 39 27	S	2	The Bright Star in the Eagle	294 19 06	08 10 01	N
	-	-	-	138 31 18	0 29 23	S	23 27 59 22 44 32	S	2	The Hand of Antinous	259 17 09	01 36 44	S
	-	-	-	148 06 00	0 17 04	N	20 01 20 00 46 38	S	3	The following Horn of Capricorn	301 24 21	15 37 01	S
the Stars in the Square of the Gr. Bear	-	-	-	161 16 20	57 50 44	N	15 34 12 45 06 16	S	2	The following Shoulder of Aquarius	327 55 42	01 38 12	S
	-	-	-	161 37 22	16 51 05	S	19 56 03 22 42 47	S	3				
the Stars in the Sqqr. of the Gr. Bear	161	37	47	63	13 58	N	11 20 00 49 40 05	S	2	The Bright Star in the Tail of Capricorn	332 58 40	17 19 10	S
of the Cup	-	-	-	164 34 01	21 20 16	S	24 45 33 25 37 33	S	4	The Mouth of the Southern Fish Fomalhaut	340 34 51	31 03 20	N
King Stars in the Sqqr. of the Gr. Bear	161	49 43	55 13	05	43 05	N	17 49 14 12 16 51	N	2	In the Flying Horse, the bright Star Scheat	342 37 09	26 35 44	N
	-	-	-	173 34 54	23 11 57	S	16 36 49 47 07 20	S	2	In the flying Horse, the bright Star Marhab	342 46 03	13 43 40	N
If the Cross	-	-	-	180 26 59	16 01 07	S	08 25 25 31 21 46 47	S	3	The Head of Andromeda	358 33 20	27 34 12	N
	-	-	-	180 27 55	21 34 49	S	06 55 58 14 29 00	S	2	In the flying Horse Algenib	339 47 00	13 39 02	N
Following in the Sqqr. of the Gr. Bear	180	27	34	59	34 48	N	27 10 40 41 29 36	N	2				
of the Crown	-	-	-	183 56 29	14 19 06	S	09 39 13 14 09 47	S	3				
the Great Bear	-	-	-	185 08 06	12 23 54	N	06 07 40 16 12 40	N	3				
the Virgin Vindemiatrix	-	-	-	190 08 55	21 34 49	S	13 33 25 18 01 54	S	2				
	-	-	-	192 30 42	17 28 04	N	05 03 05 54 19 35	N	2				

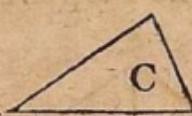
The

And for the Benefit of the Southern Navigation, I have added the Right Ascensions and Declinations of the four remarkable So-called the Croisers; deduced from Dr. Halley's Observations.

The preceding of the two Middlemost in the Sqrs. - 180 21 30 57 10 37 S N  
The Southern Foot of the Cross - 183 05 20 01 31 10  
The Northernmost of the Four - 184 10 20 55 30 10  
The following, or Easternmost of the Four - 188 10 48 59 05 57

A Table of all the Lunations and Visible Eclipses for 21 Years to come from the Beginning of

CH. F. D H	APRIL		MAY		JUNE		JY		AUGUST		SEPT.		OCTO.		NO. N. D D H	
	N. D D H	F. D D H	N. D D H	R. D L H	N. D L H	F. D D H										
6. o	29. 10.	13. 3	9. 9	14. 4	27. 5	13. 3	27. 4	12. 11	25. 9	10. 7	23. 6	19. 3	23. 2	8. 11	21. 2	
j. 8	19. 0	4. 2	18. 3	3. 6	17. 4	2. 10	16. 3	1. 10.	15. 1	29. 6	13. 10	28. 3	12. 7	27. 1	11. 5	
4. 3	8. 2	22. 8	7. 4	22. 8	6. 7	21. 1	5. 11	20. 5	4. 11	19. 5	3. 1	17. 1	2. 11	17. 5	30. 6	
3. 10	26. 7	11. 11	26. 9	11. 1	25. 1	10. 3	24. 4	9. 6	23. 7	9. 9	21. 9.	7. 1.	21. 9.	6. 2	19. 10	
1. 9	15. 2	29. 7	14. 2	29. 7	13. 2	27. 8	12. 4	26. 10	11. 8	26. 2	10. 0	24. 5	9. 5	24. 11	8. 8	
1. 1	4. 5	19. 10	4. 1	18. 7	2. 10	16. 4	1. 9.	16. 3	30. 1	15. 3	28. 6	13. 5	28. 1	12. 11	27. 6	
0. 5	23. 5	9. 2	23. 2	8. 11	21.	6. 6	20. 6	6. 2	19. 8	4. 1	7. 1.	2. 11	17. 11	2. 0	16. 6	
9. 4	13. 7	28. 4	12. 10	27. 3	11.	5. 7	10. 8	25. 2	8. 4	1. 1	21. 1	6. 2	21. 3	5. 6	2. 2	
8. 2	1. 10.	16. 4	1. 6	16. 3	0.	28. 8	13. 7	12.	25. 1	10. 9	24. 1	9. 7	23. 3			
7. 3	20. 6	5. 8	20. 6	5. 0	19.	0	18. 0	3. 10	17. 1	14. 4	29. 10	14. 2	28. 7	12. 1		
5. 9.	9. 10.	24. 2	9. 0	24.	7.	7. 1.	22. 7	20. 5	4. 8	19. 1	3. 4	18. 0	2. 3	1. 1		
4. 0.	28. 1	13. 1	28. 4	12.	10	26. 9	11. 0	24. 9	10. 2	23. 9	10. 3	22. 7	8. 3	21. 5		
3. 9	16. 4.	1. 9	16. 5	1.	30. 1	14. 10	29. 5	13. 3	27. 8	11. 5	26. 11	11. 7	26. 1	9. 8	2. 2	
2. 9	6. 1	22. 7	5. 11	3.	18. 6	3. 1.	18. 0	2. 3	16. 9	30. 3	15. 1	30. 4	13. 6	28. 8	1. 1	
2. 1	25. 1	10. 10	24. 9	9. 6	18.	3	22. 7	7. 1.	20. 8	7. 1	19. 1	4. 2	19. 6	4. 6	18. 3	
1. 4	14. 5	29. 11	14. 1	28. 7	12. 9	27. 3	11. 5	26. 10	10. 2	24. 8	8. 3	23. 8	8. 6	23. 0	7. 0	
1. 3	3. 9	18. 3	2. 6	17. 0	1.	15. 7.	29. 3	14. 6	28. 0	13. 9	26. 11	11. 6	26. 2	11. 5	24. 8	
0. 10.	22. 8	7. 1.	21. 5	7. 1	20.	5. 11	19. 8	4. 7	17. 3	3. 2	15. 11	2. 9	15. 10	30. 4	14. 10	
4. 11.	2. 26. 8	11. 4	25. 10	9. 3	24.	9	9. 0	23. 6	7. 8	22. 1	5. 4	20. 10	5. 1	19. 7	3. 11	
4.	30. 8	15. 9	29. 10	15. 2	28. 1	13. 2	27. 10	13. 5	26. 8	11. 4	24. 6	10. 2	24. 3	9. 11	22. 1	
8.	18. 9	3. 11	18. 0	3. 2	16. 7	1. 6	16. 5	1. 8	14. 6	12. 0	13. 7	28. 1	12. 7	27. 0	11. 5	

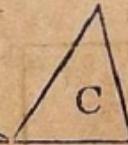
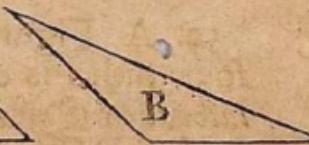
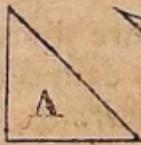


45. Triangles, with Respect to their Angles, are divided into three different Kinds, viz.

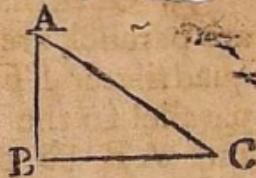
46. A Triangle having one of it's Angles, right, is called a *Right-Angled Triangle*, as A.

47. A Triangle having one of it's Angles obtuse, greater than a right Angle, is called an *Obtuse-Angled-Triangle*, as B.

48. Lastly, a Triangle, having all it's Angles acute, is called an *Acute-Angled Triangle*, as C.



49. In all right-angled Triangles, the Sides comprehending the right Angle are called the *Legs*, and the Side opposite the right Angle is called the *Hypothenuse*. Thus in the right angled Triangle ABC the right Angle being the two Sides AB



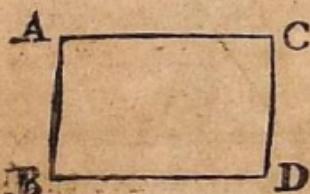
and BC which comprehend the right Angle ABC, are the *Legs* of the Triangle, and the Side AC, which is opposite to the right Angle ABC, is the *Hypothenuse* of the right-angled-Triangle ABC.

50. Both obtuse and acute angled Triangles are in general called *Oblique-Angled-Triangles*; in all which any Side is called the *Base*, and the other two the *Sides*.

51. The Perpendicular Height of any Triangle is a Line drawn from the Vertex to the Base perpendicularly; thus if the Triangle A B C be proposed, and BC be made it's Base, then A will be

the Vertex, *viz.* The Angle opposite to the Base; and if from A you draw the Line A D perpendicular to BC, then the Line A D is the Height of the Triangle ABC standing on BC as it's Base.

Hence all Triangles standing between the same Parallels have the same Height, since all the Perpendiculars are equal by the Nature of Parallels.



52. A Figure bounded by four Sides is called a *Quadrilateral* or *Quadrangular Figure*, as A B D C.

53. Quadrilateral Figures whose opposite Sides are parallel, are called *Parallelograms*. Thus in the quadrilateral Figure A B D C, if the Side A C be parallel to the Side B D which is opposite to it, and A B be parallel to C D, then the Figure A B D C is called a Parallelogram.

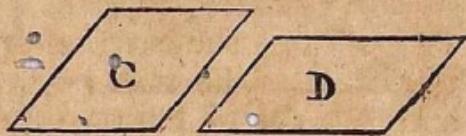
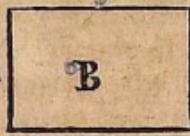
54. A Parallelogram having all it's Sides equal and Angles right, is called a *Square*; as A.

55. That which hath only the opposite Sides equal and it's Angles right, is called a *Rectangle*; as B.

56. That which hath equal Sides but oblique Angles, is called a *Rhombus*, as C; and is just an inclin'd Square.

57. That

57. That which hath only the opposite Sides equal, and the Angles oblique, is called a *Rhomboides*, as D; and may be conceived as an inclined Rect-angle.

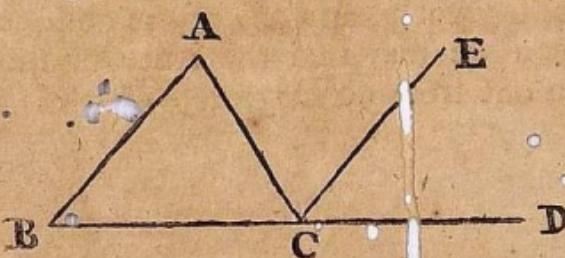


D

58. When none of the Sides are parallel to another, then the quadrilateral Figure is called a *Trapezium*.

59. Every other right-lined Figure, that has more Sides than four is in general called a *Polygon*. And Figures are called by particular Names according to the Number of their Sides, viz. One of five Sides is called a *Pentagon*, of six a *Hexagon*, of eleven a *Heptagon*, and so on. When the Sides forming the Polygon are equal to one another, the Figure is called a regular Figure or Polygon.

60. In any Triangle ABC, one of it's Legs, as BC, being produced towards D, the external Angle ACD is equal to both the internal opposite ones taken together, viz. to ABC and BAC. In order to prove this, through C draw CE parallel to AB, then since CE is parallel to AB and AC crosseth them, the Angle ECD is equal to ABC (by the 37th) and the Angle ACE equal to CAB (by the 36th) therefore the Angles ECD and ECA are equal to the Angles ABC and CAB; but the Angles ECD and ECA are together equal to the Angle ACD; therefore the Angle ACD is equal to both the Angles ABC and CAB taken together.



60. In

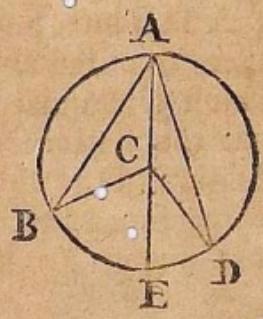
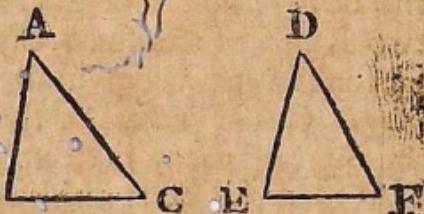
61. In any Triangle ABC all the three Angles taken together are equal to two right Angles. To prove this you must produc<sup>o</sup> BC, one of it's Legs, to any Distance, suppose to D; then by the last Proposition, the external Angle ACD, is equal to the Sum of the two internal opposite ones CAB and ABC; to both add the Angle ACB, then the Sum of the Angles ACD and ACB will be equal to the Sum of the Angles CAB and CBA and ACB. But the Sum of the Angles ACD and ACB, is equal to two right ones (by the 32d) therefore the Sum of the three Angles CAB and CBA and ACB, is equal to two right Angles that is, the Sum of the three Angles of any Triangle ACB is equal to two right Angles.

*Cor. 1.* Hence in any Triangle given, if one of it's Angles be known, the Sum of the other two is also known; for since by the last, the Sum of all the three is equal to two right Angles, or a Semicircle, it is plain, that taking any one of them from a Semicircle or 180 Degrees, the Remainder will be the Sum of the other two. Thus (in the former Triangle ABC) if the Angle ABC be 40 Degrees, by taking 40 from 180 we have 140 Degrees; which is the Sum of the two Angles BAC, ACB, the Converse of this is also plain, viz. The Sum of any two Angles of a Triangle being given, the other Angle is also known by taking that Sum from 180 Degrees.

2. In any right angled Triangle, the two acute Angles must just make up a right one between them; consequently, any one of the oblique Angles being given we may find the other by subtracting the given one from 90 Degrees, which is the Sum of both.

62. If in any two Triangles, ABC, DEF, two Legs of the one, *viz.* AB and AC, be equal to two Legs in the other, *viz.* to DE and DF, each to each respectively *viz.*  $\angle BAC$  equal to  $\angle EDF$ ; and if the Angles included between the equal Legs be equal, *viz.* the Angle BAC equal to the Angle EDF; then I say, that the remaining Leg of the one shall be equal to the remaining Leg of the other, *viz.* BC to EF; and the Angles opposite to the equal Legs shall be equal, *viz.* ABC equal to DEF being opposite to the equal Legs AC, and DF) also ACB equal to DFE (which are opposite to the equal Legs AB and DE) for if the Triangle ABC be supposed to be lifted up and put upon the Triangle DEF, and the point A on the point D; it is plain since BA and DE are of equal Length, the Point E will fall upon the Point B; and since the Angles BAC, EDF are equal, the Line AC will fall upon the Line DF, and they being of equal length, the Point C will fall upon the Point F, and so the Line BC will exactly agree with the Line EF, so the Triangle ABC will in all Respects be exactly equal to the Triangle DEF; and the Angle ABC will be equal to the Angle DEF, also the Angle ACB will be equal to the Angle DFE.

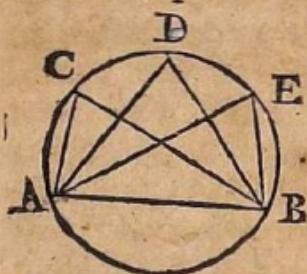
63. Any Angle, as BAD, at the Circumference of a Circle BADE, is but half the Angle BCD at the Center standing on the same Arch BED. To demonstrate this, draw through A and the Center C, the right Line ACE, then the Angle ECD is



equal

equal to both the Angles  $DAC$  and  $ADC$  (by the 60th); but since  $AC$  and  $CD$  are equal (being two Radii of the same Circle) it is plain the Angles subtended by them must be equal also; i. e. the Angle  $CAD$  equal to the Angle  $CDA$ , therefore the Sum of them is double any one of them, i. e.  $DAC$  and  $ADC$  is double of  $CAD$ , and therefore  $ECD$  is also double of  $DAC$ ; the same Way it may be proved, that  $ECE$  is double of  $CAB$ , and therefore the Angle  $BCD$  is double of the Angle  $BAD$ , or  $BAD$  the half of  $BCD$  which was to be proved.

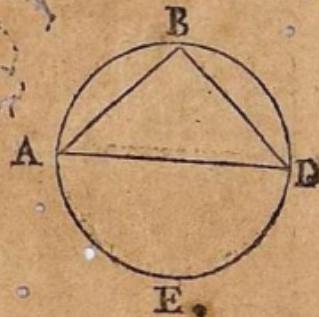
*Cor. 1.* Hence an Angle at the Circumference is measured by half the Arch it subtends, for the Angle at the Center (standing on the same Arch) is measured by the whole Arc (by the 30th); but since the Angle at the Center is double that at the Circumference, it is plain the Angle at the Circumference must be measured by only half the Arch it stands upon.



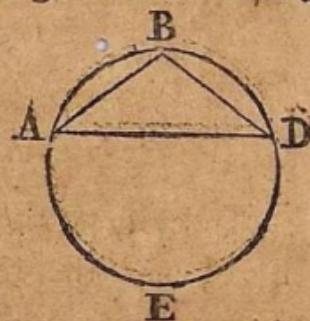
*Cor. 2.* Hence all Angles at the Circumference of a Circle, standing on the same Chord  $AB$  are equal to one another; for by the last Corollary they are all measured by the same Arc, viz. half the Arc  $AB$  which each of them subtends.

*Cor. 3.* Hence an Angle in a Segment greater than a Semicircle is less than a right Angle; thus if  $ADB$  be a Segment, greater than a Semicircle, (see the last Figure) then the Arch  $AB$ , on which it stands, must be less than a Semicircle, and the half of it less than a Quadrant or a right Angle; but the Angle  $ADB$  in the Segment is measured by the half of  $AB$ ; therefore it is less than a right Angle.

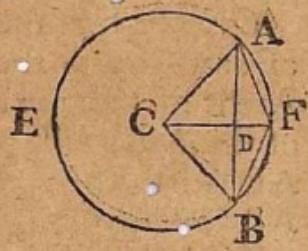
*Cor. 4.* An Angle in a Semicircle is a right Angle. For since ABD is a Semicircle, the Arch AED must also be a Semicircle; but the Angle ABD is measured by half the Arch AED, that is, by half a Semicircle or Quadrant; therefore the Angle ABD is a right one.



*Cor. 5.* Hence an Angle in a Segment less than a Semicircle, as ABD, is greater than a right Angle: for since the Arch ABD is less than a Semicircle, the Arch AED must be greater than a Semicircle, and so it's half greater than a Quadrant, i.e. than the Measure of a right Angle; therefore the Angle ABD, which is measured by half the Arch AED is greater than a right Angle.



64. If from the Center C of the Circle ABE, there be let fall the Perpendicular CD on the Chord AB, then that Perpendicular will bisect the Chord AB in the Point D. To demonstrate this; draw from the Center to the Extremities of the Chord the two Lines CA, CB; then since the Lines CA and CB are equal, the Angles CAB, CBA, which they subtend must be equal also; but the Perpendicular CD divides the Triangle ACB into two right-angled Triangles ACD and CDB, in which the Sum of the Angles ACD and CAD in the one, is equal to the Sum of the Angles DCB and CBD in the other, each being equal to a right Angle, (by Cor. 2. of Art. 61.) but CAD is equal to CBD, therefore ACD is equal to BCD. So in the two



Triangles ACD and BCD, the two Legs AC and CD in the one are equal to the two Legs BC and CD in the other, each to each respectively, and the included Angles ACD and BCD are equal; therefore the remaining Legs AD and BD are equal (by the 62d) and consequently AB bisected in D.

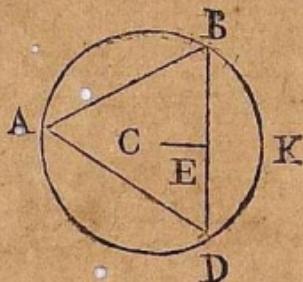
65. If from the Center C of a Circle ABE, there be drawn a Perpendicular CD on the Chord AB, and produced till it meet the Circle in F, then, I say, the Line CF bisects the Arch AB in the Point F; for (see the foregoing Figure) joining the Points A and F, F and B by the strait Lines AF, FB, then in the Triangles ADF, BDF, AD is equal to DB (by the last) and DF common to both; therefore AD and DF two Legs of the Triangle ADF, are equal to BD and DF two Legs of the Triangle BDF, and the included Angles ADF, BDF are equal, being both right, therefore (by the 62d) the remaining Legs AF and FB are equal, but in the same Circle equal Lines are Chords of equal Arches, therefore the Arches AF and FB are equal. So the whole Arch AFB is bisected in the Point F by the Line CF.

*Cor. 1.* From the 64th it follows, that any Line bisecting a Chord at right Angles is a Diameter; (if extended) for since (by the 64th) a Line drawn from the Center perpendicular to a Chord bisects that Chord at right Angles, therefore conversly a Line bisecting a Chord at right Angles, must pass thro' the Center and consequently be a Diameter.

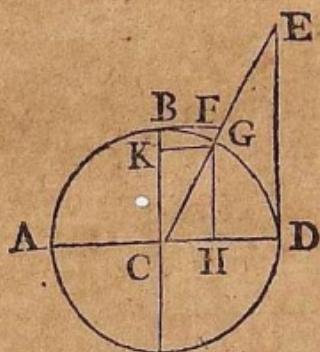
*Cor. 2.* From the two last it follows, that the Sine of any Arch is the half of the Chord of twice the Arch; for (see the foregoing Scheme) AD is the Sine of the Arch AF, by the Definition of a Sine, and AF is half the Arch AFB, and AD half the Chord AB (by the 64th); therefore the *Cor.* is plain.

66. In any Triangle, the half of each Side is the Sine of the opposite Angle; for if a Circle be supposed

sed to be drawn thro' the three angular Points A, B, and D of the Triangle ABD; then the Angle DAB is measured by Half the Arch B KD (by Cor. 1. of Art. 63d); but the half of BD, *viz.* BE is the Sine of half the Arch BKD, *viz.* the Sine of BK (by Corl. 2. of the last) which is the Measure of the Angle BAD; therefore the half of BD is the Sine of the Angle B.A D; the same Way it may be proved, that the Half of AD is the Sine of the Angle ABD, and the half of AB is the Sine of the Angle ADB.

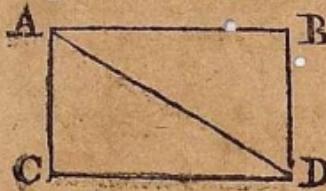


67. The Sine, Tangent, &c. of any Arch is called also the Sine, Tangent, &c. of the Angle whose Measure the Arch is; thus because the Arch GD is the Measure of the Angle GCD, and since GH is the Sine, DE the Tangent, HD the versed Sine, CE the Secant, also GK the Co-Sine, BF the Co-Tangent, and CF the Co-Secant, &c. of the Arch GD; then GH is called the Sine, DE the Tangent, &c. of the Angle GCD whose Measure is the Arch GD.



68. If two equal and parallel Lines, AB and CD, be joined by two others, AC and BD; then these shall also be equal and parallel. To demonstrate this, join the two opposite Angles A and D with the Line AD; then it is plain this Line AD divides the Quadrilateral, ACDB, into two Triangles, *viz.* ABD, ACD, in which AB, a Leg of the one, is equal to DC a Leg of the other by Supposition, and AD is common to both Triangles; and since AB is parallel to CD, the Angle B A D

will be equal to the Angle A D C, (by Art. 36.) therefore in the two Triangles, B A, and A D, and the Angle B A D, is equal to C D and D A, and the Angle A D C, that is, two Legs and the included Angle in the one, is equal to two Legs and the included Angle in the other; (by



the 62d) so B D is equal to A C, and the Angle D A C is equal to the Angle A D B, therefore the Lines B D, A C are both equal and parallel.

*Cor. 1.* Hence it is plain, that the Quadrilateral ABDC is a Parallelogram, since the opposite Sides are parallel.

*Cor. 2.* In any Parallelogram the Line joining the opposite Angles (called the Diagonal) as A D, divides the Figure into two equal Parts, since it has been proved that the Triangles ABD, ACD are equal to one another.

*Cor. 3.* It follows also, that a Triangle ACD on the same Base C D, and between the same parallels with a Parallelogram ABDC, is the half of that Parallelogram.

*Cor. 4.* Hence it is plain, that the opposite Sides of a Parallelogram are equal; for it has been proved that A B D C being a Parallelogram, A B will be equal to C D and A C equal to B D.

69. All Parallelograms on the same or equal Bases, and between the same Parallels, are equal to one another; that is, if B D and G H be equal, and the Lines B H and A F be parallel, then the Parallelograms A B D C, B D F E, and E F H G are equal to one another. For A C is equal to E F each being equal to B D (by Cor. 4. of cor.) To both add C E, then A E will be equal to C F. So in the two Triangles A B E, C D F; A B, a Leg of the one, is equal to C D, a Leg in the other; and A E is equal

21 Geometrical Propositions.

equal to CF and the Angle BAE is equal the Angle DCF (by the 37th); therefore the two Triangles ABE, CDF are equal (by the 62d); and taking the Triangle CKE from both, the Figure ABKC will be equal to the Figure KDFE; to both which add the little Triangle KBD, then the Parallelogram ABCD will be equal to the Parallelogram BDFE. The same

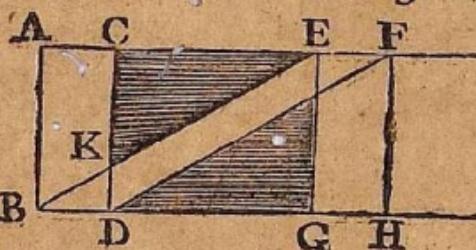
Way it may be proved, that the Parallelogram EFGH is equal to the Parallelogram EFDB; so three Parallelograms

ABDC, BDFE, and EFGH will be equal to one another.

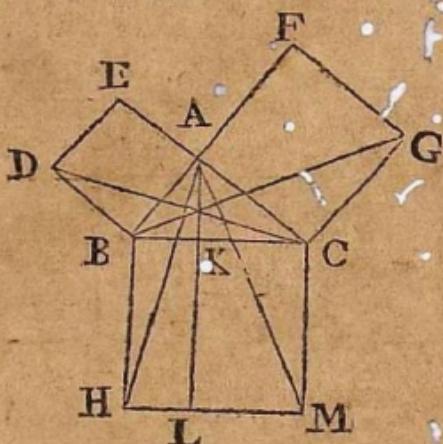
*Cor.* Hence it is plain, that Triangles on the same Base, and between the same Parallels, are equal; since they are the half of the Parallelograms on the same Base and between the same Parallels.

70. In any right-angled Triangle, ABC, the Square of the Hypotenuse BC, *viz.* BCMH is equal to the Sum of the Squares made on the two Sides AB and AC, *viz.* to ABD $\Delta$  and ACGF. To demonstrate this, thro' the Point A draw AKL perpendicular to the Hypotenuse BC, join AH, AM, DC, and BG; then it is plain that DB is equal to BA (by the 54th), also BH is equal to BC (by the same); so in the two Triangles BDC, ABH the two Legs BD and BC in the one, are equal to the two Legs AB and BH in the other; and the included Angles DBC and ABH are also equal; (for DBA is equal to CBH being both right; to both add ABC, then 'tis plain that DBC is equal to ABH) therefore the Triangles DBC, ABH are equal (by the 62d), but the Triangle DBC is half of the Square ABD $\Delta$  (by Cor. 2 of 68th) and the Triangle ABH is half the Parallelogram BK LH (by the same), therefore

half



half the Square ADBE is equal to half the Parallelogram BKLH. Consequently the Square ABDE is equal to the Parallelogram BKLH. The same Way it may be proved, that the Square ACGF is equal



to the Parallelogram K C M L. So the Sum of the Squares A B D E and A C G F is equal to the Sum of the Parallelograms B K L H and K C M L; but the Sum of these Parallelograms is equal to the Square B C M H, therefore the Sum of the Squares on AB and AC is equal to

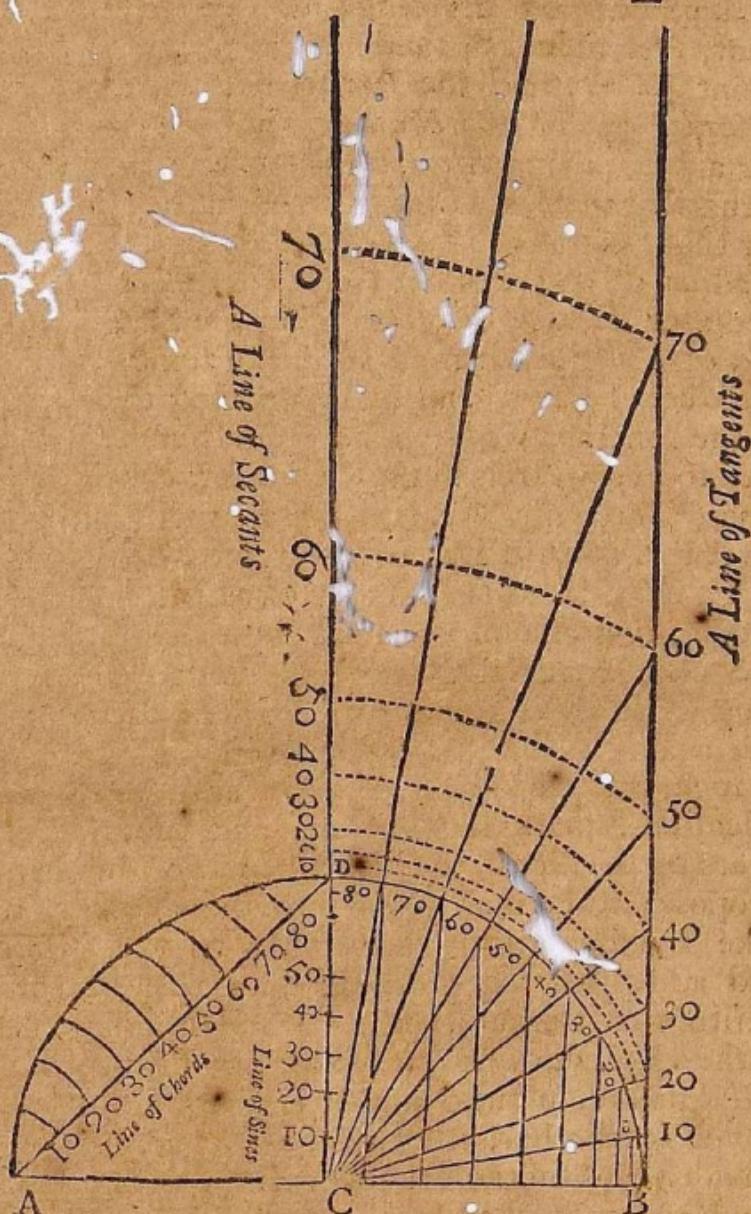
the Square on B C.

*Cor. 1.* Hence in a right-angled Triangle, the Hypotenuse and one of the Legs being given, we may easily find the other, by taking the Square of the given Leg from the Square of the Hypotenuse, and the Square Root of the Remainder will be the Leg required.

*Cor. 2.* Hence, the Legs in a right-angled Triangle being given, we may find the Hypotenuse, by taking the Sum of the Squares of the given Legs, and extracting the Square Root of that Sum.

71. If upon the Line AB there be drawn a Semi-circle ADB, whose Center is C, and on the Point C there be raised a Perpendicular to the Line A B, *viz.* CD; then 'tis plain the Arch DB is a Quadrant, or contains 90 Degrees; suppose the Arch D B to be divided into 9 equal Arches, each of which will contain 10 Degrees, then on the Point B raising BE perpendicular to the Line A B, it will be a Tangent to the Circle on the Point B, and if to every one of the Divisions of the Quadrant, *viz.* B 10, B 20, B 30, B 40, &c. you draw the Sine Tangent,

E.



gent, &c. (in the Scheme) we shall have the Sine, Tangent, &c. to every ten Degrees in the Quadrant: and the same Way we may have the Sine, Tangent, &c. to every single Degree in the Quadrant,

Quadrant, by dividing into 90 equal Parts beginning from B, and drawing the Sine, Tangent, &c. to all the Arches beginning at the same Point B. By this Method they draw the Lines of Sines, Tangents, &c. of a certain Circle on the Scale; for after drawing them on the Circle they take the Length of them, and set them off in the Line drawn for that Purpose. The same Way, by supposing the Radius of any Number of equal Parts, (suppose 1000, or 10,000, &c.) 'tis plain the Sine, Tangent, &c. of every Arch must consist of some Number of these equal Parts, and by computing them in Parts of the Radius, we have Tables of Sines, Tangents, &c. to every Arch in the Quadrant, called Natural Sines, Tangents, &c. and the Logarithms of these give us Tables of Logarithmic Sines, Tangents, &c.

To understand the Nature of which, and the Method of using them, you must know that Logarithms are only artificial Numbers, contriv'd to avoid long Operations in natural Numbers, each of which has a Logarithm belonging to it. Their Nature is such, that Addition of them answers to Multiplication in natural Numbers, and Subtraction answers to Division; that is, when two Numbers are propos'd to be multiply'd into one another, if we take the Logarithms answering to the Numbers and add them together, the Sum will be the Logarithm answering to the natural Number, which is the Product of the two Numbers proposed.

Again, when one Number is proposed to be divided by another, if from the Logarithm of the Dividend we subtract the Logarithm of the Divisor, the Remainder shall be the Logarithm of the Quotient.

Now to apply this to Practice: The first Table at the End of this Book, contains the Logarithms of all the Numbers from 1 to 10000; the Columns mark'd at the Top with (N) contain the natural

Numer.

Numbers, and the adjacent Columns contain the Logarithms of these Numbers. So to find the Logarithm of any Integer Number between 1 and 10,000 we must look in the Columns mark'd with *N* at the Top, till we find the Number propos'd; and the standing on the same Line with it on the adjacent Column is the Logarithm required.

*Ex. ple.* Let it be required to find the Logarithm of 365; by looking in the Table according to the above Direction, I find it to be 2.56229. The Reverse of this, *viz.* Given a Logarithm, to find from your Tables the natural Number answering thereto, is perform'd by looking it to the Columns mark'd with Logarithm at Top; for that which is either equal or next to the one propos'd, and the Number answering to it in the adjacent Column is that required.

*Example.* Let it be required to find the natural Number answering to the Logarithm 2.56229, by proceeding according to the above Direction I find it to be 365.

Again, if it were required to find the Logarithm of a Number, having some Decimals in it. In order to do this, you may observe in the Table of Logarithms, that the Logarithm of 10 is 1, that of 100, 2; and of 1000, 3, &c. And the Logarithms of all the intermediate Numbers between 10 and 100, have 1 for the integral Part of each, and also those between 100 and 1000 have 2 for their integral Part, and so on, which are called their Indices.

Now because any Number consisting of both Integers and Decimals, is equal to the Quotient of the whole consider'd as an Integer divided by the Denominator of the decimal Part; and since by the Nature of Logarithms, Subduction in them answers to Division in other Numbers; therefore it follows, that when a Number is given consisting both of Integers

tegers and Decimals, we can find the Logarithm answering thereto in the following Manner: viz. Find the Logarithm of the whole consider'd as an Integer; then from that take the Logarithm of the Denominator of the decimal Part, or (which is the same) from the Index of the Logarithm of the whole consider'd as an Integer, subtract a Number less by Unity than the Number of Places in the Denominator of the Fraction, and the Remainder will be the Logarithm required.

*Example 1.* Suppose you were to find the Logarithm of 365, to do this you must first look for the Logarithm of 365, which is 2.56229 then because 10 is the Denominator of the decimal Part of the propos'd Number, and 1.00000 its Logarithm, therefore from 2.56229 take 1.00000 and there remains 1.56229 the Logarithm required.

*Example 2.* And to find the Logarithm of 6.543. First find the Logarithm of 6543 consider'd as an Integer, which by the Tables you will find to be 3.81578 then since 3.00000 is the Logarithm of 1000 the Denominator of the fractional Part, therefore from 3.81578 take 3.00000 and there will remain 0.81578 which is the Logarithm required.

The Reverse of this, viz. the Logarithm of a Number consisting of Integers and Decimals being given to find that Number, is perform'd according to the following Method.

*Rule.* Look in your Table of Logarithms (without regarding the Indices) for that whose decimal Part is equal or nearly equal to the decimal Part of the Logarithm proposed; then subtract the Index of the former from that of the latter; and lastly divide the Number answering the Logarithm found in your Tables, by a Number consisting of an Unit, and as many Cyphers as there are Units in the Difference between the two Indices; or, which is the same, cut off as many Figures (beginning at the lowest)

lowest Place) of the Number answering to the Logarithm in your Table, as there are Units in the Difference of the Indices, and the Number last found will be that required.

*Example.* Suppose it were required to find the Number answering to the Logarithm 2.73608.

In Order to do this I look in the Table of Logarithms (without minding the Indices) for that whose decimal Part is equal, or nearly equal, to .73608 the decimal Part of the Logarithm propos'd, and I find it to be 3.73608; from the Index of which, *viz.* 3, I take 2, the Index of the propos'd Logarithm, and there remains 1. Lastly, I divide 5446, the Number answering the Logarithm found in the Tables, by 10, and the Quotient 544.6 is the Number required.

The Reason of this &c. the preceding Rule, is plain from the very Nature of Logarithms.

From what has been said on this Head we may easily solve the following Problem by the Logarithms: *viz.*

*Prob. 1.* Given two Numbers, as 25.6 and 134, to find the Product of their Multiplication. To solve this by the Logarithms, I first look for the Logarithm of 25.6 which I find to be 1.4 824, then for that of 134 which is 2.12710; then I add these two Logarithms together, and their Sum is 3.53534, which is the Logarithm of their Product; so I look in my Table for the Number answering to 3.53534, and I find it to be 3430, which is nearly equal to the Product of 25.6 into 134.

Again, if it were required to find the Product of 36 into 234, I proceed as in the last Example, and the Operation is as follows:

2.36922 the Logarithm of 234

1.55630 the Logarithm of 36

Sum 3.92552 the Logarithm of their Product,  
E 2 which,

which, by the Table, I find to be 8424, which is the Product of the two Numbers propos'd.

*Prob. 2.* Let it be required to find the Quotient that arises by dividing one Number by another, suppose 828 by 23.

To solve this by the Logarithms, I first look in the Tables for the Logarithm of 828, the Dividend, which I find to be 2.91803; then for the Logarithm of 23 the Divisor, which is 1.36173 and this last taken from the former Logarithm, there remains 1.55630 the Logarithm of the Quotient, which answers to the Number 65 the Quotient required.

Again, let it be required to divide 3055 by 47; by proceeding according to the last Example, the Operation will be as follows:

$$\begin{array}{r} 3.48501 \text{ the Logarithm of } 3055 \text{ the Dividend,} \\ 1.67210 \text{ the Logarithm of } 47 \text{ the Divisor,} \\ \hline 1.81291 \text{ the Logarithm of the Quotient.} \end{array}$$

which answers to the Number 65 the Quotient required.

*Prob. 3.* Three Numbers being given to find a fourth proportional to them, viz. Such as shall have the same Proportion to the third as the second has to the first.

*Rule.* Take from the Tables the Logarithm of each of the propos'd Numbers, then add the Logarithms of the second and third together, and from the Sum take the Logarithm of the first, and the Remainder shall be the Logarithm of the fourth Number requir'd.

*Example.* Let the three propos'd Numbers be 48, 66, to which we are to find a fourth proportional; by the preceding Rule, the Operation will stand as follows:

1.68124 the Logarithm of 48 the 2d Term,  
1.81954 the Logarithm of 66 the 3d Term,

3.50078 the Logarithm of their Product,  
1.55630 the Logarithm of the 1st Term, 36.

9 48 the Log. of the 4th Term requir'd.

which, by looking into the Table, I find answers to the natural Number 88, which is the 4th Proportional to the three propos'd Numbers.

Again, let it be required to find a fourth proportional to the three Numbers 24, 144, 123; by proceeding according to the foregoing Rule, the Operation will stand as follows:

2.15836 the Logarithm of the 2d Term 144.  
2.08991 the Logarithm of the 3d Term 123.

4.24827 the Logarithm of the Product,  
1.38021 the Logarithm of the 1st Term 24.

2.86806 the Log. of 738, the 4th Number requir'd.

*Prob. 4.* To find the Square of any Number by Logarithms.

*Rule.* Multiply the Logarithm of the given Number by 2, and the Product is the Logarithm of the Square sought.

*Example.* Required to find the Square of 36. First I look in the Table for the Logarithm of 36, and find it to be 1.55630, which doubled gives 3.11260 the Logarithm of the Square sought, which by Inspection I find answers to the natural Number 1296 the Square of 36, viz. the Product of 36 multiplied into itself.

*Prob. 5.* To extract the Square Root of any propos'd Number, i. e. to find a Number which multiply'd into itself, shall produce the given Number.

*Rule.*

*Rule.* Divide the Logarithm of the propos'd Number by 2, and the Quotient will be the Logarithm of the Square Root required.

*Example.* Required to find the Square Root of 1296. First I look in the Tables for the Logarithm of 1296, and find it to be 3.11261, which divided by 2 gives 1.55630 for the Logarithm of the Square Root, and the natural Number answering thereto is 36 the Root required.

If for the Sine, Tangent, &c. of every Degree and Minute in the Quadrant, in the natural Tables, we take the Logarithm agreeing to each, we shall have a Table of Logarithmic Sines, Logarithmic Tangents, &c. as is in the second Table at the End of this Book.

In which you may observe, that each Page is divided into eight Columns, the first and last of which is Minutes, and the intermediate Ones contain the Sines, Tangents and Secants; the upper and lower Columns contain Degrees; the Column of Minutes on the left Hand of each Page, answers to the Degrees in the top Column, and the Sines, Tangents, and Secants, belonging to these Degrees, and Minutes are in the Columns mark'd at the Top with the Words, Sine, Tangent, Secant; the Column of Minutes on the right Hand of each Page, answers to the Degrees in the Foot of the Page, and the Sines, Tangents, and Secants, answering to these Degrees and Minutes, are in the Columns mark'd at the Bottom with the Words, Sine, Tangent, Secant; the Degrees in the top Column beginning at 0, proceed to 44 where they end, and those at the Foot of the Page begin at 89 proceed to 45 in a decreasing Series, the Degrees in the different Columns being the Complement of each other. From what has been said, we may easily find the Sine, Tangent or Secant, of any Arch, from our Tables, by looking for the given Number of Degrees at the Head or Foot of the

Page, according as they are less or greater than 45, and in the proper side Column for the odd Minutes, if there be any; then below or above the Word, Sine, Tangent, or Secant, and on the same Line with the Minutes, we shall have that requir'd.

*Example 1.* Required to find the Sine of 36 deg. 40 min. To find this, I look at the Head of the Page for 36 deg. and in the side Column, on the left Hand, for 40 min. then below the Word Sine, and on the same Line with 40, I find 9.7009 which is that required.

*Example 2.* Requir'd the Tangent of 54 deg. 30 min. To find this, I look at the Foot of the Page (because the Degrees propos'd are greater than 45) for 54 deg. and in the right Hand side Column for 30 min. then in the Column mark'd with Tangent at it's Bottom, and on the same Line with the 30 min. in the side Column, I find 14673, which is the Log-Tangent requir'd.

The Reverse of this, viz. The Logarithm of a Sine, Tangent or Secant, being given to find the Arch belonging to it, is perform'd by only looking in the proper Column for the nearest Logarithm to that propos'd, and the Degrees and Minutes answering thereto is what was required.

In these Tables the Secants might have been wanting, because all the Proportions in which the Secants are concern'd may be wrought without them, by the Sines and Tangents only, as shall be shewn particularly in the Solution of the several Cases of plain Trigonometry.

72. The Chord, Sine Tangent, &c. of any Arch in one Circle, is to the Chord, Sine, Tangent, &c. of the same Arch in another Circle, just as the Radius of the one is to the Radius of the other; for this proportion, the greater the Radius is, the greater is the Circle described by that Radius, and consequently the greater any particular Arch of that Circle is, and

and so the Sine, Tangent, &c. of that Arch is also the greater; therefore, in general, the Chord, Sine, Tangent, &c. of any Arch is proportionable to the Radius of the Circle.

73. In all Circles the Chord of 60 is always equal in Length to the Radius. Thus in the Circle AEBD, if the Arch AEB be an Arch of 60 Degrees, then drawing the Chord AB, I say AB shall be equal to the Radius CB or AC; for in the Triangle CAB, the Angle ACB is 60 Degrees, being measured by the Arch AEB; therefore the Sum of the other two Angles is 120 Degrees, (by Cor. 1. of 61st) but

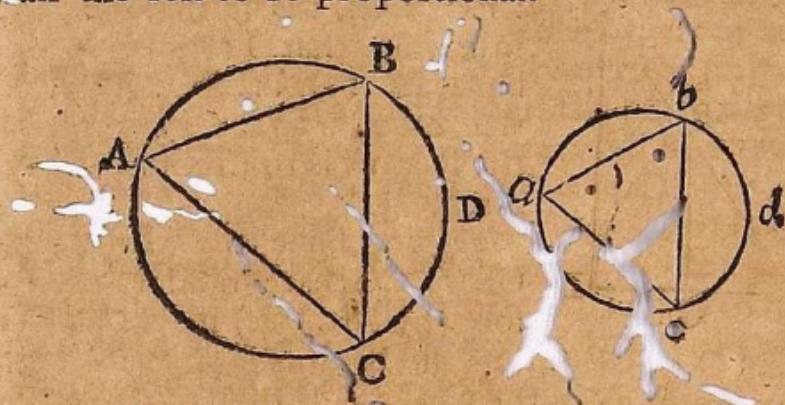


since AC and CB are equal the two Angles CAB, CBA will also be equal; consequently each of them half their sum 120, viz. 60 Degrees; therefore all the three Angles are equal to one another, consequently all the Legs, therefore AB is equal to CB.

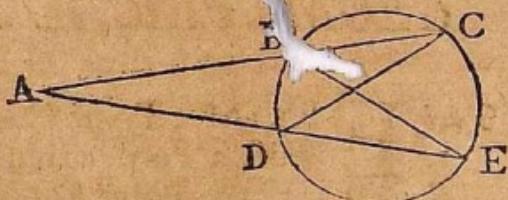
*Cor.* Hence the Radius from which the Lines on any Scale were form'd, is the Chord of 60 on the Line of Chords.

74. If in two Triangles ABC, abc all the Angles of the one be equal to all the Angles in the other, each to each respectively, that is, the Angle BAC equal to the Angle bac, the Angle ACB equal to the Angle acb, and the Angle ABC equal to the Angle abc; then the Legs opposite to the equal Angles are proportionable, viz.  $A B : ab :: A C : ac$  and  $A B : ab :: B C : bc$  and  $A C : ac :: B C : bc$ ; for being inscribed in two Circles, 'tis plain, since the Angle BAC is equal to the Angle bac, the Arch BDC is equal the Arch bdc and consequently the Chord BC is to the Chord as the Radius of the Circle ABC to the Radius of the Circle abc (by the 7<sup>th</sup>d); the same Way the Chord AB

A B is to the Chord  $ab$  in the same Proportion. So  $AB : ab :: BC : bc$ ; the same way we may prove all the rest to be proportional.

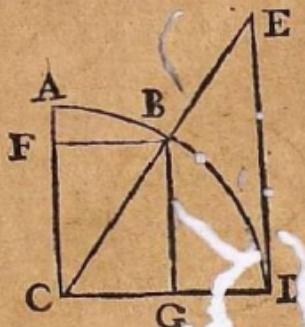


75. If from a Point A without a Circle DBCE, there be drawn two Lines ADE, ABC, each of them cutting the Circle in two Points; then, I say, the Product of the one which cuts the Circle into its external Part, viz. AC into AB is equal to the Rectangle of the other Line into its external Part, viz. AE into AD: for drawing the Lines DC, BE, 'tis plain in the two Triangles ABE, ADC, the Angle AEB in the one is equal to the Angle ACD in the other (by Cor. 2. of 63d), and the Angle at A is common; therefore, the other Angle ADC is equal to the Angle ABE (by Cor. 1. of 61.) therefore the Triangle ABE is equi-angular to the Triangle ADC; consequently  $AC : AE :: AD : AB$  by the last, and therefore  $AC$  into  $AB$  is equal to  $AE$  into  $AD$ .



76. Let ABD be a Quadrant of a Circle described by the Radius CD; BD any Arch of it, and ~~BA~~<sup>C</sup> its Complement, BG or CF the Sine, CG or BF the Co-Sine, DE the Tangent, and CE the Secant of that Arch BD. Then since the Triangles CDE, CGB are similar, or equi-angular, it will

will be by (Art. 74.)  $DE : EC :: GB : BC$  i.e. the Tangent of any Arch, is to the Secant of the same, as the Sine of it is to the Radius. Also since  $DE : EC :: GB : BC$ ,



therefore by inverting that Proportion we have  $EC : DE :: BC : GB$  i.e. the Secant is to the Tangent, as the Radius is to the Sine of any Arch.

Again, since the Triangles  $CDE$ ,  $CGB$  are similar, therefore (by Art. 74.) it will be  $CD : CE :: CG : CB$  as the Radius is to the Secant of any Arch, so is the Co-sine of that Arch to the Radius. And by inverting the Proportion we have this, viz. As the Secant of any Arch is to the Radius, so is the Radius to the Co-Sine of that Arch.

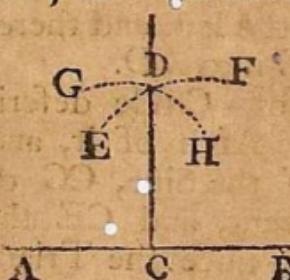
Having thus gone thro' the Theorems of *Geometry*, that are necessary for the Knowledge of *Naviga-tion*; we shall next proceed to some Problems that are useful for the Practice of that Art.

## *GEOMETRICAL PROBLEMS.*

*Prob.* **F**ROM a Point C in a given Line A B to raise a Perpendicular to that Line.

*Rule.* From the Point C take the equal Distances  $CB$ ,  $CA$  on each Side of it. Then stretch the

Compasses to any Distance greater than  $CB$  or  $CA$ , and with one Foot of them in  $B$ , sweep the Arch  $EF$  with the other; again, with the same Opening, and one Foot in  $A$ , sweep the Arch  $GH$  with the other;

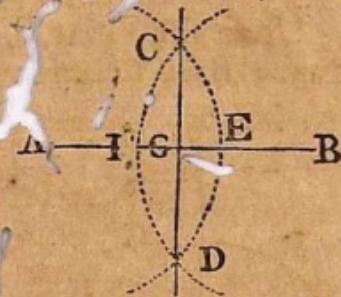


the

these two Arches will intersect one another in the Point D; then join the given Points C and D with the Line CD, and that shall be the Perpendicular required.

2. To divide a given right Line AB into two equal Parts; that is, to biseect it.

*Rule.* Take any Distance with your Compasses that you are sure is greater than half the given Line; then setting one Foot of them in B, with the other sweep the Arch DFC; and with the same Distance and one Foot in A, with the other sweep the Arch CED; these two Arches will intersect one another in the Points C, D, which is divid'd by the right Line DC which bisect AB in G.



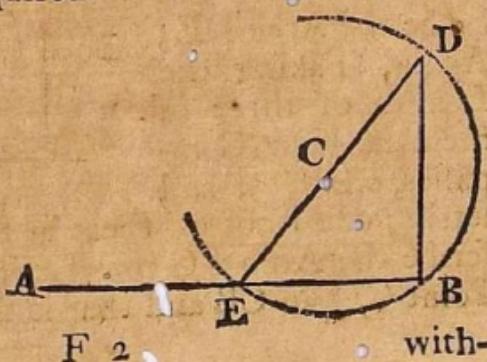
3. From a given Point D to let fall a Perpendicular on a given Line AB.

*Rule.* Set one Foot of the Compasses in the Point D, and extend the other to any Distance greater than the least Distance between the given Point and the Line, and with that Extent sweep the Arch AEB, cutting the Line in the two Points A and B, then (by the last Problem) biseect the Line AB in the Point C, lastly join C and D, and that Line CD is the Perpendicular required.



4. Upon the End B of a given right Line BA, to raise a Perpendicular.

*Rule.* Take any Extent of your Compasses, and with one Foot in B fix the other in any Point C,



### 36 Geometrical Propositions.

without the given Line, then with one Point of the Compasses in C, describe with the other, the Circle EBD, and thro' E and C draw the Diameter, ECD meeting the Circle in D; join D and B, and the right Line DB is that required; for EBD is a right Angle (by Cor. 4. of 63d).

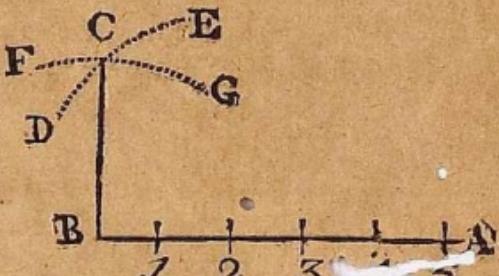
#### Another Way.

Upon the Point B as a Center, and with any Distance BA, describe the Circle ACD; set off the Radius from A to C and from C to D, then with the same Extent of the Compasses, and one Foot in C, describe with the other Foot the Arch FG, and with the same Opening on the Center D describe the Arch KH which will cut the Former in E, then join EB and that shall be the Perpendicular requir'd.



#### Another Way.

From the Point B set off with your Compasses five small equal Parts, then with the Distance of all the five taken in your Compasses, setting one Foot at the fourth Division, *viz.* in the Point 4, with the other describe the Arch DE; Again, Taking the Length of three of them in your Compasses, *viz.* B 3, and setting one Foot of them in B, with the other describe the Arch FG intersecting the former in the Point C, join CB and that is the Line required.



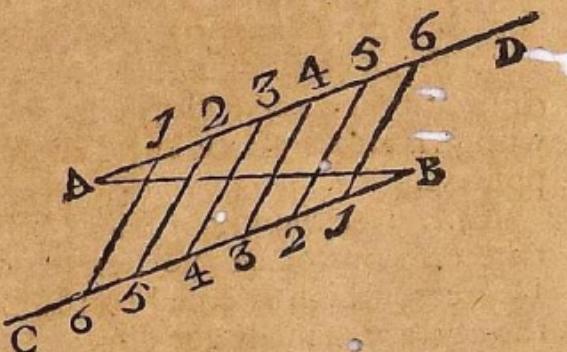
5. To draw one Line parallel to another given Line A B, that shall be distant from one another by any given Distance D.

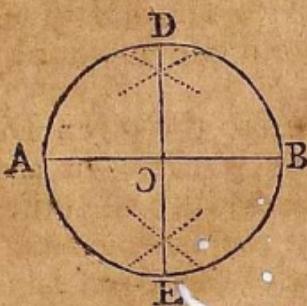
*Rule.* Extend your Compasses to the given Distance D; then setting one Foot of them in any Point of the given Line (suppose A) with the other sweep the Arch FCG; again, at the same Extent, and one Foot in any other Point of the given Line B sweep the Arch HDK, and draw the Line CD touching them, and that will be parallel to the given Line AB, and distant from it by the Line D as was requir'd.



6. To divide a given Line AB into any Number of equal Parts, suppose 7.

*Rule.* From the Point A draw any Line AD, making an Angle with the Line AB, then thro' the Point B draw a Line BC parallel to AD; and from A, with any small opening of the Compasses, set off a Number of equal Parts (on the Line AD) less by one than the propos'd Number (here 6) then from B set off the same Number of the same Parts on the Line BC, lastly, join 6 and 1, 2 and 5, 3 and 4, 4 and 3, 5 and 2, 6 and 1, and these Lines will cut the given Line as requir'd.





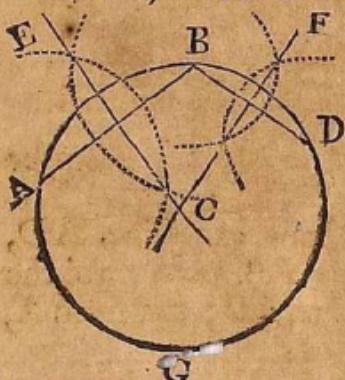
7. To quarter a given Circle, or to divide it into four equal Parts.

*Rule* Thro' the Center C of the given Circle draw a Diameter A B, then upon the Point C raise a Perpendicular D C E to the Line A B; and these two Diameters A B and

D E shall quarter the Circle.

8. Thro' three given Points A, B, and D to draw a Circle. (*Note*, the three Points must not lie in the same strait Line.)

*Rule.* Join A and B, also B and D with the strait Lines A B, B D, then by *Prob. 2*, bisect A B with the Line E C, also B D with the Line F C, which two



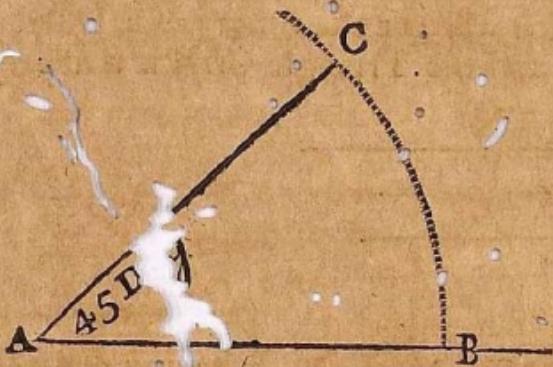
Lines will cut one another in some Point C, that is the Center of the Circle required; then fixing one Point of your Compasses in C, and stretching the other to A, describe the Circle A B D G, which will pass through the three Points given. The Reason of this

is plain from *Cor. 1. of Art. 65.*

9. From the Point A of the given Line A B, to draw another Line (suppose A C) that shall make with A B an Angle of any Number of Degrees, suppose 45.

*Rule.* Let the given Line A B be produced, then take off your Scale the Length of the Chord of 60 Degrees, which is equal to the Radius of the Circle the Scale was made for (by *Art. 73.*) And setting one Foot in A, with the other sweep the Line B C; then with your Compasses take from your Scale the Chord of 45 Degrees, and set off that Distance from B to

B to C. Lastly join A and C, and the Line AC is that requir'd. For the Angle CAB, which is measur'd by the Arch BC, is an Angle of 45 Degrees as was requir'd.



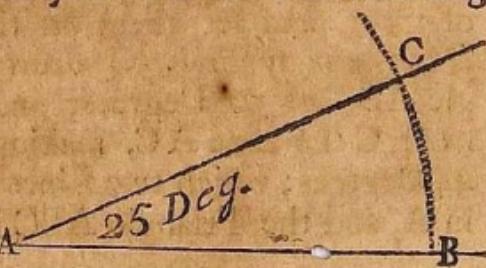
10. An Angle BAC being given, to find how many Degrees it contains.

*Rule.* With your Compasses take the Length of the Chord of 60 from your Scale. Then setting one Foot of them in A, with the other sweep the Arch BC, which is the Arch comprehended between the two Legs AB,

AC produc'd, if needful. Lastly, take with your Compasses the Distance BC, and applying it to your Line of Chords on the Scale, you'll find how many Degrees the Arch BC contains, and consequently the Degrees of the Angle BAC which was requir'd.

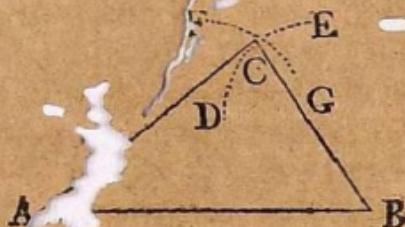
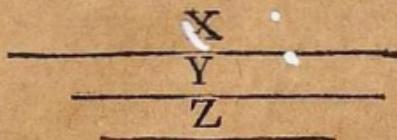
11. Three Lines X, Y, and Z being given, to form a Triangle of them, but any two of these Lines taken together, must always be greater than the third.

*R.* Make any one of them, as X, the Base; then with your Compasses take another of them, as Z,



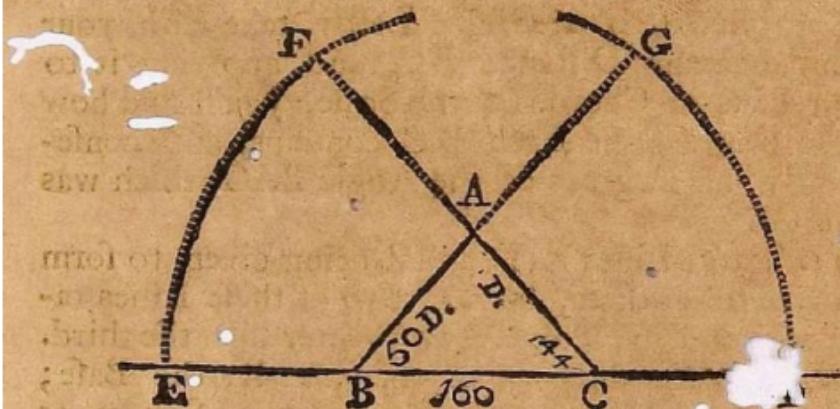
## 40. Geometrical Propositions.

Z, and setting one Foot in one End of the Line X, as B, with the other sweep the Arch DE; and taking with your Compasses the Length of the other Y, set one Foot of them in A, the other End of the Line X, and with the other sweep the Arch FG, which will cut the other in C; lastly, join CA and CB, and the Triangle CAB is that requir'd.



12. To make a Triangle having one of its Legs of any Number of equal Parts (suppose 160), and one of the Angles at that Leg 50 Degrees and the other 44 Degrees.

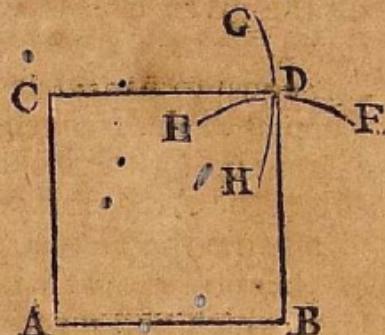
*Rule.* Draw an indefinite Line ED, then take off the Line of equal Parts with your Compasses 160 of them, and set them on the indefinite Line, as BC then (by Prob. 9.) draw BA making the Angle ABC of 50 Degrees, and by the same, draw from C the Line AC, making the Angle ACB of 44 Degrees; which two Lines will meet one another in A, and the Triangle ABC is that required.



13. Upon

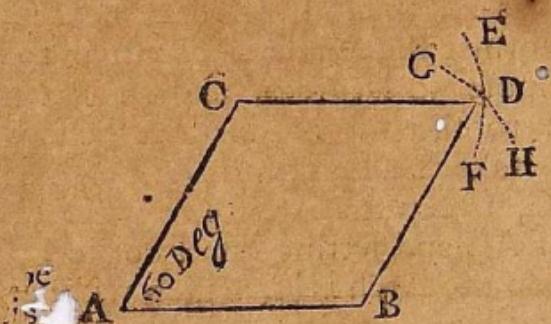
13. Upon a given Line AB to make a Square.

*Rule.* Upon the Extremity A of the given Line AB raise a Perpendicular AC (by Prob. 4.); then take AC equal to AB; and with that Extent, setting one Foot of the Compasses in C, sweep with the other Foot the Arch GH, then with the same Extent and on Foot in B, with the other sweep the Arch EF; which will meet the former in some Point D; lastly, join C and D, D and B, and the Figure ABDC will be the Square requir'd:



14. On a given Line AB to draw a Rhombus that shall have one of its Angles equal to any Number of Degrees, suppose 60 Degrees.

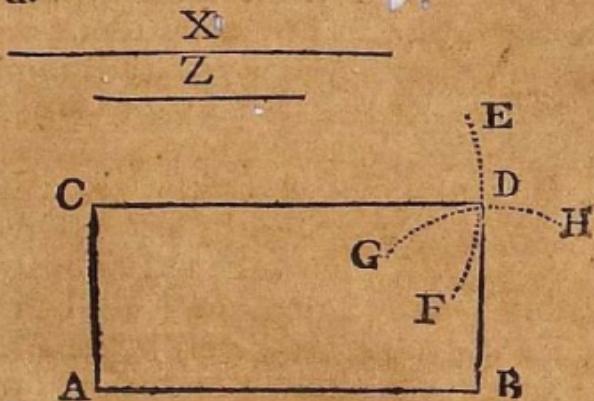
*Rule.* From the Point A of the given Line AB draw the Line AC, making the Angle CAB of 60 Deg. (by Prob. 9.); then take AC equal to AB, and with that Extent fixing one Foot of the Compasses in B, with the other describe the Arch GH, and at the same Extent fixing one Foot of the Compasses in C, with the other describe the Arch EF cutting the former in D; lastly, join CD and DB and the Figure ACDB is that requir'd.



42. Geometrical Propositions.

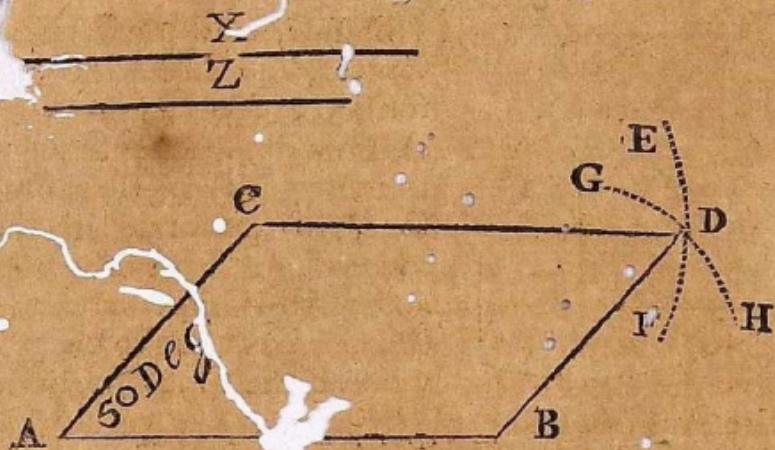
15. Given two Lines X and Z, of these two make a Rectangle.

*Rule.* Draw a Line as AB, equal in Length to one of the given Lines X, and on the Extremity A of that Line raise a Perpendicular AC, on which take AC equal to the other Line Z; then take with your Compasses the Length of the Line AB, and at that Extent fixing one Foot of them in C, with the other sweep the Arch EF; and also taking with your Compasses the Extent of the Line AC, fix one Foot of them in B, and with the other sweep the Arch GH, which will meet the former in D; lastly join CD and BD, and the Figure ABCD will be that requir'd.



16. Two Lines X and Z being given, of these to form a Rhomboides that shall have one of its Angles any Number of Degrees, suppose 50.

*Rule.* Draw a Line AB equal in Length to one of the Lines as X, then draw the Line AC, making with the former the Angle BAC equal to the propos'd, suppose 50 Degrees, and on that Line take AC equal to the given Line Z, then with your Compasses take the Length of AB, and fixing one Foot in C, sweep the Arch EF; also taking the Length of AC and setting one Foot in B, with the other sweep the Arch GH, which will meet the former in D; then join CD and BD, so the Figure ACDB will be that required.



And thus we have gone thro' all *Geometry* that is necessary for our present Business, both as to Theory and Practice. The next Thing we go on, is, the Principles of *Plane Trigonometry*.

## S E C T. II.

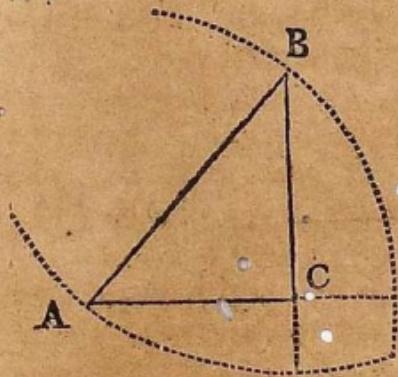
### Of Plane TRIGONOMETRY, Right and Oblique Angled.

1. PLANE TRIGONOMETRY, is that Science by which we measure the Sides and Angles of Plane Triangles.

2. Since Triangles are either right or oblique-angled; therefore Trigonometry is commonly divided into two Kinds, viz. *Rectangular* and *Oblique-angular*: and first we shall treat of *Rectangular*.

3. In any right-angled Triangle as ABC, if the Hypotenuse be made the Radius, and with that a Circle be described on the one End A as a Center; then 'tis plain that BC will be the Sine of the Angle BAC (by Art. 21. of Sect. I.) and if with the same

## Plane Trigonometry.



Distance, and on B as Center, a Circle be describ'd, 'tis plain that A C will be the Sine of the Angle A B C; therefore, in general, if the Hypotenuse of a right-angled Triangle be made the Radius, the two Legs will be the Sines of their

opposite Angles.

4. If in a right-angled Triangle D E F, one of the Legs, as D F, be made the Radius, and on the Extremity D at one of the oblique Angles, viz. that which is form'd by the Hypotenuse and the Leg made Radius) as a Center, a Circle be describ'd; 'tis plain, that the other Leg E F will be the Tangent of the Angle at D, and the Hypotenuse D E

E will be the Secant of the same Angle (by Art. 24, 25, and 67 of Sect. I.). The same Way, making the Leg E F the Radius, and on the Center E describing a Circle, the other Leg G F will become the Tangent of the Angle at E, and the Hypotenuse D E the Secant of the same.

5. It has been already shewn, at Art. 72. of Sect. I. that the Chord, Sine, Tangent, &c. of any Arch, or Angle, in one Circle, is proportionable to the Chord, Sine, Tangent, &c. of the same Arch, in any other Circle; from which, and the two foregoing Articles the Solutions of the several Cases of rectangular Trigonometry naturally follows.

6. Since Trigonometry consists in determining the Angles and Sides from others given, there arise various Cases, which are seven in Rectangular and six in Oblique-angular Trigonometry.

We shall now proceed to the Solution of the several Cases of Rectangular Trigonometry.

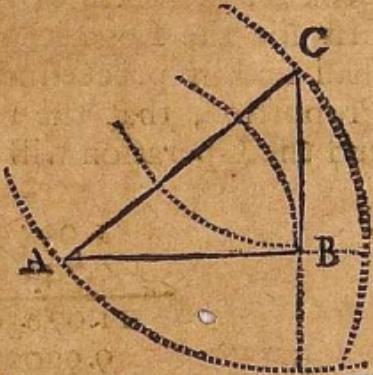
## CASE I.

*The Angles and one of the Legs given, to find the other Leg.*

Example. In the Triangle ABC right-angled at B, suppose the Leg AB, 86 equal Parts, (as Feet, Yards, Miles, &c.) and the Angle A  $33^{\circ} 40'$ . requir'd the other Leg BC in the same Parts with AB.

*Geometrically.*

Draw AB equal to 86, from any Line of equal Parts, then (by Prob. 4. of Sect. I.) upon the Point B, erect the Perpendicular BC; lastly from the Point A draw the Line AC, making with AB an Angle equal to  $33^{\circ} 40'$ , and that Line produc'd will meet BC in C, and so constitute the Triangle. The Length of BC may be found by taking it in your Compasses, and applying it to the same Line of equal Parts that AB was taken from.

*By Calculation.*

First by making the Hypotenuse AC Radius, the other two Legs will be the Sines of their opposite Angles (by Art. 3. of this) viz. AB the Sine of C, and CB the Sine of A; now since (by Art. 72. of Sect. I.) the Sine, Tangent, &c. of any Arch in one

one Circle is proportionable to the Sine, Tangent &c. of the same Arch in any other Circle, 'tis plain the Sines of the Angles A and C in the Circle described by the Radius AC, must be proportionable to the Sine of the same Arches or Angles, in the Circle, that the second Table at the End of this Book was calculated for; so the Proportion for finding BC will be

$$S, C : A B :: S, A : B C.$$

i. e. As the Sine of the Angle C in the Tables, is to the Length of AB (or Sine of C in the Circle whose Radius is AC) so is the Sine of the Angle A in the Tables, to the Length of BC (or Sine of the same Angle in the Circle whose Radius is AC).

Now the Angle A being  $33^{\circ} 40'$ , the Angle C must be  $56^{\circ} 20'$  (by Art. 61. Cor. 2. Sect. 1.) ; therefore looking in the second Table at the End of this Book for the Sines of the two Angles, and in the first for the Logarithm of 86 the given Leg, we shall find by proceeding according to the foregoing Proportion, that the required Leg BC, is 57.28; and the Operation will stand as follows.

$$\begin{array}{r} 1.95450 \quad A B \quad 86 \\ 9.74380 \quad S, A \quad 33^{\circ}, 40' \\ \hline 11.67830 \\ 9.92027 \quad S, C \quad 56^{\circ}, 20' \\ \hline 1.75803 \quad B C \quad 57.28 \end{array}$$

2dly, Making AB the Radius, 'tis plain BC, the Leg required, will be the Tangent of the given Angle A (by the 4th of this), and so the Proportion for finding BC, when AB is made the Radius, will be,

$$R : T, A :: A B : B C.$$

i. e. as the Radius in the Tables, is to the Tangent of the Angle A in the same, so is the Length of BA, or

or Radius in the Scheme, to the Length of BC or Tangent of A in the Scheme; therefore looking in the Tables for the Parts given in the foregoing Proportion, and proceeding with them according to that Rule, we shall find BC to be 57.28 as before, and the Operation will be as follows:

$$\begin{array}{r}
 9.82352 \quad T, A \quad 33^\circ, 40' \\
 1.93450 \quad A B \quad 86 \\
 \hline
 11.758 \\
 10.00000 \quad R a d. \quad 90^\circ \\
 \hline
 1.758 \quad B C \quad 57.28
 \end{array}$$

Lastly, by making BC, the Leg requir'd, the Radius, tis plain that AB will be the Tangent of C, and the Proportion for finding BC will be as follows:

$$T, C : R :: A B : B C$$

$$\begin{array}{r}
 i. e. \text{ as the Tangent of } C 56^\circ, 20' \quad 10.17648 \\
 \text{is to Radius} \quad - - - - - \quad 90^\circ \quad - \quad 10.00000 \\
 \text{so is the Length of } A B \quad - - 86 \quad - \quad 1.93450 \\
 \hline
 \end{array}$$

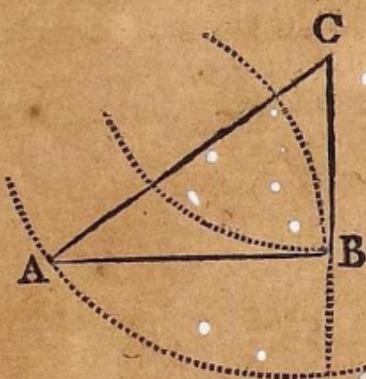
$$\begin{array}{r}
 11.93450 \\
 10.17648 \\
 \hline
 \text{to the Length of } B C \quad - \quad 57.28 \quad - \quad 1.758
 \end{array}$$

### C A S E 2.

*The Angles and one of the Legs given, to find the Hypotenuse.*

*Example.* In the Triangle ABC, suppose AB 124, and the Angle A  $34^\circ, 20'$ ; consequently the Angle C  $55^\circ, 40'$  requir'd the Hypotenuse AC, in the same Parts with AB.

## Geometrically.



This Case is constructed after the same Manner with the former, and the Hypotenuse AC is found by taking it's Length in your Compases, and applying that to the Line of equal Parts you took AB from.

## By Calculation.

1st, By making AC the Radius we shall have the following Proportion for finding AC, viz.

$$S, C : R :: A B : A C$$

i. e. as the Sine of C - - - - -	$55^{\circ} 40'$	- - - - -	9.91686
is to Radius - - - - -	$90^{\circ}$	- - - - -	10.00000
so is AB - - - - -	$124$	- - - - -	2.09342
to AC - - - - -	$150.2$	- - - - -	2.17656

2dly, Making AB the Radius we have this Proportion, viz.

$$R : \text{Sec. } A :: A B : A C$$

i. e. as Radius - - - - -	$90^{\circ}$	- - - - -	10.00000
is to the Secant of A - - - - -	$34^{\circ} 20'$	- - - - -	10.08314
so is AB - - - - -	$124$	- - - - -	2.09342
to AC - - - - -	$150.2$	- - - - -	2.17656

This may be done without the Help of the Secants; for since (by Art. 76. Sect. 1)  $R : \text{Sec. } A :: \text{Co-S. } A : R$ ; therefore the former Proportion will become

$$\text{Co-S. } A : R :: A B : A C$$

i. e. As

i. e. As the Co-Sine of A	$34^\circ, 20'$	9.91686
is to the Radius	$90^\circ$	10.00000
so is AB	124	2.09342
to AC	150.2	2.17656

3dly, Making BC the Radius, we have the following Proportion, viz.

$$T, C : \text{Sec. } C :: AB : AC$$

i. e. as the Tangent of C	$55^\circ, 40'$	10.16558
is to Sec. C	$55^\circ, 40'$	10.24872
so is AB	124	2.09342
to AC	150.2	2.17656

This likewise may be done without the Help of Secants, for since (by Art. 76. Sect. 1.)  $T, : \text{Sec.} :: S, : R$ ; therefore the former Analogy will be reduc'd to this, viz.

$$S, C : R :: AB : AC$$

where no Secants do appear, and it coincides with that in the first Supposition of this Case, so we shall not repeat the Operation.

### C A S E 3.

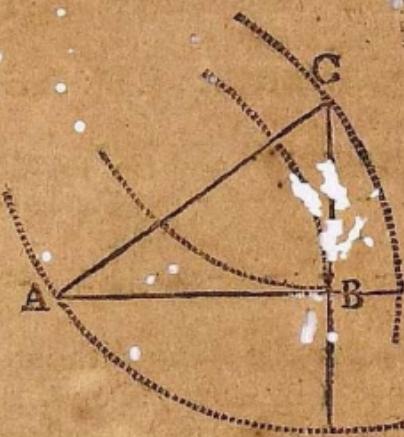
The Angles and Hypotenuse given, to find either of the Legs.

Example. In the Triangle ABC, suppose the Hypotenuse AC 146 equal Parts, and the Angle A  $36^\circ, 25'$ , consequently the Angle C  $55^\circ, 35'$ , requir'd the Leg AB.

### Geometrically.

Draw the Line AB at Pleasure, and make the Angle BAC equal to  $36^\circ, 25'$  (by Prob. 9. Sect. 1.) then take AC equal to 146 from any Line of equal

Parts; Lastly, from the Point C let fall the Perpendicular CB on the Line AB. So the Triangle is constructed, and AB may be measured from the Line of equal Parts.



### *By Calculation.*

1st, Making AC the Radius, we shall have the following Proportion, viz.

$$R : S, C :: AC : AB$$

i. e. as Radius	90°	10.00000
is to the Sine of C	53°, 35'	- 9.90565
so is AC	146	2.16435
to AB	117.5	2.07000

2dly, Making AB the Radius, we have the following Analogy, viz.

$$\text{Sec. A} : R :: AC : AB$$

i. e. as the Secant of A	36°, 25'	- 10.09435
is to Radius	90	10.00000
so is AC	146	2.16435
to AB	117.5	2.07000

This may be done without the help of Secants, for since (by Art. 76. Sect. I.) Sec. : R :: R : Co-S; therefore the former Proportion may be reduc'd to this, viz.

R :

R : Co-S, A :: AC : AB

which is the same with the Proportion in the first Supposition.

3dly, By supposing BC the Radius, we have the following Proportion, viz.

Sec. C : T. C :: AC : AB

i. e. as the Secant of C  $53^{\circ} 35'$  : 10.22647  
 is to the Tangent of C  $53^{\circ} 35'$  : 10.13212  
 so is AC - - - - - : 146 - - - 2.16435  
 to AB - - - - - : 117.5 - - - 2.07000

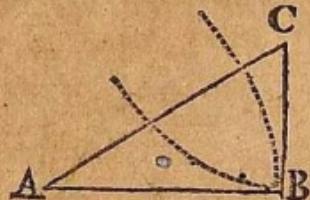
#### C A S E 4.

The two Legs being given to find the Angles.

Example. In the Triangle ABC, suppose AB 94 and BC 56. requir'd the Angles A and C.

#### Geometrically.

Draw AB equal to 94, from any Line of equal Parts, then from the Point B raise BC perpendicular to AB (by Prob. 4. Sect. 1.) and take BC from the former Line of equal Parts equal to 56; Lastly, join the Points A and C with the strait Line AC, so the Triangle is constructed, and the Angles may be measur'd by Prob. 10. Sect. 1.



#### By Calculation.

1st, Supposing AB the Radius, we have this Analogy, viz.

AB : BC :: R : T. A

i. e. as AB - - - 94 - - - 1 - - 1.97313  
 is to BC - - - 56 - - - 1 - - 1.74819  
 so is the Radius - -  $90^{\circ}$  - - - 10.00000  
 to the Tangent of A  $30^{\circ}, 47'$  - - - 9.77506

2dly, Making BC the Radius we have this Proportion, viz.

$$BC : BA :: R : T.C$$

i.e. as BC - - - 56 - - - - 1.74819  
 is to AB - - - 94 - - - - 1.97313  
 so is the Radius - 90° - - - - 10.00000  
 to the Tangent of C 59°, 13' - - - 10.22494

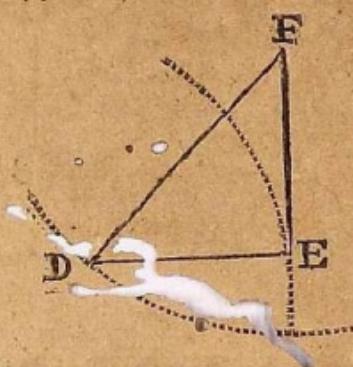
### C A S E . 5.

*The Hypotenuse, and one of the Legs given, to find the Angles.*

*Example.* In the Triangle DEF, suppose the Leg DE 83, and the Hypotenuse DF 126, requir'd the Angles D and F.

### Geometrically.

Draw the Line DE 83, from any Line of equal Parts, and from the Point E raise the Perpendicular



EF, then take the Length of DF 126, from the same Line of equal Parts, and setting one Foot of your Compasses in D, with the other cross the Perpendicular EF in F; Lastly, join D and F, so the Triangle is constructed, and the Angles may be measured by Prob. 10. Sect. I.

### By Calculation.

3dly, Making DF the Radius, we have this Proportion, viz.

$$DF : DE :: R : S.F$$

i.e. as

# Plane Trigonometry.

53

i.e. as DF	—	126	—	2.10037
is to DE	—	83	—	1.91908
so is the Radius	—	90°	—	10.00000
to the Sine of F	—	41°, 12'	—	9.81871

2dly, By supposing DE the Radius, we have the following Analogy, viz.

$$DE : DF :: R : \text{Sec. } D$$

i.e. as DE	—	83	—	1.91908
is to DF	—	126	—	2.10037
so is the Radius	—	90°	—	10.00000
to the Secant of D	—	48°, 48'	—	10.18129

This may be done without the Help of Secants, for since (by Art. 76. Sect. I.)  $R : \text{Sec. } D :: \text{Co-S} : R$ ; therefore the preceding Analogy will become this, viz.

$$DF : DE :: R : \text{Co-S. } D.$$

in which no Secants do appear; and it plainly coincides with the Proportion deduc'd from the first Supposition.

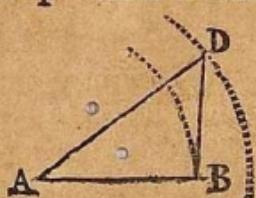
## C A S E . 6.

*The two Legs given to find the Hypothenuse.*

*Example.* In the Triangle ABD, suppose the Leg AB, 64, and BD 56, requir'd the Hypothenuse.

*Geometrically.*

The Construction of this Case is perform'd the same Way as in the fourth Case, and the Length of the Hypothenuse AB is found by taking it in your Compasses, and applying it to the same Line of equal Parts, that the two Legs were taken from.



By

## By Calculation.

This Case being a Compound of the 4<sup>th</sup> and 2<sup>d</sup> Cases, we must first find the Angles by the 4<sup>th</sup> thus:

$$AB : DB :: R : T, A.$$

i. e. as the Leg AB - - 64 - - 1.8063  
 is to the Leg DB - - 56 - - 1.74819  
 so is the Radius - - 90 - - 10.00000  
 to the Tangent of A - - 41°, 11' - - 9.94201

Then by the 2<sup>d</sup> Case we find the Hypotenuse requir'd thus:

$$S, A : R :: BD : AD$$

i. e. as the Sine of A - 41°, 11' - 9.81854  
 is to the Radius - 90° - - 10.00000  
 so is the Leg BD - 56 - - 1.74819  
 to the Hypotenuse AD 85.05 - - 1.92965

This Case may also be solv'd after the following Manner, viz.

From twice the Log. of the greater Side AB 3.61236  
 subtract the Log. of the lesser Side BD - 1.74819

and there remains - - - - - 1.86417  
 the Logarithm of 73.15 to which adding the lesser Side BD, we shall have 189.15 whose Log. is 2.11093  
 to which ad'. the Log. of the lesser Side BD 1.74819

and the Sum will be - - - - - 3.85912  
 the half of which is - - - - - 1.92956  
 the Logarithm of the Hypotenuse required.

Or it may be done by adding the Square of the two Sides together, and taking the Logarithm of that Sum, the half of which is the Logarithm of the Hypotenuse requir'd thus in the present Case:

The

The Square of AB (64) is - - - -	4096
The Square of BD (56) is - - - -	<u>3136</u>

The Sum of these Squares, is - - - -	7232
The Logarithm of which, is - - - -	3.85926
The half of which, is - - - -	1.92963
The Logarithm of 85.05 the Length of the Hypothenuse requir'd.	

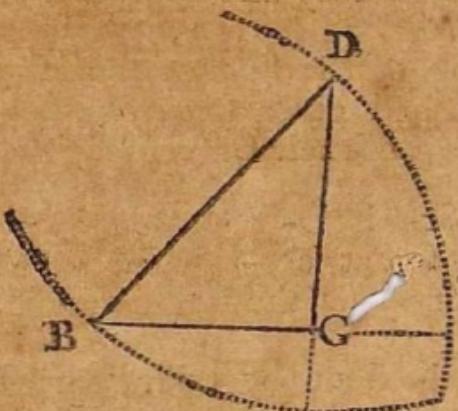
## C A S E 7.

*The Hypothenuse and one of the Legs given, to find the other Leg.*

*Example.* In the Triangle BGD, suppose the Leg BG, 87, and the Hypotenuse BD 142, requir'd the Leg DG.

*Geometrically.*

The Construction here is the same as in Case 5. the same Things being given; and the Leg DG is



found by taking its Length in your Compasses, and applying that to the same Line of equal Parts, the others were taken from.

## By Calculation.

The Solution of this Case depends upon the 1<sup>st</sup> and 5<sup>th</sup>; and first we must find the Oblique Angles by Case 5<sup>th</sup>, thus;

$$DB :: BG :: R : S, D$$

i. e. as the Hypoth. DB - 142 - - -	2.15229
is to the Leg BG - - - 87 - - -	1.93952
so is Radius ————— 90°, ————— 10.00000	
to the Sine of D ————— 37°, ————— 9.78723	

Then by Case 1<sup>st</sup> we find the Leg DG requir'd, thus;

$$R : S, B :: BD : DG.$$

i. e. as Radius ————— 90° ————— 10.00000	
is to the Sine of B - 52°, 13' - - -	9.89781
so is the Hypoth. DB 142 ————— 2.15229	
to the Leg DG - 112.2 ————— 2.05010	

The Leg DG may also be found in the following Manner, viz.

to the Log. of the Sum of the Hypothenuse and given Leg, viz. 229 { 2.35984  
add the Log. of their Difference, viz. 55-1.74036

and their Sum is - - - - - 4.10020  
the Half of that is - - - - - 2.05010  
the Log. of 112.2 the Leg requir'd.

Or it may be done by taking the Square of the given Leg from the Square of the Hypothenuse, and the Square Root of the Remainder is the Leg requir'd thus in the present Case;

the Square of the Hypotenuse 142, is - 20164  
 the Square of the Leg BG 87, is - - - 7569  
 the Difference of them is - - - - 12595  
 whose Logarithm is - - - - 4.10020  
 and half of that Logarithm is - - - 2.05010  
 which answers to the Natural Number 112.2 the Leg requir'd.

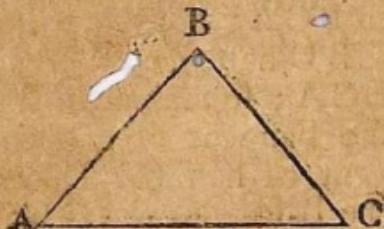
Thus we have gone thro' the seven Cases of right-angled Plane Trigonometry, from which we may observe;

1. That to find a Side, when the Angles are given, any Side may be made the Radius.
2. To find an Angle, one of the given Sides must of Necessity be made the Radius.

We now proceed to the Solution of the six Cases of Oblique-angled Plane Trigonometry, in order to which we must premise the following Theorems.

*Theorem 1.*: In any Triangle, the Sides are proportional to the Sines of the opposite Angles. Thus in the Triangle ABC, I say  $AB : BC :: \sin C : \sin A$  and  $AB : AC :: \sin C : \sin B$ ; also  $AC : BC :: \sin B : \sin A$ .

*Demonstration.*: Let the Triangle ABC be inscrib'd in a Circle; then 'tis plain, from Art. 66. Sect. 1. that the half of each Side is the Sine of its opposite Angle; but (by Art. 72. Sect. 1.) the Sines of these Angles in Tabular Parts, are proportional to the Sines of the same in any other Measure; therefore in the Triangle ABC, the Sines of the Angles will be as the Halves of their opposite Sides; and since the Halves are as the Wholes, it follows that the Sines of the Angles are as their opposite Sides, i. e.  $\sin C : \sin A :: AB : BC$ , &c.

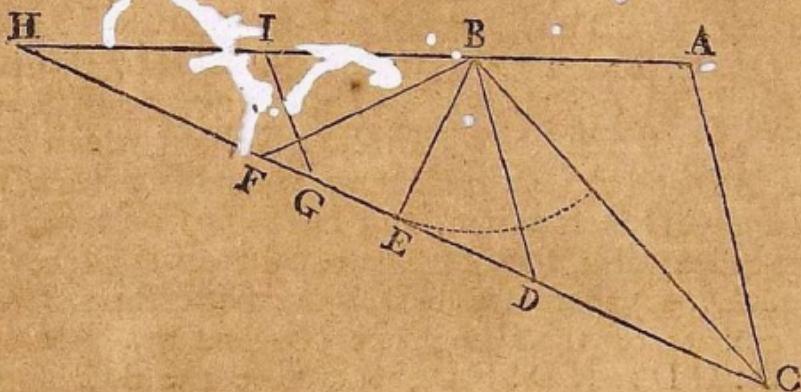


*Theor. 2.* In any plane Triangle, as ABC, the Sum of the Sides, AB and BC is to the Difference of these Sides, as the Tangent of half the Sum of the Angles at the Base, viz. A and C, is to the Tangent of half the Difference of these Angles.

*Demon.* Produce AB, and make BH equal to BC, join HC, and from B let fall the Perpendicular BE, thro' B draw BD parallel to AC, and make HF equal to CD, and join BF; also take BI equal to BA, and draw IG parallel to BD or AC.

Then 'tis plain that AH will be the Sum, and HI the Difference of the Sides AB and BC; and since HB is equal to BC, and BE perpendicular to HC, therefore HE is equal to EC, and BD being parallel to AC and IG, and AB equal to BI, therefore CD or HF is equal to GD, and consequently HG is equal to FD, and half HG is equal to half FD or ED. Again, Since HB is equal to BC, and BE perpendicular to HC; therefore the Angle EBC is half the Angle HBC; but (by Art. 60. Sect. I.) the Angle HBC is equal to the Sum of the Angles A and C, consequently the Angle EBC is equal to half the Sum of the Angles A and C. Also since HB is equal to BC, and HF equal to CD, and the included Angles BHF, BCD equal, it follows (by Art. 62. Sect. I.) that the Angle HBF is equal to the Angle DBC, which is equal to BCA (by Art. 36. Sect. I.) and since HBD is equal to the Angle A (by Art. 37. Sect. I.) and HBF equal to PCA; therefore FBD is the Difference, and EBD half the Difference of the two Angles A and BCA; so making EB the Radius, 'tis plain EC is the Tangent of half the Sum, and ED the Tangent of half the Difference of the two Angles at the Base. Now IG being parallel to AC, the Triangles HIG and HAC will be equiangular, consequently (by Art. 74. Sect. I.) AH : IH :: CH : GH, but the Wholes are as their Halves; therefore

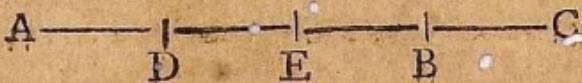
~~AH : IH :: CH : GH~~; and since  $\frac{1}{2} CH$  is equal to  $\frac{1}{2} EC$ , and  $\frac{1}{2} GH$  equal to  $\frac{1}{2} FD$  equal to  $ED$ ; therefore  $AH : IH :: EC : ED$ . Now  $AH$  is the Sum, and  $IH$  the Difference of the Sides, also  $EC$  is the Tangent of half the Sum, and  $ED$  the Tangent of half the Difference of the two Angles at the Base; consequently in any Triangle, as the Sum of the Sides is to their Difference, so is the Tangent of half the Sum of the Angles at the Base, to the Tangent of half their Difference.



Theor. 3. If to half the Sum of two Quantities be added half their Difference, the Sum will be the greater of them, and if from half their Sum be subtracted half their Difference, the Remainder will be the least of them.

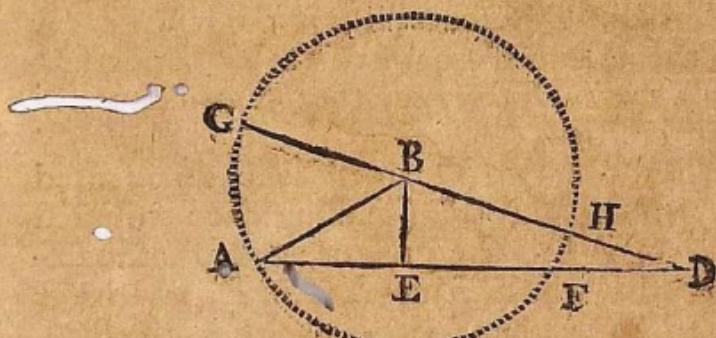
Demon. Let the two Quantities be represented by the Lines  $AB$  and  $BC$  (making one continued Line) whereof  $AB$  is the greater, and  $BC$  the less. Bisect the whole Line  $AC$  in  $E$ , and make  $AD$  equal to  $EC$ ; then 'tis plain  $AC$  is the Sum, and  $DB$  the Difference of the two Quantities, and  $AE$  or  $EC$  their half Sum, and  $ED$  or  $EB$  their half Difference. Now if to  $AE$  we add  $EB$ , 'tis plain the Sum will be  $AB$ , that is, to half the Sum we add half the Difference, the Sum will be the greater Quantity; also if from  $EC$  we take  $EB$ ,

the Remainder will be BC, that is, if from half the Sum we take half the Difference of two Quantities, the Remainder will be the least of them.



*Theor. 4.* In any right lin'd Triangle, ABD, the Base AD is to the Sum of the Sides AB and BD, as the Difference of the Sides is to the Difference of the Segments of the Base made by the Perpendicular BE, viz. the Difference between AE and ED.

*Demon.* Produce DB till it be equal to BA the lesser Leg; and on B as a Center, with the Distance BA or BG describe the Circle ACHF, which will cut BD and AD in the Points H and F; then 'tis plain, GD is the Sum, and HD the Difference of the Sides; also, since AE is equal to EF (by Art. 64. Sect. 1.) therefore FD is the Difference of the Segments of the Base; but (by Art. 75. Sect. 1.)  $AD:GD::HD:FD$ ; therefore the Base is to the Sum of the Sides, &c. as was to be proved.



### CASE I.

In any oblique-angled plane Triangle; two Sides, and an Angle opposite to one of them, given, to find the Angle opposite to the other.

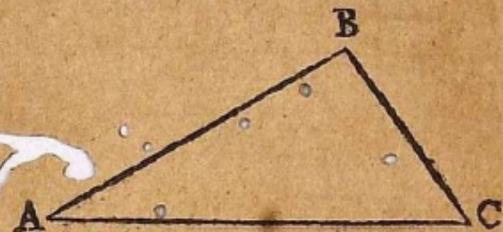
Example,

In the Triangle ABC, suppose AB = 16, BC = 84, and the Angle C, opposite to BA, =  $56^\circ 20'$ ; requir'd the Angle A opposite to BC.

### Geometrically.

Draw the Line AC, and at any Point of it, suppose C, make the Angle C equal to  $56^\circ 30'$  (by Prob. 10. Sect. 1.)

take C equal to  $84$ ; and with the Length of  $150$  taken from the Line of equal Parts with CB) in your



Compasses, fixing one Foot in B, with the other cross AC in A. Lastly, join A and B; so the Triangle is constructed, and the requir'd Angle A may be measur'd by Prob. 11. Sect. 1.

### By Calculation.

By Theorem 1. we have the following Proportion for finding the Angle A, viz.

$$AB : S, C :: BC : S, A.$$

i.e. as the Leg AB =  $156^\circ$  = 2.19512  
is to the Sine of its opposite Angle C,

$$\begin{array}{rcl} 56^\circ 20' & - & 9.92111 \\ \text{so is the Leg BC} & - & 84 \\ & - & \hline & 1.84539 \\ & & 2.19312 \end{array}$$

to the Sine of its opp. Angle A  $26^\circ 41' 9.65227$

### CASE 2.

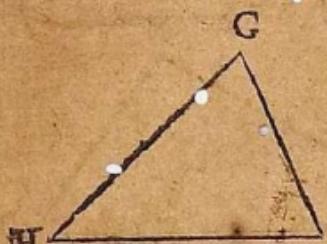
The Angles, and a Side opposite to one of them, given to find a Side opposite to another.

Example

*Example.* In the Triangle H B G, suppose the Angle H  $46^{\circ}$ ,  $15'$ , and the Angle B  $54^{\circ}$ ,  $22'$ ; consequently the Angle G  $79^{\circ}$ ,  $23'$ , and the Leg H B  $125$ , requir'd HG.

### Geometrically.

Draw H B  $125$ , from any Line of equal Parts,



and make the Angle H  $46^{\circ}$ ,  $15'$ , and B  $54^{\circ}$ ,  $22'$ , then produce the Lines H G and B G, till they meet one another in the Point G; so the Triangle is constructed, and

H G is measured by taking its Length in your Compasses, and applying it to the same Line of equal Parts that H B was taken from.

### By Calculation.

By the first of the preceding Theorems, we have this Analogy for finding H G, viz.

$$S, G : H B :: S, B : H G.$$

i.e. as the Sine of G -	$79^{\circ}, 23'$	-	9.99250
is to the Leg H B -	$125$	- - -	2.09691
so is the Sine of B - -	$54^{\circ}, 22'$	-	9.90996
to the Leg H G - - -	$103.4$	- - -	2.01437

### CASE 3.

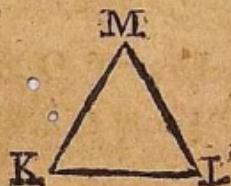
*Two Sides and an Angle opposite to one of them, given, to find the third Side.*

*Example.* In the Triangle K L M, suppose the Side K L  $126$  equal Parts, and K M  $130$  of these Parts, and the Angle L (opposite to K M)  $63^{\circ}, 20'$ , requir'd the Side M L.

Geometrically.

## Geometrically.

The Geometrical Construction of this Case is the same with that in Case 1. (there being the same Things given in both) and the Leg M L may be measur'd by applying it to the same Line of equal Parts that the other two were taken from.



## By Calculation.

The Solution of this Case depends upon the two preceding; and first we must find the other two Angles by Case 1. thus;

$$MK : S, L :: KL : S, M.$$

i. e. as the Side MK - - 130 - - - - 2.11394  
 is to the Sine of L - - 63°, 20' - 9.95116  
 so is the Side KL - - 126 - - - - 2.10037  
 to the Sine of M - - 60°, 1' - 9.93750

Then by Case 2. we find the requir'd Leg M L thus;

$$S, L : MK :: S, K : M L.$$

i. e. as the Sine of L - 63°, 20' - 9.95116  
 is to MK - - - - - 130 - - - - - 2.11394  
 so is the Sine of K - - 53, 39 - - - - 9.90602  
 to M L - - - - - 117.2 - - - - - 2.06850

## C A S E 4.

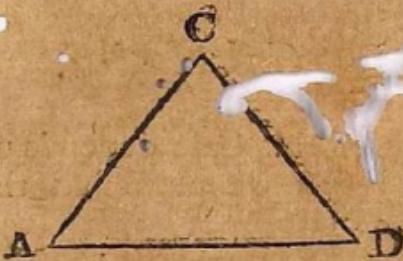
Two Sides and the contain'd Angle given, to find the other two Angles.

Example.

*Example.* In the Triangle ACD, if AC 103, and AD 126, and the Angle A  $54^{\circ}, 30'$ , requir'd the Angles C and D.

### Geometrically.

Draw AD 126 equal Parts, and make the Angle A,  $54^{\circ}, 30'$ ; then set 103 equal Parts from A to C. Lastly, join C and D; and so the Triangle is con-



structed, and the Angles C and D may be measur'd by the Line of Chords.

### By Calculation.

The Solution of this Case depends upon the second and third of the preceding Theorems; and first we must find the Sum and Difference of the Sides, and half the Sum of the unknown Angles. Thus,

the Leg AD is	- - - - -	126
the Leg AC is	- - - - -	103

their Sum is	- - - - -	229
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and their Difference is	- - - - -	23
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the Sum of the three Angles A, D and C is $180^{\circ}$	- - - - -	
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the Angle A is	- - - - -	$54^{\circ}, 30'$
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so the Sum of the Angles C and D will be $125^{\circ}, 30'$	- - - - -	
and half their Sum is	- - - - -	$62^{\circ}, 45'$

then

~~Then by Theorem 2.~~ we have the following Proportion, viz.

As the Sum of the Sides AD and AC 229 2.35984  
is to their Difference - - - - - 23 1.36173  
so is the Tang. of half the Sum  $\frac{1}{2} \cdot 62^\circ . 45'$  10.28816  
of the unknown Angles - - - - - to the Tang. of half their Diff.  $\frac{1}{2} \cdot 11^\circ . 2'$  9.29005

Now having half the Sum and half the Difference of the two unknown Angles C and D, we find the Quadrant of each of them by *Theorem 3.* thus;  
To half the Sum of the Angles C and D  $62^\circ . 45'$   
add half their Difference - - - - -  $\frac{11^\circ . 02}{73^\circ . 47}$   
and the Sum to be a greater Angle C - -  $\underline{\underline{73^\circ . 47}}$

Again, from half the Sum - - - - - 62 . 45  
take half the Difference - - - - -  $\underline{\underline{11 . 02}}$

and there will remain the lesser Angle D  $\underline{\underline{51 . 43}}$

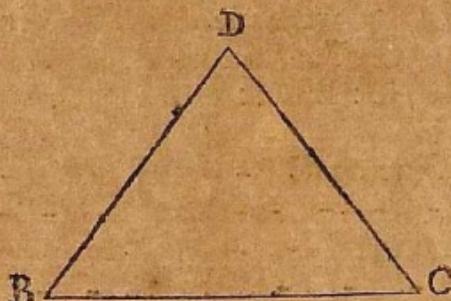
### C A S E 5.

*Two Sides and the Contain'd Angle given, to find the third Side.*

*Example.* In the Triangle BCD, suppose BC 154, and BD 133, and the Angle B  $56^\circ . 03'$  requir'd the Side CD.

### Geometrically.

The Geometrical Construction of this Case is the



same with that of the last, and the Length of DC  
K is

is found by taking its Length in your ~~Compasses~~, and applying it to the same Line of equal Parts that the two Legs were taken from.

### By Calculation.

The Solution of this Case depends upon the second and fourth; and first we must find the Angles by the last Case, thus;

As the Sum of the Sides BD and BC 28. 2.45788  
 is to their Difference - - - - 21 1.32222  
 so is the Tangent of half the Sum of the Angles D and C 6.58' 10.27372  
 to the Tangent of half their Diff. 7, 50 9.13806

So by *Theorem 3.* we have the Angles D and C, thus;

to half the Sum of the Angles D and C - 61°. 58'  
 add half their Difference - - - - 7 . 50

and the Sum is the greater Angle D - 69 . 48

Also from half the Sum - - - - 61 . 58  
take half the Difference - - - - 7 . 50

and there remains the lesser Angle C - - 54 . 08

Then by *Case 2.* we have the following Analogy for finding DC the Leg requir'd, viz.

$$S, C : BD :: S, B : DC.$$

i.e. as the Sine of C - 54°, 08' - 9.90869  
 is to BD - - - - 133 - - - - 2.12385  
 so is the Sine of B - - 56, 03 - - 9.91883  
 to DC - - - - 136.2 - - - - 2.13399

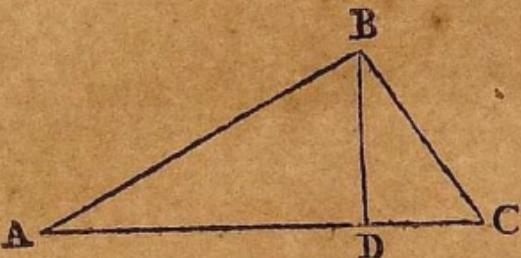
## CASE 6.

*Three Sides given, to find the Angles.*

*Example.* In the Triangle ABC, suppose AB 156, BC 84, and AC 185.7; requir'd the Angles A, B, and C.

*Geometrically.*

Make AC 185.7 from any Line of equal Parts, and from the same ~~Line~~, taking 156, the Length of AB, in your Compasses, fix one Foot of them in A, and with the other sweep an Arch; then take 84, the Length of BC, and fixing one Foot in C,



with the other sweep an Arch, which will cross the former in B; Lastly, join the Points BA and BC, so the Triangle will be constructed, and the Angles may be measur'd by the Line of Chords.

*By Calculation.*

Let fall the Perpendicular BD from the Vertex B, upon the Base AC, which will divide the Base into the two Segments AD and DC, and to find the Lengths of these, we have, by Theorem 4. the following Proportion, viz.

As the Base AC - - - - - 1857 - - 2.26393  
 is to the Sum of the Sides AB and BC 240 - - 2.38031  
 so is the Difference of the Sides - - 72 - - 1.85733  
 to the Diff. of the Segments of the Base 93 - - 1.96871

And having the Sum of the Segments, *viz.* the whole Base, and their Difference, we find the Segments themselves, by *Theorem 3.* thus;

To half the Sum of the Segments - - - - -	92.8
add half their Difference - - - - -	46.5
and the Sum is the greater Segment AD - - - - -	139.3
Also from half the Sum of the Segments - - - - -	92.8
take half their Difference - - - - -	46.5
the Remainder is the lesser Segment DC - - - - -	46.3

Now the Triangle ABC is divided by the Perpendicular DB into two Right-angled Triangles, ADB, and DBC; in the first of which are given the Hypotenuse AB 156, and the Base AD 139.3 to find the oblique Angles, for which we have (by *Case 5. of Rectangular Trigonometry*) the following Analogy, *viz.*

As AB - - - - - 156 - - - - -	2.19312
is to AD - - - - - 139.3 - - - - -	2.14395
so is the Radius - - - - - 90° - - - - -	10.00000
to the Co-Sine of the Angle A 26°, 40' - - - - -	9.95083

Also the Angle C is found by the same Case, thus;

As BC - - - - - 84 - - - - -	1.92428
is to CD - - - - - 46.3 - - - - -	1.66558
so is the Radius - - - - - 90° - - - - -	10.00000
to the Co-Sine of C 56°, 30' - - - - -	9.74130
	Having

Having found the two Angles A and C, we have the third, B, by taking the Sum of the other two from 180, thus;

The Sum of all the three Angles is	-	180°
The Sum of A and C is	-	83. 10
The Angle B is	-	96. 50

All the Proportions us'd for the Solutions of the several Cases in *Plane Trigonometry*, may be performed by the Scale and Compass. On the Scale there are several Logarithmic Lines, viz. one of Numbers, another of Sines, and one of Tangents, &c. And the Way of working a Proportion by these is this, viz. Extend your Compasses from the first Term of your Proportion, found on the Scale, to the second, and with that Extent, fixing one Foot in the third Term, the other will reach the fourth Term requir'd.

### S E C T. III.

#### Of the Principles of GEOGRAPHY and ASTRONOMY.

1. THE Land and Water of this Earth make up a Composition of a Spherical Form, or rather an Oblong Figure, which is call'd the *Terraqueous Globe*.

2. This Globe moves round its Axis in 24 Hours, from West to East; and thereby causing the Celestial Bodies to revolve, apparently from East to West, in the same Time, makes the Vicissitudes of Day and Night.

3. These two Points in which the Axis of the Earth meets the Surface, are call'd the Poles of the Earth; and if the Axis be produc'd on both Sides, to the Heavens, it will cut them in two opposite Points call'd the *Celestial Poles*. The one toward the North, is called the *Arctic Pole*; and the other towards the South, the *Antarctic*.

4. Circles upon a Sphere, are either Great or Lesser. A *Great Circle*, is that whose Plane passes thro' the Center of the Sphere, or whose Diameter is equal to the Diameter of the Sphere. A *Lesser Circle* is that whose Plane does not pass through the Center of the Sphere, or whose Diameter is less than the Diameter of the Sphere.

*Cor. 1.* Hence it is plain, that all great Circles upon a Sphere divide it into Halves, and all lesser Circles divide it unequally.

*Cor. 2.* And since all great Circles have the same Center, viz. that of the Sphere, it is plain they must bisect one another.

5. Since the Earth moves round its Axis, 'tis plain that every Point in the Surface (except the two Poles which are at rest) will describe the Circumference of a Circle; and that which is describ'd by a Point lying in the middle between the two Poles, is call'd the *Equator*, or *Equinoctial Line*, or simply the *Line*.

6. If the Plane of the Equator be produc'd to the Heavens, it will there mark out a Circle call'd the *Celestial Equator*, which will divide the Earth and Heavens into two Hemispheres, that towards the North call'd the *Northern Hemisphere*, and that towards the South, the *Southern*.

7. Great Circles passing through the Poles of the World, and cutting the Equator at Right Angles, are call'd *Meridians*; and that which passes over any Place, is call'd the Meridian of that Place.

8. The Distance of any Place upon the Earth, from the Equator, counted in Degrees upon the Meridian, is call'd the *Latitude* of that Place; and it is either North or South, according as it lies upon the North or South Side of the Equator.

9. Since by the Rotation of the Earth about it's Axis, every Point upon it's Surface describes a Circle, 'tis plain all the Points between the Equator and Poles, must describe Circles parallel to the Equator; and these are called *Parallels of Latitude*.

10. The *Difference of Latitude* between two Places, is the Arch of a Meridian, contain'd between the Parallels of Latitude passing over these Places.

*Cor. 1.* Hence if the two Places lie both on the same Parallel, they will have no Difference of Latitude.

*Cor. 2.* If the Places lie both on the same Side of the Equator, and on different Parallels, then their Difference of Latitude is found by taking the lesser Latitude from the greater.

*Cor. 3.* But if the Places lie on different Sides of the Equator, then their Difference of Latitude is equal to the Sum of the two Latitudes.

11. The *Complement of the Latitude* of any Place, is that Latitude taken from 90 Degrees, or the Distance of the Place from the nearest Pole.

12. The *Longitude* of any Place upon the Earth, is an Arch of the Equator intercepted between the first Meridian, and the Meridian passing thro' the proposed Place. Which is equal to the Angle at the Pole formed by the first Meridian, and the Meridian of the Place.

13. The first Meridian may be placed at Pleasure, passing through any Place; as *London*, *Paris*, *Teneriff*, &c. and the Longitudes counted from it will be either East or West, according as they lie on the East or West Side of that Meridian.

14. The *Difference of Longitude* between two Places upon the Earth, is an Arch of the Equator, comprehended between the two Meridians of these Places: and the greatest possible is 180 Degrees, *viz.* when the two Places lie on opposite Meridians.

15. Since by the Motion of the Earth about its Axis, every Point upon the Surface describes the Circumference of a Circle or 360 Degrees, in 24 Hours time, 'tis plain in one Hour it must describe 15 Degrees; therefore any Place lying 15 Degrees to the Eastward of another, has the Sun upon its Meridian 1 Hour sooner than that other; so when it is Twelve a Clock in the Easternmost Place, it will be but Eleven in the other.

*Cor.* Hence the Difference of Longitude may be converted into Difference of Time, by allowing 1 Hour for every 15 Degrees, and proportionally for Minutes, &c. also Difference of Time may be converted into Difference of Longitude, by allowing 15 Degrees for every Hour, and proportionally for other Time. Consequently by knowing the one, we can find the other.

16. If we suppose a Plane touching the Surface of the Earth in any Point, (upon which a Spectator is standing) and produced to the Heavens, it will there make a Circle called the *Horizon*, which separates the Visible from the Invisible Part of the Heavens. This Horizon is properly the *sensible Horizon*; the *true or rational Horizon* is a great Circle parallel to the sensible, and passing through the Center of the Earth, which divides the Heavens and Earth into two Halves, called the *Upper* and *Lower Hemispheres*.

17. These two Horizons, when produced to the Heavens, may, without any sensible Error, be supposed to coincide the Distance between them, or the Earth's Semidiameter, vanishing when compared with such a Distance.

18. Since

18. Since the Earth moves round its Axis from West to East, 'tis plain a Spectator upon its Surface, together with his Horizon, must move the same Way; consequently these Celestial Bodies towards the East, that were before inconspicuous, will become visible, the Horizon being depressed below them; and those towards the West, that were before in View, will become invisible, the Horizon being elevated above them. And hence arises the apparent Motion of all the Heavenly Bodies, by which they appear to describe Circles round the Poles, parallel to the Celestial Equator, which are greater or less, according as they are more or less distant from the nearest Pole.

19. When any Celestial Body comes first in View, or when it is on the Eastern Side of the Horizon, it is then said to *Rise*; and when by its apparent Motion it comes to the Meridian, it is then said to *Culminate*: And lastly, when it begins to disappear, or is upon the Western Side of the Horizon, it is then said to *Set*.

23. If through the Center of the Earth there be drawn a Line perpendicular to the Plane of the Horizon, and produc'd to the Heavens, it will there mark out two Points; the one, which is directly over our Heads, is call'd the *Zenith*; and the opposite Point thereto, which is invisible to us, ~~and~~ directly under our Feet, is call'd the *Nadir*.

21. *Vertical or Azimuth Circles*, are great Circles passing through the Zenith and Nadir, and cutting the Horizon at Right Angles. Among the Vertical Circles there are two principal ones, viz. the Meridian, which passes thro' the Zenith, Nadir, and Poles, and cuts both the Equator and Horizon at Right Angles; the Points in which it cuts the Horizon are the South and North Points; and the other principal Vertical, call'd the *Prime-Vertical*, is that which cuts the Meridian at Right Angles,

and meets the Horizon in two opposite Points, call'd the East and West Points.

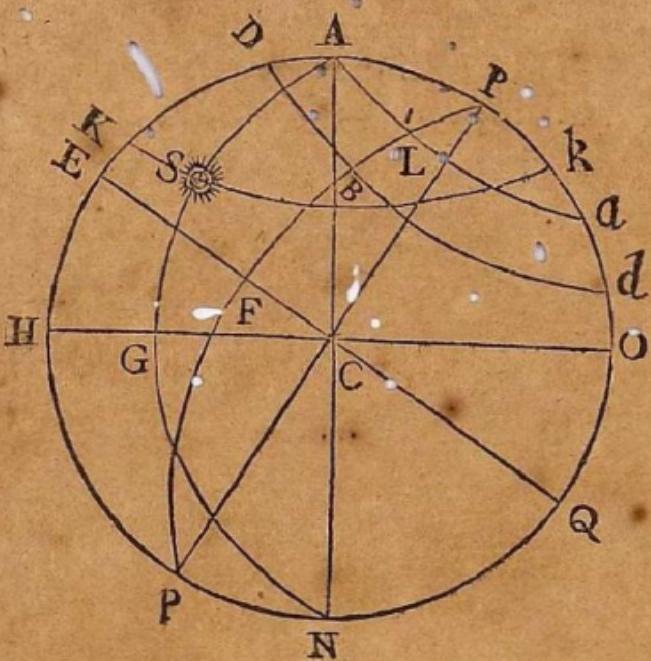
22. Lesser Circles, parallel to the Horizon, are call'd *Almicanthers*, or *Parallels of Altitude*. And these continually decrease, the nearer they are to the Zenith.

24. The *Altitude*, or Depression of any Heaven Body, above or below the Horizon, is an Arch of a Vertical Circle, intercepted between the Horizon and Center of the Object.

25. The *Zenith-Distance* of any Heavenly Object, is that Arch of the Vertical Circle passing thro' it, intercepted between the Center of the Object and the Zenith, which is always the Complement of the Altitude.

26. Let the Circle A H N O represent the Earth, projected on the Plane of some Meridian, A soine Place upon that Meridian; draw the Diameter H O at a Quadrant, or 90 Degrees, Distance from A; then H O will represent the Horizon of the Place A (by Art. 16. of this). Let P and  $p$  be the two Poles; consequently P p, the Axis of the Earth, and the Diameter E Q at Right Angles with that, will represent the Equator, (by Art. 5.) make P a equal to P A, and draw the Circle A a parallel to the Equator E Q, and this will be the Parallel of Latitude the Place A lies on. The Arch A E will be the Latitude of the Place A, and A P, the Complement of its Latitude (by Art. 8. and 11.) the Point in the Heavens directly above A will be the Zenith, and that directly above N will be the Nadir of the Place A (by Art. 20.) the great Circle A C N will be the Prime Vertical, (by Art. 21.) and the Points H and O will be the South and North Points, and C will represent the East and West Points in the Horizon of A. Let S be any Heavenly Object, and A S N a Vertical or Azimuth Circle passing thro' the Center of the Object; also K S its Parallel

Parallel of Altitude ; then SG will be the Altitude and SA the Zenith Distance of the Object S ( by Art. 24. and 25.). Again, let any other Place upon

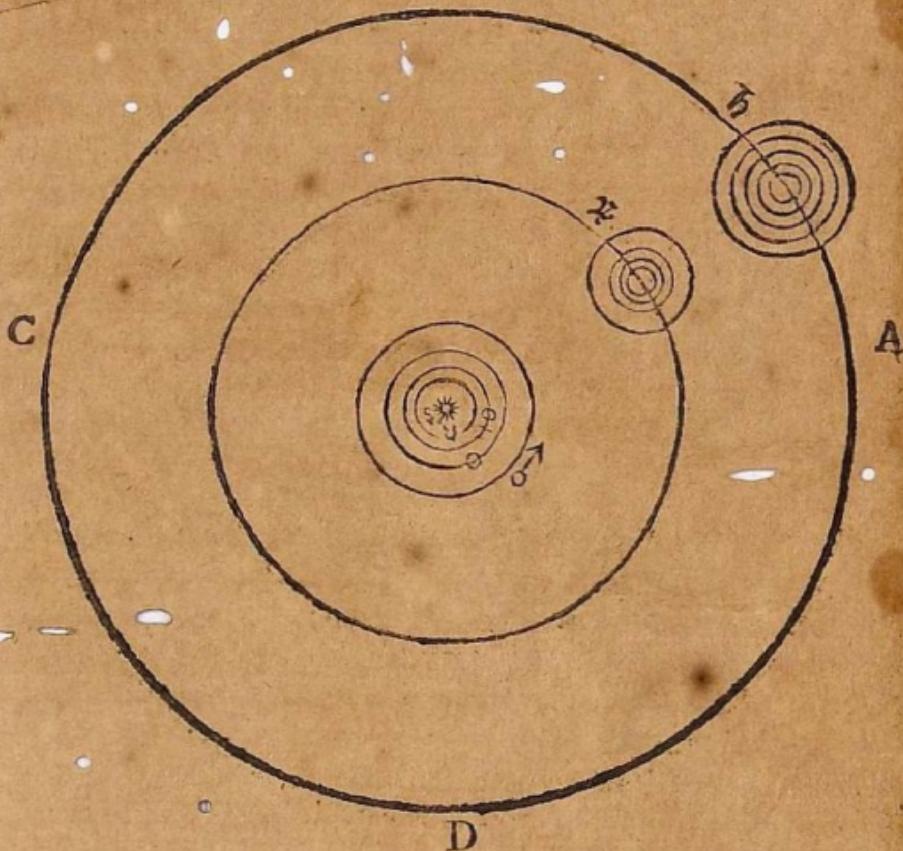


the Earth be assum'd, as B, and its Meridian will be PB<sub>p</sub>, and its Parallel of Latitude DB<sub>d</sub>; then the Latitude of B will be BF or DE, and the Complement of its Latitude will be BP or DP. Also the Difference of Latitude between the two Places A and B, will be BL or DA ( by Art. 10.). If the Meridian passing through A, be suppos'd the first Meridian, then the Longitude of B will be EF ( by Art. 12.) but if the Meridian of A be not suppos'd the first Meridian, then the Difference of Longitude between the two Places A and B will be EF ( by Art. 14.)

27. The System of the Universe ( according to the latest Astronomers ) is as follows, viz. The Sun is

is suppos'd to be in the common Center of Gravity, of six Opake Spherical Bodies, called Planets, which are at different Distances from the Sun, and perform their several Periods round him in different Times; the Names of these Planets, and the Characters by which they are express'd, are as follows, viz. Mercury ♀, Venus ♀, the Earth Θ,

B



*Mars ♂, Jupiter ♀, and Saturn ♂.* And they all move round the Sun, from West to East, in Orbs, very little inclin'd to one another, and the Planes of their Orbs cut one another in Lines passing thro' the Center of the Sun; consequently a Spectator, plac'd

place'd in the Center of the Sun, will be in the Plane of each of their Orbs, and will there view the Planets performing their several Periods round him, from West to East, according to the Order of the Letters ABCD, (in the annex'd Scheme) and in different Times, viz. *Mercury* ♀, which is nearest the Sun, moves round his Orb in 87 Days; *Venus* ♀, which is next to *Mercury*, performs her Period in 224 Days and 17 Hours, or about 8 Months. The Planet which is third in Order from the Sun, is our Earth ♦, which performs its Circuit in 365 Days, 5 Hours, and 49 Minutes, or a Year. Next to the Earth is *Mars* ♂, who moves round his Orb in 686 Days and 23 Hours, or a little less than 2 Years. Then *Jupiter* ♪, whose Orb is vastly extended beyond that of *Mars*, performs his Circuit in 4322 Days, 12 Hours, which is about 12 Years. And lastly, *Saturn* ♫, who is further distant from the Sun, completes his Revolution in 10759 Days and 7 Hours, which is something less than 30 Years. Their Distances from the Sun express'd in the Scheme, are nearly proportional to their true Distance in the Heavens.

28. Three of the Planets, viz. *Mars*, *Jupiter*, and *Saturn*, whose Orbs are beyond that of the Earth, are called *superior Planets*; and the two Planets, *Venus* and *Mercury*, whose Orbs are between the Earth's Orb and the Sun, are called the *inferior Planets*.

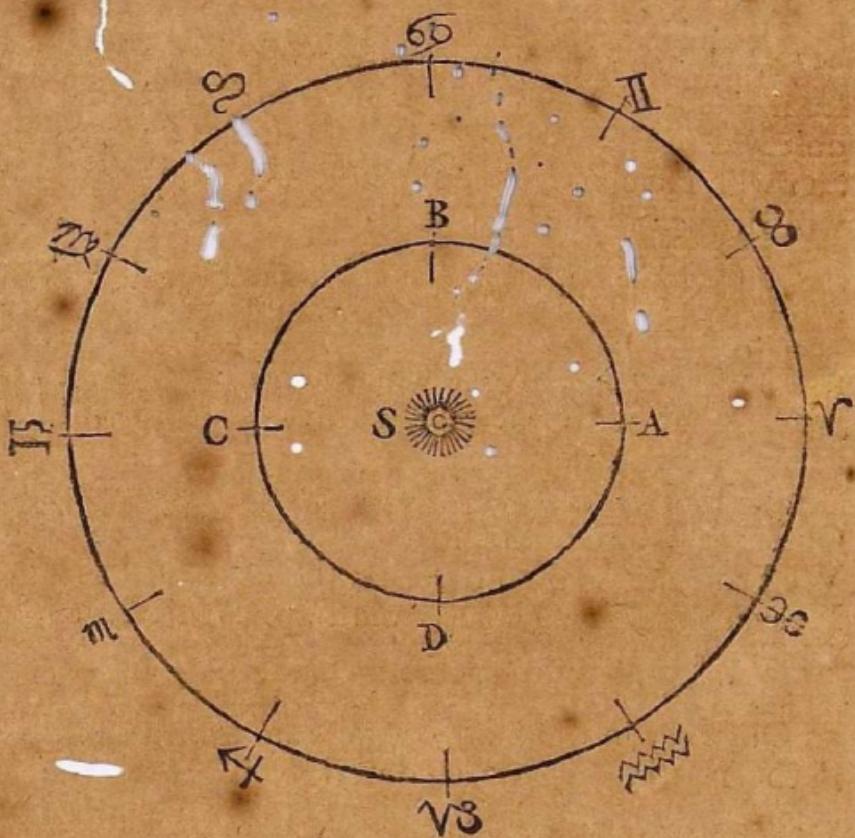
29. The three Planets, *Jupiter*, *Saturn*, and the Earth, are observed to have other smaller ones, constantly attending them, called *Secondary Planets*, or *Satellites*. These Satellites always attend their respective Primaries in their Revolutions about the Sun, and at the same Time they are constantly moving about them; the Earth has one, viz. the Moon,

*Moon*, which attends it in its Annual Revolution about the Sun, and at the same Time moves round it as a Center, in about 27 Days, and 7 Hours. *Jupiter* has four Satellites attending him, which are at different Distances from him, and move round him in different Times, *viz.* that which is innermost or nearest his Body, revolves in 1 Day 18 Hours; the next describes its Orbit in 3 Days and 13 Hours; the third moves round in 7 Days and 3 Hours; and that which is farthest from *Jupiter's* Body, performs its Circuit in 16 Days and 18 Hours. *Saturn* has five Satellites moving round him as a Center, which are at different Distances from his Body, and perform their Revolutions in different Times, *viz.* the first or nearest to him, performs its Circuit in 1 Day, 21 Hours; the second in 2 Days, 17 Hours; the third, in 4 Days 13 Hours; the fourth, in 15 Days, 22 Hours; and the fifth, or the most remote from the Body of *Saturn*, completes its Revolution in 79 Days and 8 Hours.

30. The fix'd Stars are suppos'd to be of the same Matter with the Sun, and made for the same Ends, *viz.* each of them the Center of its own proper System, having Planets moving round it as our Sun has.

31. Having given a cursory View of the System of the Universe, we shall now consider the Motion of the Earth, a little more particularly. Let S represent the Sun in the Center, A B C D the Orbit of the Earth, and  $\text{v} \approx \text{y}$ , the Heaven of the fix'd Stars; then if the Observer be suppos'd to be plac'd in the Sun at S, 'tis plain, when the Earth is in the Point A of its Orbit, it will appear to be at the fix'd Star  $\text{v}$ , and while in moving from West to East, it goes from the Point A of its Orbit to B, it will appear to the Observer at S to pass by

the fix'd Stars ν ρ π Σ; and in moving from B to C, it will appear to pass by the fix'd Stars



Σ η Π ≈; and from C to D, the fix'd Stars ≈ μ τ ψ; and from D to A the fix'd Stars νς ≈ κ ν. Again, let the Observer be remov'd from the Sun to the Earth, then 'tis plain, when the Earth is in the Point A of its Orbit, the Sun S will appear to be in the opposite Point of the Heavens, viz. at the fix'd Star ≈; and while the Earth is moving in its Orbit from A to B, the Sun will appear to pass by the fix'd Stars ≈ μ τ νς; also, while the Earth moves from B to A, the Sun will appear to have mov'd from νς, by the fix'd Stars ≈ κ, &c. to ≈; consequently the Sun, to an Inhabitant

habitant of the Earth will appear to pass over the same fix'd Stars, and towards the same Part of the Heavens, i. e. from West to East, as the Earth appear'd to an Observer in the Sun.

32. Hence arises the apparent Motion of the Sun from West to East. So that if any fix'd Star be observ'd to rise with the Sun, some Days after, the Sun will have mov'd more Easterly, and the Star will rise before the Sun, and also set before it: Also if a Star, in or near the Path which the Sun appears to describe in his Annual Motion, and at some Distance from the Sun, be observ'd above the Horizon after Sun-set, it will some Time after that appear to set with the Sun, and for a while will not be visible at Night.

33. The same Way the Sun will appear to an Observer in any of the other Planets to move from West to East, and to describe the same Orbit in the Heavens that the Planet would appear to do to an Observer in the Sun.

34. The Circle in the Heavens that the Earth to an Observer in the Sun, or the Sun to an Observer in the Earth, appears to describe, is called the *Ecliptic*, and it is divided into twelve equal Parts, called *Signs*, each containing 30 Degrees, viz. the  $\frac{1}{12}$  of 360. The Names and Characters by which these Signs are usually express'd, are as follows.

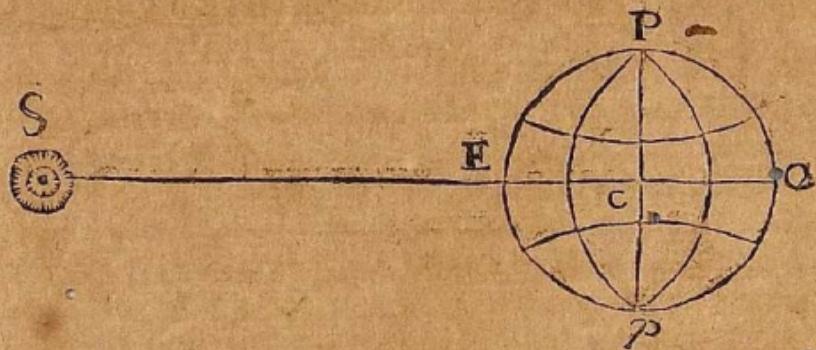
        
Aries, Taurus, Gemini, Cancer, Leo, Virgo, Libra,

       
Scorpio, Sagittarius, Capricornus, Aquarius, Pisces,

35. Since the Earth is a Spherical Body exposed to the Rays of the Sun, 'tis plain, half of its Body must be enlightned, while the other Half is in Darknes; and if there be a Line drawn from the

ter of the Sun to that of the Earth; and a plane Perpendicular to that Line passing through the Center of the Earth; then this Plane will cut the Earth in a great Circle, which will separate the enlightened from the darkned Hemisphere; and this Circle is called the *Terminator* of Light and Darkness upon the Earth.

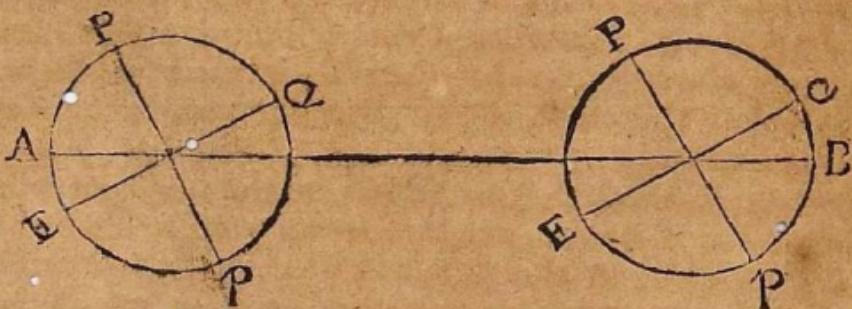
36. If the Line of the Earth's Equator lay in the Plane of the Ecliptic, and consequently the Earth's Axis were perpendicular to the Ecliptic, then the *Terminator* of Light and Darkness would be a Meridian; for let the Circle  $P\text{E}pQ$  represent the Earth,  $P$  and  $p$  its two Poles,  $\text{EQ}$  the Equator,  $C$  the Center of the Earth, and  $S$  the Sun lying in the same Plane with  $\text{EQ}$ ; then, by the last Article, the *Terminator* must be perpendicular to  $SC$ , and consequently, in this Case, to the Plane of the Equator  $\text{EQ}$ ; but since all great Circles perpendicular to the Equator must pass thro' the Poles, and so be Meridians, it follows, that in this Case the *Terminator* must be a Meridian, as  $Pp$ . And since all Meridians bisect the Equator (by Art. 4. Cor. 2. of this) they must also bisect its Parallels;



consequently the *Terminator*, which is here a Meridian, must bisect the Equator and all its Parallels;

so the Half of each Parallel must be always enlightened, and the other Half in Darkness; and since by the Motion of the Earth about its Axis, every Point upon its Surface, except the Poles, describes a Circle parallel to the Equator; it plainly follows, that if the Plane of the Equator lay in the Plane of the Ecliptic, every Point upon the Earth's Surface, except the two Poles, would have the Sun as long above its Horizon as below it, and so there would be a constant Equality of Day and Night, *viz.* 12 Hours each; and the two Poles would have the Sun constantly moving round their Horizon.

37. The Axis of the Earth is observ'd to be inclin'd to the Plane of the Ecliptic at an Angle of about  $66\frac{1}{2}$  Degrees, and consequently the Plane of the Equator must be inclin'd to the Ecliptic, at an Angle of  $23\frac{1}{2}$  Degrees, *viz.* the Complement of the former. Also the Axis of the Earth in its Annual Motion about the Sun, keeps always parallel to the same Line; so if there be a Line drawn thro' the Center of the Sun, parallel to the Earth's Axis, while in any Point of its Orbit, that Line will continue parallel to the Axis, whatever Point of the Orbit the Earth be in (at least in a Year's



Time the Difference is insensible). And this must necessarily happen, if the Earth had no other Motion

tion but a progressive one in its Orbit, and a Rotation about its Axis. For suppose any Spherical Body, as  $P E p Q$ , whose Center moves along the Line  $A B$ ; and while in  $A$ , let any Diameter of it, as  $P P$ , be assum'd, inclin'd any Way to the Line  $A B$ ; then 'tis plain, if the Body had no other but the progressive Motion, when it has come to  $B$ , the Diameter  $P p$  will still be parallel to its former Situation, while in the Point  $A$ ; and if the same Body be suppos'd also to move round its Axis  $P p$ , 'tis plain, all Parts of it would consequently be changing their Situations, except the Axis which is no Way affected by the Rotation, and consequently the Axis must always keep parallel to the same Right Line.

38. Since the Plane of the Equator is inclin'd to the Plane of the Ecliptic, therefore they must intersect one another in a Right Line passing thro' the Centers of the Earth and Sun, and so the Plane of the Ecliptic must cut the Earth in a great Circle, which will be inclin'd to the Equator at an Angle of  $23\frac{1}{2}$  Degrees, and this will mark out upon the Earth's Surface, the Path of the Sun in his Annual Motion; the Line in which the Equator intersects the Ecliptic, must always be parallel to the same Line, whatever Point of the Orb the Earth be in; for since (by the last Art.) the Earth's Axis always preserves a Parallelism, and that Line being always inclin'd to the Axis at the same Angle, 'tis plain therefore, that it must also keep a constant Parallelism.

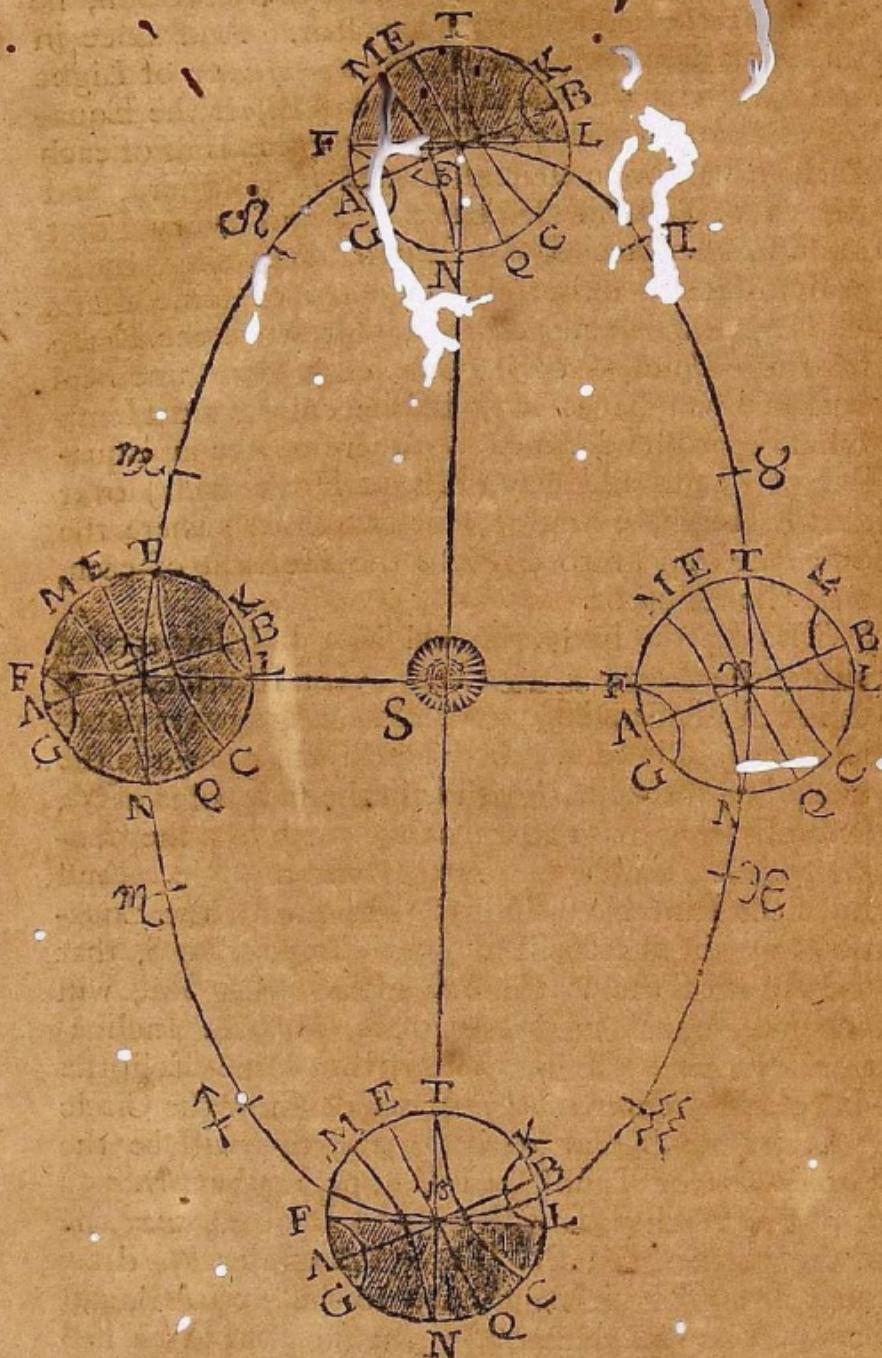
39. If through the Center of the Sun there be drawn a Line perpendicular to the Plane of the Ecliptic; then this Line is called the Axis of the *Ecliptic*; and the two opposite Points in which the Axis meets the Heavens, are called the *Poles of the Ecliptic*.

40. That great Circle in the Heavens which passes thro' the Poles of the World and the Points of intersection, of the Ecliptic and Equator, is called the *Equinoctial Colure*. And that great Circle which is at Right Angles with the former, and passes thro' the Poles of the Ecliptic and World, is called the *Solstitial Colure*. The four Points in which these Colures cut the Ecliptic, are called the *Cardinal Points*. These two in which the Equinoctial Colure meets the Ecliptic, are called *Equinoctial Points*; because (as shall be shewn) when the Sun is in either of them there is an Equality of Day and Night to the Inhabitants of the Earth; and the two Points in which the Solstitial Colure cuts the Ecliptic, are called the *Solstitial Points*; because when the Sun comes to either of these Points, he is then at his greatest Distance from the Equator, and is beginning to return to it again.

41. To explain the Phænomena, or Appearances that arise from the Earth's Annual Motion about the Sun: Suppose  $\text{v} \text{z} \text{v} \text{z}$  the Earth's Orbit, and S the Sun; through S draw the Right Line  $\text{S} \text{v}$ , parallel to the common Line of Intersection, of the Ecliptic and Equator, and meeting the Ecliptic in the two Points  $\text{v}$  and  $\text{z}$ ; also thro' S draw the Line  $\text{w} \text{S} \text{w}$  perpendicular to the former; then 'tis plain, when the Earth is in the Point  $\text{z}$  of its Orb, the Line  $\text{S} \text{z}$ , joining the Centers of the Sun and Earth, will coincide with the common Intersection of the Ecliptic and Equator, and so lie in the Plane of the Equator, and consequently be perpendicular to the Earth's Axis; and since (by Art. 35.) this Line is also perpendicular to the Terminator of Light and Darkness, 'tis plain that the Axis of the Earth will lie in the Plane of the Terminator, which therefore must pass thro' the two Poles, and so be a Meridian; also the Sun will appear in the opposite Point of the Orbit at  $\text{v}$ , viz. in the Line  $\text{z} \text{S} \text{z}$

so produc'd, that i. in the Plane of the Equator; and consequently by his apparent daily Motion, he will describe the Celestial Equator. And since in this Situation of the Earth, the Terminator of Light and Darkness is a Meridian, it will bisect the Equator and its Parallels; consequently the Half of each Parallel will be in the enlightened Hemisphere, and the other Half in the darkned; and every Point upon the Surface of the Earth, describing, by its daily Motio., either the Equator or some of its Parallels; it plainly follow, that when the Earth is in the Point  $\omega$  of its O. b, each Place upon its Surface, will be as long in the enlightened Hemisphere as in the darkned, i. e. there will be an Equality of Night and Day (*viz.* 12 Hours each) over all the Earth, except at the two Poles, where the Sun will appear to describe the Horizon of each, *viz.* the Equator.

The Earth, by its Annual Motion being carried along the Signs  $m\ \tau$ , the Line of Interfection of the Ecliptick and Equator remaining always parallel to itself, it cannot now be directed towards the Sun; but when the Earth is in the first Point of  $vs$ , it must make, with the Line  $S\ w$ , joining the Centers of the Earth and Sun, a Right Angle. And since the Line  $S\ w$  is not in the Plane of the Equator, but of the Ecliptic, the Angle  $B\ w\ S$ , that the Axis of the Earth  $AB$  makes with  $S\ vs$ , will be acute, equal to  $66\frac{1}{2}$  Degrees, *viz.* the Inclination of the Axis of the Earth to the Ecliptic. Thro' the Center of the Earth  $w$ , draw the Circle  $FL$ , perpendicular to  $S\ vs$ , and this will be the Terminator of Light and Darkness, (by Art. 35.) and the Arch  $BL$  will be  $23\frac{1}{2}$  Degrees, *viz.* the Complement of  $TB$ . Thro' the Center  $vs$ , draw the Circle  $QE$  perpendicular to the Axis  $AB$ , and this will be the Equator; then, since the Arch  $EB$  is equal to the Arch  $TL$ , (being each a Quadrant) by



ET equal to BL, i.e.  $23\frac{1}{2}$  Degrees. Make the Arch

Arch EM equal to ET, and thro' the Points T and M draw the Circles TC, MN parallel to the Equator; then 'tis plain, that when the Earth is in the Point  $\nu$  of its Orbit, the Sun will be perpendicular to the Point T, distant from the Equator EQ, toward the North Pole B,  $23\frac{1}{2}$  Degrees, which is his greatest Declination North. The Parallel TC is called the *Tropic of Cancer*, and the Circle in the Heavens concentric with this, which the Sun appears to describe at that Time, is called the *Celestial Tropic of Cancer*; because the Sun at that time appears to be in the Sign  $\Sigma$ . And because of the Earth's Rotation about its Axis, 'tis plain, that all the Points situate upon the Parallel TC, will have the Sun, when upon their Meridian, in their Zeniths. Also, when the Earth is in this Position, 'tis plain, that the *Terminator of Light* and *Darkness* FL, will go beyond the North Pole B to L,  $23\frac{1}{2}$  Degrees distant from B; and consequently the South Pole A must be as far, from the Terminator LF in the darkned Hemisphere. Thro' the Points L and F, draw the Circles LK, FG parallel to the Equator, and these Circles are called *Polar Circles*, that towards the North is called the *Artic Circle*, and that towards the South is called the *Antarctic Circle*. Now, since the Earth moves round upon its Axis AB, 'tis evident, that every Point within the Artic Polar Circle KL, will, at that time, have a continued Day; and on the contrary, every Point within the Antarctic Polar Circle FG, will have a continued Night.

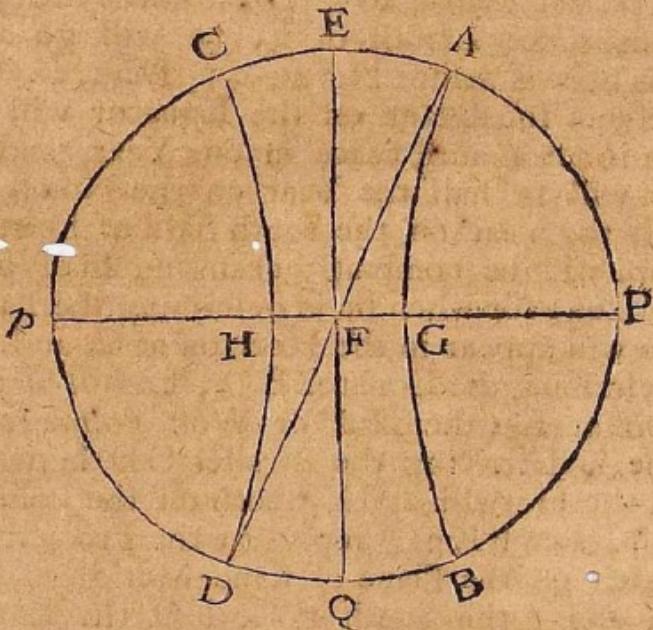
Again, the Earth moving forwards through the Signs  $\approx$   $\ast$  to  $\gamma$ , the Sun will appear to move thro' the Signs  $\Xi$ ,  $\Omega$ ,  $\mathcal{X}$ , and by Degrees to return again to the Equator; and when the Earth has come to the Point  $\gamma$  of its Orbit, the Sun will appear to be at  $\approx$ . Now the common Intersection of the Ecliptic and Equator still remaining parallel to the Line

∴ S  $\nu$ , 'tis plain; that when the Earth has come to  $\nu$ , the Line S  $\nu$ , joining the Centers of the Earth and Sun, will lie in the Plane of the Equator; and consequently the Sun will appear in the Celestial Equator, and there will be an Equality of Night and Day, the same Way as when the Earth was in  $\approx$ ; and in this Situation, the Terminator of Light and Darkness will again pass through the two Poles.

The Earth moving forwards through the Signs  $\nu$ ,  $\delta$ ,  $\pi$ , the Sun will appear to move thro' the opposite Signs  $\approx$ ,  $m$ ,  $\tau$ , gradually declining from the Equator, towards the South Pole; and when the Earth comes to  $\mathfrak{S}$ , the Sun appears to be in  $\nu$ . Now, since the Axis of the Earth A B, does not change its Inclination to the Ecliptic; the Earth will have the like Aspect and Position with respect to the Sun, as it had when in the Point  $\nu s$  of its Orbit; but with this Difference, that he is now as far on the South Side of the Equator, as (when the Earth was in  $\nu$ ) he was on the North Side, i. e.  $23\frac{1}{2}$  Degrees, and is perpendicular to the Point N; the Parallel N M is called the *Tropic of Capricorn*, and the Circle in the Heavens concentric to this which he appears to describe at this time, is called the *Celestial Tropic of Capricorn*; because at this time the Sun appears to be in the Sign  $\nu$ ; also, all within the North Polar Circle K L, which was enlightened when the Earth was at  $\nu s$ , is now in Darkness, and all within the South Polar Circle, is now enlightened.

42. We shall now consider more particularly the Appearances that happen to the different Places upon the Earth, arising from its Annual Motion about the Sun, in Conjunction with the Rotation about its Axis. In order to which we must consider, that the Inhabitants of this Earth, with respect to their Situation upon it, are divided into three Kinds, viz. First, Such as live upon the Equator. Secondly,

condly; Such as live between the Poles and Equator.  
 Thirdly. Such as live upon either Pole. As for those  
 that live upon the Equator; Let  $E \not p Q P$  be the  
 Projection of the Earth upon the Plane of some  
 Meridians,  $P$  the North, and  $p$  the South Pole,  $EQ$   
 the Equator and  $E$  some Place upon it; also  $DA$   
 the Ecliptic,  $CD$  the *Tropic of Capricorn*, and  $AB$   
 the *Tropic of Cancer*. Then 'tis plain, that an In-  
 habitant upon the Equator, suppose at  $E$ , will have  
 the two Pole  $P$  and  $p$  in his Horizon, which there-  
 fore must be a Meridian. And since all Meridians  
 bisect the Equator and its Parallel's at Right Angles,  
 and all the Heavenly Bodies describing Parallel's in  
 their apparent diurnal Motion; 'tis evident, that in



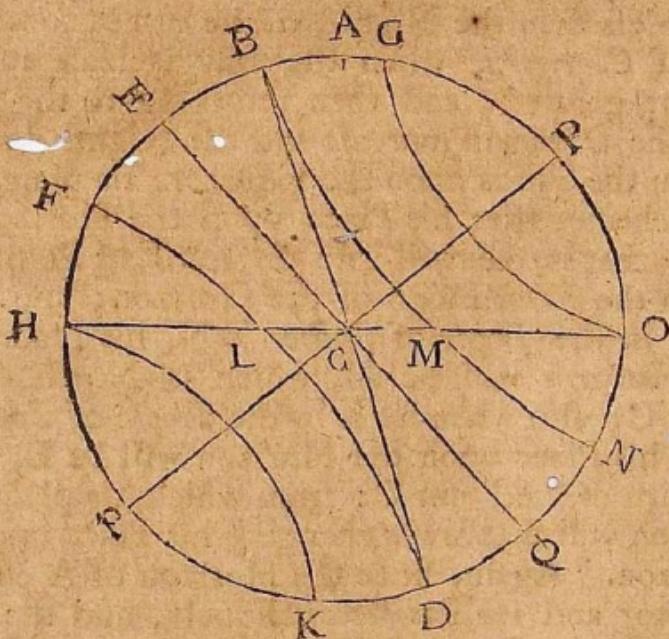
one intire Revolution of the Earth about its Axis,  
 all the Heavenly Bodies must come in View, and  
 they must rise and set perpendicular to the Horizon,  
 and be as long above it as below, i. e. twelve Hours  
 each. Now the Sun always describing some Paral-  
 lel, or the Equator itself, in his diurnal Motion; it

follows, that to an Inhabitant upon the Equator there must be a constant Equality of Night and Day, *viz.* twelve Hours each; and when the Sun in his Annual Motion comes to be perpendicular to the Point F, he will then describe the Equator in his diurnal Motion; and consequently when he comes upon the Meridian of any Place, E, on the Equator, he will be in the Zenith of it; and moving on in the Ecliptic till he be perpendicular to the Point A, (when he is at his greatest Declination from the Equator towards the North Pole P, *viz.*  $23\frac{1}{2}$  Degrees) he will then describe the *Tropic of Cancer* AB, and when he comes on the Meridian of E, he will be remov'd from the Zenith towards the North  $23\frac{1}{2}$  Degrees; and moving still on in the Ecliptic, he will appear to return towards the South, and passing the Zenith of E, he will go as far South as he was before North,  $23\frac{1}{2}$  Degrees. Consequently an Inhabitant on the Equator will have the Sun in his Zenith twice in one Year, and also the Sun will be half the Year on the North Side, and half the Year on the South Side of him; and therefore will be constantly changing his Place in the Horizon; for when he is describing the Parallel AB, he will appear in the Horizon at G, and when he is describing the Equator EQ, he will be in the Horizon at F (the East or West Points); also when he is describing the Parallel CD he will appear in the Horizon at H, South off the Point F.

Again, Let PE  $\rho$  Q represent the Projection of the Earth on the Plane of some Meridian, P the North, and  $\rho$  the South Pole, EQ the Equator, and A some Place upon that Meridian, lying between the Equator and North Pole, whose Horizon is HO; also BD the Ecliptic, BN the *Tropic of Cancer*, and FD the *Tropic of Capricorn*; through the Points H and O draw the Parallels OG, HK. Then 'tis plain, that to an Inhabitant at A, the

North

North Pole P will be elevated above, and the South Pole p depress'd as much below the Horizon; and the Horizon will cut the Equator and its Parallels obliquely. Now, since the Horizon and Equator are both great Circles, they must bisect one another (by Art. Cor. 2.); therefore half the Equator will be above, and half below the Horizon; consequently, when the Sun is perpendicular to the Point C, that is, when he appears to be in the Equator, there will be an equality of Night and Day. And since the Horizon cuts the Parallels obliquely, it must therefore cut them unequally; and 'tis plain from the Scheme, that of those Parallels which lie between the Equator and nearest Pole, the greater Part is above the Horizon, and the lesser below; and those that lie on the other Side of the Equator, have the lesser Part above, and the greater

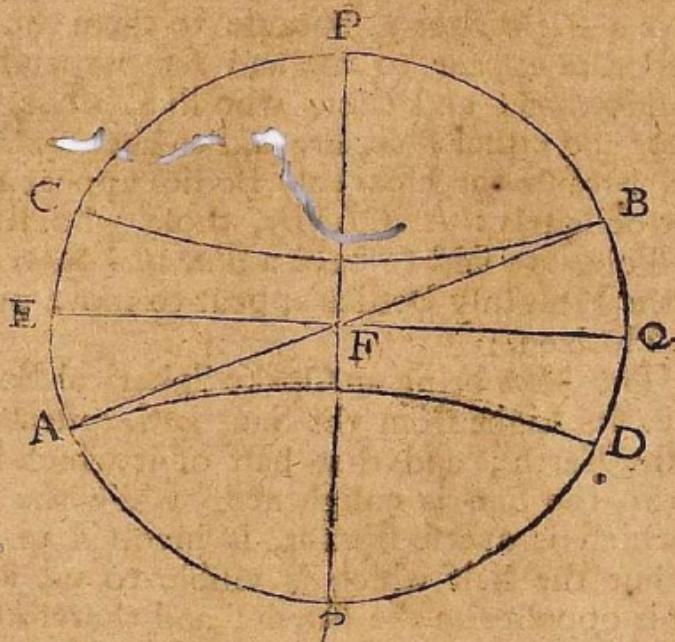


below the Horizon; and the nearer the Parallels are to the Poles, the more unequally are they cut by the Horizon. Consequently, while the Sun is

upon the North Side of the Equator, and by his diurnal Motion describing Parallel lying between the Equator and North Pole; 'tis plain, he will be longer above than below the Horizon of the Place A; and when he comes to his greatest Declination North, and then describes the *Tropic of Cancer*, 'tis plain, the Days must then be at the longest to the Place A; also the Sun returning towards the Equator, he will describe Parallels, whose Parts above the Horizon grow still nearer to an Equality with those below; and so the Days will still decrease, and come nearer to an Equality with the Nights, till he come to the Equator, when the Day and Night are equal; and proceeding from the Equator towards the South Pole, he will then describe Parallels lying between the Equator and South Pole, whose least Part is above, and greatest Part below the Horizon, and consequently the Days will still grow less than the Nights, till he comes to the *Tropic of Capricorn*, when the Day is least and the Night greatest; and then returning to the Equator, the Days will increase and the Nights decrease. When the Sun is upon the Equator, 'tis plain, from the Scheme, that his Place upon the Horizon will be C, that is, he will rise on the East Point, and set on the West Point of the Horizon; and when he is in the *Tropic of Cancer* BN, his Place upon the Horizon will be M, which is North of the Point C; also when he is in the *Tropic of Capricorn* FD, his Place upon the Horizon will be L, which is South of the Point C; from which 'tis plain, that the Sun will be always changing his Place upon the Horizon. Again, since the Horizon of A cuts the Equator and its Parallels obliquely, and the Heavenly Bodies by their apparent diurnal Motion, describing Parallels, 'tis plain, they must rise and set obliquely; also all of them within the Parallel

GO can never rise or set, but must be constantly in View; for which Reason this Parallel GO is called, *The Circle of constant Apparition*; and all within the Parallel HK can never come in View, but be constantly below the Horizon; and therefore the Parallel HK is called, *The Circle of Perpetual Occultation*.

Lastly, Let I E p Q represent the Projection of the Earth upon some Meridian, P the North, and p the South Pole, EQ the Equator, AB the Ecliptic, BC the *Tropic of Cancer*, and AD the *Tropic of Capricorn*; then 'tis plain, that the Equator is the Horizon of both Poles, and consequently the Northern Hemisphere must always be in View, and the Southern always hid to an Inhabitant at P; also the Heavenly Bodies will appear to move in Circles parallel to the Horizon, and the fix'd Stars



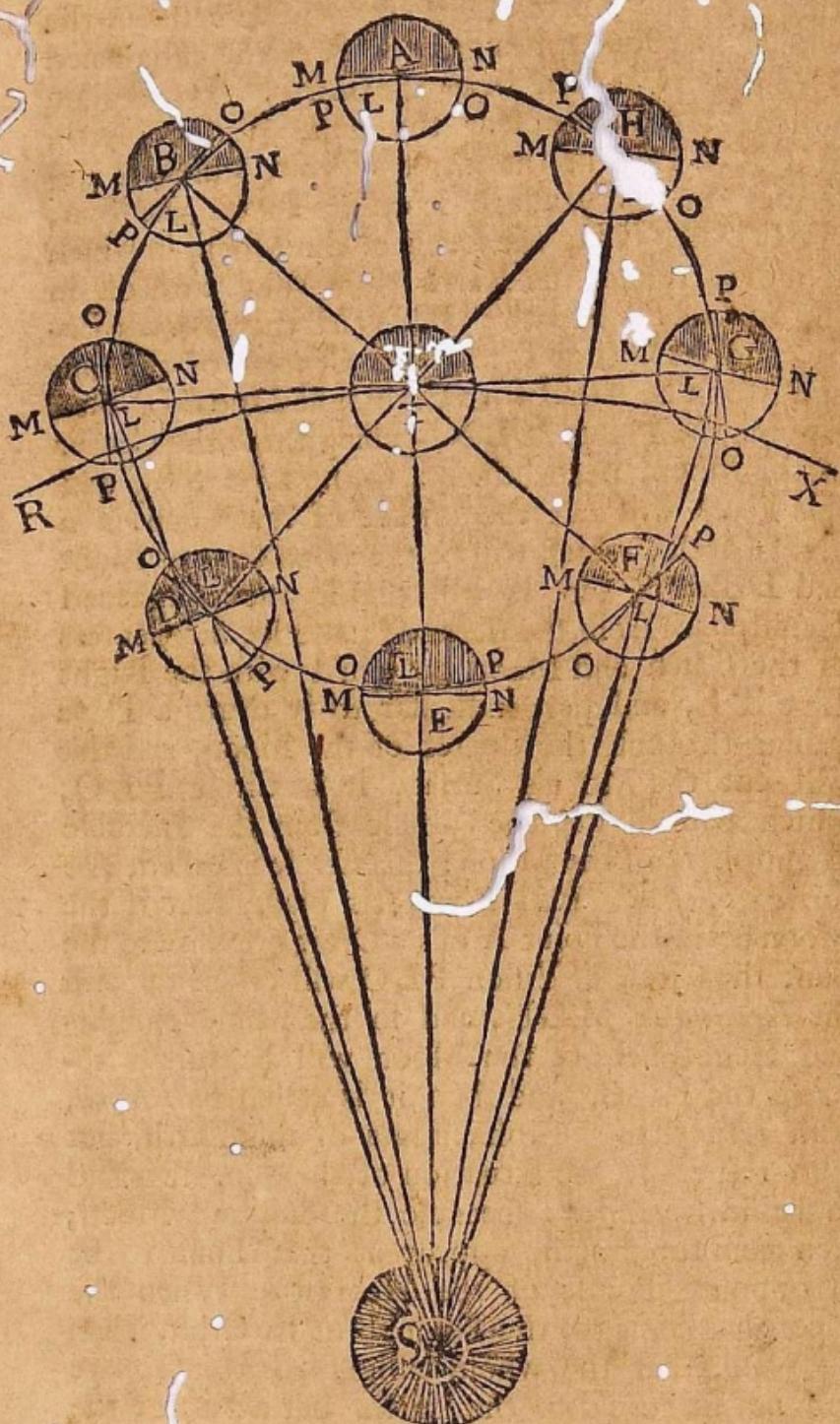
will ever describe the same Parallels, and always have the same Height above the Horizon. When the Sun by his Annual Motion comes to be perpendicular

dicular to the Point F, and then describes the Equator, 'tis plain, he will be in the Horizon of both Poles, and by his diurnal Motion will appear to move quite round it: and since half the Ecliptic FB is above, and the other half FA below the Horizon of P, 'tis plain, all the time the Sun is in describing that half of the Ecliptic on the North Side of the Equator, he will be above the Horizon of P, and all the time he is in describing the other half on the South Side of the Equator, he will be below the Horizon of P; from which 'tis plain, that an Inhabitant of either Pole will have half a Year continued Day, and as long Night. And since the Sun's greatest Distance from the Equator, South or North, is  $23\frac{1}{2}$  Degrees, 'tis plain, his greatest Altitude, or Depression, above or below the Horizon of either Pole, must be  $23\frac{1}{2}$  Degrees.

43. Those that live upon the Equator are said to have a *Right Sphere*, because to them the Heavenly Bodies appear to rise and set perpendicular to the Horizon; and those who live between the Equator and either Pole, are said to have an *Oblique Sphere*, because the Heavenly Bodies appear to rise and set obliquely: And Lastly, those who live on either Pole, are said to have a *Parallel Sphere*, because the Heavenly Bodies appear to move parallel to the Horizon.

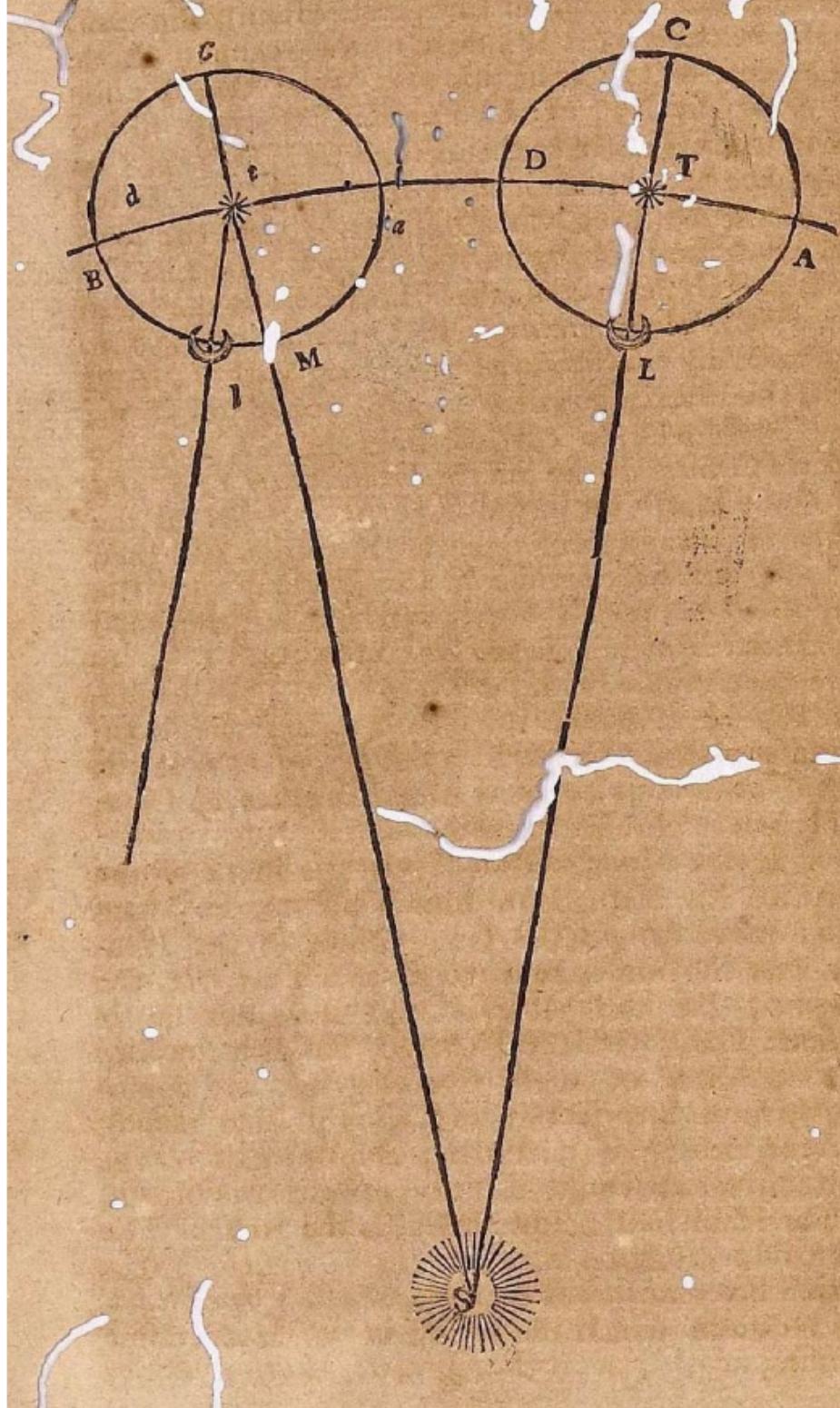
44. The *Moon* being an Opake Spherical Body, it receives its Light from the Sun, and reflects that upon the Earth; and that half of it which is opposite to the Sun is enlightened, while the other half, which is averse from it, is involv'd in Darkness; but the half which is visible to us, is that which is opposite to the Earth; and therefore, according to the various Situations of the Moon, with respect to the Earth and Sun, it will have different Illuminations; for sometimes a greater, and sometimes

times a lesser Part of the enlightened Hemisphere is turn'd to the Earth, and likewise sometimes the whole, and sometimes none at all of the enlightened Hemisphere is seen from the Earth. To explain which, let S represent the Sun, T the Earth, R T X a Part of the Earth's Orbit, which it describes in its Annual Motion about the Sun, A B C D E F G H, the Orbit of the Moon, in which it moves round the Earth from West to East, in the Space of a Month; P N O M the Moon's Body, and its Center L; let the Centers of the Sun and Moon be join'd with the Right Line S L, then suppose the Plane M L N, passing thro' the Center of the Moon, perpendicular to the Line S L; and this Plane will cut the Surface of the Moon in a great Circle, which will be the *Terminator* of Light and Darkness, *viz.* it will divide the enlightened Hemisphere from the darkned; also let the Centers of the Earth and Moon be join'd with the Right Line T L, and perpendicular to it draw a Plane passing through the Center of the Moon, and this will cut the Moon's Surface in a Circle P L O, which will divide the Visible from the Invisible Hemisphere of the Moon; this Circle is called, *The Circle of Vision*. And 'tis plain, that if the Moon be in the Point A of its Orbit opposite to the Sun, the Circle of Vision P L O will co-incide with the Terminator M L N, and so the whole enlightened Hemisphere of the Moon will be turn'd towards the Earth, and then it is called *Full Moon*, with respect to the Inhabitants of this Earth, but with respect to the Situation of the Sun, it is said to be in *Opposition*; because the Sun and Moon, seen from the Earth, appear at that Time to be in opposite Points of the Heavens. When the Moon has come to the Point B of its Orbit, then 'tis plain, that the whole enlightened Hemisphere will not be turn'd to the Earth, but a Part of the Moon



as M P, will be without the visible Hemisphere, and therefore the visible illuminated Part cannot be circular, but will appear gibbous; when the Moon is in the Point C of her Orbit, and the Angle C TS a Right Angle, then the Angle T CS will also be a Right Angle (at least differing little from it) for because of the vast Distance of the Sun, from the Earth and Moon, the Lines S T, S C may be taken as parallel consequently the Circle of Vision will bisect the *Terminator* at Right Angles, and so only one half of the enlightened Hemisphere will be in the Visible, and then the Moon appears to be halv'd, and is call'd *Half-Moon*. In this Situation the Moon is only a Quadrant's Distance from the Sun, and therefore it is said to be in one of its *Quadratures*. The Moon proceeding to D, 'tis plain, that in this Situation only a small Part P N of the enlightened Hemisphere is turn'd to the Earth, and the greatest Part N O of the visible Hemisphere is darkned; and consequently, because of the spherical Figure of the Moon, it will then appear horned and its *Horns* will be turned towards the West. When the Moon is arriv'd at E, 'tis plain, the Circle of Vision will again co-incide with the *Terminator*, and the whole darkned Hemisphere will be turn'd to the Earth, and then it is said to be *New Moon*; but with respect to its Situation with the Sun, it is said to be in *Conjunction*, because it appears to be in the same Point of the Ecliptic with the Sun; and when it has mov'd a little forward to F, 'tis plain, Part of the enlightened Hemisphere, viz. M O, will be in the visible, and so it will again appear horned, and having them turn'd towards the East; also when at G it will appear halv'd, and when at H gibbous; and *Lastly*, when it comes to A it will again appear full.

45. Tho' (as it was said in Art. 29.) the Moon moves quite round its Orbit in 27 Days, and 7 Hours, nearly, call'd the *Periodic Month*; yet the

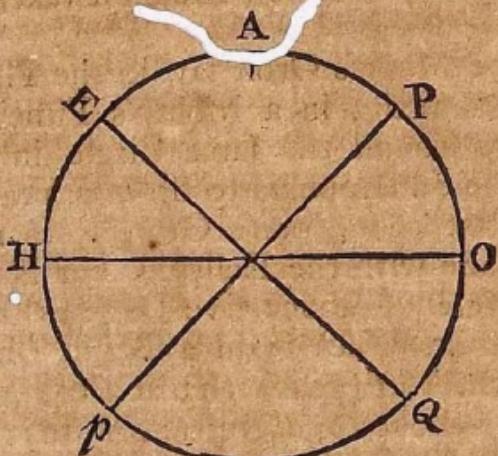


Time it takes from the Conjunction with the Sun, to the next, is greater; being 29 Days, and about 12 Hours, which is call'd, *the Synodic Month*; for let S be the Sun, T the Earth, A B a Part of the Earth's Orbit about the Sun, and A L D C the Orbit of the Moon; then when the Earth is in T, let the Moon be in L, in Conjunction with the Sun; and when the Moon is moving from L round its Orbit L A C D, 'tis plain, that the Earth in the mean Time will be moving on in its Orbit about the Sun, and carrying the Moon's Orbit along with it. And when the Moon has mov'd quite round its Orbit, the Earth will be carried from T to t, and the Moon's Orbit will be in the Situation, *l a c d*, and the Point L will be in the Line *t l*, parallel to the former *T L*, and consequently the Moon will then be in *l*; but will not be in Conjunction with the Sun, till it has mov'd a little further, and describ'd the Arch *l M*, which is similar to the Arch *t T*, because the Angles *l t M*, *t S T* are equal (by Art. 36. Sect. 1.) And hence it is that though the Moon moves round its  $\Omega$  in 27 Days, 7 Hours, yet from New moon to New Moon it takes 29 Days, 12 Hours.

46. If the Moon's Orbit lay in the Plane of the Ecliptic, 'tis plain, in a Month's Time the Moon would move round the same Circle in the Heavens, that the Sun appears to do in a Year, viz. the Ecliptic; but the Moon's Orbit does not lie in the same Plane with the Ecliptic, but is inclin'd to it at an Angle of about five Degrees, and consequently must intersect it in a Right Line passing thro' the Center of the Earth; and one half of the Orbit will be above the Ecliptic towards the North, and the other half below, towards the South. The Line of Intersection is call'd, *the Line of the Nodes*, the two Extremities of which are called, *the Nodes*. The Node in which the Moon is, when ascending

above the Ecliptic towards the North, is called, *the Ascending Node*, or, *Dragon's Head*, for Brevity's sake marked thus, ♀; and the opposite one, viz. that in which the Moon is, when descending below the Ecliptic towards the South, is called, *the Descending Node*, or, *Dragon's Tail*, marked thus, ♂. Hence 'tis plain, that the Moon cannot appear in the Ecliptic above twice in one Period, viz. when it is in the Nodes; and in other Points of its Orbit, it will be more or less distant from the Ecliptic, according as it is more or less removed from the nearest Node; these two opposite Points in the Orbit, that lie in the Middle between the Nodes, are called, *the Limits*; and when the Moon is in either of these, she is then at her greatest Distance from the Ecliptic.

47. The Height of the nearest Pole above the Horizon of any Place, is equal to the Latitude of that Place. For let A be any Place upon the Earth, AHO its Meridian, HO the Horizon, EQ the Equator, P and  $p$  the two Poles; then 'tis plain, AE will be the Latitude of the Place, and,



PO the Height of the nearest Pole above the Horizon. Now since the Arches PE and AO are equal,

equal, being each a Quadrant; from both take the common Arch A P, and there will remain A E equal to P O; that is, the Height of the Pole above the Horizon is equal to the Latitude. Also, since the Arches A H and E P are equal, being both Quadrants, from both take the common Arch A E, and there will remain E H equal to A P; that is, the Height of the Equator above the Horizon of any Place, is equal to the Complement of the Latitude of that Place.

48. Great Circles passing thro' the Poles of the Ecliptic, and cutting it at Right Angles, are called Secondaries of the Ecliptic.

49. *The Latitude* of any Heavenly Body is an Arch of the Secondary, passing thro' the Center of the Object, intercepted between it and the Ecliptic; and it is either North or South, according as the Object is on the North or South Side of the Ecliptic.

50. *The Longitude* of any Celestial Body is an Arch of the Ecliptic, intercepted between the Secondary passing thro' that Body, and the first Point of *Aries*.

51. *The Declination* of any Heavenly Body is an Arch of a Meridian, passing over that Body, intercepted between the Center of it and the Celestial Equator; and it is either North or South, according as the Body is on the North or South Side of the Equator.

52. Since the Sun by his annual Motion is always either approaching nearer to, or going further from, the Equator; 'tis plain, he must be continually changing his Declination. In the third Table, at the End of this Book, you have his Declination for every Day of the Year; in which you may observe, that in the Top Columns stand the Year, Month, and Kinds of the Declination, *viz.* whether it be South or North; and in the Left-hand Column stands

stands the Day of the Month, the other Columns contain the Declinations answerable to these; consequently to find the Sun's Declination for any Day, suppose the twentieth of *April*, 1731. I look at the Top for the Year 1731, and the Month *April*, and in the side Column for 20, then in the Column below *April*, and on the same Line with 20, I find  $14^{\circ} 59'$  for his Declination North; and the same Way his Declination may be found for any other Day. But you must observe, that this Table is calculated only for the Meridian of *London*, and the Noon there; that is, it shews the Declination of the Sun when upon the Meridian of *London*; and consequently to find the Sun's Declination for any other Time of the Day, we must consider whether the given Time be before or after Noon; if it be before, then say, as 24 Hours is to the Difference between the Declination of the Sun, the Noon of the preceding Day, and his Declination the Noon of the present Day; so is the Time from Noon last Day, to a fourth Proportional; which, if the Declination be increasing, must be added to, but if decreasing, subtracted from, the Sun's Declination the Noon of the preceding Day; and the Sum, or Remainder, is the Declination from the present Time.

*Example.* Suppose it were required to find the Sun's Declination, on the fourth Day of *April* 1731, at 8 Hours, 25 Minutes in the Morning. To do this, I first look in the Tables for the Sun's Declination, the fourth Day of *April* 1731, and find it to be  $9^{\circ} 39'$ , then I look for it the third Day, and find it to be  $9^{\circ} 17'$ , the Difference of these is  $22'$ ; then I say, as 24 Hours is to  $22'$ ; so is 20 Hours 25 Minutes, the Time elapsed since last Noon, to  $18'$ ; which added to  $9^{\circ} 17'$  (because the Declination is increasing) gives  $9^{\circ} 35'$ , for the Sun's present Declination. Again, if the Time proposed be after Noon; then to find the Declination for that

that Time, we must look in the Tables for the Sun's Declination, at Noon of the present Day; and for the same, the Noon of the following Day, and take the Difference of these Declinations; then say, as 24 Hours is to the Difference of the Declinations, so is the Time elapsed since Noon, to a fourth Proportional; which added to, or subtracted from, the Sun's Declination the present Day at Noon (according as the Declination is increasing or decreasing) gives the Sun's Declination at the Time proposed.

*Example.* Suppose it were required to find the Sun's Declination on the twelfth Day of July 1731, at 4 Hours, 23 Minutes after Noon. To do this we must first look in the Tables for the Sun's Declination the twelfth Day of July 1731, and will find it to be  $20^{\circ} 13'$ ; then for his Declination the following Day, which is  $20^{\circ} 01'$ , and the Difference between these two is  $12'$ ; then say, as 24 Hours is to  $12'$ , so is 4 Hours, 23 Minutes, the Time elapsed since Noon, to  $2'$ , which (because the Sun's Declination is decreasing) subtracted from  $20^{\circ} 13'$ , the Declination of the Sun at Noon of the present Day, leaves  $20^{\circ} 11'$ , the Sun's Declination for the Time proposed.

And since the Table of the Sun's Declination, at the End of this Book, is fitted to the Meridian of London, 'tis plain, it cannot serve for the Meridian of any other Place, lying on the East or West Side of the Meridian of London; for while the Sun, by his apparent diurnal Motion, is passing from one Meridian to another, he is at the same Time still moving on in the Ecliptic, and consequently altering his Declination. Now to find the Declination of the Sun, when he is on the Meridian of any Place, lying on the East or West Side of London, we must take the Difference of Longitude between London and the given Place (or if the Meridian of

*London* be supposed the first Meridian, we must take the Longitude of the Place) and convert this into Difference of Time, which will shew the Time, before or after Noon at *London*, the Sun is upon the Meridian of the Place proposed; *viz.* if the Place lie on the East-Side of *London*, the Time will be before Noon; but if on the West, it will be after Noon; then finding, according to the preceding Examples, the Sun's Declination at the Time proposed, the same will be his Declination, when on the Meridian of the proposed Place.

This may be done another Way, *viz.* by the Help of the Table of Variation of the Sun's Declination, to every 15 Degrees of Longitude from the Meridian of *London*, annexed to the Table of Declination; the Upper Column of which contains the Degrees, and the Left-hand side Column contains the Minutes of the Sun's daily Variation; and the other Columns contain the Minutes answering to the Degrees and Minutes in the Top and Side Columns. Now, to find the Sun's Declination any Day, when he is on the Meridian of any Place, lying on the East or West Side of *London*, by this Table; we must first find the Sun's Declination for the present, and for the following Day; and the Difference between these two will give us the daily Variation at that Time; then look in the Table of Variation, &c. at the Top, for the Difference of Longitude between *London* and the proposed Place, and in the side-Column for the Minutes of Variation; then below these Degrees in the Top, and on the same Line, with the Variation in the side-Column, we will find the Variation required; which, if the proposed Place be West of *London*, and the Declination increasing, must be added to the Declination for the present Day, and the Sum is the Declination required; but if the Declination be

creasing, then the Variation subtracted from the Declination gives that required ; again, if the Place be on the East-Side of *London*, and the Declination encreasing, then the Variation subtracted from the Declination for that Day, leaves the Declination required ; but if the Declination be decreasing, then the Variation added to the Declination gives that required.

*Example.* Let it be required to find the Sun's Declination, when he is on the Meridian of *St. Lucia* (whose Longitude from *London* is  $60^{\circ} 15'$  West) on the sixth Day of *April 1731*. To do this, I first look in the Tables for the Declination of the Sun the sixth Day of *April 1731*, and find it to be  $19^{\circ} 15'$ , then for the same the following Day, and I find it to be  $19^{\circ} 29'$ , the Difference of which is 14 Minutes, the Sun's daily Variation at that time ; then I look in the Top of the Table of Variation, &c. for  $60$ , the Difference of Longitude, and in the side Column for  $14$ ; and below  $60$ , and in the same Line with  $14$ , I find 2 Minutes, which (because the Place is West off *London*, and the Declination encreasing) I add to  $19^{\circ} 15'$ , and the Sum is  $19^{\circ} 17'$ , the Sun's Declination at *St. Lucia* the sixth Day of *April 1731*.

From this you may observe, that the Method of solving this Problem by the Table of Variation, &c. is not near so good as the former ; for here we can only enter the Table with a Number of Degrees, which is either  $15^{\circ}$ , or some Multiple of it below  $195^{\circ}$ , and all the odd Degrees and Minutes must be thrown away ; but in the former Method we can use any Number of Degrees and Minutes.

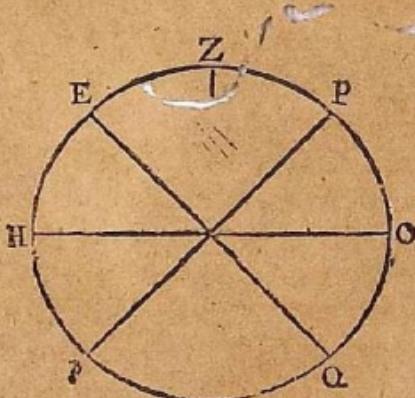
53. And since the fix'd Stars always keep the same Places in the Heavens (at least in a few Years their Variation is insensible) 'tis plain, their Declination must still be the same.

## S E C T. IV.

**T**O find the Latitudes of Places by the Meridian-Altitude, and Declination of any Celestial Object.

This Problem admits of several Cases, according as the observed Object is situate with respect to the Equator, and Place of Observation ; which are as follows.

*Case I.* When the Sun or Star observed has no Declination, or is upon the Equator, then the Zenith-Distance of the Object is equal to the Latitude of the Place, which is North-Latitude if the Sun or Star come to the Meridian, on the South-

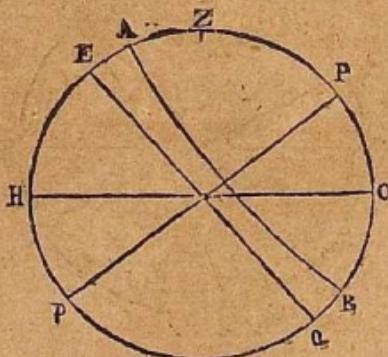


side of the Zenith ; but South, if on the North-side. For in the annexed Scheme, let Z represent the Place of Observation, PQ p E its Meridian, EQ the

the Equator, H O the Horizon, P the North, and Q the South-pole; then 'tis plain, since the observed Object is supposed to have no Declination, that EQ will represent the Path of its Diurnal Motion, and when it comes upon the Meridian, Z E will be its Zenith Distance, which is manifestly equal to the Latitude of the Place Z. And when the Object at E is South off Z, 'tis plain the Place Z must be North off E, and consequently the Latitude will be North.

*Case 2.* If the Sun or Star, when on the Meridian, is in the Zenith; then the Declination of the Object is the same with the Latitude of the Place. For it is evident, that in this Case they are equally distant from the Equator, and on the same Side of it; consequently, if the Declination be North, the Latitude will also be North, and if South, South.

*Case 3.* If the Sun or Star be between the Equator and Place of Observation, then the Latitude of the Place is equal to the Sum of the Zenith Distance and Declination of the Object; and it is of the ~~same~~ Name with the Declination, viz. if the Decli-



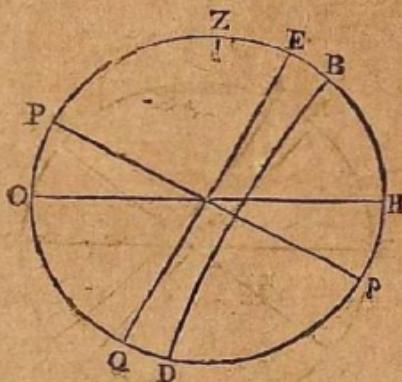
nation be North, the Latitude is also North, & *e contra.* For in the adjacent Scheme, let AB represent the Parallel described by the observed Ob-

ject in its Diurnal Motion, and A its Place upon the Meridian, situate between Z, the Place of Observation, and EQ the Equator; then 'tis plain that ZE, the Latitude of the Place Z, is equal to the Sum of EA the Declination, and AZ the Zenith-Distance, and if the Declination be North, & *e contra*; since in this Case the Object and Place of Observation lie both on the same Side of the Equator.

*Example.* Suppose on the Twelfth Day of April, 1732, the Sun, when on the Meridian, had  $52^{\circ}, 12'$  of Altitude, and consequently  $37^{\circ}, 48'$  Zenith-Distance, required the Latitude of the Place of Observation.

the Sun's Declination that Day is -  $12^{\circ}, 40'$  N.  
his Zenith-Distance - - - - -  $37, 48$   
the Sum is the Latitude, *viz.* - - -  $50, 28$  N.

*Case 4.* If the Sun or Star be on the contrary Side of the Equator, with the Place of Observation, and



consequently both Declination and Zenith-Distance be of the same Name, *viz.* either both North or both South; then the Latitude is found by taking the

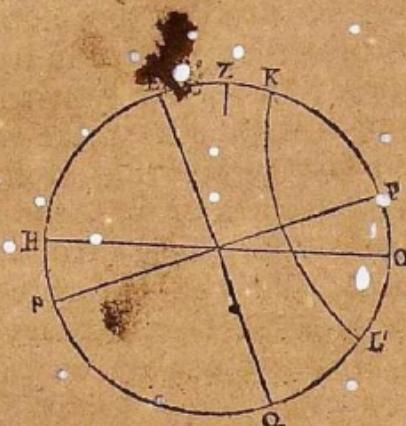
the Declination from the Zenith-Distance, and it is of a contrary Name with the Declination. For in the adjacent Figure let  $B D$  represent the Parallel described by the observed Object in its Diurnal Motion, on the other Side of the Equator  $F.Q.$ , with the Place  $Z$ , and  $B$  will be its Place when upon the Meridian; then 'tis plain, that if from  $ZB$ , the Zenith-Distance, be taken  $BE$  the Declination, there will remain  $ZE$ , the Latitude of the Place of Observation  $Z$ , and the Latitude will be of a contrary Name with the Declination; since in this Case, the Object and Place are on contrary Sides of the Equator.

*Example.* Being at Sea the Twelfth Day of January 1732, I found the Meridian-Altitude of the Sun to be  $43^{\circ} 15'$ ; consequently his Zenith-Distance  $46^{\circ} 45'$ , and he was South off me: Required the Latitude of the Place of Observation, and which Way it is.

From the Meridional Zenith-Distance  $46^{\circ} 45'$ , S. take the Sun's Declination - - - -  $19^{\circ} 35'$ , S. there remains the Latit. of the Place -  $27^{\circ} 10'$ , N. When the Zenith-Distance and Declination are equal, and both of the same Name, then the Latitude vanishes, and consequently the Place is situated on the Equator.

*Case 5.* If the Sun or Star be between the Place of Observation and the nearest Pole, and consequently both Declination and Zenith-Distance be of the same Name; then, from the Declination subtract the Zenith-Distance, and the Remainder is the Latitude of the Place of Observation, and it is of the same Name with the Declination. For in the annex'd Scheme, let  $K L$  represent the Parallel described by the observed Object in its Diurnal Motion, and  $K$  will be its Place when upon the Meridian; then 'tis plain, that if from  $KE$  the Declination, be taken  $ZK$ , the Meridional Zenith-Distance, there

there will remain Z E, the Latitude of the Place, which will be of the same Name with the Declina-



tion, since the Object and Place of Observation are in this Case upon the same Side of the Equator.

*Example 1.* Suppose on the Twenty-third Day of June 1733, I observed the Meridian-Altitude of the Sun to be  $82^{\circ}, 4'$ ; consequently his Zenith-Distance  $7^{\circ}, 56'$ : Required the Latitude of the Place of Observation, and which Way it is.

The Sun's Declination that Day is - -  $22^{\circ}, 55'$  N.  
his Zenith-Distance is - - - - -  $7, 56$  N.  
the Difference is the Latitude, viz. - -  $14, 59$  N.

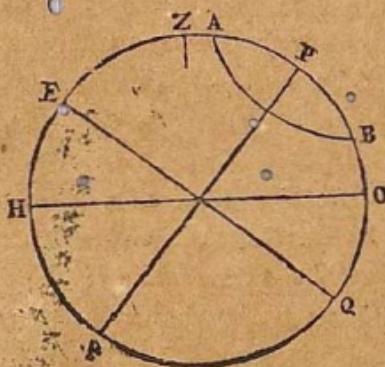
*Example 2.* Being at Sea, I observed the Meridian-Altitude of the middlemost Star in the Tail of the Great Bear, to be  $56^{\circ}, 44'$  North; consequently its Zenith-Distance  $33^{\circ}, 16'$ , and its Declination being  $56^{\circ}, 22'$  North: Required the Latitude of the Place of Observation, and which Way it is.

From the Declination - - - - -  $56^{\circ}, 22'$  N.  
take the Zenith-Distance - - - -  $\underline{33, 16}$  N.

there remains the Latitude - - -  $23, 06$  N.

*Case 6.*

**Case 6.** If the Sun or Star be between the Horizon and the elevated Pole, then to the Altitude add the Complement of the Declination, and the Sum will be the Latitude of the Place of Observation, and of the same Name with the Declination. For let AB be the Parallel described by the Object in its diurnal Motion, B its Place on the Meridian, when between the Horizon and elevated Pole; then



tis plain, that if to BO the Altitude, be added BP, the Complement of the Declination of the Object, the Sum PO will be equal to the Height of the Pole above the Horizon, which (by Art. 47. Sect. 3.) is equal to the Latitude of the Place of Observation Z, and it will be of the same Name with the Declination, since both the Place and the Object are on the same Side of the Equator.

*Example.* Being at Sea, I observed the bright Star of the Harp on the Meridian, between the Horizon and elevated Pole, its Altitude being  $8^{\circ} 33'$ , and Declination  $33^{\circ}, 33'$  North. Required the Latitude of the Place of Observation.

To the Complement of the Declinat.  $51^{\circ}, 27' N.$   
add the Altitude - - - - -  $8, 33 N.$   
the Sum is the Latitude - - - -  $60, 00 N.$

*Case 7.*

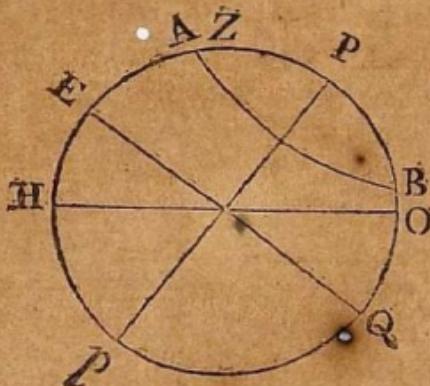
*Case 7.* When the observed Object does not set, and consequently the Complement of its Declination less than the Latitude of the Place; then 'tis plain, the Object will be twice upon the Meridian in 24 Hours, viz. at its least and greatest Altitude, when the Altitude is least, the Object is then between the Horizon and elevated Pole, and by that Altitude and Declination of the Object, the Latitude of the Place may be found, (as in the last Case); but when the Altitude is greatest, the Object is then on the other Side of the Pole. Now, with these two Meridian-Altitudes, without knowing the Declination of the Object, we can find the Latitude of the Place thus; if the two Altitudes be both on the same Side of the Zenith, then from the greatest subtract the least, and half the Remainder added to the least gives the Latitude, of the same Name with the Zenith-Distance; for in the preceding Scheme, where AB represented the Parallel of Declination, described by the Object in its diurnal Motion, BO its least, and AO its greatest Meridian-Altitude, 'tis plain, if from AO be taken BO, the Difference will be AB, the half of which, PB, added to BO, gives PO the Height of the Pole above the Horizon, equal to the Latitude of the Place.

*Example.* Being at Sea, I observed the Northernmost of the two preceding Stars in the Square of the Great Bear, which did not set, and found the least Altitude to be  $23^{\circ} 12'$ , and the greatest  $72^{\circ} 46'$ , both North off my Zenith. Required the Latitude of the Place of Observation.

From the greatest Altitude	- - -	$72^{\circ} 46' N.$
take the least	- - - - -	$23 , 12$
the Remainder is	- - - - -	$49 , 34$
the half of which is	- - - - -	$24 , 47$
to which adding the least Altitude	- - - - -	$23 , 12$
the Sum will be	- - - - -	$47 , 59$
		which

which is equal to the Latitude of the Place, and it is North, because the Zenith Distance is on the North-Side.

But if the greatest and least Meridian Altitudes of the Objects be upon different Sides of the Zenith, *viz.* the one upon the North, and the other upon the South-Side; then, from the Supplement of the greatest Altitude, subtract the least, and half the Remainder added to the least Altitude, will give the Latitude of the Place of Observation, which will be of the same Name with the least Altitude, *viz.* North; if the least Altitude be North of the Place, & *e contra*. For in the annex'd Figure, let BA represent the Parallel described by the Object in its diurnal Motion, B and A the Places of the Object when upon the Meridian, on contrary Sides of the Zenith Z; BO its least Altitude, and HA its greatest, the Supplement whereof is AO. Now 'tis plain, that if from AO we take OB, the Remainder will be AB, the half of



which, PB, added to BO, makes PO the Height of the Pole above the Horizon, or Latitude of the Place Z; which will be North, if the least Altitude BO be on the North-Side of the Place, because in this Case the North-Pole will be elevated.

*Example.* Being at Sea, I observed the Sun when he did not set, and found his least Meridian Altitude to be  $3^{\circ} 29'$ , on the North-Side of the Zenith, and his greatest Meridian Altitude was  $41^{\circ} 29'$ , on the South-Side: Required the Latitude of the Place of Observation.

From the Supplement of the Sun's greatest Meridian Altitude - - -  $136^{\circ}, 31'$   
 take his least Altitude - - - - -  $3, 29$   
 and there remains - - - - -  $133, 02$   
 the half of which is - - - - -  $66, 31$   
 to which adding the least Altitude -  $3, 29$   
 the Sum is - - - - -  $70, 00$  N.  
 the Latitude of the Place of Observation.

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## S E C T. V.

### Of the Elements of Chronology.

1. **T**IME considered abstractly, without any Relation to external Objects, flows always equally and uniformly, and it is called Absolute, True, and Mathematical Time, or, simply, Duration. But that which commonly goes under the Name of Time, is a certain Part of Duration, measured by the simple and uniform Motion of some Body, such as the Motion of the Celestial Bodies; and particularly of the Sun and Moon; this is called Relative, Apparent, or Vulgar Time.

2. Time is divided into Years, Months, Weeks, Days, Hours, Scruples or Minutes, &c.

3. A Day is of two Kinds, viz. *Natural* or *Artificial*; a *Natural Day* is that Space of Time that flows while the Sun moves from any Meridian, till he comes to the same again. An *Artificial Day* is that

that Space of Time that the Sun continues above the Horizon, and the Time he continues below it is called a Night.

4. An Hour is a certain determinate Part of the Day, and is either *Equal* or *Unequal*. An *Equal Hour* is the Twenty-fourth Part of a Natural Day; and an *Unequal Hour* is the twelfth Part of an Artificial Day, which is also called a *Diurnal-Hour*, as the twelfth Part of the Night is called a *Nocturnal-Hour*; these are likewise called *Temporary Hours*, because at different Seasons of the Year they are of different Lengths; for a diurnal Hour in the Summer is longer, and a Nocturnal shorter, than in the Winter; but in the Equinoctial Day, a *Diurnal Hour* is equal to a *Nocturnal*, and then they are called, *Equinoctial Hours*.

5. The *Diurnal Hours* begin at the rising, and end at the setting of the Sun; and the *Nocturnal Hours* begin at the setting, and end at the rising of the Sun. These Hours were anciently in use among the *Jews* and *Romans*, and at present among the *Turks*. They were anciently called *Planetary Hours*, because in every Hour one of the seven Planets was suppos'd to preside over the World; thus for Example, on *Sunday*, the first Hour from Sun-rising was allotted to the *Sun*, the second fell to *Venus*, the third to *Mercury*, and so on to the rest in order, *viz.* to the *Moon*, *Saturn*, *Jupiter* and *Mars*; by which Means, the first Hour from Sun-rising, the next Day fell to the *Moon*; from which it was called *Monday*, and so on thro' the other Days of the Week, each Day getting its Name from the Planet that was supposed to preside the first Hour of that Day.

6. The Day in different Nations begins at different Times. Thus the *Babylonians*, *Affyrians*, and several other Eastern Nations began their Day at Sun-rising: The Hour after that, they called the

First Hour, and so counted on till they come to the Twenty-fourth, or last Hour, which was the Hour before Sun-rising. The Jews and Grecians began their Day at Sun-set; as at this Time the Italians, Sicilians, Bohemians, Poles and Austrians do; the Hour before the Sun-set they call the last, or Twenty-fourth Hour; and the Hour after the Sun is set, they call the first Hour; and so count on to the Twenty-fourth, when the Sun sets again.

7. The Egyptians and Romans anciently began their Day at Mid-night; which was followed by Hipparchus, Copernicus, and other Astronomers, in their Astronomical Observations, and is still retained in Britain, France, Spain, and most other Places in Europe; but the Arabs and modern Astronomers begin the Day at Noon, viz. when the Sun is upon the Meridian.

8. A Week is a Succession of seven Natural Days, each of which has a particular Name allotted to it, viz. the first is called *Sunday*; the second *Monday*, and so on.

9. A Month is a certain System of Days, consisting of something more or less than thirty Days, and is of two Kinds, viz. Astronomical or Civil; an *Astronomical Month* is that which is governed either by the Motion of the Sun, or that of the Moon; and consequently is of two Kinds, viz. *Solar* or *Lunar*. A *Solar Month* is that Time which the Sun takes to run through a whole Sign, or the twelfth Part of the *Ecliptic*; and a *Lunar Month* is that which is measured by the Motion of the Moon round the Earth, and is of three Kinds, viz. *Periodical*, *Synodical*, and that of *Illumination*; the *Periodical* and *Synodical Months* are defin'd in Art. 45. Sect. 3. and the *Month of Illumination* or *Apparition*, is that Space of Time contained between the Day that the *Moon* begins to appear after Change, to the Day that she disappears; and this consists of

~~Two~~, eight Days nearly. A Civil or Political Month differs from the Astronomical, and consists of more or fewer Days, according to the Institution of the Country in which they are used.

10. A Year is a certain System of Months, and is either Astronomical or Civil; the Astronomical Year is of two Kinds, viz. Solar, or Lunar; and the Solar Year, is either Sidereal or Tropical. The Sidereal Year is that Space of Time that the Sun takes to move from a fix'd Star till he returns to the same again; and it consists of 365 Days, 6 Hours, 9 Minutes, and 14 Seconds; the Tropical Year is that Space of Time, which flows while the Sun moves from any one of the Cardinal Points, till he returns to the same again; and it consists of 365 Days, 5 Hours, 48 Minutes, and 57 Seconds, and commonly gets the Name of the Solar Year.

11. A Lunar Year consists of a certain Number of Months, and is either Common or Embolismic. A Common Lunar Year consists of twelve Synodic Lunations, and an Embolismic contains thirteen.

12. The Civil or Political Year consists of a certain Number of Days, more or fewer, according to the Laws and Customs of the Countries in which it is received.

13. Since the Common Lunar Year consists of twelve Synodic Months, or 354 Days nearly, and the Solar consists of 365 Days, (throwing away the odd Hours and Minutes) 'tis plain, that the Solar Year will exceed the Lunar by about 11 Days; and consequently in the Space of about Thirty-three Years the Beginning of the Lunar Year will be carried through all the Seasons; and hence it is called the Moveable Lunar Year. This Form of the Year is used at this Time by the Turks and Arabians; and because in three Years Time, the Solar exceeds the Lunar by 33 Days; therefore to keep the

the Luhar Months in the same Seasons and Times of the Solar Year, or near it, they added a whole Month to the Lunar Year, every third Year, and so made it consist of thirteen Months; this Year they called the Embolistic Year, and the additional Month, the Embolimean or Intercalary Month. This Form of the Lunar Year is called the fix'd Lunar Year; and it was used by the Greeks and Romans till Julius Cesar's Time.

14. The Egyptians made use of the Solar Years, and made each consist of 365 Days, which wants of the Tropical Year almost 6 Hours; and consequently the Egyptian Year began always 6 Hours sooner than the immediately preceding Tropical Year; by which Means, in four times 365 or 1460 Years, (called the Great Canicular Year or Sothic Period) the Beginning of the Year moved thro' all the Seasons.

15. Julius Cesar, in order to reduce the Civil or Political Year nearly to an Equality with the Tropical, and considering that the Tropical Year consisted of 365 Days, and 6 Hours nearly, which exceeded the Civil Year by 6 Hours each Year, and consequently in four Years exceeded it by one whole Day; he ordered, that to every fourth Year there should be one whole Day added, and so made it consist of 366 Days, by which Means the Civil and Solar Years were reduced pretty near to an Equality. This additional Day was put in the Month of February; and because in the common Year, the Twenty-fourth Day of February was called by the Romans, the sixth of the Kalends of March, therefore he ordering that this Day should be added after the Twenty-fourth Day of February, and called by the same Name; there happened every fourth Year two Sixths of the Kalends of March, and hence that Year was called Bissextile or Leap Year. This Way is still retained, and made use of by us.

16. But the true Length of the Year being 365 Days, 5 Hours, and 49 Minutes nearly, and by the Julian Account 365 Days and 6 Hours; 'tis plain, the Civil Year exceeds the Solar by 11 Minutes yearly. Consequently, if the Sun any Year enters the Equinoctial on the Twentieth Day of March at Noon, the next Year, he will enter the Equinoctial the same Day, 11 Minutes before Noon, the next, 22 Minutes before Noon, and so on. Consequently in 131 Years the Solar will anticipate the Civil Year, by one whole Day; and so either Equinox will not happen always on the same Day of the Civil Year, but be carried in a Retrograde Order thro' all the Days of it. This was what put Pope Gregory the XIII<sup>th</sup>, upon reforming the Julian Kalendar; for finding that at the Time of the Nicene Council, when the Time of celebrating Easter was instituted, the Vernal Equinox happened the Twenty-first Day of March; and by flowing continually backwards, it happened at his Time, in the Year in 1572, on the Eleventh Day of March, anticipating its former Time, by 10 whole Days; he ordered that these 10 Days should be taken out of the Kalendar, and the Eleventh Day of March should be reckon'd the Twenty-first; and to prevent the Seasons of the Year from going any more backwards, as they were before, he ordered that every hundred Year of the Christian Æra (which according to the Julian Kalendar is Bissextile) should be a common Year, and so consist only of 365 Days; but this being too much, therefore every four hundredth Year was to remain Bissextile or Leap-Year. This Form of the Year is receiv'd in France, Spain, Germany, Italy, and other Countries that allow of the Pope's Authority; as also in Holland, and several other Places where the Reformed Religion is profess'd. But the British and other Reformed Northern Nations still

still retain the Julian Form, which is ~~the~~ Old Style, and the Gregorian, New Style.

17. A *Kalendar* is a regular Disposition of the Days in the Civil Years into Months and Weeks; each Day of every Week being distinguished from another by one of the first seven Letters of the Alphabet, *viz.* A, B, C, D, E, F, G. Beginning at the first of *January*; to it is annexed the Letter A, to the second the Letter B, to the third C, and so on to the seventh, to which is annexed the Letter G; and beginning again with the Letters, to the eighth is annexed A, to the ninth B, to the tenth C, and so on thro' the rest of the Days of the Year, each of them having one of these Letters annexed to it. Hence 'tis plain, that whatever Letter is placed against any Day of any Week, that Letter will be placed against that Day through the whole Year: Thus; If the first Day of *January*, against which stands the Letter A, be a *Sunday*; then all the Days in the *Kalendar* having the Letter A standing against them, will be *Sundays*. Also if the Fourth Day of *January*, against which stands the Letter D, be a *Sunday*, then all the Days in the *Kalendar*, having D annexed to them, will be *Sundays*. That Letter which answers to the *Sundays* throughout the Year, is called the *Dominical* or *Sunday Letter*, for that Year.

But since the *Common Year* consists of 365 Days, if that be divided by seven, the Quotient will be 52 Weeks, and one Day over; and since if nothing remained, then whatever Day of the Week the Year began on, the same Day of the Week would be the first Day of each succeeding Year; 'tis plain, that whatever Day of the Week any Year begins on, the same Day of the Week will be the last Day of the Year; and consequently, if the First Day of *January*, to which is annexed the Letter A, be *Sunday*, the last Day of the Year will be *Sunday*.

Year will be *Sunday*, and the first of the next will be *Monday*, and the first *Sunday* of the Year will fall on the seventh Day, to which is annexed the Letter G, which therefore will be the *Dominical Letter* all that Year; and since the Year began on *Monday*, it will also end on *Monday*, and the first Day of the next Year will be *Tuesday*; consequently the first *Sunday* will fall on the sixth Day, to which is annexed F, which therefore will be the *Dominical Letter* all that Year. And the same Way the *Dominical Letter* the Year following will be E, and for the next D; and in this retrograde Order the *Dominical Letter* is carried successively thro' the seven, after which it begins again.

18. From what has been said 'tis plain, that if the Year consisted of 365 Days exactly after a Period of seven Years, the same Day of each Month would fall on the same Day of the Week. But because every fourth Year is *Bissextile*; consisting of 366 Days, which is equal to 52 Weeks, and 2 Days; therefore if that Year begins on a *Sunday*, it will end on *Monday*, and the next will begin on *Tuesday*, and the first *Sunday* of that Year will fall on the sixth Day of *January*, to which is annex'd the Letter F, which will be the *Dominical Letter* for the Year following the *Leap Year*, whose *Dominical Letter* was A. And since the *Bissextile* or *Leap Year* returns every fourth Year, 'tis plain the Series of *Dominical Letters* will be interrupted, and will not return till after four times Seven, or twenty eight Years. And hence arises the Cycle of twenty eight Years called the *Solar Cycle*, which being completed, the Days of the Month return in the same Order to the same Day of the Week.

19. And since in every *Leap-Year* the *Intercalary* Day is placed between the twenty third and twenty fourth Day of *February*, and so makes

two twenty Fourths of *February*; which in the *Kalendar* are esteemed as one and the same Day, and have the same Letter affixed to them, and which by our Way of Reckoning are called the twenty fourth and twenty fifth Day of *Februari*; 'tis plain the Order of the *Dominical Letter* will at that Time be interrupted, and the succeeding Letter will take Place; thus if in a *Leap Year* the first of *January* be *Sunday*, and consequently the *Dominical Letter A*; the twenty fourth Day of *Februari*, will fall upon a *Friday*, and the twenty fifth on a *Saturday*; and since both these Days are mark'd in the *Kalendar* with the same Letter *F*; the following Day, which is *Sunday*, will be mark'd with *G*, which Letter will mark out all the *Sundays*, and consequently be the *Dominical Letter*, the remaining Part of the Year. And hence it is that every *Leap-Year* has two *Dominical Letters*, the first of which serves from the Beginning of the Year to the twenty fourth or twenty fifth Day of *Februari*, and then the other takes Place, and serves for the rest of the Year.

20. The first Year of the *Solar Cycle* was plac'd in a *Leap Year*, having for it's *Dominical Letters G* and *F*, whence the *Dominical Letter* for the second is *E*, for the third *D*, for the fourth *C*; and the fifth Year of the *Cycle* is again *Bissextile*, whose *Dominical Letters* are *B* and *A*, consequently the *Dominical Letter* for the sixth Year is *G*, and so on, as in the following Table which shows the *Dominical Letter* for every Year in the *Cycle*.

1	GF	5	BA	9	DC	13	FE	17	AG	21	CB	25	ED
2	E	6	G	10	B	14	D	18	F	22	A	26	C
3	D	7	F	11	A	15	C	19	E	23	G	27	B
4	C	8	E	12	G	16	B	20	D	24	B	28	A

Whence 'tis plain, that by knowing the Year of the *Cycle*, we can find the *Dominical Letter* answering thereto from the Table. Now since the first Year of the *Christian Era* happen'd on the tenth Year of the *Cycle*, and consequently 9 Years of the *Cycle* were elaps'd before the *Christian Era* commenced; therefore to find the Year of the *Solar Cycle* for any Year of the *Christian Era*, and the *Dominical Letter* belonging to it; we must add 9 to the given Year and divide the Sum by 28, then the Quotient will show how many complete *Cycles* have past since the first Year of the *Solar Cycle*, that the *Christian Era* commenc'd in, and the Remainder, if there be any, will show the current Year of the *Cycle*; but if there be no Remainder then the Year is the last, or twenty eighth Year of the current *Solar Cycle*; and having found the Year of the *Cycle*, we have the *Dominical Letter* answering it from the preceding Table.

*Example.* Suppose it were required to find what Year of the *Solar Cycle* the Year 1734 is, and the *Dominical Letter* belonging to it.

*First,* I add 9 to the given Year and the Sum is 1743, which divided by 28, the Quotient 62 shows that there are 62 complete *Cycles* elaps'd, since the first Year of that *Cycle* in which the *Christian Era* commenced and the Remainder 7 shows that the Year 1734 is the seventh Year of the current *Cycle*; then looking in the preceding Table, for the seventh Year of the *Cycle*, I find the *Dominical Letter* answering thereto is F.

21. Since the Revolutions of the *Sun* and *Moon* are found constantly to be the same, the *Moon* moving with about thirteen Times the Velocity of the *Sun*; it follows, that after a certain Number of Revolutions, they must meet again in the same Point of the Heavens they did some time before,

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which by Meton the Athenian, was said to be 19 Years just; after the Expiration of which Time the new and full Moons were supposed to happen on the same Day and Time of that Day, and in the same Month, they did 19 Years before that. This Cycle is from its Author called the *Metonic Cycle*; & so 'tis called the *Lunar Cycle*.

22. This Cycle began 1 Year before the Commencement of the Christian Era, and consequently to find what Year of the Cycle any Year in the Christian Era is; we must to the given Year add 1, and divide the Sum by 19; then the Quotient will show how many Cycles have revolv'd since the Commencement of the Christian Era, and the Remainder will shew what Year of the Cycle the present Year is; if there be no Remainder then the given Year will be the last or nineteenth Year of the Cycle. The Year of the Cycle answering to any given Year, is, for its great Use in determining the Times of the new and full Moon, and thereby knowing what Day of the Month Easter-Day falls upon, called the *Golden Number* or *Prime* for that Year.

*Example.* Required the *Golden Number* for the Year 1732.

First, I add one to the given Year, and the Sum is 1733, this divided by 19, gives 91 for the Quotient, and 4 for the Remainder; which shows that there have revolved 91 complete *Lunar Cycles* since the first Year of that Cycle in which the Christian Era commenced, and that the given Year is the fourth Year of the current Cycle, consequently 4 is the *Prime* or *Golden Number* for the Year 1732.

23. It has been shown, at Art. 13. of this, that the *Solar Years* exceed the *Lunar* by 11 Days nearly; consequently if the Moon be New, or in Conjunction with the Sun, on the last Day, or thirty first

first of December in any Year on the last Day of the next Year it will be 11 Days past Conjunction, and on the last Day of the following Year it will be 22 Days after new Moon; but because in the succeeding Year this amounts to 33 Days, and 30 Days being allowed for a complete Moon: 'tis plain, in that Year there will have happened 13 Conjunctions, and the Moon will be 3 Days past Change on the last Day of it; consequently on the last Day of the next Year the Moon will be 14 Days past the Conjunction, and so continually increasing by eleven Days yearly, till after the End of 19 Years it will become the same as before. The Age of the Moon or Number of Days past since the Conjunction, on the last Day of any Year is called the *Epact* for the succeeding Year.

24. Now since the *Epact* for the first Year of the *Lunar Cycle* was 11, the *Epact* for the Second will be 22, for the Third 3, for the Fourth 14, for the Fifth 25, and so on constantly increasing by 11; it follows that to find the *Epact* for any Year, we must multiply the *Golden Number* for that Year by 11, and divide the Product by 30, and the Quotient, if there be any, will shew how many *Embolimean* or *Intercalary* Months have happened since the first Year of the current *Cycle*, and the Remainder will be the *Epact* for the given Year; or will shew how many Days has elapsed between the last Day of the former Year and the immediately preceding Conjunction.

*Example.* Required the *Epact* for the Year 1735.

*First,* By Art. 22. I find the *Golden Number* for the Year 1735 to be 7, which multiplied by 11, gives 77, and this divided by 30 gives 2 for the Quotient and 17 for the Remainder, and consequently there have been 2 *Intercalary* Months since the Commencement of the current *Cycle* to the Year 1735, and 17 is the *Epact* for that Year, or it is the

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the Age of the Moon, the last Day of December

1734.

25. Since by Art. 23. the *Epaet* for any Year shews the Age of the Moon on the last Day of the preceding Year, 'tis plain if to the *Epaet* we add 1, the Sum will be the Age of the Moon the first Day of that Year; but because the *Synodical Month*, or time between any two immediate Conjunctions, is equal to 29 Days and an Half, and *January* containing 31 Days; therefore if to the Age of the Moon on the first of *January* be added  $1\frac{1}{2}$  (or to avoid Fractions) 2 Days, the Sum will be the Age of the Moon on the first of *February*; and because in common Years the Days in *January* and *February* taken together make 59, which is exactly equal to two intire Lunations, therefore the Age of the Moon on the first of *January* will be the same with its Age on the first of *March*, and consequently to its Age on the first of *January*, there is nothing added, in common Years, for its Age on the first of *March*; but in *Leap Years* the Sum of the Days in *January* and *February* being 60, which is more than two intire Lunations by 1 Day, it is evident that in this Case, we must add 1 Day to the Moon's Age on the first of *January*, and the Sum will be its Age on the first of *March*. And by the same Way of Reasoning it will appear, that to find the Age of the Moon on the first Day of any Month, we must add to its Age on the first of *January* the following Numbers, viz. for *February* 2, for *March* 0, in common Years, and 1 in *Leap Years*, for *April* 2, for *May* 3, for *June* 4, for *July* 5, for *August* 6, for *September* 8, for *October* 8, for *November* 10, and for *December* 10. These additional Numbers are called the Numbers of the Months.

26. From what has been said in the two last Articles there naturally follows this Rule for finding the *Age of the Moon* on any Day, of a given Year, *viz.* To the *Epact* for the given Year, add the Day of the Month and Number of the Month, and if the Sum be less than 30 it is the Age of the Moon required; but if it exceed 30 then take 30 from it and the Remainder is the Moon's Age.

*Example.* Required the Moon's Age on the 13th Day of May 1733.

*First,* By Art. 24. I find the *Epact* for that Year to be 25 to which adding 13 the Day of the given Month and 3 the Number of it, the Sum is 41; from which taking 30 there remains 11, the Moon's Age on the given Day.

27. Since the Moon takes 30 Days from one Conjunction with the Sun to the next following, 'tis plain she must be 15 Days old when Full, and  $7\frac{1}{2}$  when in the first Quarter; and  $22\frac{1}{2}$  Days old when in the last Quarter. Consequently to find in any Month of a given Year the Day of the Moon's Change, and when Full, and when in either Quarter, we have this Rule, *viz.* Assume any Day of that Month at Pleasure, and by the last Art. find the Age of the Moon on that Day; then if it be 15 the Moon will be Full that Day, and counting  $7\frac{1}{2}$  Days backwards and forwards from that Day, we'll have the Times of the first and last Quarters, and by counting backwards and forwards from it, 15 Days we'll have the Times of the last and next Change. But if the Age of the Moon be greater than 15, then take 15 from it and the Remainder will show how many Days have run since last Full Moon. So counting those backwards we'll have the Day the last Full Moon happen'd on; and by knowing that, we can find the Days of the Change and either Quarter as before. Again, if the Age of the Moon on the assumed Day be less than 15, then

then take that from 15, and the Remainder will show how many Days are to run till the next Full Moon; and therefore counting so many forwards, we will have the Day of the Full Moon, by which we may find the Days of the Change, and either Quarter as above.

*Example.* Required the Times of Full Moon, New Moon, and first and last Quarters in October 1734.

First, I assume any Day at Pleasure, suppose the tenth of that Month; then by the last Art. I find the Moon's Age on that Day to be 24 Days, from which taking 15 there remains 9, the Number of Days since the last Full Moon; therefore counting so many Days backwards, I find the Full Moon happens on the first Day of that Month, and counting  $7\frac{1}{2}$  Days forwards from that I find that the last Quarter happens on the ninth Day; then from the first Day, on which the Full Moon happens, counting 15 Days forwards, I find that the Change falls on the 16 Day, and reckoning  $7\frac{1}{2}$  Days forward from that, I find that the first Quarter falls on the twenty fourth Day.

28. When the Moon is in Conjunction with the Sun, then they both come to the Meridian at the same Time; but the Moon moving still Easterly with a Velocity much greater than that of the Sun, 'tis evident that when the Sun comes on the Meridian the next Day, the Moon will be on the East Side of it, and consequently cannot be upon the Meridian till some time after the Sun; and because she completes her Revolution in 30 Days, therefore in that Time, the Difference of Time between the Sun and Moon's being on the Meridian will run thro' the whole 24 Hours: and hence by observing any Day how long Time the Moon takes to be upon the Meridian after the Sun, we may by this find the Age of the Moon that Day, making the following Proportion, viz. As 24 Hours, the whole Difference

Difference of Time, is to 30 Days, the whole Number of Days from Change to Change, so is the observed Difference of Time on any Day, to the Days Run since the last Change, or the Age of the Moon at that Time.

*Example.* Suppose on any Day the Moon is observed to be upon the Meridian 5 Hours after the Sun; Required the Age of the Moon at that Time. Make it, as 24 is to 30, so is 5 to  $6\frac{1}{2}$ ; consequently the Moon is  $6\frac{1}{2}$  Days old at the Time of Observation.

29. The Moon moving round her Orbit, or 360 Degrees, in 30 Days, she must move 12 Degrees in 1 Day; but since her Motion is from West to East, and an Heavenly Body, 15 Degrees to the Eastward of another being 1 Hour later of Coming to the Meridian than that other; therefore making it as 15 Degrees is to 1 Hour, so is 12 Degrees to  $\frac{1}{4}$  of an Hour, or 48 Minutes; we find that the Moon is always 48 Minutes later of Coming to the Meridian any Day, than she was the Day before; and because she comes on the Meridian at the same Time with the Sun on the Day of her Change; therefore to find her Southing, or Time of her Coming on the Meridian, any Day, we must first find her Age (by Art. 26.) for that Day, then this multiplied by 48, will give the Minutes of Difference of Time between the Sun and Moon's Coming on the Meridian; which divided by 60, will shew how many Hours and Minutes the Moon is later of Coming on the Meridian than the Sun; and counting so many forwards from twelve of the Day, we have the Time of the Moon's Southing. If the Hours and Minutes found as above be less than 12, then that will be the Time of the Moon's Southing after Noon; but if greater than 12, then take 12 from them, and the Remainder will be the Time of the Moon's Southing in the Morning.

*Example.* Required the Time of the Moon's Southing on the 12th of October 1732.

*First,* (By Art. 26.) I find the Age of the Moon that Day to be 4 Days, which multiplied by 48 gives 192 Minutes, for the Difference of Time between the Sun and Moon's Coming to the Meridian that Day; and this divided by 60 gives 3 Hours and 12 Minutes; which being less than 12 Hours, is the Time of the Moon's Southing after Noon.

*Example 2.* Required the Time of the Moon's Southing the 21st Day of May 1733.

*First,* (By Art. 26.) I find the Moon's Age that Day to be 19 Days, which multiplied by 48 gives 912 Minutes, the Difference of Time between the Sun and Moon's being on the Meridian that Day, and this reduced makes 15 Hours and 12 Minutes; from which taking 12, there remains 3 Hours 12 Minutes, which shews that on the 22d of May 1733. the Moon comes on the Meridian at 12 Minutes past 3 in the Morning.

30. It was said at Art. 20. of this, that the first Year of the *Solar Cycle* was *Leap-Year*; consequently the fifth must be *Leap-Year*, and the ninth must also be *Leap-Year*; but the *Christian Era* commencing on the tenth Year of the *Solar Cycle*, therefore the first Year of that was the first after *Leap-Year*, and the fourth was *Leap-Year*, also the eighth, twelfth, sixteenth, &c, were *Leap-Years*; whence to find whether any proposed Year of the *Christian Era* be *Leap-Year*, or how many it is past the last *Leap-Year*; we must divide the proposed Year by 4, and if nothing remain, then the proposed Year is *Leap-Year*; but if any thing remain, that will show how many Years have past since last *Leap-Year*.

*Example.* Requir'd whether the Year 1730 be *Leap-Year*, or how many since last *Leap-Year*:

I divide the proposed Year 1730. by 4, and there remains 2, so I conclude that the Year 1730 is the second after *Leap Year*.

31. It has been shewn at Art. 17, of this, that to every Day of the Year there is annexed one of the first seven Letters of the Alphabet, beginning with A, which is always annexed to the first of *January*, and in any common Year, the Letter annexed to the first Sunday of *January* is called the *Dominical Letter* for that Year; but each *Leap Year* having two *Dominical Letters* (by Art. 19.) the first of which serves from the Beginning of the Year to the twenty fourth or twenty fifth of *February*, and the other for the rest of the Year; consequently the *Dominical Letter* for any common Year, will shew what Day of *January* the first Sunday of that Year happens upon, reckoning from A (which is annexed to the first of *January*) according to the natural Order of the Letters, and in any *Leap-Year* the first of it's two *Dominical Letters* will shew what Day of *Jan.* the first Sunday of that Year falls on, counting from A, as above; thus in the Year 1730, the *Dominical Letter* is D, so counting from A, viz. making A one, B two, C three, and D four, I find that the first Sunday of that Year falls on the fourth Day of *January*; and by knowing what Day of *January* the first Sunday of any Year falls on, we may know what Day of the Week the first Day of that Year falls upon, by counting so many Days back from Sunday; thus, since in the Year 1730, the first Sunday falls upon the fourth of *January*; therefore the third will be Saturday, the second Friday, and the first Thursday; consequently the Year 1730, begins upon Thursday. From what has been said there ariseth the following Rule for finding what Day of the Week any Day of a given Year falls upon, viz. Find the Day of the Week answering to the first of *January* that

Year; then add together the Days contained in each Month from the Beginning of the Year to the Month in which the proposed Day is, and to this add the Day of the given Month: Lastly, divide this Sum by 7, and if nothing remain, then the Day of the Week, preceding that Day which answers to the first of January that Year, is the Day answering to the proposed Day; but if anything remain, then counting so many forward (beginning with that Day the first of January falls on) we shall have the Day of the Week, the proposed Day falls upon. Note, The Days contained in each Month, are as follow, viz. January 31, February 28 in common Years, and 29 in Leap-Years, March 31, April 30, May 31, June 30, July 31, August 31, September 30, October 31, November 30, December 31.

*Example.* Required what Day of the Week the eighth of July 1730 falls upon.

*First,* By the preceding Rule in this Article, I find that the first of January 1730, falls upon a Thursday; then to the Numbers, 31, 28, 31, 30, 31, 30, answering to the elapsed Months, I add 8 the Day of the given Month, and the Sum 189 divided by 7, there remains nothing, so I conclude that the 8th of July 1730 falls upon a Wednesday.

*Example 2.* Required what Day of the Week the twenty first of March 1730 falls upon.

By proceeding as in the last Example, I find after Division that 3 remain, and the Year beginning upon a Thursday, therefore counting Thursday 1, Friday 2, and Saturday 3, I find that the proposed Day falls upon Saturday.

• 32. According to the Decree of the Nicene Council (which is followed by the Church of England) the Sunday after the fourteenth Day of that Moon which happens after the twenty first of March inclusively, i. e. after the Commencement of the

twenty first of March, is *Easter Sunday*. And since the fourteenth Day of that Moon, or the *Paschal Full-Moon* can never happen before the twenty first of March, nor after the eighteenth of April; therefore *Easter Day* can never happen sooner than the twenty second of March, nor later than the twenty fifth of April. Now to find what Day of March or April, *Easter Day* falls upon in any Year, we have from the foregoing *Articles*, the following Rule, viz. First, (by Art. 26.) find the Age of the Moon on the twenty first of March that Year, and if it be 14, then by the last *Article* find the Day of the Week answering to it, and the Sunday following is *Easter Day*; but if the Moon's Age on the twenty first of March be not 14, then reckon forward to the Day in which her Age is 14 and by the last *Article*, find the Day of the Week answering to that Day, and reckoning forward to the next Sunday, we shall have the Day required.

*Example.* Required when *Easter-Day* happens in the Year 1730.

First, I find (by Art. 26.) that the Age of the Moon on the twenty first of March 1730, is 13; consequently counting 1 forward, I find that the 14 Days of the Moon, or the *Paschal Full-Moon*, happens on the twenty second Day of March; then (by Art. 31.) I find that the twenty second of March 1730, is *Sunday*; therefore counting forwards to the next Sunday, which is *Easter Day*, I find it happens on the twenty ninth of March. Note, In *Leap-Years*, instead of the twenty first of March you must use the twentieth; because in these Years *February* is increased by one Day.

33. From the *Cycles* of the Sun and Moon (explained in Art. 18. and 21.) multiplied into one another, there arises another *Cycle* of 532 Years, called the *Victorian or Dionysian Cycle*, from Dionysius

sus it's Author; after the completing of which not only the *New-Moons* and *Full-Moons* return to the same Day of the Month nearly; but likewise the Days of every Month return to the same Days of the Week; and consequently the *Dominical Letters*, and all the *Moveable Feasts*, return in the same Order: whence this *Cycle* is called the *Great Paschal Cycle*. Now, because the *Christian Era* commenced on the 457th Year of the *Cycle*; therefore to find the Year of the *Dionysian Period* for any Year of the *Christian Era*, we have the following Rule, viz. To the current Year of the *Christian Era*, add 458, and divide the Sum by 532; then the Quotient will shew how many *Periods* have past since the Beginning of that in which the *Christian Era* commenced, and the Remainder will shew the Year of the *Dionysian Period*, answering to the given Year.

*Example.* Required the Year of the *Dionysian Period*, for the Year of *Christ* 1733.

First, I add to 1733 the Number 457, and the Sum is 2190; then I divide this by 532, and the Quotient is 4, and Remainder 62; consequently there has past 4 *Dionysian Periods* since the Beginning of that in which the *Christian Era* commenced, and the given Year is the 62d of the Current *Cycle*.

34. Besides the *Cycles* of the *Sun* and *Moon* there is another *Cycle* consisting of 15 Years, called the *Cycle of Indiction*, which hath no Connection with the Celestial Motions, and which was made use of by the *Romans* for some *Civil Purposes*, and is still used by the *Popes of Rome* in their *Bulls* and *Diploma's*. The Year before the Birth of CHRIST was the third Year of this *Cycle*; and consequently to find the Year of *Indiction* for any Year in the *Christian Era*, we have this Rule, viz. to the given Year, add 3, and divide the Sum by

by 15, then if there be no Remainder, the given Year is the fifteenth of the Indiction; but if there be any Remainder that will shew what Year of the Indiction the given Year is; and the Quotient will shew how many complete Cycles of Indiction have past since the first Year of that in which the Christian Era commenced.

Example, Required the Year of Indiction, for the Year 1733 of the Christian Era.

First, I add 3 to the given Year, and the Sum is 1736; then I divide this Sum by 15, and the Quotient is 115, and Remainder 11. Consequently there has been 115 complete Cycles of Indiction from the first Year of that in which the Christian Era commenced, and the Year 1733, is the 11th Year of Indiction.

35. From the Multiplication of the three Cycles, viz. the Solar of 28 Years, the Lunar of 19, and that of Indiction of 15; arises a Period of 7980 Years, called the Great Julian Period. This is supposed to have begun 764 Years before the Creation of the World, and is not yet completed; consequently it must comprehend all the Actions that have happened from the Beginning of the World; and since the Year before Christ was the 4713th Year of this Period, therefore to find what Year of the Julian Period any current Year is, we must to the given Year of Christ, add 4713, and the Sum will be the required Year of the Julian Period.

Example, Required what Year of the Julian Period answers to the current Year of Christ 1734.

To the given Year 1734, I add 4713, and the Sum 6447, shews that the current Year of Christ 1734 is the 6447th Year of the Julian Period.

36. As in the Heavens, there are certain Points from which Astronomers begin their Computations; so likewise there are certain Points of Time, from which, as Roots Chronological Computations begin; and

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and all memorable Actions are recorded by *Historians* according to the Series of Years following these Roots, or fixed Points of Time which are called *Epocha's* or *Aera's*. The most celebrated and best known to us, is the *Christian Era*, which commenced on the first of *January*, immediately following the Birth of *Christ*.

37. The most Ancient *Epocha*, is that of the Creation of the World ; which commenced 3050 Years before *Christ*. The next to this is that of the *Deluge*, which began 2956 Years before *Christ*. Then follows the *Epocha of the Olympiads*, which was the most antient and famous *Epocha* among the *Greeks*, and other *Eastern Nations* ; each *Olympiad* contained 4 Years, and they had their Rise from certain Games that were celebrated by the *Grecians* every fourth Year ; in Honour of *Jupiter Olympius*, which were called *Olympic Games*. The Beginning of this *Epocha*, is supposed to have been on the 777th Year before *Christ*, and in the 3931th Year of the *Julian Period*. The next *Epocha*, is that of the Building of *Rome*, which began about the End of the third Year of the Sixth *Olympiad*, 764 Years before *Christ*, and in the 3959th Year of the *Julian Period*. Then follows the *Era of Nabonassar King of Babylon*, from the Beginning of whose Reign it commenced. This *Era* is famous among *Astronomers*, being made use of by *Ptolomy*, *Albategnus*, &c. as a proper *Era* for computing the Motions of the Celestial Bodies from. It began according to *Ptolomy*, on the fourth of the *Kalends of March*, 747 Years before *Christ*, in the 3966th Year of the *Julian Period*, and in the seventh Year after the Building of *Rome*, and in the second Year of the eighth *Olympiad*. The next is the *Epocha of Alexander the Great*, which commenced at his Death ; and this happened about the middle of the Spring,

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in the first Year of the 114th Olympiad, 324 Years before Christ, in the 4390th Year of the Julian Period, and in the 424th Year of the Æra of Nabonassar. There are several other Epochas besides these already mentioned of less Note, which I shall pass over, it not being the Design here to give a particular Description of all the Epochas and their several Uses, but only to give a general Account of the most remarkable among them.

38. Since by the Rotation of the Earth about its Axis, the Moon appears to move quite round from East to West in 24 Hours, therefore in that Time she must pass over all the Points in the Compass, and so must move from one Point to the next succeeding in 45 Minutes. Consequently in moving from the North Point to the South, she must take 12 Hours, and from the North, to the N E, or from the South to the S W 45 Minutes; also from the North to the N N E, or from the South to S S W; 1 Hour 30 Minutes; and so on as in the following Table.

Points	H: , , M.	Points
N	12 , , 00	S
N b E	0 , , 45	S b W
N N E	1 , , 30	S S W
N E b N	2 , , 15	S W b S
N E	3 , , 00	S W
N E b E	3 , , 45	S W b W
E N E	4 , , 30	W S W
E b N	5 , , 15	W b S
E	6 , , 00	W
E b S	6 , , 45	W b N
E S E	7 , , 30	W N W
S E b E	8 , , 15	N W b W
S E	9 , , 00	N W
S E b S	9 , , 45	N W b N
S S E	10 , , 30	NN W
S b E	11 , , 15	N b W

39. The Flux and Reflux, or Ebbing and Flowing of the Seas, does constantly respect the Motion of the Moon, and in every Place when the Moon is on a certain Point of the Compass, or at a certain Distance from the Meridian, it is then high Water at that Place; and since the Moon is twice at the same Distance from the Meridian, or in two opposite Points of the Compass, in her diurnal Motion; therefore in most Places there is a double Ebbing and Flowing in a little more than 24 Hours. There has been found by Observation, for the most remarkable Coasts, the Points upon which the Moon is when it is high Water in each of them; as in the following Table.

*A TABLE of the most remarkable Sea-Coasts, in an Alphabetical Order; shewing in each of them the Points of the COMPASS, the MOON must be on, when it is high Water.*

**A.**

At Abarwark, ENE and WSW.

At Abermerick and Antwerp, E and W.

At Alborough, SE and S, and NW and N.

At Amsterdam and Armenties, NE and SW.

At Army, NNE, and SSW.

**B.**

At Beachy and Blacktail, and before the Race of Blanquet, N and S.

At Blackness in Bluet, at Bell Isle, NNE, and SSW.

Without Bluet, and at Berwick, NEE and SW and S.

At the River Bourdeax, the South Coast of Britaigne, the Coast of Biscay, and at Bookness, N E, and SW.

At Brest, before the Bass, the River of Bourdeaux within the Haven, NE and SW and SSW.

In the Breefound, Bloy, and Baltimore, ENE, and WSW.

Before Bremen, and at Blackney, and in the Channel before Bourdeaux, E and W.

At Bridgewater, ESE, and WNW.

At Bristol Key, Eb S, and W and N.

At Buller deep, SSE, and NNW.

**C.**

Before the Haven of Caen, in the Chamber, between Cripplesand and the

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the Creyl, and at Oulhof, S E, and N b W.

At Caldy, and in the Bay of Carmarthen, E b N, and W. b S.

Without Calais, at Corpus Christi Point, before and at Camfer, N NE, and S S W.

Between Calais and Dover, before Conquer, and at the N. Cape, S. GV.

At the Caskets, and at Chamberness, S E b S, and N W b N.

Between Guernsey and the Caskets, before Cromer, before the Caskets at Guernsey, at Seven Sifts, and at Caskets, S E, and N W.

In the Chamber of 1, and S b W.

Without the Caskets in the Channel, S E b E, and N W b W.

At Concale E and W.

In Condado N and S.

At Cork, Calais, Cape Clear, and in the Creek, E N E, and W S W.

At Cows in the Foss of Caen, in Calais Road, and in Chamberness Road, S S E, and N N W.

## D.

At Dartmouth, E and W.

At Diep, Dover, and in the Downs, S S E, and N N W.

At Dover Pier, and before Dunkirk, N and S.

At Denbigh and Downs, in the Road, N E b N, and S W b S.

At Dublin, S S E, and N N W.

At Dunbar, S E, and N W.

At Dungeness and Dymose, S E b S, and N W b N.

At Dungenfan, E N E, and W S W.

## E.

At Edam N N E, and S S W.

At Emden, before the Elve, before the Eyder, and before Erichsins, N and S.

Before the Eastern and Western Emes, and Engemonts, S E and N W.

## F.

In the Fair Isle Roads, and at the North Foreland, S b E, and N b W.

At the Frith, and at the S. Foreland, S S E, and N N W.

Before the Fen, in the Channel, N N E, and S S W.

At Flamborough and Bradlington, E, and S W.

On the Coast of Flanders, N and S.

Without the Banks of Flanders, N E, and S W.

At Flushing, N b E, and S b W.

On the Coast of Flanders, N and S.

At the Form, is Foy, at Falmouth, E b N, and W b S.

Without the Fly, S E b E, and N W b W.

Before the Coast of Friesland, and the Fly, E S E, and W N W.

Between Foy and Falmouth, in the in the Channel, and at Fonteufs, E b S, W b N.

At Frize, and the Fair Isle, N W, and S E.

## G.

In the Road of Gibraltar, at Graveling, and before Cherburgh, N and S.

Before Goree, at Guernsey, and at Gravesend, N N E, and S S W.

At Groin, at Gascoign, and the Coast of Galicia, N E, and S W.

Thwart of Guernsey, in the Channel, S E b S, and N W b N.

## H.

Before Humbergh, at Hull, at the Holms, and before Humber's Mouth, E and W.

At Hampton Key, before the Hever, before Horn, N and S.

At Harlem, Havre de Grate, and Homehead, S E and N W.

Before Hartlepool, N E, and S W.

At St. Helen's, at Harwich, and without the Banks of Harwick, S S E, and N N W.

At Humber, E b N, and W b S.

Under Holy Island, and at Horn, N N E, and S S W.

At Headcliff-Foot, N E b E, and S W b S.

## I.

In all the Havens on the S. Coasts of Ireland, E b N, and W b S.

On the W. Coasts of Ireland, N E, and S W.

At Jutland Islands, N and S.

At

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## K.

- At Kelliers, N E, and S W.
- At Kentish Knock, N and S.
- At Kildnyn, E S E, and W N W.
- At Kildrive, S E, and N W.
- At Kingfale, E N E, and W S W.

At Lambay, S E b S, and N W b W.

- At Leith, N and S.
- At Lynn, E b S, and W b N.
- At Lisbon, N L b N, and S W b S.
- At the Lizard, by the Land, E S E, and W N W.
- At Leoſtoff, and thwart of it without the Banks, S E b S, and N W b N.

- In Leoſtoff Road, and Longſand Head, S S E, and N N W.
- At London, N E, and S W.
- At Londey, E and W.
- Thwart of Londey, and before Lynn, E b N, and W b S.

## M.

- Within the Maes, at Malden, N b E, and S b W.
- Before the Maes, and before St. Matthew's Point, N E b E, and S W b W.
- In St. Magnes Sound, and at the Magnes Castle, S E b E, and N W b W.

- At the Isle of Man, S E, and N W.
- Before Margate, S b E, and N b W.
- In Milford, at Moonleſs, at St. Mattoes, E b N, and W b S.
- Between Monſhole and Falmoſth, and in Milford Haven, E S E, and W N W.

- In Monſhole, at St. Matthews, and within Mounts Bay, E N E and W S W.

## N.

- Between the Naxe, and Warhead of Lower, S b E, and N b W.
- Before the River of Nants, N E, and S W.
- At the Needles, at the Isle of White, S E b E, and N W b W.

- A. Newcastle, E b N, and W b S.
- At Newport, half Tide, N and S.
- At the West End of the Nore, N b E, and S b W.
- Before St. Nicholas, E b S, and W b N.
- All the Coast of Normandy, and Picardy, S S E, and N N W.

## O.

- At Orfordness, S E b S, and N W b N.
- At Orfordness, without the Banks, and between Orford and Orwell-Waves, S S E, and N N W.
- Orkney, within the Sands, S S E, and N b W.
- At Orkney, N E, and S W.
- At Orkney, S E, and N W.

## P.

- At St. Paul's in the Haven, E and W.
- At the Pens, Porthus, and Poſthu, N E, and S W.
- In Plymouth, and before St. Paul's, E b N, and W b S.
- Thwart of Plymouth, E S E, and W N W.
- Before Podeſſemeck, E b S, and W b N.
- At the Race of Portland, S E, and N W.
- At Portſmouth, half Tide, N and S.

## Q.

- At Queenborough, N and S.

## S

- In the Steve, between Uſham and Scilly, at the Shooe, at the Spit, at Southampton, and all along the Swin, N and S.
- Upon the Coast of Spain, and in Shetland, N E and S W.
- At Seilly, in the Sound, Scarburgh, and at Staples, N E b E, and S W b W.
- At Seven Isles, without the Haven, in the Broad Sound, E N E, and W S W.
- At the Mouth of Severn, between Scilly and the Lizard, at the Spnm and Stockton, E b N, and W b S.
- Without

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Without Scilly, in the Channel, and  
Salcombe, E and W.

At Sedmouth, and at the Start, E b S,  
and W b N.

Off the Start in the Channel, E S E,  
and W N W.

Within the Seyn, and before She  
bergh, and at Seven Clifts, S E, and  
N V.

At Shoram, S E b S, and N V S.

A Seyn Head, S E, and N L W.

## T.

Within Terven, N & E, and S b W.  
Before Terven, before the River  
of Thames, and at Taverne, NNE,  
and SSW.

Before the Trees, and Tinmonthe,  
before the Bay of Tinmouth, N E, and  
S W.

At the Clifts of the Texel, ENE,  
and W SW.

In Torbay, and before the Texel, E  
and W.

In the Road of the Texel, E S E,  
and W N W.

At Torgon, S E b S, and N W b N.

## U.

Before Urek, N and S.  
At Use, NE, and S W.  
Between Ushant, and the Main,  
N E b S, and S W b W.  
St. Vallery, S S E, and N N W.

## W.

At Winchelsea, Nb E, and S b W.

At the Weilings, and from the W.  
End of the Wight, N N E, and S S W.

Before the Weilings, N E b N, and  
S W b S.

At Whitby, NE, and S W.

In the Sea of Wales, and Severn,  
E N E, and W S W.

In Wales, E / N, and W b S.

At Wells, at Weymouth, and at Wa-  
terford, E and W.

At Weymouth Key, E b S, and W b N.

At the Ness, by Wieringhen, at Wits-  
terton, E S E, and W N W.

Thwart the Isle of Wight, in the  
Channel, all within the Isle of Wight,  
between the Isle of Wight, and Beachy,  
by the Shore, S E b E, and N W b W.

At the East End of Wight, and on  
Wierington Flats, S E, and N W.

## Y.

Before Yarmouth, N N E, and S S W.

At Tonghall, E N E, and W S W.

At Yarmouth, S E b E, and N W b  
W.

In Yarmouth Road, in Yarmouth Ha-  
ven, S S E, and N N W.

## Z.

On the Coast of Zealand, N N E,  
and S S W.

In the Zierick Sea, N E, and S W.

40. By knowing the Point of the Compass, the  
Moon is on when it is high Water at any Place,  
we know by Art. 38. the Time she takes to move  
from the Meridian to that Point; and since we can  
find by Art. 29. the Time of the Moon's coming on  
the Meridian any Day; therefore to find the Time  
of high Water at any Place, and on any Day, we  
have this Rule, viz. To the Hours and Minutes  
of the Moon's Southing (found by Art. 29.) add the  
Hours and Minutes answering to the Point of flow-  
ing

ing (found from the Table of Art. 38.) the Sum is the Time of full Sea requir'd; counting from Noon or Midnight.

*Example.* Requir'd the Time of High Water at Bristol Key, on the tenth of May 1731.

First, By Art. 29; I find the Moon comes on the Meridian that Day, 48 Minutes past 2 at Night, then because by the Table in the last Article the Moon must be on the E b S, or W b S Point of the Compass before it be high Water at Bristol; and since by the Table of Art. 28. it takes 6 Hours, 45 Minutes, in moving from the Meridian to either of these Points; therefore to the 48 Minutes before found, I add 6 Hours, 45 Minutes and the Sum is 7 Hours, 33 Minutes in the Morning, the Time of full Sea at Bristol, for the Day proposed, which is also the Time at Night, when it is full Sea again, that Day.



S E C T. VI.

*Concerning the LOG-LINE and COMPASS.*

1. THE Method commonly made use of for measuring the Ship's Way at Sea, or how far the runs in a given Space of Time, is by the *Log-Line*, and *Half-Minute Glass*.

2. The *Log* is a flat Piece of Wood, in Shape like a Flounder, having a Piece of Lead fasten'd to its Bottom, which makes it stand or swim upright in the Water; to this *Log* is tied or fastned a long Line, which is called the *Log-Line*; and this is commonly divided into certain Spaces, each of which is, or ought to be, such proportional Part of a nautical Mile (60 of which make a Degree of a great Circle on the Earth) as half a Minute (the Time allow'd for the Experiment) is of an Hour.

3. These Spaces are called *Knots*, because at the End of each of them, there is a Piece of Twine with *Knots* in it, interwoven between the Strands of the *Line*, which shews how many of these Spaces or *Knots* are run out during the half Minute. They commonly commence or begin to be counted, at the Distance of about 10 Fathom, or 60 Feet from the *Log*; that so the *Log*, when it is hove over Board, may be out of the *Eddy* of the Ship's *Wake* before

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before they begin to count, and for the more ready Discovery of this Point of Commencement, there is commonly fastned at it a Piece of red Rag.

4. The *Log* being thus prepar'd, and heve over Board from the *Poop*, and the Line veer'd out (by the Help of a Reel, that turns easily, and about which it is wound) as fast as the *Log* will carry it away, or rather as the Ship fails from it, it will shew according to the Time of Veering, how far the Ship has run in a given Time; and consequently her Rate of Sailing.

5. A Degree of a *Meridian*, which is a great Circle on the Earth, according to the exactest Measures, contains about 69.545 English Miles; and each Mile, by the Statute being 5280 Feet, therefore a Degree of a *Meridian* will be about 367200 Feet; whence the  $\frac{1}{60}$  of that, viz. a Minute, or nautical Mile, must contain 6120 standard Feet; consequently since  $\frac{1}{60}$  Minute is the  $\frac{1}{240}$  Part of an Hour, and each *Knot* being the same Part of a nautical Mile (by Art. 2.) It follows, that each *Knot* will contain the  $\frac{1}{20}$  Part of 6120 Feet, viz. 51 Feet.

6. Hence it is evident, that whatever Number of *Knots* the Ship runs in half a Minute, the same Number of Miles she will run in one Hour; supposing her to run with the same Degree of Velocity during that Time, and therefore it is the general Way to heave the *Log* every Hour, to know her Rate of Sailing; but if the Force or Direction of the Wind vary, and not continue the same during the whole Hour, or if there has been more Sail set, or any Sail handed, that so the Ship has run swifter or slower in any Part of the Hour, than she did at the Time of heaving the *Log*; then there must be Allowance made accordingly for it, and this must be according to the Discretion of the Artist.

7. Sometimes when the Ship is before the Wind, and there is a great Sea setting after her, it will bring home the Log, and consequently the Ship will sail faster than is given by the Log. In this Case it is usual, if there be a very great Sea, to allow one Mil in ten, and less in Proportion, if the Sea be not so great. But for the Generality, the Ship's Way is really greater than that given by the Log; and therefore in Order to have the Reckoning rather before than behind the Ship, (which is the rarest Way) it will be proper to make the Space of the Log-Line between Knot and Knot, to consist of 50 Feet instead of 51. Some, upon the Supposition that 60 Miles make a a Degree on the Meridian, make the Distance between Knot and Knot 42 Feet; when at the same Time, by common Experience they are oblig'd to lessen the Half-Minute-Glass by near 6 Seconds, making it to run only 24 Minutes nearly; which plainly is correcting one Mistake by another.

8. If the Space between Knot and Knot on the Log-Line should happen to be too great in Proportion to the Half-Minute-Glass, viz. greater than 50 Feet; then the Distance given by the Log, will be too short, and if that Space be too small, then the Distance run (given by the Log) will be too great; therefore to find the true Distance run in either Case, having measured the Distance between Knot and Knot, we have the following Proportion, viz.

As the true Distance 50 Feet, is to the measured Distance, so is the Miles of Distance given by the Log, to the true Distance in Miles that the Ship has run.

Example 1. Suppose a Ship runs at the Rate of 6 $\frac{1}{2}$  Knots in half a Minute, but measuring the Space between Knot and Knot, I find it to be 56 Feet; Required the true Distance in Miles.

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Making it as 50 Feet is to 56 Feet, so is 6.25 Knots to 7 Knots; I find that the true Rate of sailing is 7 Miles in the Hour.

*Example 2.* Suppose a Ship runs at the Rate of 6½ Knots in half a Minute, but measuring the Space between Knot and Knot, I find it to be only 44 Feet: Required the true Rate of sailing.

Making it as 50 Feet, is to 44 Feet, so is 6.5 Knots, to 5.72 Knots; I find that the true Rate of Sailing is 5.72 Miles in the Hour.

9. Again, supposing the Distance between Knot and Knot on the Log-Line to be exactly 50 Feet, but that the Glass is not 30 Seconds; then if the Glass require longer Time to run than 30 Seconds, the Distance given will be too great, if estimated by allowing 1 Mile for every Knot run, in the Time the Glass runs; and on the Contrary, if the Glass, require less Time to run than 30 Seconds, it will give the Distance sail'd too small. Consequently to find the true Distance in either Case, we must measure the Time the Glass requires to run out (by the Method in the following Article) then we have the following Proportion, *viz.*

As the Number of Seconds the Glass runs, is to half a Minute, or 30 Seconds, so is the Distance given by the Log, to the true Distance.

*Example 1.* Suppose a Ship runs at the Rate of 7½ Knots in the Time the Glass runs, but measuring the Glass, I find it runs 34 Seconds: Required the true Distance sail'd.

Making it as 34 Seconds is to 30 Seconds, so is 7.5, to 6.6; I find that the Ship sails at the Rate of 6.6 Miles an Hour.

*Example 2.* Suppose a Ship runs at the Rate of 6½ Knots, but measuring the Glass, I find it runs only 25 Seconds: Required the true Rate of Sailing.

Making it as 25 Seconds, is to 30 Seconds, so is 6.5 Knots, to 7.8 Knots; I find that the true Rate of Sailing is 7.8 Miles an Hour.

10. In Order to know how many Seconds the Glass runs, you may try it by a Watch or Clock, that vibrates ~~Seconds~~ <sup>1</sup> seconds; but if neither of these be at Hand, then take a Line, and to the one End fastening a Plummets, hang the other upon a Nail or Peg, sc. as the Distance from the Peg to the Center of the Plummets be  $39\frac{1}{2}$  Inches: Then this put into Motion will vibrate Seconds, i. e. every Time it passes the Perpendicular you are to count one Second; consequently by observing the Number of Vibrations that it makes during the Time the Glass is running, we know how many Seconds the Glass runs.

11. If there be an Error both in the Log-Line and Half-Minute-Glass, viz. if the Distance between Knot and Knot on the Log-Line, be either greater or less than 50 Feet, and the Glass runs either more or less than 30 Seconds, then the finding of the Ship's true Distance will be somewhat more complicate, and admit of three Cases, viz.

*Case 1.* If the Glass runs more than 30 Seconds, and the Distance between Knot and Knot be less than 50 Feet, then the Distance given by the Log-Line, viz. by allowing 1 Mile for each Knot the Ship sails while the Glass is running, will always be greater than the true Distance; since either of these Errors give the Distance too great. Consequently to find the true Rate of Sailing in this Case, we must first find (by Art. 8.) the Distance, on the Supposition that the Log-Line is only wrong, and then with this (by Art. 9.) we shall find the true Distance.

*Example.* Suppose a Ship is found to run at the Rate of 6 Knots; but examining the Glass, I find it runs 35 Seconds, and measuring the Log-Line, I

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find the Distance between Knot and Knot to be but 46 Feet: Required the true Distance run.

First, By Art. 8. we have the following Proportion, viz. As 50 Feet : 46 Feet :: 6 Knots : 5.52 Knots. Then by Art. 9. As 35 Seconds : 30 Seconds :: 5.52 Knots : 4.73 Knots. Consequently the true Rate of Sailing is 4.73 Miles an Hour.

Case 2. If the Glass be less than 30 Seconds, and the Space between Knot and Knot be more than 50 Feet; then the Distance given by the Log, will always be less than the true Distance, since either of these Errors lessen the true Distance.

Example. Suppose a Ship is found to run at the Rate of 7 Knots, but examining the Glass, I find it runs only 25 Seconds, and measuring the Space between Knot and Knot on the Log-Line, I find it is 54 Feet: Required the true Rate of Sailing.

First, By Art. 9. As 25 Seconds : 30 Seconds :: 7 Knots : 8.4 Knots. Then by Art. 8. As 50 Feet : 54 Feet :: 8.4 Knots : 9.072 Knots. Consequently the true Rate of Sailing is 9.072 Miles an Hour.

Case 3. If the Glass runs more than 30 Seconds, and the Space between Knot and Knot be greater than 50 Feet, or if the Glass runs less than 30 Seconds, and the Space between Knot and Knot be less than 50 Feet; then since in either of these two Cases the Effects of the Errors are contrary, 'tis plain the Distance will sometimes be too great and sometimes too little, according as the greater Quantity of the Error lies; as will be evident from the following Examples.

Example 1. Suppose a Ship is found to run at the Rate of  $9\frac{1}{2}$  Knots per Glass, but examining the Glass, it is found to run 36 Seconds, and by measuring the Space between Knot and Knot, it is found to be 58 Feet: Required the true Rate of Sailing.

First,

First, By Art. 3. As 50 Feet : 58 Feet :: 9.5 Knots : 11.02 Knots. Then by Art. 9. As 38 Seconds : 30 Seconds :: 11.02 Knots : 8.7 Knots. Consequently the Ship's true Rate of Sailing is 8.7 Miles an Hour.

Example 2. Suppose a Ship runs at the Rate of 6 Knots per Glass; but examining the Glass, it is found to run only 20 Seconds, and by measuring the Log-Line, the Distance between Knot and Knot is found to be but 38 Feet: Required the true Rate of Sailing.

First, By Art. 8. As 50 Feet : 38 Feet :: 6 Knots : 4.56 Knots. Then by Art. 9. As 20 Seconds : 30 Seconds :: 4.56 Knots : 6.84 Knots. Consequently the true Rate of Sailing is 6.84 Miles an Hour.

But if in this Case it happen, that the Time the Glass takes to run, be to the Distance between Knot and Knot, as 30, the Seconds in half a Minute, is to 50, the true Distance between Knot and Knot; then 'tis plain, that whatever Number of Seconds the Glass consists of, and whatever Number of Feet is contain'd between Knot and Knot; yet the Distance given by the Log-Line will be the true Distance in Miles.

12. Though the Method of measuring the Ship's Way by the Log-Line, described in the foregoing Articles, be that which is now commonly made use of; yet it is subject to several Errors, and these pretty considerable. For first, the Half-Minute or Quarter-Minute-Glasses (by which, and the Log, the Ship's Way is determin'd) are seldom or never true, because dry and wet Weather have a great Influence on them; so that at one Time they may run more, and at another Time fewer than thirty Seconds, and 'tis evident that a small Error in the Glass, will cause a sensible one in the Ship's Way. Again, the chief Property of the Log is to have it

it swim upright, or perpendicular to the *Horizon*; but this is too often wanting in *Logs*, because few Seamen examine whether it is so or not, and generally take it upon Trust, being satisfied, if it weigh a little more at the Stern than the Head; and from this there flows an Error in the Reckoning, for if the *Log* does not swim upright, it will not hold Water, nor remain steady in the Place where it is heav'd, since the least Check of the Hand, in veering the Line will make it come up several Feet; this repeated will make the Errors become Fathoms, and perhaps Knots, which how insignificant soever they appear, are Miles and Parts of Miles, and amount to a good deal in a long Voyage. Another Inconvenience attending the *Log-Line* is its stretching and shrinking; for when a new Line is first used, let it be ever so well stretched upon the Deck, and measured as true as possible, yet after wetting it shrinks considerably; and consequently to be the better assur'd of the Ship's Way by the *Log-Line*, we ought to measure and alter the Knots on it every Time before we use it; but this is seldom done oftner than once a Week, and sometimes not above once or twice in a whole Voyage; also when the Line is measured to its greatest Degree of shrinking, it is generally left there; and when by much Use, it comes to stretch again it is seldom or never mended, though it will stretch beyond what it first shrunk. These and many other Errors too well known, attending that Method of measuring the Ship's Way by the *Log-line*, plainly answers for a great many Errors committed in Reckonings. So 'tis to be wish'd that either this Method were improved or amended, or that some other Method less subject to Error, were found out. There was a Machine sometime ago invented by Mr. Henry de Saumarez, of the Island of Guernsey, for measuring the Ship's Way, called the

## Of the Log-Line and Compass. 15:

*Marine Surveyor*, which is indeed less subject to Error than the *Log-line*, and was found by several Experiments to answer the End much more exactly than the *Log-line*; a Description of which may be seen in the *Philosophical Transactions* of the Royal Society, Vol. xxxiii. for the Months of November and December 1725; and also in those for the Months of March and April 1726; and for March and April 1729.

13. It was said at Art. 21. Sect. 3 that the Meridian and *Prime Vertical* of any Place cuts the *Horizon* in 4 Points, at 90 Degrees Distance from one another, viz. the *North*, *South*, *East* and *West*; that Part of the Meridian which extends itself from the Place to the *North Point of the Horizon*, is called the *North Line*; that which tends to the *South Point of the Horizon*, is called the *South Line*; and that Part of the *Prime Vertical* which extends towards the Right Hand of the Observer, when his Face is turn'd to the *North*, is called the *East Line*; and lastly, that Part of the *Prime Vertical* which tends towards the Left Hand, is called the *West Line*; the four Points in which these Lines meet the *Horizon*, are called the *Cardinal Points*.

14. In Order to determine the *Course* of the *Winds*, and to discover their various Alterations or Shiftings; each Quadrant of the *Horizon* intercepted between the *Meridian* and *Prime Vertical*, is usually divided into eight equal Parts, and consequently the whole *Horizon* into thirty two; and the Lines drawn from the Place on which the Observer standeth, to the Points of Division in his *Horizon*, are called *Rumb Lines*, the four principal of which are those described in the preceding Article, each of them having its Name from the *Cardinal Point* in the *Horizon* towards which it tends; the rest of the *Rumb-Lines* have their Names compounded of

the

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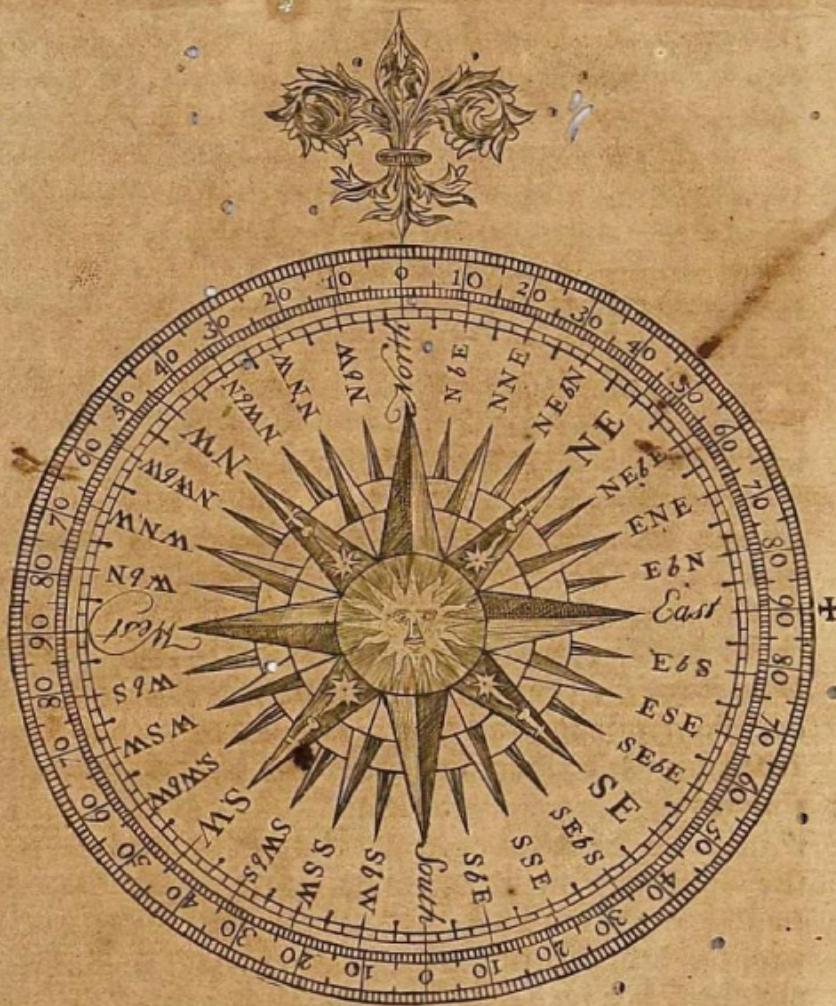
the principal Lines on each Side of them, as in the following Figure ; and over whichsoever of these Lines the Course of the Wind is directed, that Wind takes its Name accordingly.

15. The Instrument commonly used at Sea for directing the Ship's Way, is called the *Mariners Compass*; which consists of a *Chard* and two *Boxes*. The *Chard* is a Circle made to represent the *Horizon*, whose Circumference is quartered and divided into Degrees, and also into thirty two equal Parts, by Lines drawn from the Center to the several Points of Division called *Points of the Compass*. On the Back-side of the *Chard*, and just below the *South* and *North Line*, is fixed a *Steel Needle*, with a *Brass Cupola*, or hollow Center in the Middle, which is plac'd upon the End of a fine *Pin*, upon which the *Chard* may easily turn about; the *Needle* is touch'd with a *Load-Stone*, by which a certain Virtue is infus'd into it, that makes it (and consequently the *South* and *North Line* on the *Chard*, above it) hang nearly in the Plane of the *Meridian*, by which Means the *South* and *North Lines* on the *Chard* produc'd would meet the *Horizon* in the *South* and *North Points*; and consequently all the other Lines on the *Chard* produc'd would meet the *Horizon* in their respective Points.

16. The *Chard* is represented in the annexed Scheme, in which you may observe, that the Capital Letters N, S, E, W, denote the four Cardinal Points, viz. N the *North*, S the *South*, &c. and the small Letter b signifies the Word *by*: the *Rumbs* in the Middle between any two of the Cardinals, are express'd by the Letters denoting those Cardinals, that which denotes the Point lying in the *Meridian* having the Precedence; thus the *Rumb* in the Middle between the *North* and *East* is express'd N E, which is to be read *North-East*; also

# Of the Log Line and Compas. 153

also S W denotes the South-West Rumb, &c. the other Rumbs are express'd according to their Situ-

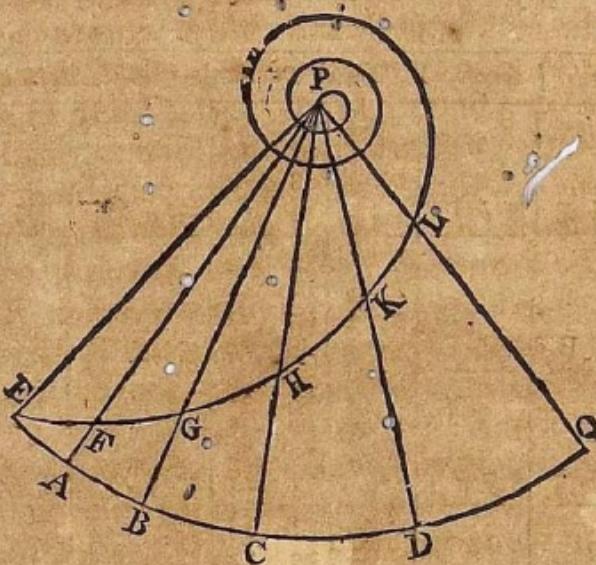


ation with respect to these middle Rumbs, and the nearest Cardinals, as is plain from the prefixed Scheme.

17. The *Card* is put into a round *Box*, made for it, having a Pin erected in the Middle, upon which the hollow Center of the *Needle* is fix'd, so as the *Card* may lie Horizontal, and easily vibrate according to the Motion of the *Needle*; the *Box* is covered over with a smooth Glass, and is hung in a brass Hoop upon two cylindrical Pins, diametrically opposite to one another, and this Hoop is hung within another brass Circle, upon two Pins at right Angles with the former. These two Circles, and the *Box*, are placed in another square wooden *Box*, so that the innermost *Box*, and consequently the *Card*, may keep Horizontal, which way soever the Ship heels.

18. Since the *Meridians* do all meet at the *Poles*, and there form certain Angles with one another; and since if we move never so little towards the *East* or *West*, from one Place to another, we thereby change our *Meridian*, and in every Place the *East* and *West Line* being perpendicular to the *Meridian*; it follows, that the *East* and *West Line* in the first Place, will not coincide with the *East* and *West Line* in the second, but be inclin'd to it, at a certain Angle: and consequently all the other *Rhumb Lines* at each Place, will be inclin'd to each other, they always forming the same Angles with the *Meridian*. Hence it follows that all *Rumbs*, except the four Cardinals, must be *Curves* or *Heliospherical Lines*, always tending towards the *Pole*, and approaching it by infinite Gyrations or Turnings, but never falling into it. Thus let *P* be the *Pole*, *E*. *Q* an Arch of the Equator, *P E*, *P A*, &c. *Meridians*, and *E F G H K L* any *Rumb*; then because the Angles *P E F*, *P F G*, &c. are by Nature of the *Rumb-Line* equal, it is evident that it will form a *Curve-Line* on the Surface of the *Globe*, always approaching the *Pole P*, but never falling into it; for if

for if it were possible for it to fall into the *Pole*; then it would follow, that the same Line could cut



an infinite Number of other Lines at equal Angles, in the same Point; which is absurd.

19. Because there are 32 *Rumbs* (or Points in the *Compass*) equally distant from one another, therefore the Angle contain'd between any two of them adjacent, will be  $11^{\circ}$ ,  $15'$  viz.  $\frac{1}{32}$  Part of  $360^{\circ}$ ; and so the Angle contain'd between the *Meridian*, and the N b E, will be  $11^{\circ}$ ,  $15'$ , and between the *Meridian* and the N N E, will be  $22^{\circ}$ ,  $30'$ , and so of the rest, as in the following Table.

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A Table of the Angles which every Point of the Compass makes with the Meridian.

North.	South.	1 Points.	D. M. 1	North.	1	South.
N b E	S b E	I 1 $\frac{1}{4}$ $\frac{1}{2}$ $\frac{3}{4}$	2 05 08 15	N b W	S b W	
N N E	S S E	I 2 $\frac{1}{4}$ $\frac{1}{2}$ $\frac{3}{4}$	14 16 19 30	NNW	SSW	
N E b N	S E b S	2 3 $\frac{1}{4}$ $\frac{1}{2}$ $\frac{3}{4}$	25 28 30 33	N W b N	S W b S	
N E	S E	4. 4 $\frac{1}{4}$ $\frac{1}{2}$ $\frac{3}{4}$	34 22 11 00	N W	S W	
N E. b E	S E b E	4 5 $\frac{1}{4}$ $\frac{1}{2}$ $\frac{3}{4}$	47 50 53 56 49	N W b W	S W b W	
E N E	E S E	6 6 $\frac{1}{4}$ $\frac{1}{2}$ $\frac{3}{4}$	67 70 73 75 30	W N W	W S W	
E b N	E b S	7 7 $\frac{1}{4}$ $\frac{1}{2}$ $\frac{3}{4}$	78 81 84 87 45	W b N	W b S	
East		8	90 00	West		

# Of Plane Sailing.

## S E C T. VII.

### Of Plane Sailing.

1. THIS Method of Sailing supposes the Earth to be a *Plane*, and the *Meridians* parallel to one another; and likewise the *Parallels of Latitude* at equal Distance from one another, as they really are upon the *Globe*. Tho' this Method be in it self evidently *false*; yet in a short Run, and especially near the *Equator*, an Account of the Ship's Way, may be kept by it tolerably well.

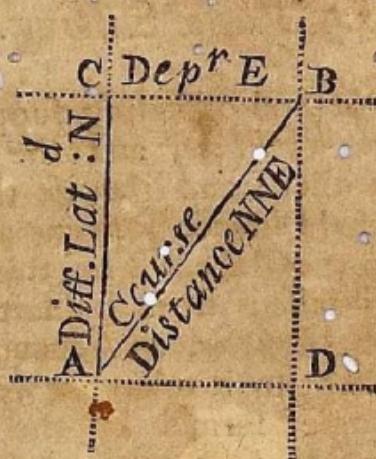
2. The Angle form'd by the *Meridian* and Rumb, that a Ship sails upon, is called the *Ship's Course*, Thus if a Ship sails on the NNE Rumb, then her *Course* will be  $22^{\circ}, 30'$ , and so of others.

3. The Distance betwixt two Places lying on the same Parallel counted in Miles of the *Equator*, or the Distance of one Place from the *Meridian* of another, counted as above, on the Parallel passing over that Place, is called *Meridional-Distance*; which in *Plane-Sailing*, goes under the Name of *Departure*.

4. Let A denote a certain Point on the Earth's Surface, A C its *Meridian*, and A D the Parallel of Latitude passing thro' it; and suppose a Ship to sail from A on the NNE Rumb till she arrive at B; and thro' B draw the Meridian BD (which according the Principles of *Plane-Sailing*, must be Parallel to CA) and the Parallel of Latitude BC; then the Length of AB, viz. how far the Ship has sail'd upon the NNE Rumb, is called her *Distance*; AC or BD will be her *Difference of Latitude*, or *Northing*, CB will be her *Departure*, or *Easting*, and the Angle CAB will be her *Course*.

Hence

Hence it is plain, that the Distance sail'd, will always be greater, than either the *Difference of Latitude*, or *Departure*, it being the Hypotenuse of a right-angled Triangle, whereof the other two are the *Legs*; except the Ship sails either on a *Meridian*,



or a *Parallel of Latitude*; for if the Ship sails on a *Meridian*, then it is plain, that her *Distance* will be just equal to her *Difference of Latitude*, and she will have no *Departure*; but if she sail on a *Parallel*, then her *Distance* will be the same with her *Departure*, and she will have no *Difference of Latitude*. It is evident also from the Scheme, that if the *Course* be less than 4 Points, or 45 Degrees, its Complement, viz. the other *Oblique Angle*, will be greater than 45 Degrees, and so the *Difference of Latitude* will be greater than the *Departure*; but if the *Course* be greater than 4 Points, then the *Difference of Latitude* will be less than the *Departure*; and lastly, if the *Course* be just 4 Points, the *Difference of Latitude* will be equal to the *Departure*.

5. Since the *Distance*, *Difference of Latitude*, and *Departure*, form a right-angled Triangle, in which the *Oblique Angle* opposite to the *Departure*

is the Course, and the other its Complement; therefore having any two of these given, we can (by Sect. 2.) find the rest; and hence arise the Cases of Plane-Sailing, which are as follow.

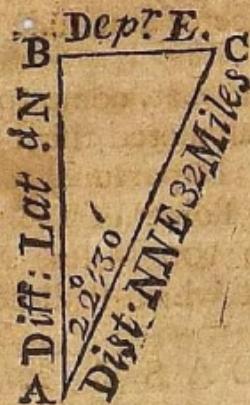
## CASE I.

*Course and Distance given, to find the Difference of Latitude and Departure.*

*Example.*

Suppose a Ship sails from the Latitude of  $30^{\circ} 25'$  North; NNE, 32 Miles. Requir'd the Difference of Latitude and Departure, and the Latitude come to.

The Geometrical Construction of this Case, is the same as in Case 3. of Right-Angled Trigonometry, the



same Things being given in both; and from it we have the following Analogy, for finding the Departure, viz.

As Radius	10.00000
to the Distance A C - 32 - - -	1.50515
	so

so is the Sine of the Course A  $22^\circ, 30' . 9.58284$   
 to the Departure BC . . . . . 12.25 . 1.08799  
 so the Ship had made 12.25 Miles of Departure  
 Easterly, or has got so far to the Eastward of her  
 Meridian. Then for the Difference of Latitude,  
 or Northing, the Ship has made, we have, by Case  
 3. of Rectangular Trigonometry, the following Ana-  
 logy, viz.

As Radius	10.00000
is to the Distance AC . . . . .	32 . 1.50515
so is the Co-Sine of the Course A $22^\circ, 30' . 9.96562$	
to the Diff. of Lat. AB . . . . .	29.57 . 1.47077

so the Ship has differ'd her Latitude, or made of  
 Northing 29.57 Minutes.

And since her former Latitude was North, and  
 her Difference of Latitude also North. Therefore,

To the Latitude sail'd from . . . . .	$30^\circ, 25' N$
add the Difference of Latitude . . . . .	$00 , 29.57$

---

and the Sum is the Lat. come to .  $30 , 54.57 N$

By this Case is calculated the Table of Difference  
 of Latitude, and Departure, to every Degree,  
 Point, and quarter Point of the Compass; for the  
 Distance from 1 to 100 Miles, at the End of this  
 Section; the Use of which shall be there explain'd.

### C A S E 2.

*Course and Difference of Latitude given, to find  
 the Distance and Departure.*

### Example.

Suppose a Ship in the Latitude of  $45^\circ, 25'$   
 North, sails N  $\frac{1}{2} E$  Easterly, till she come to  
 the

# Of Plane Sailing.

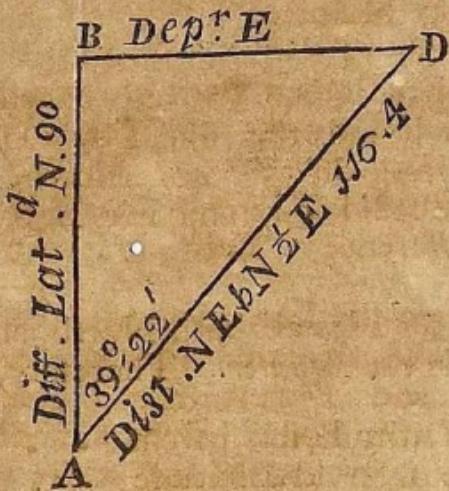
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the Latitude of  $46^{\circ} 55'$  North. Required the Distance and Departure made good upon that Course.

Since both Latitudes are Northerly, and the Course also Northerly. Therefore,

From the Latitude come to . . . .  $46^{\circ} 55'$   
 subtract the Latitude sail'd from . . . .  $45^{\circ} 25'$   
 and there remains . . . .  $01^{\circ} 30'$   
 the Difference of Latitude, equal to 90 Miles.

The Geometrical Construction of this Case, is the same with that of Case 1. of Rectangular Trigonometry



try, and by it we have the following Analogy, for finding the Departure BD, viz.

As Radius	10.00000
is to the Diff. of Latitude A B : 90 .	$1.95424$
so is the Tangent of Course A .. $39^{\circ} 22'$ 9.91402	
to the Departure B D . . . . 73.84 .	$1.86828$
so the Ship has got 73.84 Miles to the Eastward of her former Meridian.	

Y

Again

## Of Plane Sailing.

Again, for the Distance A D, we have by *Case 2<sup>d</sup>* of *Rectangular Trigonometry*, the following Proportion, viz.

As Radius . . . . .	,	10.00000
is to the Secant of the Course. . . . .	$39^{\circ}, 22'$	10.11176
so is the Diff. of Latitude A B . . . . .	$90^{\circ}$	1.95424
to the Distance A D. . . . .	116.4	2.06600

## C A S E 3.

*Difference of Latitude and Distance given, to find the Course and Departure.*

## Example.

Suppose a Ship sails from the Latitude of  $56^{\circ}, 50'$  North, on a Rumb between South and West, 126 Miles, and she is then found by Observation to be in the Latitude of  $55^{\circ}, 40'$  North. Required the Course she sail'd on, and her Departure from the Meridian.

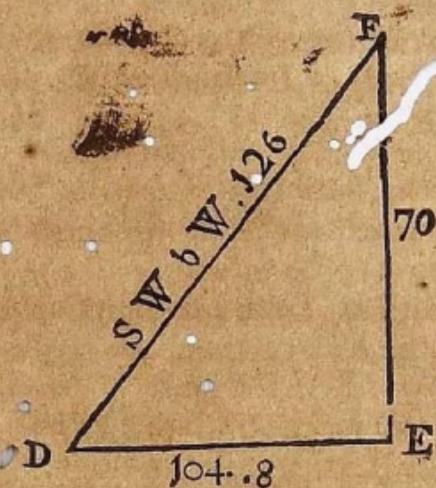
Since the Latitudes are both North, and the Ship sailing towards the Equator. Therefore,

From the Latitude sail'd from . . . . .  $56^{\circ}, 50'$   
 subtract the observ'd Latitude . . . ,  $55, 40'$   
 and the Remainder . . . . .  $01, 10$   
 equal to 70 Miles, is the Difference of Latitude.

# Of Plane Sailing.

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This Case is constructed the same Way as Case 5. of Rectangular Trigonometry, and by it we have th-



following Proportion for finding the Angle of the Course F, *viz.*

As the Distance sail'd D F . . . 126 . . . 2.10037  
 is to Radius . . . . . 10.00000  
 so is the Diff. of Latitude F E . 70 . . . 1.84510  
 to the Co-Sine of the Course F .  $56^{\circ} 15' 9.74473$   
 which, because she sails between South and West,  
 will be South  $56^{\circ} 15'$  West, or SW b W. Then  
 for the Departure, we have, by Case 3. of Rectan-  
 gular Trigonometry, the following Proportion, *viz.*

As Radius . . . . . 10.00000  
 is to the Distance sail'd D F . 126 . . . 2.10037  
 so is the Sine of the Course F .  $56^{\circ} 15' 9.91985$   
 to the Departure D E . . . 104.8 . . . 2.02022  
 consequently she has made 104.8 Miles of Depar-  
 ture Westerly.

## CASE 4.

*Difference of Latitude and Departure given, to find Course and Distance.*

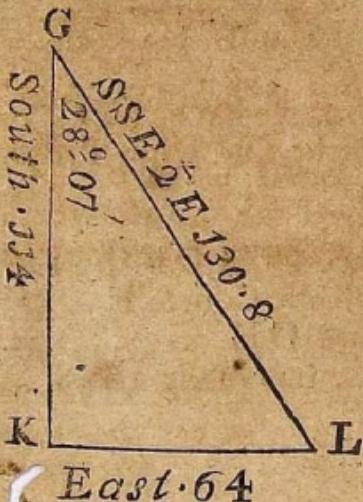
## Example.

Suppose a Ship sails from the Latitude of  $44^{\circ} 50'$  North, between South and East, till she has made 64 Miles of Easting, and is then found by Observation to be in the Latitude of  $42^{\circ} 56'$  North. Requir'd the Course and Distance made good.

Since the Latitudes are both North, and the Ship sailing towards the Equator. Therefore,

From the Latitude sail'd from  $44^{\circ} 50' \text{ N}$   
take the Latitude come to  $42^{\circ} 56'$   
and there remains  $01^{\circ} 54'$   
equal to 114 Miles, the Difference of Latitude or Southing.

This Case is constructed the same Way, as Case 4. of Rectangular Trigonometry, and by it we have the



following Proportion to find the Course KGL, viz.  
As

## Of Plane Sailing.

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As the Diff. of Latitude G K - 114 - - 2.05690  
is to Radius - - - - - 10.00000  
so is the Departure K L - - 64 - 1.80618  
to the Tang. of the Course G - 29°, 19' 1.74928  
which because the Ship is sailing between South  
and East, will be South 29°, 19' East or SSE  
 $\frac{1}{2}$  East nearly.

Then for the Distance, we shall have, by Case 2. of  
Rectangular Trigonometry, the following Analogy,  
viz.

As Radius - - - - - 10.00000  
is to the Diff. of Latitude G K 114 - 2.05690  
so is the Secant of the Course - 23, 19' 10.05952  
to the Distance G L - - - 130.8 - 2.11642  
consequently the Ship has sail'd on a SSE  $\frac{1}{2}$  East  
Course 130.8 Miles.

### C A S E 5.

*Distance and Departure given, to find the Course  
and Difference of Latitude.*

### Example.

Suppose a Ship at Sea, sails from the Latitude of 34°, 24' North, between North and West 124 Miles, and is found to have made of Westing 86 Miles. Required the Course steer'd, and the Difference of Latitude or Northing made good.

This

## Of Plane Sailing.

This Case is constructed the same Way as Case 5. of Rectangular Trigonometry, and by it we have the



following Proportion for finding the Course A D B, viz.

As the Distance A D - - - 124 - - - 2.09342  
 is to Radius - - - - - 10.00000  
 so is the Departure A B - - 86 - - - 1.93450  
 to the Sine of the Course D -  $43^\circ, 54'$  - 9.84108  
 so the Ship's Course is North  $43^\circ, 54'$  West, or  
 NW  $\frac{1}{4}$  N  $\frac{3}{4}$  West nearly.

Then for the Difference of Latitude, we have by Case 3. of Rectangular Trigonometry, the following Analogy.

As Radius - - - - - 10.00000  
 is to the Distance A D - - 124. - 2.09342  
 so is the Co-sine of the Course -  $43^\circ, 54'$  9.85726  
 to the Diff. of Latitude B D -  $89.35$  - 1.95108  
 which is equal to 1 Degree, and 29 Minutes nearly.

ly. Hence to find the Latitude the Ship is in, since both Latitudes are North, and the ship sailing from the Equator. Therefore,

To the Latitude sail'd from - - -  $35^{\circ}, 24'$   
add the Difference of Latitude - - - , 29

the Sum is - - - - - 35, 53  
the Latitude the Ship is in North.

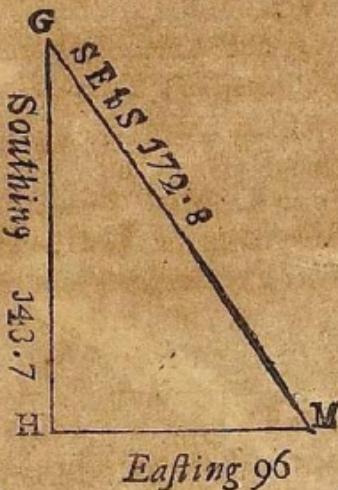
## C A S E 6.

*Course and Departure given, to find the Distance and Difference of Latitude.*

## Example.

Suppose a Ship at Sea, in the Latitude of  $24^{\circ}, 30'$  South, sails S E by S, till she has made of Easting 96 Miles. Required the Distance and Difference of Latitude made good on that Course.

This Case is projected the same Way as Case 1. of Rectangular Trigonometry, and by Case 2. we have



the following Proportion for finding the Distance, viz. As

As the Sine of the Course G  $33^{\circ} 45'$  - 9.74474  
 is to the Departure H M - 96 - - - 1.98227  
 so is Radius - - - - - 10.00000  
 to the Distance G M - 172.8 - - - 2.23753

Then for the Difference of Latitude, we have by Case 1. of Rectangular Trigonometry, the following Analogy, viz.

As the Tang. of the Course -  $33^{\circ} 45'$  - 9.82489  
 is to the Departure H M - 96 - - - 1.98227  
 so is Radius - - - - - 10.00000  
 to the Diff. of Latitude G H 143.7 - - - 2.15738  
 equal to  $2^{\circ} 24'$  nearly. Consequently since the Latitude the Ship sail'd from was South, and she sailing still towards the South.

To the Latitude sail'd from - - -  $24^{\circ} 30'$   
 add the Difference of Latitude - - -  $2^{\circ} 24'$

and the Sum - - - - -  $26^{\circ} 54'$   
 is the Latitude she is come to South.

6. When a Ship stems several Courses in 24 Hours, then the Reducing all these into one, and thereby finding the Course and Distance made good upon the Whole, is commonly called the Resolving of a *Traverse*.

7. At Sea they commonly begin each Day's Reckoning from the *Noon* of that Day, and from that Time, they set down all the different Courses and Distances stemm'd by the Ship till *Noon* the next Day upon the *Log-Board*; then from these several Courses and Distances had from the *Compass* and *Log-Line*, they compute the Difference of Latitude and Departure for each Course (by Case 1. of *Plane-Sailing*) are set down in a Table called the *Traverse-Table*, which consists of five Columns; in the first of which

are placed the Courses and Distances in the two, next, the Differences of Latitude belonging to these Courses, according as they are North or South, and in the two last are placed the Departures belonging to these Courses, according as they are East or West. Then they sum up all the Northings, and all the Southings; and taking the Difference of these they know the Difference of Latitude made good by the Ship, in the last 24 Hours, which will be North or South, according as the Sum of the Northings or Southings is greatest; the same way by taking the Sum of all the Eastings, and likewise of all the Westings, and subtracting the lesser of these from the greater, the Difference will be the Departure made good by the Ship, last 24 Hours, which will be East or West according as the Sum of the Eastings is greater or less than the Sum of the Westings; then from the Difference of Latitude and Departure made good by the Ship last 24 Hours, found as above, they find the true Course and Distance made good upon the whole (by Case 4. of Plane-Sailing), as also the Course and Distance to the intended Port.

### Example.

Suppose a Ship at Sea, in the Latitude of  $48^{\circ}$ ,  $24'$  North at Noon any Day, is bound to a Port in the Latitude of  $43^{\circ} 40'$  North, whose Departure from the Ship is 144 Miles East; consequently the direct Course and Distance of the Ship is S S E  $\frac{1}{2}$  E 315 Miles; but by reason of the shifting of the Winds she is oblig'd to steer the following Courses till Noon next Day, viz. S E  $\frac{1}{2}$  S 56 Miles, SSE 64 Miles, N W  $\frac{1}{2}$  W 48 Miles, S  $\frac{1}{2}$  W  $\frac{1}{2}$  West 54 Miles, and S E  $\frac{1}{2}$  S  $\frac{1}{2}$  E 74 Miles. Required the Course and Distance made good the last 24 Hours, and the Bearing

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ing and Distance of the Ship from the intended Port,

The Solution of this *Traverse* depends entirely on the 1st and 4th Cases of *Plane-Sailing*; and first, we must (by Case 1.) find the Difference of Latitude and Departure for each Course. Thus,

1 Course S E by S Distance 56 Miles.  
For Departure.

As Radius - - - - -	10.00000
is to the Distance - - - - -	1,74819
so is the Sine of the Course - - - - -	$33^{\circ}, 45'$ 9.74474
to the Departure - - - - -	31.11 - - 1.49293

For Difference of Latitude.

As Radius - - - - -	10.00000
is to the Distance - - - - -	1.74819
so is the Co-Sine of the Course - - - - -	$33^{\circ}, 45'$ 9.91985
to the Diff. of Latitude - - - - -	46.57 - - 1.06804

2. Course S S E and Distance 64 Miles.  
For Departure.

As Radius - - - - -	10.00000
is to the Distance - - - - -	1.80618
so is the Sine of the Course - - - - -	$22^{\circ}, 30'$ 9.58284
to the Departure - - - - -	24.5 - - 1.38902

For Difference of Latitude.

As Radius - - - - -	10.00000
is to the Distance - - - - -	1.80618
so is the Co-Sine of the Course - - - - -	$22^{\circ}, 30'$ 9.96562
to the Diff. of Latitude - - - - -	59.13 - - 1.77180

3. Course

Of Plane Sailing.

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3. Course NW by W and Distance 48 Miles,  
For Departure.

As Radius	.	.	.	10.00000
is to the Distance	.	.	48.	1.68124
so is the Sine of the Course	.	56°, 15'	.	9.91985
to the Departure	.	39.91	.	1.60109

For Difference of Latitude.

As Radius	.	.	.	10.00000
is to the Distance	.	.	48	1.68124
so is the Co-Sine of the Course	.	56°, 15'	9.74474	
to the Diff. of Latitude	.	26.67	.	1.42598

4. Course S by W  $\frac{1}{2}$  West and Distance 54 Miles,  
For Departure.

As Radius	.	.	.	10.00000
is to the Distance	.	.	54	1.73239
so is the Sine of the Course	.	16°, 52'	9.46262	
to the Departure	.	15.67	.	1.19501

For Difference of Latitude.

As Radius	.	.	.	10.00000
is to the Distance	.	.	54	1.73239
so is the Co-Sine of the Course	.	16°, 52'	9.98050	
to the Diff. of Latitude	.	51.67	.	1.71329

5. Course SE by S  $\frac{1}{2}$  East and Distance 74 Miles.

As Radius	.	.	.	10.00000
is to the Distance	.	.	74	1.86923
so is the Sine of the Course	.	39°, 22'	9.80228	
to the Departure	.	46.94	.	1.67151

For

## For Difference of Latitude.

As Radius . . . . . 10.00000  
 is to the Distance . . . . 74. . . 1.86923  
 so is the Co-Sine of the Course.  $39^{\circ}, 22'$ . 9.88824  
 to the Difference of Latitude. 57.21 . . 1.75747

Now these several Courses and Distances together with the Differences of Latitude and Departures deduced from them, being set down in their proper Columns in the *Traverse-Table*, will stand as follows.

## The Traverse Table.

Courses. Distan.	Diff. of Lat.	Departure.		
	N.	S.	E.	W.
SE $\frac{1}{2}$ S 56	—	46.57	31.11	—
SSE 64	—	59.13	24.5	—
NW $\frac{1}{2}$ W 48	26.67	—	—	39.91
S $\frac{1}{2}$ W $\frac{1}{2}$ W 54	—	51.67	—	15.67
SE $\frac{1}{2}$ S $\frac{1}{2}$ E 74	—	57.21	46.94	—
	—	—	—	—
	26.67	214.58	102.55	55.58
		26.67	55.58	
Dif. of Lat.	187.91	46.97	Dep.	

Hence it is plain, since the Sum of the Northings is 26.67, and of the Southings 214.58, the Difference between these, viz. 187.91 will be the Soathing made good by the Ship, the last 24 Hours; also the Sum of the Eastings being 102.55, and of the Westings 55.58, the Difference 46.97 will be the Easting or Departure made good by the Ship's last 24 Hours; consequently to find the true Course and Distance made good by the Ship in that Time, it will be by Case of 4. *Plane-Sailing.* As

As the Diff. of Latitude . . 187.91 . . 2.27393  
 is to Radius . . . . . 10.00000  
 so is the Departure . . . 46.97 . . 1.67182  
 to the Tang. of Course . . . 14°, 03' . . 9.39789  
 which is S  $\frac{1}{2}$  E  $\frac{1}{2}$  East nearly. Then for the Distance it will be

As Radius . . . . . 10.00000  
 is to the Diff. of Latitude . . 187.91 . . 2.27393  
 so is the Sec. of the Course . . 14°, 03' . . 10.01319  
 to the Distance . . . . . 193.7 . . 2.28712  
 consequently the Ship has made good the last 24 Hours, on a S  $\frac{1}{2}$  E  $\frac{1}{2}$  East Course, 193.7 Miles; and since the Ship is sailing towards the Equator. Therefore,

From the Latitude sail'd from . . . 48°, 24' N take the the Diff. of Latitude made good 3, 08' S there remains . . . . . 45, 16' N the Latitude the Ship is in North. And because the Port the Ship is bound for, lies in the Latitude of 43°, 40' North, and consequently South of the Ship. Therefore,

From the Latitude the Ship is in . . . 45°, 16' N take the Latitude she is bound for . . . 43°, 40' N and there remains . . . . . 1, 36' or 96 Miles, the Difference of Latitude or Southing the Ship has to make. Again, the whole Easting the Ship had to make being 144 Miles, and she having already made 46.97 or 47 Miles of Easting; therefore the Departure or Easting, she still has to make will be 97 Miles. Consequently to find the direct Course and Distance between the Ship and the intended Port, it will be by Case 4. of Plane-Sailing.

As the Diff. of the Latitude	96.	.	.	8.98227
is to the Radius	.	.	.	10.00000
so is the Departure	.	97.	.	1.98677
to the Tang. of the Course	.	45°, 19'	10.0045°	

And,

As Radius	.	.	.	10.00000
is to the Diff. of Latitude	.	96.	.	1.98227
so is the Sec. of the Course	.	45°, 19'	10.15293	
to the Distance	.	136.5	.	2.13520

whence the true Bearing and Distance of the intended Port is S E 136.5 Miles.

8. In the following Table, computed by Case 1. of *Plane-Sailing*, for the more ready working a Traverse, you may observe; that in the top-Column of each Page are placed the Courses beginning at 1 Degree, and proceeding thro' the several Degrees, Points, and quarter Points, to 45 Degrees, the bottom-Column beginning with 45°, where the upper ends and proceeding to 90 Degrees, the Degrees in the upper and lower Columns being the Complements of one another. The two side-COLUMNS in each Page contain the Distances, *viz.* those on the left Hand contain the Distances from 1 to 50, and those on the right-Hand Page contain the Distances from 50 to 100. The other intermediate Columns contain the Differences of Latitude and Departures, answering to the Courses in the top and Distances in the side-Columns. The Use of this will be plain, from the following Example.

### Example 1.

Suppose the Course to be S E by S, East, and Distance 48 Miles. Required the Difference of Latitude and Departure.

First

*First*, I look in the Top-Column for  $3\frac{1}{2}$  Points (because it is less than 4 Points, or 45 Degrees) and in the side-Column on the left-Hand Page (because the Distance is less than 50) for the Distance 48; then below the  $3\frac{1}{2}$  Points, and on the same Line with 48, I find 37.1 for the Difference of Latitude, and 30.4 for the Departure.

### Example 2.

Suppose the Course N E  $\frac{1}{2}$  E, and the Distance 76 Miles. Required the Difference of Latitude and Departure.

*First*, I look in the bottom-Column for the Course, *viz.* 5 Points (because it exceeds 4 Points or 45 Degrees) and in the side Column on the right-Hand Page (because the Distance exceeds 50) for the Distance 76; then above the Course, and on the same Line with the Distance, I find 63.2 for the Departure, and 42.2 for the Difference of Latitude.

If the given Distance exceed the Limits of the Table, *i. e.* be greater than 100, then that Distance must be divided into two or more Parts, each of which must be less or equal to 100; then find as in the preceding Examples, the Difference of Latitude and Departure for each Distance on the given Course, and the Sum of these Differences of Latitudes will be the Difference of Latitude required, also the Sum of the Departures, will be the Departure required.

### Example 3.

Suppose the Course S W  $\frac{1}{2}$  S, and Distance 146 Miles. Required the Difference of Latitude and Departure.

*First*,

*First*, I divide the given Distance into two, *viz.* 100 and 46; then the Differences of Latitude and Departures answering to these on a SW b S Course, found in the Table, will be as follows, *viz.*

Course.	Dist.	Diff. of Lat.	Depart.
SW b S	100	83.1	55.6
	46	38.2	25.5
	146	121.3	81.1

The Sum of the Differences of Latitude, *viz.* 121.3 is the Difference of Latitude required, and the Sum of the Departures, *viz.* 81.1 is the Departure required.

After the same Manner may a Traverse be wrought by the Table, *viz.* by finding the Difference of Latitude and Departure (from the Table) to each Course and Distance, and setting them down in their proper Columns in the Traverse-Table, and then working as in the foregoing Example of a Traverse.

### Example.

Suppose a Ship in the Latitude of  $36^{\circ} 43'$  North, sails on the following Courses, *viz.* S E b S, 56 Miles, S S E 42 Miles, S b W 64 Miles, and N E b N 40 Miles. Required the Course and Distance made good upon the whole, and the Latitude the Ship has come to.

*First*, I take from the Table, the Difference of Latitude and Departure belonging to each Course and Distance, and these set down in their proper Columns

Columns in the *Traverse Table*, will stand as follows,

Courses.	Distan.	Diff. of Lat.	Departure.		
		N.	S.	E.	W.
SEbS	56	—	46.6	31.1	—
SSE	43	—	39.7	16.5	—
SbW	64	—	62.8	—	12.5
N Eb N	40	33.3	—	22.2	—
		33.3	149.1	69.8	12.5
			33.3	12.5	
<i>Diff. of Lat.</i>		115.8	57.3	<i>Dep.</i>	

Whence it is plain, that the Difference of Latitude made good is 115.8 Miles, and the Departure is 57.3 Miles; then, for the direct Course and Distance it will be, (by Case 4. of *Plane Sailing*.) As the Difference of Lat. - 115.8 - 2.09968 is to Radius - - - - - 10.00000 so is the Departure - - - 57.3 - 1.75815 to the Tangent of the Course 24°. 30' 9.65847 which, because the Ship is sailing between the South and East, will be SSE  $\frac{1}{4}$  East nearly. Again, for the Distance it will be,

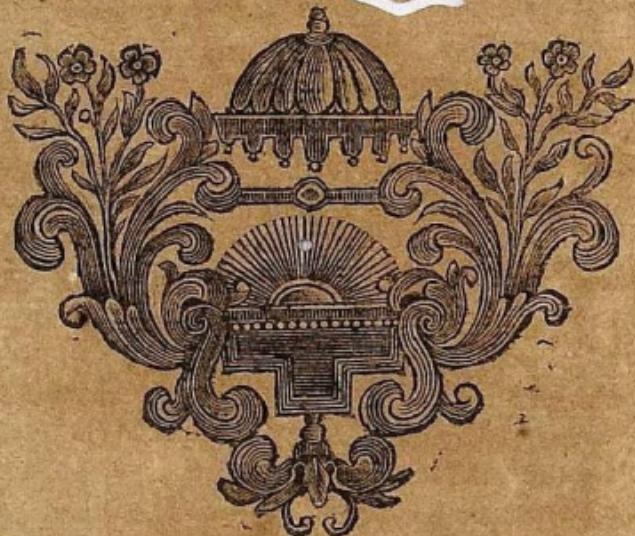
As Radius - - - - - 10.00000  
is to the Difference of Lat. 115.8 - 2.09968  
so is the Sec. of the Course 24°. 30' - 10.04098  
to the Distance - - - 138.3 - - 2.14066

And since the Ship is sailing towards the Equator, consequently diminishing her Latitude, therefore,

From the Latitude sail'd from - - -  $36^{\circ} 43' N$   
Subtract the Difference of Latitude  $1, 55 S^{\circ}$   

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and there remains - - - - -  $34, 48 N$   
the Latitude the Ship has come to.



A L A R G E

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A L A R G E and very U S E F U L  
T A B L E  
O F

Difference of LATITUDE and  
DEPARTURE, in Minutes and  
Tenth Parts, to every *Degree* and  
*Quarter-Point* of the Compass, for  
the Exact Working of a *Traverse.*

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## A TABLE of Difference

Dif.	1 Deg.	2 Deg.	3 Point	3 Deg.	4 Deg.	5 Deg.	Dif.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	01.0	00.0	01.0	00.0	01.0	00.0	01.0
2	02.0	00.0	02.0	00.1	02.0	00.1	02.0
3	03.0	00.1	03.0	00.1	03.0	00.2	03.0
4	04.0	00.1	04.0	00.1	04.0	00.2	04.0
5	05.0	00.1	05.0	00.2	05.0	00.2	05.0
6	06.0	00.1	06.0	00.2	06.0	00.3	06.0
7	07.0	00.1	07.0	00.2	07.0	00.3	07.0
8	08.0	00.1	08.0	00.3	08.0	00.4	08.0
9	09.0	00.2	09.0	00.3	09.0	00.4	09.0
10	10.0	00.2	10.0	00.4	10.0	00.5	10.0
11	11.0	00.2	11.0	00.4	11.0	00.5	11.0
12	12.0	00.2	12.0	00.4	12.0	00.6	12.0
13	13.0	00.2	13.0	00.5	13.0	00.6	13.0
14	14.0	00.2	14.0	00.5	14.0	00.7	14.0
15	15.0	00.3	15.0	00.6	15.0	00.7	15.0
16	16.0	00.3	16.0	00.6	16.0	00.8	16.0
17	17.0	00.3	17.0	00.6	17.0	00.8	17.0
18	18.0	00.3	18.0	00.6	18.0	00.9	18.0
19	19.0	00.3	19.0	00.7	19.0	00.9	19.0
20	20.0	00.4	20.0	00.7	20.0	00.9	20.0
21	21.0	00.4	21.0	00.7	21.0	01.0	21.0
22	22.0	00.4	22.0	00.8	22.0	01.1	22.0
23	23.0	00.4	23.0	00.8	23.0	01.1	23.0
24	24.0	00.4	24.0	00.8	24.0	01.1	24.0
25	25.0	00.4	25.0	00.9	25.0	01.2	25.0
26	26.0	00.5	26.0	00.9	26.0	01.3	26.0
27	27.0	00.5	27.0	00.9	27.0	01.3	27.0
28	28.0	00.5	28.0	01.0	28.0	01.4	28.0
29	29.0	00.5	29.0	01.0	29.0	01.4	29.0
30	30.0	00.5	30.0	01.1	30.0	01.5	30.0
31	31.0	00.5	31.0	01.1	31.0	01.6	31.0
32	32.0	00.6	32.0	01.1	31.9	01.6	31.9
33	33.0	00.6	33.0	01.2	32.9	01.6	32.9
34	34.0	00.6	34.0	01.2	33.9	01.7	33.9
35	35.0	00.6	35.0	01.2	34.9	01.7	34.9
36	36.0	00.6	36.0	01.3	35.9	01.8	35.9
37	37.0	00.7	37.0	01.3	36.9	01.8	36.9
38	38.0	00.7	38.0	01.3	37.9	01.9	37.9
39	39.0	00.7	39.0	01.4	38.9	01.9	38.9
40	40.0	00.7	40.0	01.4	39.9	02.0	39.9
41	41.0	00.7	41.0	01.4	40.9	02.0	40.9
42	42.0	00.7	42.0	01.5	41.9	02.1	41.9
43	43.0	00.8	43.0	01.5	42.9	02.1	42.9
44	44.0	00.8	44.0	01.5	43.9	02.2	43.9
45	45.0	00.8	45.0	01.6	44.9	02.2	44.9
46	46.0	00.8	46.0	01.6	45.9	02.2	45.9
47	47.0	00.8	47.0	01.6	46.9	02.3	46.9
48	48.0	00.8	48.0	01.7	47.9	02.3	47.9
49	49.0	00.9	49.0	01.7	48.9	02.4	48.9
50	50.0	00.9	50.0	01.8	49.9	02.4	49.9
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
	89 Deg.	88 Deg.	7 $\frac{3}{4}$ Point	87 Deg.	86 Deg.	85 Deg.	Dif.

## of Latitude and Departure.

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D.	1 Deg.	2 Deg.	3 Point	3 D. eg.	4 Deg.	5 Deg.	Dif.						
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.						
51	51.0	00.9	51.0	01.8	50.9	02.5	50.9	02.7	50.9	03.6	50.8	04.4	51
52	52.0	00.9	52.0	01.8	51.9	02.5	51.9	02.7	51.9	03.6	51.8	04.5	52
53	53.0	00.9	53.0	01.8	52.9	02.6	52.9	02.8	52.9	03.7	52.8	04.6	53
54	54.0	00.9	54.0	01.9	53.9	02.6	53.9	02.8	53.9	03.8	53.8	04.7	54
55	55.0	01.0	55.0	01.9	54.9	02.7	54.9	02.9	54.9	03.8	54.8	04.8	55
56	56.0	01.0	56.0	02.0	55.9	02.7	55.9	02.9	55.9	03.9	55.8	04.9	56
57	57.0	01.0	57.0	02.0	56.9	02.8	56.9	03.0	56.8	04.0	56.8	05.0	57
58	58.0	01.0	58.0	02.0	57.9	02.8	57.9	03.0	57.8	04.1	57.8	05.1	58
59	59.0	01.0	59.0	02.1	58.9	02.9	58.9	03.1	58.8	04.1	58.8	05.2	59
60	60.0	01.0	60.0	02.1	59.9	02.9	59.9	03.1	59.8	04.2	59.8	05.2	60
61	61.0	01.1	61.0	02.1	60.9	03.0	60.9	03.2	60.8	04.3	60.8	05.3	61
62	62.0	01.1	62.0	02.2	61.9	03.0	61.9	03.3	61.8	04.3	61.8	05.4	62
63	63.0	01.1	63.0	02.2	62.9	03.1	62.9	03.3	62.8	04.4	62.8	05.5	63
64	64.0	01.1	64.0	02.3	63.9	03.1	63.9	03.4	63.8	04.5	63.8	05.6	64
65	65.0	01.1	65.0	02.3	64.9	03.2	64.9	03.4	64.8	04.5	64.7	05.7	65
66	66.0	01.1	66.0	02.3	65.9	03.3	65.9	03.5	65.8	04.6	65.7	05.8	66
67	67.0	01.2	66.9	02.3	66.9	03.3	66.9	03.5	66.8	04.7	66.7	05.9	67
68	68.0	01.2	67.9	01.4	67.9	03.3	67.9	03.5	67.8	04.8	67.7	05.9	68
69	69.0	01.2	68.9	02.4	68.9	03.4	68.9	03.6	68.8	04.8	68.7	06.0	69
70	70.0	01.2	69.9	02.4	69.9	03.4	69.9	03.7	69.8	04.9	69.7	06.1	70
71	71.0	01.2	70.9	02.5	70.9	03.5	70.9	03.7	70.8	04.9	70.7	06.2	71
72	72.0	01.3	71.9	02.5	71.9	03.5	71.9	03.8	71.8	05.0	71.7	06.3	72
73	73.0	01.3	72.9	02.5	72.9	03.6	72.9	03.8	72.8	05.1	72.7	06.4	73
74	74.0	01.3	73.9	02.6	73.9	03.6	73.9	03.9	73.8	05.2	73.7	06.5	74
75	75.0	01.3	74.9	02.6	74.9	03.7	74.9	03.9	74.8	05.2	74.7	06.6	75
76	76.0	01.3	75.9	02.7	75.9	03.7	75.9	04.0	75.8	05.3	75.7	06.6	76
77	77.0	01.3	76.9	02.7	76.9	03.8	76.9	04.0	76.8	05.4	76.7	06.7	77
78	78.0	01.4	77.9	02.7	77.9	03.8	77.9	04.1	77.8	05.4	77.7	06.8	78
79	79.0	01.4	78.9	02.8	78.9	03.9	78.9	04.1	78.8	05.5	78.7	06.9	79
80	80.0	01.4	79.9	02.8	79.9	03.9	79.9	04.2	79.8	05.6	79.7	07.0	80
81	81.0	01.4	80.9	02.8	80.9	04.0	80.9	04.2	80.8	05.7	80.7	07.1	81
82	82.0	01.4	81.9	02.9	81.9	04.0	81.9	04.3	81.8	05.7	81.7	07.2	82
83	83.0	01.4	82.9	02.9	82.9	04.1	82.9	04.4	82.8	05.8	82.7	07.3	83
84	84.0	01.5	83.9	02.9	83.9	04.1	83.9	04.4	83.8	05.9	83.7	07.4	84
85	85.0	01.5	84.9	03.0	84.9	04.2	84.9	04.5	84.8	05.9	84.7	07.4	85
86	86.0	01.5	85.9	03.0	85.9	04.2	85.9	04.5	85.8	06.0	85.7	07.5	86
87	87.0	01.5	86.9	03.0	86.9	04.3	86.9	04.6	86.8	06.1	86.7	07.6	87
88	88.0	01.5	87.9	03.1	87.9	04.3	87.9	04.6	87.8	06.2	87.7	07.7	88
89	89.0	01.5	88.9	03.1	88.9	04.4	88.9	04.7	88.8	06.2	88.7	07.8	89
90	90.0	01.6	89.9	03.1	89.9	04.4	89.9	04.7	89.8	06.3	89.7	07.9	90
91	91.0	01.6	90.9	03.2	90.9	04.5	90.9	04.8	90.8	06.4	90.7	08.0	91
92	92.0	01.6	91.9	03.2	91.9	04.5	91.9	04.8	91.8	06.4	91.6	08.0	92
93	93.0	01.6	92.9	03.2	92.9	04.6	92.9	04.9	92.8	06.5	92.6	08.1	93
94	94.0	01.6	93.9	03.3	93.9	04.6	93.9	04.9	93.8	06.6	93.6	08.2	94
95	95.0	01.6	94.9	03.3	94.9	04.7	94.9	05.0	94.8	06.6	94.6	08.3	95
96	96.0	01.7	95.9	03.4	95.9	04.7	95.9	05.0	95.8	06.7	95.6	08.4	96
97	97.0	01.7	96.9	03.4	96.9	04.8	96.9	05.1	96.8	06.8	96.6	08.5	97
98	98.0	01.7	97.9	03.4	97.9	04.8	97.9	05.1	97.8	06.9	97.6	08.6	98
99	99.0	01.7	98.9	03.5	98.9	04.9	98.9	05.2	98.8	06.9	98.6	08.7	99
100	100.0	01.7	99.9	03.5	99.9	04.9	99.9	05.2	99.8	07.0	99.6	08.7	100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dif.
	89 Deg.	88 Deg.	7 3 Point	87 Deg.	86 Deg.	85 Deg.							

Diff.	$\frac{1}{2}$ Point		Deg.		Deg.		8 Deg.		$\frac{3}{4}$ Point		9 Deg.		Diff.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Lat.	Lat.	Dep.	Lat.	Dep.	
1	01,0	00,1	01,0	00,1	01,0	00,1	01,0	00,1	01,0	00,1	01,0	00,1	1
2	02,0	00,2	02,0	00,2	02,0	00,2	02,0	00,3	02,0	00,3	02,0	00,3	2
3	03,0	00,3	03,0	00,3	03,0	00,4	02,0	00,4	03,0	00,4	03,0	00,5	3
4	04,0	00,4	04,0	00,4	04,0	00,5	04,0	00,6	04,0	00,6	03,9	00,6	4
5	05,0	00,5	05,0	00,5	05,0	00,6	04,9	00,7	04,9	00,7	04,9	00,8	5
6	06,0	00,6	06,0	00,6	06,0	00,7	05,9	00,8	05,9	00,9	05,9	00,9	6
7	07,0	00,7	07,0	00,7	07,0	00,8	06,9	01,0	06,9	01,0	06,9	01,1	7
8	08,0	00,8	07,9	00,8	07,9	01,0	07,9	01,1	07,9	01,2	07,9	01,2	8
9	09,0	00,9	08,9	00,9	08,9	01,1	08,9	01,2	08,9	01,3	08,9	01,4	9
10	09,9	01,0	09,9	01,0	09,9	01,2	09,9	01,4	09,9	01,5	09,9	01,6	10
11	10,9	01,1	10,9	01,1	10,9	01,3	10,9	01,5	10,9	01,6	10,9	01,7	11
12	11,9	01,2	11,9	01,2	11,9	01,5	11,9	01,7	11,9	01,8	11,8	01,9	12
13	12,9	01,3	12,9	01,4	12,9	01,6	12,9	01,8	12,9	01,9	12,8	02,0	13
14	13,9	01,4	13,9	01,5	13,9	01,7	13,9	01,9	13,8	02,1	13,8	02,2	14
15	14,9	01,5	14,9	01,6	14,9	01,8	14,8	02,1	14,8	02,2	14,8	02,3	15
16	15,9	01,6	15,9	01,7	15,9	01,9	15,8	02,2	15,8	02,3	15,8	02,5	16
17	16,9	01,7	16,9	01,8	16,9	02,1	16,8	02,4	16,8	02,5	16,8	02,7	17
18	17,9	01,8	17,9	01,9	17,9	02,2	17,8	02,5	17,8	02,6	17,8	02,8	18
19	18,9	01,9	18,9	02,0	18,9	02,3	18,8	02,6	18,8	02,8	18,7	03,0	19
20	19,9	02,0	19,9	02,1	19,9	02,4	19,8	02,8	19,8	02,9	19,7	03,1	20
21	20,9	02,1	20,9	02,2	20,8	02,6	20,8	02,9	20,8	03,1	20,7	03,3	21
22	21,9	02,2	21,9	02,3	21,8	02,7	21,8	03,1	21,8	03,2	21,7	03,4	22
23	22,9	02,2	22,9	02,4	22,8	02,8	22,8	03,2	22,7	03,4	22,7	03,6	23
24	23,9	02,3	23,9	02,5	23,8	02,9	23,8	03,3	23,7	03,5	23,7	03,8	24
25	24,9	02,4	24,9	01,6	24,8	03,0	24,8	03,5	24,7	03,7	24,7	03,9	25
26	25,9	02,5	25,9	02,7	25,8	03,2	25,7	03,6	25,7	03,8	25,7	04,1	26
27	26,9	02,6	26,9	02,8	26,8	03,3	26,7	03,7	26,7	04,0	26,7	04,2	27
28	27,9	02,7	27,8	02,9	27,8	03,4	27,7	03,9	27,7	04,1	27,7	04,4	28
29	28,9	02,8	28,8	03,0	28,8	03,5	28,7	04,0	28,7	04,2	28,6	04,5	29
30	29,9	02,9	29,9	03,1	29,8	03,7	29,7	04,2	29,7	04,4	29,6	04,7	30
31	30,8	03,0	30,8	03,2	30,8	03,8	30,7	04,3	30,7	04,5	30,6	04,9	31
32	31,8	03,1	31,8	03,3	31,8	03,9	31,7	04,4	31,6	04,7	31,6	05,0	32
33	32,8	03,2	32,8	03,4	32,7	04,0	32,7	04,6	32,6	04,8	32,6	05,2	33
34	33,8	03,3	33,8	03,5	33,7	04,1	33,7	04,7	33,6	05,0	33,6	05,3	34
35	34,8	03,4	34,8	03,7	34,7	04,3	34,7	04,9	34,6	05,1	34,6	05,5	35
36	35,8	03,5	35,8	03,8	35,7	04,4	35,6	05,0	35,6	05,3	35,5	05,6	36
37	36,8	03,6	36,8	03,9	36,7	04,5	36,6	05,1	36,6	05,4	36,5	05,8	37
38	37,8	03,7	37,8	04,0	37,7	04,6	37,6	05,3	37,6	05,6	37,5	06,0	38
39	38,8	03,8	38,8	04,1	38,7	04,8	38,6	05,4	38,6	05,7	38,5	06,1	39
40	39,8	03,9	39,8	04,2	39,7	04,9	39,6	05,6	39,6	05,9	39,5	06,3	40
41	40,8	04,0	40,8	04,3	40,7	05,0	40,6	05,7	40,6	06,0	40,5	06,4	41
42	41,8	04,1	41,8	04,4	41,7	05,1	41,6	05,8	41,5	06,1	41,5	06,6	42
43	42,8	04,2	42,8	04,5	42,7	05,2	42,6	06,0	42,5	06,3	42,5	06,7	43
44	43,8	04,3	43,7	04,6	43,7	05,4	43,6	06,1	43,5	06,5	43,5	06,9	44
45	44,8	04,4	44,7	04,7	44,7	05,5	44,6	06,3	44,5	06,6	44,5	07,0	45
46	45,8	04,5	45,7	04,8	45,7	05,6	45,5	06,4	45,5	06,7	45,5	07,2	46
47	46,8	04,6	46,7	04,9	46,7	05,7	46,5	06,5	46,5	06,9	46,4	07,3	47
48	47,8	04,7	47,7	05,0	47,6	05,9	47,5	06,7	47,5	07,0	47,4	07,5	48
49	48,8	04,8	48,7	05,1	48,6	06,0	48,5	06,8	48,5	07,2	48,4	07,7	49
50	49,8	04,9	49,7	05,2	49,6	06,1	49,5	07,0	49,5	07,3	49,4	07,8	50
D	Dep.	Lat.	D	Lat.	D	Lat.	D	Lat.	D	Lat.	D	Lat.	D
D	$\frac{1}{2}$ Point	4 Deg.	B	3 Deg.	S	2 Deg.	7	$\frac{1}{2}$ Point	8	1 Deg.	F	7	

	Point	6 Deg.	7 Deg.	8 Deg.	Point	o Deg	D						
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.						
S1	50° 7'	05.0	50° 7'	05.3	50° 9'	06.2	50° 5'	07.1	50° 4'	07.5	50° 4'	08.0	S1
S2	51° 7'	05.1	51° 7'	05.4	51° 6'	06.3	51° 5'	07.2	51° 4'	07.6	51° 4'	08.1	S2
S3	52° 7'	05.2	52° 7'	05.5	52° 6'	06.6	52° 5'	07.4	52° 4'	07.8	52° 3'	08.3	S3
S4	53° 7'	05.3	53° 7'	05.6	53° 6'	06.6	53° 5'	07.5	53° 4'	07.9	53° 3'	08.4	S4
S5	54° 7'	05.4	54° 7'	05.8	54° 6'	06.7	54° 5'	07.6	54° 4'	08.1	54° 3'	08.6	S5
S6	55° 7'	05.5	55° 7'	05.9	55° 6'	06.9	55° 5'	07.8	55° 4'	08.2	55° 3'	08.7	S6
S7	56° 7'	05.6	56° 7'	06.0	56° 6'	07.0	56° 5'	07.9	56° 4'	08.4	56° 3'	08.9	S7
S8	57° 7'	05.7	57° 7'	06.1	57° 6'	07.3	57° 4'	08.1	57° 4'	08.5	57° 3'	09.1	S8
S9	58° 7'	05.8	58° 7'	06.2	58° 6'	07.5	58° 4'	08.2	58° 4'	08.7	58° 3'	09.2	S9
S10	59° 7'	05.9	59° 7'	06.3	59° 5'	07.3	59° 4'	08.3	59° 4'	08.8	59° 3'	09.4	S10
S11	60° 0'	7 106.0	60° 7'	06.4	60° 5'	07.4	60° 4'	08.5	60° 3'	08.9	60° 2'	09.5	S11
S12	61° 1'	06.1	61° 6'	06.5	61° 5'	07.6	61° 4'	08.6	61° 3'	09.1	61° 2'	09.7	S12
S13	62° 2'	06.2	62° 6'	06.6	62° 5'	07.7	62° 4'	08.8	62° 3'	09.2	62° 2'	09.9	S13
S14	63° 3'	06.3	63° 6'	06.7	63° 5'	07.8	63° 4'	08.9	63° 3'	09.4	63° 2'	10.0	S14
S15	64° 4'	06.4	64° 6'	06.8	64° 5'	07.9	64° 4'	09.1	64° 3'	09.5	64° 2'	10.2	S15
S16	65° 5'	06.5	65° 9'	06.5	65° 5'	08.0	65° 4'	09.2	65° 3'	09.7	65° 2'	10.3	S16
S17	66° 6'	06.6	66° 0'	07.0	66° 5'	08.2	66° 3'	09.3	66° 3'	09.8	66° 2'	10.5	S17
S18	67° 7'	06.7	67° 6'	07.1	67° 5'	08.3	67° 3'	09.3	67° 3'	10.0	67° 2'	10.6	S18
S19	68° 8'	06.8	68° 6'	07.2	68° 5'	08.4	68° 3'	09.6	68° 2'	10.1	68° 1'	10.8	S19
S20	69° 7'	06.9	69° 6'	07.3	69° 5'	08.5	69° 3'	09.7	69° 2'	10.3	69° 1'	10.9	S20
S21	70° 0'	7 107.0	70° 6'	07.4	70° 5'	08.7	70° 3'	09.9	70° 4'	10.4	70° 3'	11.1	S21
S22	71° 1'	07.1	71° 6'	07.5	71° 5'	08.8	71° 3'	10.0	71° 2'	11.0	71° 1'	11.3	S22
S23	72° 2'	07.2	72° 6'	07.6	72° 4'	08.9	72° 3'	10.2	72° 2'	11.7	72° 1'	11.4	S23
S24	73° 3'	07.3	73° 6'	07.7	73° 4'	09.0	73° 3'	10.3	73° 2'	11.9	73° 1'	11.6	S24
S25	74° 4'	07.4	74° 6'	07.8	74° 4'	09.1	74° 3'	10.4	74° 2'	11.0	74° 1'	11.7	S25
S26	75° 5'	07.5	75° 6'	07.9	75° 4'	09.3	75° 3'	10.6	75° 2'	11.1	75° 1'	11.9	S26
S27	76° 6'	07.5	76° 6'	08.0	76° 4'	09.4	76° 1'	10.7	76° 2'	11.3	76° 0'	12.0	S27
S28	77° 7'	07.6	77° 6'	08.1	77° 4'	09.5	77° 1'	10.9	77° 1'	11.4	77° 0'	12.1	S28
S29	78° 8'	07.7	78° 6'	08.3	78° 4'	09.6	78° 2'	11.0	78° 1'	11.6	78° 0'	12.4	S29
S30	79° 6'	07.8	79° 6'	08.4	79° 4'	09.8	79° 2'	11.1	79° 1'	11.7	79° 0'	12.5	S30
S31	80° 0'	07.9	80° 5'	08.5	80° 4'	09.9	80° 2'	11.3	80° 1'	11.9	80° 0'	12.7	S31
S32	81° 6'	08.0	81° 5'	08.6	81° 4'	10.0	81° 2'	11.4	81° 1'	12.0	81° 0'	12.8	S32
S33	82° 6'	08.1	82° 5'	08.7	82° 4'	10.1	82° 2'	11.5	82° 1'	12.2	82° 0'	13.0	S33
S34	83° 6'	08.2	83° 5'	08.8	83° 3'	10.2	83° 2'	11.7	83° 1'	12.3	83° 0'	13.1	S34
S35	84° 6'	08.3	84° 5'	08.9	84° 4'	10.3	84° 2'	11.8	84° 1'	12.5	83° 9'	13.3	S35
S36	85° 6'	08.4	85° 5'	09.0	85° 4'	10.4	85° 2'	12.0	85° 1'	12.6	84° 9'	13.4	S36
S37	86° 6'	08.5	86° 5'	09.1	86° 3'	10.5	86° 1'	12.1	86° 0'	12.8	85° 9'	13.6	S37
S38	87° 6'	08.6	87° 5'	09.2	87° 3'	10.7	87° 1'	12.3	87° 0'	12.9	86° 9'	13.8	S38
S39	88° 6'	08.7	88° 5'	09.3	88° 3'	10.9	88° 1'	12.4	88° 0'	13.1	87° 9'	13.9	S39
S40	89° 6'	08.8	89° 5'	09.4	89° 3'	11.0	89° 1'	12.5	89° 0'	13.2	88° 9'	14.1	S40
S41	90° 6'	08.9	90° 5'	09.5	90° 3'	11.1	90° 1'	12.7	90° 0'	13.4	89° 9'	14.2	S41
S42	91° 6'	09.0	91° 5'	09.6	91° 3'	11.2	91° 1'	12.8	91° 0'	13.5	90° 9'	14.4	S42
S43	92° 6'	09.1	92° 5'	09.7	92° 3'	11.3	92° 1'	12.9	92° 0'	13.6	91° 8'	14.5	S43
S44	93° 5'	09.2	93° 5'	09.8	93° 3'	11.5	93° 1'	13.1	93° 0'	13.8	92° 8'	14.7	S44
S45	94° 5'	09.3	94° 5'	09.9	94° 3'	11.6	94° 1'	13.2	94° 0'	13.9	93° 8'	14.9	S45
S46	95° 5'	09.4	95° 5'	10.0	95° 3'	11.7	95° 1'	13.4	95° 0'	14.1	94° 8'	15.0	S46
S47	96° 5'	09.5	96° 5'	10.1	96° 3'	11.8	96° 0'	13.5	95° 9'	14.2	95° 8'	15.2	S47
S48	97° 5'	09.6	97° 5'	10.2	97° 3'	12.0	97° 0'	13.6	96° 9'	14.4	96° 8'	15.3	S48
S49	98° 5'	09.7	98° 5'	10.3	98° 3'	12.1	98° 0'	13.8	97° 9'	14.5	97° 8'	15.5	S49
S50	99° 5'	09.8	99° 5'	10.4	99° 2'	12.2	99° 0'	13.9	98° 9'	14.7	98° 8'	15.6	S50
Dif.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Dif.	
Dif.	7 1/2 Point	84 Deg	83 Deg	82 Deg	7 1/2 Point	81 Deg							

Dift.	10 Deg.	11 Deg.	1 Point	2 Deg.	13 Deg.	14 Deg.	Dif.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	01,0 00,1	01,0 00,2	01,0 00,4	01,0 00,2	01,0 00,3	01,0 00,2	1
2	02,0 00,3	02,0 00,4	02,0 00,4	02,0 00,4	01,9 00,4	01,9 00,5	2
3	02,9 00,5	02,9 00,6	02,9 00,6	02,9 00,6	02,9 00,7	02,9 00,7	3
4	03,9 00,7	03,9 00,8	03,9 00,8	03,9 00,8	03,9 00,8	03,9 01,0	4
5	04,9 00,8	04,9 00,9	04,9 01,0	04,9 01,0	04,9 01,0	04,8 01,2	5
6	05,9 01,0	05,9 01,1	05,9 01,2	05,9 01,3	05,9 01,3	05,8 01,4	6
7	06,9 01,2	06,9 01,3	06,9 01,4	06,8 01,5	06,8 01,6	06,8 01,7	7
8	07,9 01,4	07,8 01,5	07,8 01,6	07,8 01,7	07,8 01,8	07,8 01,9	8
9	08,9 01,6	08,8 01,7	08,8 01,8	08,8 01,9	08,8 02,0	08,7 02,2	9
10	09,8 01,7	09,8 01,9	09,8 02,0	09,8 02,1	09,7 02,3	09,7 02,4	10
11	10,8 01,9	10,8 02,1	10,8 02,1	10,8 02,3	10,7 02,5	10,7 02,7	11
12	11,8 02,1	11,8 02,4	11,8 02,3	11,7 02,5	11,7 02,7	11,6 02,9	12
13	12,8 02,2	12,8 02,5	12,7 02,5	12,7 02,7	12,7 02,8	12,6 03,1	13
14	13,8 02,4	13,7 02,7	13,7 02,7	13,7 02,9	13,6 03,1	13,6 03,3	14
15	14,8 02,6	14,7 02,9	14,7 02,9	14,7 03,1	14,6 03,3	14,5 03,6	15
16	15,7 02,8	15,7 03,0	15,7 03,1	15,6 03,3	15,6 03,6	15,5 03,9	16
17	16,7 02,5	16,7 03,2	16,6 03,3	16,6 03,5	16,6 05,8	16,5 04,2	17
18	17,7 03,3	17,7 03,4	17,7 03,6	17,6 03,7	17,5 04,0	17,5 04,4	18
19	18,7 03,5	18,6 03,6	18,6 03,7	18,6 03,9	18,5 04,2	18,4 04,6	19
20	19,7 03,5	19,6 03,8	19,6 03,9	19,6 04,2	19,5 04,5	19,4 04,8	20
21	20,7 03,6	20,6 04,1	20,6 04,1	20,5 04,4	20,5 04,7	20,4 05,1	21
22	21,7 03,8	21,6 04,2	21,6 04,3	21,5 04,6	21,4 04,9	21,3 05,3	22
23	22,6 04,0	22,6 04,4	22,6 04,5	22,5 04,8	22,4 05,2	22,3 05,6	23
24	23,6 04,2	23,6 04,6	23,5 04,7	23,5 05,0	23,4 05,4	23,3 05,8	24
25	24,6 04,5	24,5 04,8	24,5 04,9	24,4 05,2	24,4 05,6	24,3 06,0	25
26	25,6 04,5	25,5 05,0	25,5 05,1	25,4 05,4	25,3 05,8	25,2 06,3	26
27	26,6 04,7	26,5 05,1	26,5 05,3	26,4 05,6	26,3 06,1	26,2 06,5	27
28	27,6 04,9	27,5 05,3	27,4 05,5	27,4 05,8	27,3 06,3	27,2 06,8	28
29	28,6 05,0	28,5 05,5	28,4 05,7	28,4 06,0	28,3 06,5	28,1 07,0	29
30	29,5 05,2	29,4 05,7	29,4 05,8	29,3 06,2	29,2 06,7	29,1 07,3	30
31	30,5 05,4	30,4 06,0	30,4 06,0	30,3 06,4	30,2 07,0	30,1 07,5	31
32	31,5 05,5	31,4 06,1	31,4 06,2	31,3 06,6	31,2 07,2	31,0 07,7	32
33	32,5 05,7	32,4 06,3	32,4 06,4	32,3 06,8	32,1 07,4	32,0 08,0	33
34	33,5 05,9	33,4 06,5	33,4 06,6	33,3 07,1	33,1 07,6	33,0 08,2	34
35	34,5 06,1	34,4 06,7	34,4 06,9	34,2 07,2	34,1 07,9	34,0 08,5	35
36	35,4 06,2	35,3 06,9	35,3 07,0	35,2 07,5	35,1 08,1	34,9 08,7	36
37	36,4 06,4	36,3 07,1	36,3 07,2	36,2 07,7	36,0 08,3	35,9 09,0	37
38	37,4 06,6	37,3 07,2	37,3 07,4	37,2 07,9	37,0 08,5	36,9 09,2	38
39	38,4 06,8	38,3 07,4	38,2 07,6	38,1 08,1	38,0 08,9	37,8 09,4	39
40	39,4 06,9	39,3 07,6	39,2 07,8	39,1 08,3	39,0 09,0	38,8 09,7	40
41	40,4 07,1	40,2 07,8	40,2 08,0	40,1 08,5	39,9 09,2	39,8 09,9	41
42	41,4 07,3	41,2 08,0	41,1 08,2	41,1 08,7	40,9 09,4	40,7 09,7	42
43	42,3 07,5	42,2 08,2	42,1 08,4	42,1 08,9	41,9 09,7	41,7 09,9	43
44	43,3 07,7	43,2 08,4	43,1 08,6	43,0 09,1	42,9 09,9	42,7 09,9	44
45	44,3 07,8	44,2 08,6	44,1 08,8	44,0 09,4	43,8 10,1	43,7 11,0	45
46	45,3 08,0	45,2 08,8	45,1 09,0	45,0 09,6	44,8 10,3	44,6 11,2	46
47	46,3 08,1	46,1 09,0	46,1 09,2	46,0 09,8	45,8 10,6	45,6 11,4	47
48	47,3 08,3	47,1 09,2	47,1 09,4	47,0 10,0	46,7 10,8	46,6 11,6	48
49	48,3 08,5	48,1 09,3	48,1 09,6	48,0 10,2	47,7 11,0	47,5 11,9	49
50	49,3 08,7	49,0 09,5	49,0 09,8	49,0 10,4	48,7 11,2	48,5 12,1	50
Dif.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dif.
78	80 Deg.	79 Deg.	7 Point	78 Deg.	77 Deg.	76 Deg.	77

## of Latitude and Departure.

185

	10 Deg.	11 Deg.	1 Point	12 Deg.	13 Deg.	14 Deg.	Dif.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.2	08.8	50.1	09.7	50.0	10.0	49.7
52	51.2	09.0	51.0	09.9	51.0	10.1	50.7
53	52.2	09.2	52.0	10.1	52.0	10.3	51.8
54	53.2	09.4	53.0	10.3	53.0	10.5	52.8
55	54.2	09.5	54.0	10.5	53.9	10.7	53.8
56	55.1	09.7	55.0	10.7	54.9	10.9	54.8
57	56.1	09.9	56.0	10.8	55.9	11.1	55.8
58	57.1	10.1	56.9	11.1	56.9	11.3	56.7
59	58.1	10.2	57.9	11.3	57.9	11.5	57.7
60	59.1	10.4	58.9	11.4	58.8	11.7	58.7
61	60.1	10.6	59.9	11.6	59.8	11.9	59.7
62	61.1	10.8	60.9	11.8	60.8	12.1	60.6
63	62.0	10.9	61.8	12.0	61.8	12.3	61.6
64	63.0	11.1	62.8	12.2	62.8	12.5	62.6
65	64.0	11.3	63.8	12.4	63.7	12.7	63.6
66	65.0	11.5	64.8	12.6	64.7	12.9	64.5
67	66.0	11.6	65.8	12.8	65.7	13.1	65.5
68	67.0	11.8	66.7	13.0	66.7	13.3	66.5
69	68.0	12.0	67.7	13.2	67.7	13.5	67.5
70	68.9	12.2	68.7	13.4	68.7	13.7	68.5
71	69.9	12.3	69.7	13.5	69.6	13.9	69.4
72	70.9	12.5	70.7	13.7	70.6	14.0	70.4
73	71.9	12.7	71.7	13.9	71.6	14.2	71.4
74	72.9	12.8	72.6	14.1	72.5	14.4	72.4
75	73.9	13.0	73.6	14.3	73.5	14.6	73.4
76	74.8	13.2	74.6	14.5	74.5	14.8	74.3
77	75.8	13.4	75.6	14.7	75.5	15.0	75.3
78	76.8	13.5	76.6	14.9	76.5	15.2	76.3
79	77.8	13.7	77.5	15.1	77.5	15.4	77.3
80	78.8	13.9	78.5	15.3	78.5	15.6	78.2
81	79.8	14.5	79.5	15.5	79.4	15.8	79.2
82	80.8	14.2	80.5	15.6	80.4	16.0	80.2
83	81.7	14.4	81.5	15.8	81.4	16.2	81.2
84	82.7	14.6	82.5	16.0	82.4	16.4	82.2
85	83.7	14.8	83.4	16.2	83.4	16.6	83.2
86	84.7	14.9	84.4	16.4	84.3	16.8	84.2
87	85.7	15.1	85.4	16.6	85.3	17.0	85.1
88	86.7	15.3	86.4	16.8	86.3	17.2	86.1
89	87.6	15.4	87.4	17.0	87.3	17.4	87.1
90	88.6	15.6	88.3	17.2	88.3	17.6	88.0
91	89.6	15.8	89.3	17.4	89.2	17.7	89.0
92	90.6	16.0	90.3	17.6	90.2	17.9	90.0
93	91.6	16.1	91.3	17.7	91.2	18.1	91.0
94	92.6	16.3	92.3	17.9	92.2	18.3	92.0
95	93.5	16.5	93.3	18.1	93.2	18.5	92.9
96	94.5	16.7	94.2	18.3	94.2	18.7	93.9
97	95.5	16.8	95.2	18.5	95.1	18.9	94.9
98	96.5	17.0	96.6	18.7	96.1	19.1	95.9
99	97.5	17.2	97.2	18.9	97.1	19.3	96.8
100	98.5	17.4	98.2	19.1	98.1	19.5	97.8
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
	80 Deg.	79 Deg.	7 Point.	78 Deg.	77 Deg.	76 Deg.	Dif.

Diff.	18 Deg.	17 Deg.	16 Deg.	15 Deg.	14 Point	Diff.						
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	01.0	00.2	01.0	00.3	01.0	00.3	01.0	00.3	01.0	00.3	00.9	00.3
2	01.9	00.5	01.9	00.5	01.9	00.5	01.9	00.6	01.9	00.6	01.9	00.6
3	02.9	00.7	02.9	00.9	02.9	00.8	02.9	00.9	02.9	00.9	02.8	00.9
4	03.9	01.0	03.9	01.0	03.9	01.1	03.8	01.1	03.8	01.1	03.8	01.2
5	04.8	01.2	04.8	01.3	04.8	01.3	04.8	01.5	04.8	01.5	04.8	01.5
6	05.8	01.5	05.8	01.5	05.8	01.6	05.8	01.7	05.7	01.7	05.7	01.8
7	06.8	01.7	06.8	01.8	06.8	01.9	06.8	02.0	06.7	02.0	06.7	02.1
8	07.8	01.9	07.7	02.1	07.7	02.2	07.7	02.3	07.6	02.3	07.6	02.5
9	08.7	02.2	08.7	02.3	08.6	02.5	08.6	02.6	08.6	02.6	08.6	02.8
10	09.7	02.4	09.7	02.6	09.6	02.8	09.6	02.9	09.6	02.9	09.5	03.1
11	10.7	02.6	10.6	02.8	10.6	03.0	10.5	03.2	10.5	03.2	10.5	03.4
12	11.6	02.9	11.6	03.1	11.5	03.3	11.5	03.5	11.5	03.5	11.4	03.7
13	12.6	03.2	12.6	03.4	12.5	03.6	12.4	03.8	12.4	03.8	12.4	04.0
14	13.6	03.4	13.5	03.6	13.5	03.9	13.4	04.1	13.4	04.1	13.3	04.3
15	14.5	03.6	14.5	03.9	14.4	04.1	14.4	04.4	14.3	04.4	14.3	04.6
16	15.5	04.0	15.5	04.1	15.4	04.4	15.3	04.6	15.3	04.7	15.2	04.9
17	16.5	04.1	16.4	04.4	16.3	04.7	16.3	04.9	16.3	05.0	16.2	05.2
18	17.5	04.4	17.4	04.7	17.3	05.0	17.2	05.2	17.2	05.3	17.1	05.6
19	18.4	04.6	18.4	04.9	18.3	05.2	18.2	05.5	18.2	05.5	18.1	05.9
20	19.4	04.9	19.3	05.2	19.2	05.5	19.1	05.8	19.1	05.8	19.0	06.1
21	20.4	05.1	20.3	05.4	20.2	05.8	20.1	06.1	20.1	06.1	20.0	06.5
22	21.3	05.4	21.2	05.7	21.1	06.1	21.0	06.4	21.1	06.4	20.9	06.8
23	22.3	05.6	22.2	06.0	22.1	06.3	22.0	06.7	22.0	06.7	21.9	07.1
24	23.3	05.8	23.2	06.2	23.1	06.6	23.0	06.8	22.9	07.0	22.8	07.4
25	24.2	06.0	24.1	06.5	24.0	06.9	23.9	07.3	23.9	07.3	23.8	07.7
26	25.2	06.3	25.1	06.7	24.9	07.2	24.9	07.5	24.9	07.6	24.7	08.0
27	26.2	06.6	26.1	07.0	25.9	07.4	25.8	07.8	25.8	07.9	25.7	08.3
28	27.2	06.8	27.0	07.2	26.9	07.7	26.8	08.1	26.8	08.2	26.6	08.6
29	28.1	07.0	28.0	07.5	27.8	08.0	27.8	08.4	27.7	08.5	27.6	09.0
30	29.1	07.3	29.0	07.9	28.8	08.3	28.7	08.7	28.7	08.8	28.5	09.3
31	30.1	07.5	29.9	08.0	29.8	08.5	29.7	09.0	29.6	09.1	29.5	09.6
32	31.0	07.9	30.9	08.3	30.7	08.8	30.6	09.3	30.6	09.3	30.4	10.0
33	32.0	08.0	31.9	08.5	31.7	09.1	31.6	09.6	31.6	09.6	31.4	10.2
34	33.0	08.3	32.8	08.9	32.7	09.4	32.5	09.9	32.5	09.9	32.3	10.5
35	33.9	08.5	33.8	09.0	33.6	09.6	33.5	10.2	33.5	10.2	33.3	10.8
36	34.9	08.7	34.8	09.3	34.6	09.9	34.4	10.4	34.4	10.5	34.2	11.1
37	35.9	09.0	35.7	09.6	35.6	10.2	35.4	10.7	35.4	10.8	35.2	11.4
38	36.9	09.2	36.7	09.8	36.5	10.5	36.4	11.0	36.3	11.1	36.1	11.7
39	37.8	09.5	37.7	10.1	37.5	10.7	37.3	11.3	37.3	11.4	37.1	12.0
40	38.8	09.7	38.6	10.3	38.4	11.0	38.3	11.6	38.2	11.7	38.0	12.4
41	39.8	10.0	39.6	10.6	39.4	11.3	39.2	11.9	39.2	12.0	39.0	12.7
42	40.7	10.2	40.6	10.9	40.4	11.6	40.2	12.2	40.2	12.3	39.9	13.0
43	41.7	10.4	41.5	11.1	41.3	11.8	41.1	12.5	41.1	12.6	40.9	13.3
44	42.7	10.7	42.5	11.5	42.3	12.1	42.1	12.8	42.1	12.9	41.8	13.6
45	43.6	10.9	43.5	11.7	43.3	12.4	43.1	13.1	43.0	13.1	42.8	13.9
46	44.6	11.2	44.4	11.9	44.2	12.7	44.0	13.3	44.0	13.4	43.7	14.2
47	45.6	11.4	45.4	12.2	45.2	12.9	45.0	13.6	44.9	13.7	44.7	14.5
48	46.5	11.7	46.4	12.4	46.1	13.3	45.9	13.9	45.9	14.0	45.6	14.8
49	47.5	11.8	47.1	12.7	47.1	13.5	46.9	14.2	46.9	14.3	46.6	15.1
50	48.5	12.1	48.3	12.9	48.1	13.8	47.8	14.5	47.8	14.6	47.5	15.4
Dif.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
6 <sup>2</sup>	Point.	75 Deg.	74 Deg.	74 Point.	73	Deg.	72	Deg.	72	Deg.	71	Deg.

	$\frac{1}{2}$ Point	15 Deg.	16 Deg.	$\frac{1}{2}$ Point	17 Deg.	18 Deg.	D.						
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.						
51	+9.5	12.4	49.2	13.2	+9.0	14.0	48.8	14.8	+8.8	14.9	48.5	15.8	51
52	50.4	12.6	50.2	13.5	+9.9	14.3	49.7	15.0	+9.7	15.2	49.4	16.1	52
53	51.4	12.9	51.2	13.7	50.9	14.6	50.7	15.4	50.7	15.5	50.4	16.4	53
54	52.4	13.1	52.2	14.0	51.9	14.9	51.7	15.7	51.6	15.8	51.3	16.7	54
55	53.3	13.4	53.1	14.2	52.9	15.2	52.6	16.0	52.6	16.1	52.3	17.0	55
56	54.3	13.6	54.1	14.5	53.8	15.4	53.6	16.2	53.8	16.4	53.3	17.3	56
57	55.3	13.8	55.1	14.8	54.8	15.7	54.5	16.5	54.5	16.7	54.2	17.6	57
58	56.3	14.0	56.1	15.0	55.7	16.0	55.5	16.8	55.5	17.0	55.2	17.9	58
59	57.3	14.3	57.0	15.3	56.3	16.3	56.5	17.1	56.5	17.2	56.1	18.2	59
60	58.2	14.6	58.0	15.5	57.7	16.5	57.4	17.4	57.4	17.5	57.1	18.5	60
61	59.2	14.8	58.9	15.8	58.6	16.8	58.4	17.7	58.4	17.8	58.0	18.8	61
62	60.1	15.1	59.9	16.1	59.6	17.1	59.3	18.0	59.3	18.1	59.0	19.1	62
63	61.1	15.3	60.8	16.3	60.5	17.4	60.3	18.3	60.2	18.4	59.9	19.5	63
64	62.1	15.5	61.8	16.6	61.5	17.6	61.2	18.6	61.2	18.7	60.9	19.8	64
65	63.0	15.8	62.9	16.8	62.5	17.9	62.2	18.9	62.2	19.0	61.8	20.1	65
66	64.0	16.0	63.7	17.1	63.4	18.2	63.1	19.1	63.1	19.3	62.8	20.4	66
67	65.0	16.3	64.7	17.4	64.4	18.5	64.1	19.4	64.1	19.6	63.7	20.7	67
68	66.0	16.5	65.7	17.6	65.4	18.7	65.1	19.7	65.1	19.9	64.4	21.0	68
69	66.9	16.8	66.6	17.9	66.3	19.0	66.0	20.0	66.0	20.2	65.6	21.3	69
70	67.9	17.0	67.6	18.1	67.3	19.3	67.0	20.3	66.9	20.5	66.6	21.6	70
71	68.9	17.2	68.6	18.3	68.4	19.6	67.9	20.6	67.9	20.8	67.5	21.9	71
72	69.8	17.5	69.5	18.6	69.2	19.8	68.9	20.9	68.8	21.0	68.5	22.2	72
73	70.8	17.7	70.5	18.9	70.2	20.1	69.8	21.2	69.8	21.3	69.4	22.6	73
74	71.8	18.0	71.5	19.1	71.1	20.4	70.8	21.5	70.8	21.6	70.4	22.9	74
75	72.7	18.2	72.4	19.4	72.1	20.7	71.6	21.8	71.7	21.9	71.3	23.2	75
76	73.7	18.5	73.4	19.7	73.0	20.9	72.7	22.1	72.7	22.1	72.3	23.5	76
77	74.7	18.7	74.4	19.9	74.0	21.2	73.7	22.3	73.6	22.4	73.2	23.8	77
78	75.7	18.9	75.3	20.2	75.0	21.5	74.6	22.6	74.6	22.8	74.2	24.1	78
79	76.6	19.2	76.3	20.4	75.9	21.8	75.6	22.9	75.5	23.1	75.1	24.4	79
80	77.6	19.4	77.3	20.7	76.9	22.0	76.6	23.2	76.5	23.4	76.1	24.7	80
81	78.6	19.7	78.2	21.0	77.9	22.3	77.5	23.5	77.5	23.7	77.0	25.0	81
82	79.5	19.9	79.1	21.2	78.8	22.6	78.4	23.8	78.4	24.0	78.0	25.3	82
83	80.5	20.2	80.2	21.5	79.8	23.5	79.4	24.1	79.4	24.3	78.9	25.6	83
84	81.5	20.4	81.1	21.7	80.8	23.1	80.3	24.4	80.3	24.5	79.9	26.0	84
85	82.4	20.7	82.1	22.0	81.7	23.2	81.4	24.4	81.3	24.6	80.8	26.3	85
86	83.4	20.9	83.1	22.2	82.7	23.7	82.3	25.0	82.2	25.1	81.8	26.6	86
87	84.4	21.4	84.0	22.5	83.6	24.0	83.3	25.2	83.2	25.4	82.7	26.9	87
88	85.4	21.6	85.0	22.8	84.6	24.2	84.2	25.5	84.1	25.6	83.7	27.2	88
89	86.3	21.8	86.0	23.0	85.6	24.5	85.2	25.8	85.1	26.0	84.6	27.5	89
90	87.3	22.0	86.4	23.3	86.5	24.8	86.1	26.1	86.1	26.5	85.6	27.8	90
91	88.3	22.1	87.	23.5	87.5	25.1	87.1	26.4	87.0	26.6	86.5	28.1	91
92	89.2	22.4	88.5	23.8	88.4	25.3	88.5	26.7	88.0	26.9	87.5	28.4	92
93	90.2	22.6	89.8	24.1	89.4	25.5	89.0	27.0	88.9	27.2	88.4	28.7	93
94	91.2	22.8	90.8	24.3	90.4	25.9	90.0	27.3	89.9	27.5	89.4	29.0	94
95	92.1	23.1	91.8	24.6	91.2	26.2	90.9	27.6	90.8	27.8	90.3	29.3	95
96	93.1	23.3	92.7	24.8	92.3	26.4	91.9	27.9	91.8	28.1	91.3	29.7	96
97	94.1	23.6	93.7	25.1	93.2	26.7	92.8	28.2	92.8	28.4	92.3	30.0	97
98	95.1	23.8	94.7	25.4	94.2	27.0	93.8	28.4	93.7	28.6	93.2	30.3	98
99	96.0	24.1	95.6	25.6	95.2	27.3	94.7	28.7	94.7	28.9	94.2	30.6	99
100	97.0	24.7	96.6	25.9	96.1	27.6	95.7	29.0	95.6	29.2	95.1	30.9	100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
	15 Point	75 Deg.	74 Deg.	1/2 Point	73 Deg.	72 Deg.							

Diff.	19 Deg.				1½ Points		20 Deg.				21 Deg.		22 Deg.				2 Points		Diff.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	00.9	00.3	00.9	00.3	00.5	00.3	00.9	00.4	00.5	00.4	00.9	00.4	00.9	00.4	00.9	00.4	00.9	00.4	1
2	01.9	00.6	01.9	00.7	01.5	00.7	01.9	00.7	01.8	00.7	01.8	00.7	01.8	00.8	00.7	01.8	00.8	00.8	2
3	02.8	01.0	02.8	01.0	02.8	01.0	02.8	01.0	02.8	01.0	02.8	01.1	02.8	01.1	02.8	01.1	02.8	01.1	3
4	03.8	01.3	03.8	01.3	03.8	01.4	03.7	01.4	03.7	01.4	03.7	01.5	03.7	01.5	03.7	01.5	03.7	01.5	4
5	04.7	01.6	04.7	01.7	04.7	01.7	04.7	01.7	04.7	01.8	04.6	01.9	04.6	01.9	04.6	01.9	04.6	01.9	5
6	05.5	01.9	05.6	02.0	05.6	02.0	05.6	02.1	05.6	02.2	05.5	02.3	05.5	02.3	05.5	02.3	05.5	02.3	6
7	06.6	02.3	06.6	02.4	06.6	02.4	06.5	02.5	06.5	02.6	06.5	02.7	06.5	02.7	06.5	02.7	06.5	02.7	7
8	07.6	02.6	07.5	02.7	07.5	02.7	07.5	02.9	07.4	03.0	07.4	03.1	07.4	03.1	07.4	03.1	07.4	03.1	8
9	08.5	02.9	08.5	03.0	08.5	03.1	08.4	03.2	08.3	03.4	08.3	03.4	08.3	03.4	08.3	03.4	08.3	03.4	9
10	09.5	03.3	09.4	03.4	09.4	03.4	09.3	03.6	09.2	03.7	09.2	03.8	09.2	03.8	09.2	03.8	09.2	03.8	10
11	10.4	03.6	10.4	03.7	10.3	03.8	10.3	03.9	10.2	04.1	10.2	04.1	10.2	04.1	10.2	04.1	10.2	11	
12	11.3	03.9	11.3	04.0	11.3	04.7	11.2	04.5	11.1	04.5	11.1	04.6	11.1	04.6	11.1	04.6	11.1	04.6	12
13	12.3	04.2	12.2	04.1	12.2	04.1	12.1	04.7	12.0	04.0	12.0	05.0	12.0	05.0	12.0	05.0	12.0	05.0	13
14	13.2	04.6	13.2	04.7	13.2	04.8	13.1	05.0	13.0	05.2	12.9	05.4	12.9	05.4	12.9	05.4	12.9	05.4	14
15	14.2	04.9	14.1	05.1	14.1	05.1	14.0	05.4	13.9	05.6	13.9	05.7	13.9	05.7	13.9	05.7	13.9	05.7	15
16	15.1	05.2	15.1	05.4	15.0	05.4	14.9	05.7	14.8	06.0	14.8	06.1	14.8	06.1	14.8	06.1	14.8	06.1	16
17	16.1	05.6	16.0	05.7	16.0	05.8	15.9	06.1	15.8	06.4	15.7	06.5	15.7	06.5	15.7	06.5	15.7	06.5	17
18	17.0	05.9	16.9	06.1	16.9	06.3	16.8	06.4	16.7	06.7	16.6	06.8	16.6	06.8	16.6	06.8	16.6	06.8	18
19	18.0	06.1	17.9	06.4	17.9	06.5	17.7	06.8	17.6	07.1	17.6	07.3	17.6	07.3	17.6	07.3	17.6	07.3	19
20	18.9	06.5	18.9	06.7	18.8	06.8	18.7	07.2	18.5	07.5	18.5	07.6	18.5	07.6	18.5	07.6	18.5	07.6	20
21	19.9	06.8	19.7	07.1	19.7	07.2	19.6	07.5	19.5	07.9	19.4	08.0	19.4	08.0	19.4	08.0	19.4	08.0	21
22	20.8	07.2	20.7	07.4	20.7	07.5	20.5	07.9	20.4	08.2	20.3	08.4	20.3	08.4	20.3	08.4	20.3	08.4	22
23	21.7	07.5	21.7	07.7	21.6	07.9	21.5	08.2	21.3	08.6	21.2	08.8	21.2	08.8	21.2	08.8	21.2	08.8	23
24	22.7	07.8	22.6	08.1	22.5	08.2	22.4	08.6	22.2	09.0	22.2	09.1	22.2	09.1	22.2	09.1	22.2	09.1	24
25	23.6	08.1	23.5	08.4	23.5	08.5	23.3	09.0	23.2	09.4	23.1	09.6	23.1	09.6	23.1	09.6	23.1	09.6	25
26	24.6	08.5	24.5	08.8	24.4	08.9	24.3	09.3	24.1	09.7	24.0	09.9	24.0	09.9	24.0	09.9	24.0	09.9	26
27	25.5	08.8	25.4	09.1	25.4	09.2	25.2	09.7	25.0	10.1	24.9	10.3	24.9	10.3	24.9	10.3	24.9	10.3	27
28	26.5	09.1	26.4	09.4	26.2	09.6	26.1	10.0	26.0	10.5	25.9	10.7	25.9	10.7	25.9	10.7	25.9	10.7	28
29	27.4	09.4	27.3	09.8	27.3	09.9	27.1	10.4	26.9	10.9	26.8	11.1	26.8	11.1	26.8	11.1	26.8	11.1	29
30	28.4	09.8	28.2	10.1	28.2	10.3	28.0	10.7	27.8	11.1	27.7	11.5	27.7	11.5	27.7	11.5	27.7	11.5	30
31	29.3	10.1	29.2	10.4	29.1	10.6	28.9	11.1	28.7	11.6	28.6	11.9	28.6	11.9	28.6	11.9	28.6	11.9	31
32	30.3	10.4	30.1	10.8	30.1	10.9	29.9	11.5	29.7	12.0	29.6	12.1	29.6	12.1	29.6	12.1	29.6	12.1	32
33	31.2	10.7	31.1	11.1	31.1	11.3	30.8	11.8	30.6	12.4	30.5	12.6	30.5	12.6	30.5	12.6	30.5	12.6	33
34	32.1	11.1	32.0	11.5	32.0	11.6	31.8	12.2	31.5	12.7	31.4	13.0	31.4	13.0	31.4	13.0	31.4	13.0	34
35	33.1	11.4	33.0	11.8	32.9	12.0	32.7	12.5	32.4	13.1	32.3	13.4	32.3	13.4	32.3	13.4	32.3	13.4	35
36	34.0	11.7	33.9	12.1	33.8	12.3	33.6	12.9	33.4	13.5	33.3	13.8	33.3	13.8	33.3	13.8	33.3	13.8	36
37	35.0	12.1	34.8	12.5	34.7	12.6	34.5	13.3	34.3	13.9	34.2	14.2	34.2	14.2	34.2	14.2	34.2	14.2	37
38	35.9	12.4	35.8	12.8	35.7	13.0	35.5	13.6	35.2	14.2	35.1	14.5	35.1	14.5	35.1	14.5	35.1	14.5	38
39	36.9	12.8	36.7	13.1	36.6	13.3	36.4	14.0	36.2	14.6	36.1	14.9	36.0	14.9	36.0	14.9	36.0	14.9	39
40	37.8	13.0	37.7	13.5	37.6	13.7	37.3	14.3	37.1	15.0	36.9	15.3	36.9	15.3	36.9	15.3	36.9	15.3	40
41	38.8	13.3	38.6	13.8	38.5	14.0	38.3	14.7	38.0	15.3	37.9	15.7	37.9	15.7	37.9	15.7	37.9	15.7	41
42	39.7	13.7	39.5	14.1	39.5	14.4	39.2	15.1	38.9	15.7	38.8	16.1	38.8	16.1	38.8	16.1	38.8	16.1	42
43	40.7	14.0	40.5	14.5	40.4	14.7	40.1	15.4	39.9	16.1	39.7	16.5	39.7	16.5	39.7	16.5	39.7	16.5	43
44	41.7	14.3	41.4	14.8	41.3	15.1	41.1	15.8	40.8	16.5	40.6	16.8	40.6	16.8	40.6	16.8	40.6	16.8	44
45	42.6	14.6	42.4	15.2	42.2	15.5	42.0	16.1	41.7	16.8	41.5	17.2	41.5	17.2	41.5	17.2	41.5	17.2	45
46	43.5	15.0	43.3	15.5	43.3	15.7	42.9	16.5	42.6	17.2	42.5	17.5	42.5	17.5	42.5	17.5	42.5	17.5	46
47	44.4	15.3	44.2	15.8	44.2	16.1	43.9	16.8	43.6	17.5	43.5	17.8	43.5	17.8	43.5	17.8	43.5	17.8	47
48	45.4	15.6	45.2	16.2	45.1	16.4	44.8	17.2	44.5	17.9	44.3	18.2	44.3	18.2	44.3	18.2	44.3	18.2	48
49	46.3	15.9	46.1	16.5	46.0	16.8	45.7	17.6	45.4	18.3	45.2	18.7	45.2	18.7	45.2	18.7	45.2	18.7	49
50	47.5	16.3	47.1	16.8	47.0	17.1	46.7	17.9	46.4	18.6	46.2	19.2	46.2	19.2	46.2	19.2	46.2	19.2	50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
	7	1	Deg.	6	1	Point	7	0	Deg.	6	9	Deg.	6	8	Deg.	6	6	Points.	

	19 Deg	18 Point	20 Deg	21 Deg	22 Deg	2 Points	Dif.						
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.					
51	48,2	16,6	48,0	17,1	47,9	17,4	47,6	18,3	47,3	19,1	47,1	19,5	\$1
52	49,2	16,9	49,0	17,5	48,9	17,8	48,5	18,0	48,2	19,4	48,0	19,9	\$2
53	50,1	17,3	49,9	17,9	49,8	18,1	49,5	19,0	49,1	19,8	49,0	20,3	\$3
54	51,1	17,6	50,8	18,2	50,7	18,5	50,4	19,3	50,1	20,2	49,9	20,7	\$4
55	52,0	17,9	51,8	18,5	51,7	18,8	51,3	19,7	51,0	20,6	50,8	21,0	\$5
56	52,9	18,2	52,7	19,9	52,6	19,7	52,3	20,1	51,9	21,0	51,7	21,4	\$6
57	53,0	18,6	53,7	19,2	53,6	19,5	53,2	20,4	52,8	21,3	52,7	21,8	\$7
58	54,8	18,9	54,6	19,5	54,5	19,8	54,1	20,8	53,8	21,7	53,6	22,2	\$8
59	55,7	19,2	55,5	19,9	55,4	20,2	55,1	21,1	54,9	22,1	54,5	22,6	\$9
60	56,7	19,6	56,5	20,2	56,4	20,5	56,1	21,5	55,6	22,5	55,4	23,0	\$10
61	57,7	19,9	57,4	20,5	57,3	20,9	56,9	21,9	56,5	22,8	56,3	23,3	\$11
62	58,5	20,2	58,4	20,9	58,3	21,0	57,9	22,3	57,5	23,2	57,3	23,7	\$12
63	59,6	20,5	59,3	21,2	59,2	21,5	58,8	22,6	58,4	23,6	58,2	24,1	\$13
64	60,5	20,8	60,3	21,6	60,1	21,9	59,7	22,9	59,3	24,0	59,1	24,5	\$14
65	61,5	21,1	61,2	21,9	61,1	22,2	60,7	23,3	60,3	24,3	60,0	24,9	\$15
66	62,4	21,5	62,1	22,2	62,0	22,6	61,6	23,6	61,2	24,7	61,0	25,3	\$16
67	63,3	21,8	63,1	22,6	63,0	22,9	62,5	24,0	62,1	25,1	61,9	25,6	\$17
68	64,3	22,1	64,0	22,9	63,9	23,3	63,5	24,4	63,0	25,5	62,8	26,0	\$18
69	65,2	22,5	65,0	23,2	64,8	23,6	64,4	24,7	64,0	25,8	63,7	26,4	\$19
70	66,1	22,8	65,9	23,6	65,8	23,9	65,3	25,1	64,9	26,2	64,7	26,8	\$20
71	67,1	23,1	66,8	23,9	66,7	24,2	66,3	25,4	65,8	26,6	65,6	27,2	\$21
72	68,1	23,4	67,8	24,2	67,7	24,6	67,2	25,8	66,7	27,0	66,5	27,6	\$22
73	69,0	23,8	68,7	24,6	68,6	25,0	68,1	26,2	67,7	27,3	67,4	27,9	\$23
74	70,0	24,1	69,7	24,9	69,5	25,3	69,1	26,5	68,6	27,7	68,4	28,3	\$24
75	70,9	24,4	70,6	25,3	70,5	25,6	70,0	26,9	69,5	28,1	69,3	28,7	\$25
76	71,9	24,7	71,5	25,6	71,4	26,0	70,9	27,2	70,5	28,5	70,2	29,1	\$26
77	72,8	25,1	72,5	25,9	72,4	26,3	71,9	27,6	71,4	28,8	71,1	29,5	\$27
78	73,7	25,4	73,4	26,3	73,3	26,7	72,8	27,9	72,3	29,2	72,1	29,8	\$28
79	74,7	25,7	74,4	26,6	74,2	27,0	73,7	28,3	73,2	29,6	73,0	30,2	\$29
80	75,6	26,0	75,3	26,9	75,1	27,5	74,7	28,7	74,2	30,0	73,9	30,6	\$30
81	76,6	26,4	76,3	27,3	76,1	27,7	75,0	29,0	75,1	30,3	74,8	31,0	\$31
82	77,5	26,7	77,2	27,6	77,1	28,0	76,5	29,4	76,0	30,7	75,8	31,4	\$32
83	78,5	27,1	78,1	28,0	78,0	28,4	77,5	29,7	76,9	31,1	76,7	31,8	\$33
84	79,4	27,4	79,1	28,3	78,0	28,7	78,4	30,1	77,9	31,5	77,6	32,1	\$34
85	80,4	27,7	80,1	28,6	79,9	29,1	79,3	30,5	78,8	31,8	78,6	32,5	\$35
86	81,3	28,0	81,0	29,0	80,8	29,4	80,3	30,8	79,7	32,2	79,4	33,0	\$36
87	82,3	28,3	81,9	29,3	81,8	29,7	81,2	31,2	80,7	32,6	80,4	33,3	\$37
88	83,2	28,6	82,8	29,6	82,7	30,1	81,1	31,5	81,0	33,0	81,3	33,7	\$38
89	84,1	29,0	83,8	30,0	83,6	30,4	83,1	31,9	82,5	33,3	82,2	34,1	\$39
90	85,1	29,3	84,7	30,2	84,0	30,8	84,0	32,3	83,4	33,7	83,1	34,4	\$40
91	85,0	29,6	85,7	30,7	85,5	31,1	84,9	32,6	84,4	34,1	84,1	34,8	\$41
92	87,0	29,9	86,5	31,0	86,4	31,5	85,9	33,0	85,3	34,5	85,0	35,2	\$42
93	88,0	30,3	87,6	31,3	87,4	31,8	86,8	33,3	86,2	34,8	85,9	35,6	\$43
94	88,9	30,6	88,5	31,7	88,3	32,1	87,7	33,7	87,2	35,2	86,8	36,0	\$44
95	89,8	30,9	89,4	32,0	89,3	32,5	88,7	34,0	88,1	35,6	87,8	36,3	\$45
96	90,4	31,3	90,4	32,1	90,2	32,9	89,6	34,4	89,0	35,9	88,7	36,7	\$46
97	91,7	31,6	91,5	32,7	91,1	33,2	90,5	34,8	89,9	36,3	89,6	37,1	\$47
98	91,7	31,9	92,3	33,0	92,1	33,5	91,5	35,1	90,9	36,7	90,5	37,5	\$48
99	93,6	32,7	93,2	33,3	93,0	33,9	92,4	35,5	91,8	37,1	91,5	37,9	\$49
100	94,5	32,9	94,2	33,7	94,0	34,2	93,4	35,8	92,7	37,5	92,4	38,3	\$50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dif.
	71 Deg.	6 1/2 Point	70 Deg.	6 9 Deg.	6 8 Deg.	6 Points							

## A TABLE of Difference

D.	23 Deg.		24 Deg.		25 Deg.		26 Deg.		27 Deg.		D.
	Lat.	Dep.									
1	100.9	00.4	100.9	00.4	100.9	00.4	100.9	00.4	100.9	00.4	1
2	201.8	00.8	201.8	00.8	201.8	00.8	201.8	00.8	201.8	00.8	2
3	302.8	01.2	302.7	01.2	302.7	01.2	302.7	01.2	302.7	01.2	3
4	403.7	01.6	403.6	01.6	403.6	01.7	403.6	01.7	403.6	01.8	4
5	504.6	01.9	504.6	02.0	504.5	02.1	504.5	02.1	504.5	02.2	5
6	605.5	02.3	605.5	02.4	605.4	02.5	605.4	02.6	605.4	02.6	6
7	706.4	02.7	706.4	02.8	706.3	03.0	706.3	03.0	706.3	03.1	7
8	807.4	03.1	807.3	03.2	807.2	03.4	807.2	03.4	807.2	03.5	8
9	908.3	03.5	908.2	03.7	908.1	03.8	908.1	03.8	908.1	03.9	9
10	1009.2	03.9	1009.1	04.1	1009.1	04.2	1009.0	04.3	1009.0	04.4	10
11	1110.1	04.3	1110.0	04.5	1110.0	04.6	1109.9	04.7	1109.9	04.8	11
12	1211.0	04.7	1211.0	04.9	1210.9	05.1	1210.8	05.1	1210.8	05.3	12
13	1312.0	05.1	1312.0	05.5	1311.8	05.5	1311.7	05.6	1311.7	05.7	13
14	1412.9	05.5	1412.8	05.7	1412.7	05.9	1412.7	05.9	1412.6	06.1	14
15	1513.8	05.9	1513.7	06.1	1513.6	06.3	1513.6	06.4	1513.5	06.6	15
16	1614.7	06.2	1614.6	06.5	1614.5	06.8	1614.5	06.8	1614.4	07.0	16
17	1715.6	06.6	1715.5	06.9	1715.4	07.2	1715.4	07.3	1715.3	07.4	17
18	1816.6	07.0	1816.4	07.3	1816.3	07.6	1816.3	07.7	1816.2	07.9	18
19	1917.5	07.4	1917.4	07.7	1917.2	08.0	1917.2	08.1	1917.1	08.3	19
20	2018.4	07.8	2018.5	08.1	2018.1	08.4	2018.1	08.5	2018.0	08.8	20
21	2119.3	08.2	2119.2	08.5	2119.0	08.9	2119.0	09.0	2118.9	09.2	21
22	2220.2	08.6	2220.1	08.9	2219.5	09.3	2219.9	09.4	2219.8	09.9	22
23	2321.1	09.0	2321.0	09.3	2320.8	09.7	2320.8	09.8	2320.7	10.0	23
24	2422.1	09.4	2421.9	09.8	2421.1	10.1	2421.1	10.3	2421.0	10.5	24
25	2523.0	09.8	2522.8	10.2	2522.7	10.5	2522.6	10.7	2522.5	11.1	25
26	2623.9	10.2	2623.7	10.6	2623.6	11.0	2623.5	11.1	2623.4	11.4	26
27	2724.8	10.5	2724.7	11.0	2724.5	11.4	2724.4	11.5	2724.3	11.8	27
28	2825.8	10.9	2825.6	11.4	2825.4	11.8	2825.3	12.0	2825.2	12.4	28
29	2926.7	11.3	2926.5	11.8	2926.3	12.3	2926.2	12.4	2926.1	12.7	29
30	3027.6	11.7	3027.4	12.2	3027.2	12.7	3027.1	12.8	3027.0	13.1	30
31	3128.5	12.1	3128.3	12.6	3128.1	13.1	3128.0	13.3	3127.9	13.6	31
32	3229.5	12.5	3229.2	13.0	3229.0	13.5	3228.9	13.7	3228.8	14.0	32
33	3330.4	12.9	3330.1	13.4	3329.9	13.9	3329.8	14.1	3329.7	14.4	33
34	3431.3	13.3	3431.1	13.8	3430.8	14.4	3430.7	14.5	3430.6	14.9	34
35	3532.2	13.7	3532.0	14.2	3531.7	14.8	3531.6	15.0	3531.5	15.3	35
36	3633.1	14.1	3632.9	14.6	3632.6	15.2	3632.5	15.4	3632.4	15.8	36
37	3734.1	14.4	3733.8	15.0	3733.5	15.6	3733.4	15.8	3733.2	16.2	37
38	3835.0	14.8	3834.7	15.4	3834.4	16.0	3834.3	16.2	3834.1	16.6	38
39	3935.9	15.2	3935.6	15.9	3935.3	16.5	3935.3	16.7	3935.0	17.1	39
40	4036.8	15.6	4036.5	16.3	4036.2	16.9	4036.2	17.1	4035.9	17.5	40
41	4137.7	16.0	4137.5	16.7	4137.2	17.3	4137.1	17.5	4136.8	18.0	41
42	4238.7	16.4	4238.4	17.1	4238.1	17.7	4238.0	18.0	4237.7	18.4	42
43	4339.6	16.8	4339.3	17.5	4339.0	18.2	4338.9	18.4	4338.6	18.9	43
44	4440.5	17.2	4440.2	17.9	4439.9	18.6	4439.8	18.8	4439.5	19.3	44
45	4541.4	17.6	4541.1	18.3	4540.8	19.0	4540.7	19.2	4540.4	19.7	45
46	4642.3	18.0	4642.0	18.7	4641.7	19.4	4641.6	19.7	4641.3	20.2	46
47	4743.3	18.4	4742.9	19.1	4742.6	19.9	4742.5	20.1	4742.2	20.6	47
48	4844.2	18.8	4843.8	19.5	4843.5	20.3	4843.4	20.5	4843.1	21.0	48
49	4945.1	19.2	4944.8	19.9	4944.4	20.7	4944.3	20.9	4944.0	21.5	49
50	5046.0	19.5	5045.7	20.3	5045.3	21.1	5045.2	21.4	5044.9	21.9	50
D.	Dep.	Lat.	D.								
67	Deg.	66	Deg.	65	Deg.	5	Point	64	Deg.	63	Deg.

## of Latitude and Departure.

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	23 Deg	24 Deg	25 Deg	26 Deg	Point.	26 Deg	27 Deg	Dif.					
Dif.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.					
53	46.9	19.9	46.6	20.7	46.2	21.5	46.1	22.8 45.8 22.3 45.4 23.2 51					
52	47.9	20.3	47.5	21.1	47.1	22.0	47.0	22.2 46.7 22.8 46.3 23.5 52					
53	48.3	20.7	48.4	21.5	48.0	22.4	47.9	22.7 47.6 23.2 47.2 24.1 53					
54	49.7	21.1	49.3	22.0	48.9	22.8	48.8	23.1 48.5 23.7 48.1 24.5 54					
55	50.6	21.5	50.2	22.4	49.8	23.2	49.7	23.5 49.4 24.1 49.0 25.0 55					
56	51.5	21.9	51.2	22.8	50.7	23.7	50.6	23.9 50.3 24.5 49.9 25.4 56					
57	52.5	22.3	52.1	23.3	51.7	24.1	51.5	24.4 51.2 25.0 50.8 25.9 57					
58	53.4	22.7	53.0	23.6	52.6	24.5	52.4	24.8 52.1 25.4 51.7 26.3 58					
59	54.3	23.0	53.9	24.0	53.5	24.9	53.3	25.2 53.0 25.9 52.6 26.8 59					
60	55.2	23.4	54.8	24.4	54.4	25.4	54.2	25.6 53.9 26.3 53.5 27.2 60					
61	56.1	23.8	55.7	24.8	55.3	25.8	55.1	26.1 54.8 26.7 54.4 27.7 61					
62	57.1	24.2	56.5	25.2	56.2	26.2	56.0	26.5 55.7 27.2 55.2 28.1 62					
63	58.0	24.6	57.5	25.6	57.1	26.6	56.9	26.9 56.6 27.6 56.1 28.6 63					
64	58.9	25.0	58.3	26.0	58.0	27.0	57.9	27.4 57.5 28.0 57.0 29.1 64					
65	59.8	25.4	59.4	26.4	58.9	27.5	58.8	27.8 58.4 28.5 57.9 29.5 65					
66	60.7	25.8	60.3	26.8	59.8	27.9	59.7	28.2 59.4 28.9 58.8 30.0 66					
67	61.7	26.2	61.2	27.2	60.7	28.3	60.6	28.6 60.2 29.4 59.7 30.4 67					
68	62.6	26.6	62.1	27.7	61.6	28.7	61.5	29.1 61.1 29.8 60.6 30.9 68					
69	63.5	27.0	63.0	28.1	62.5	29.2	62.4	29.6 62.0 30.2 61.5 31.3 69					
70	64.4	27.3	63.9	28.5	63.4	29.6	63.3	29.9 62.9 30.7 62.4 31.8 70					
71	65.4	27.7	64.9	28.9	64.3	30.0	64.2	30.4 63.8 31.1 63.3 32.2 71					
72	66.3	28.1	65.8	29.3	65.2	30.4	65.1	30.8 64.7 31.6 64.2 32.7 72					
73	67.2	28.5	66.7	29.7	66.2	30.8	66.0	31.2 65.6 32.0 65.0 33.1 73					
74	68.1	28.9	67.6	30.1	67.1	31.3	66.9	31.6 66.5 32.4 65.9 33.6 74					
75	69.0	29.3	68.5	30.5	68.0	31.7	67.8	32.1 67.4 32.9 66.8 34.1 75					
76	70.0	29.7	69.4	30.9	68.9	32.1	68.7	32.5 68.3 33.3 67.7 34.5 76					
77	70.9	30.1	70.3	31.3	69.8	32.5	69.6	32.9 69.2 33.7 68.6 35.0 77					
78	71.8	30.5	71.2	31.7	70.7	33.0	70.5	33.4 70.1 34.2 69.5 35.4 78					
79	72.7	30.9	72.1	32.1	71.6	33.5	71.4	33.8 71.0 34.6 70.5 35.9 79					
80	73.6	31.3	73.1	32.5	72.5	33.8	72.3	34.2 71.9 35.9 71.3 36.3 80					
81	74.6	31.6	74.0	32.9	73.4	34.2	73.2	34.6 72.8 35.5 72.2 36.8 81					
82	75.5	32.0	74.9	33.3	74.3	34.7	74.1	35.1 73.7	35.9 73.1 37.2 82				
83	76.4	32.4	75.8	33.8	75.2	35.1	75.0	35.5 74.6	36.4 74.0 37.7 83				
84	77.3	32.8	76.7	34.2	76.1	35.5	75.9	35.9 75.5	36.8 74.8 38.1 84				
85	78.8	33.2	77.6	34.6	77.0	35.9	76.8	36.3 76.4	37.3 75.7 38.6 85				
86	79.2	33.6	78.6	35.0	77.9	36.3	77.7	36.8 77.3	37.7 76.6 39.0 86				
87	80.1	34.0	79.5	35.4	78.8	36.8	78.6	37.2 78.2	38.1 77.5 39.5 87				
88	81.0	34.4	80.4	35.8	79.7	37.2	79.5	37.6 79.1	38.6 78.4 40.0 88				
89	81.9	34.8	81.3	36.2	80.7	37.6	80.5	38.1 80.0	39.0 79.3 40.4 89				
90	82.8	35.2	82.2	36.6	81.6	38.0	81.4	38.5 80.9	39.4 80.2 40.9 90				
91	83.7	35.6	83.1	37.0	82.5	38.5	82.3	38.9 81.8	39.8 81.1 41.3 91				
92	84.7	35.9	84.0	37.4	83.4	38.9	83.2	39.3 82.7	40.3 82.0 41.8 92				
93	85.5	36.3	85.0	37.8	84.3	39.3	84.1	39.8 83.6	40.8 82.9 42.2 93				
94	86.5	36.7	85.9	38.2	85.2	39.7	85.0	40.2 84.5	41.2 83.8 42.7 94				
95	87.4	37.1	86.8	38.6	86.1	40.1	85.9	40.6 85.4	41.6 84.6 43.1 95				
96	88.4	37.5	87.7	39.0	87.0	40.6	86.8	41.0 86.3	42.1 85.5 43.6 96				
97	89.3	37.5	88.6	39.4	87.9	41.0	87.7	41.5 87.2	42.5 86.4 44.0 97				
98	90.2	38.3	89.5	39.9	88.8	41.4	88.6	41.9 88.1	43.0 87.3 44.5 98				
99	91.1	38.7	90.4	40.3	89.7	41.6	89.5	42.3 89.0	43.4 88.2 44.9 99				
100	92.0	39.1	91.4	40.7	90.6	42.3	90.4	42.7 89.9	43.8 89.1 45.5 100				
Diff.	67	Deg.	66	Deg.	65	De8.	5 <sup>2</sup>	Point.	64	Deg.	63	Deg.	Dif.

	28 Deg.		$\frac{1}{2}$ Point		29 Deg.		30 Deg.		2 $\frac{1}{4}$ Poin		31 Deg.		Dif.
Dif.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Dif.
1	00,9	00,5	00,5	00,5	00,9	00,5	00,9	00,5	00,9	00,5	00,9	00,5	0
2	01,8	00,9	01,8	00,9	01,7	01,0	01,7	01,0	01,7	01,0	01,7	01,0	0,2
3	02,6	01,4	02,6	01,4	03,6	01,4	02,6	01,5	02,6	01,5	02,6	01,5	3
4	03,5	01,9	03,5	01,9	03,5	01,9	03,5	02,0	03,4	02,1	03,4	02,1	4
5	04,4	02,3	04,4	02,4	04,7	02,4	04,3	02,5	04,3	02,6	04,3	02,6	5
6	05,3	02,8	05,3	02,8	05,2	02,9	05,2	03,0	05,5	03,1	05,2	03,1	6
7	06,2	03,3	06,2	03,3	06,1	03,4	06,1	03,5	06,0	03,6	06,1	03,6	7
8	07,1	03,8	07,1	03,8	07,0	03,9	07,0	04,0	06,9	04,1	06,9	04,1	8
9	07,9	04,2	07,9	04,2	07,9	04,4	07,8	04,5	07,7	04,6	07,7	04,6	9
10	08,8	04,7	08,8	04,7	08,7	04,8	08,7	05,0	08,6	05,1	08,6	05,1	10
11	09,7	05,2	09,7	05,2	09,6	05,3	09,5	05,5	09,4	05,6	09,4	05,7	11
12	10,6	05,6	10,6	05,6	10,5	05,8	10,4	06,0	10,3	06,2	10,3	06,2	12
13	11,5	06,1	11,5	06,1	11,4	06,	11,3	06,5	11,1	06,7	11,2	06,7	13
14	12,3	06,6	12,3	06,6	12,2	06,8	12,1	07,0	12,0	07,	12,0	07,1	14
15	13,2	07,0	13,2	07,1	13,1	07,3	13,0	07,5	12,9	07,7	12,9	07,7	15
16	14,1	07,5	14,1	07,5	14,0	07,7	13,9	08,0	13,7	08,2	13,7	08,2	16
17	15,0	08,0	15,0	08,0	14,9	08,2	14,7	08,5	14,6	08,7	14,6	08,8	17
18	15,9	08,4	15,9	08,5	15,7	08,7	15,6	09,0	15,4	09,2	15,4	09,3	18
19	16,8	08,9	16,8	08,9	16,6	09,2	16,4	09,5	16,3	09,8	16,3	09,8	19
20	17,7	09,4	17,6	09,4	17,5	09,7	17,3	10,0	17,1	10,3	17,1	10,3	20
21	18,5	09,9	18,5	09,9	18,4	10,2	18,2	10,5	18,0	10,8	18,0	10,8	21
22	19,4	10,3	19,4	10,3	19,2	10,7	19,0	11,0	18,9	11,3	18,9	11,3	22
23	20,3	10,9	20,3	10,9	20,1	11,1	19,9	11,5	19,7	11,8	19,7	11,8	23
24	21,2	11,3	21,2	11,3	21,0	11,6	20,8	12,0	20,6	12,3	20,6	12,4	24
25	22,1	11,7	22,0	11,8	21,9	12,1	21,6	12,5	21,4	12,8	21,4	12,9	25
26	23,0	12,3	22,9	12,3	22,7	12,6	22,5	13,0	22,3	13,4	22,3	13,4	26
27	23,8	12,7	23,8	12,8	23,6	13,1	23,4	13,5	23,1	13,9	23,1	13,9	27
28	24,7	13,1	24,7	13,1	24,5	13,6	24,2	14,0	24,0	14,4	24,0	14,4	28
29	25,6	13,6	25,6	13,7	25,4	14,1	25,1	14,5	24,9	14,9	24,9	14,9	29
30	26,5	14,1	26,5	14,1	26,2	14,5	26,0	15,0	25,7	15,4	25,7	15,4	30
31	27,4	14,5	27,3	14,6	27,1	15,0	26,9	15,5	26,6	15,9	26,6	16,0	31
32	28,2	15,0	28,2	15,1	28,0	15,5	27,7	16,0	27,4	16,4	27,4	16,5	32
33	29,1	15,5	29,1	15,5	28,9	16,0	28,6	16,5	28,3	17,0	28,5	17,0	33
34	30,0	16,0	30,0	16,0	29,7	16,5	29,5	17,0	29,2	17,5	29,1	17,5	34
35	30,9	16,4	30,9	16,5	30,6	17,0	30,3	17,5	30,0	18,0	30,0	18,0	35
36	31,8	16,9	31,7	17,0	31,5	17,4	31,1	18,0	30,9	18,5	30,9	18,5	36
37	32,7	17,4	32,6	17,4	32,4	17,5	32,0	18,5	31,7	19,0	31,7	19,1	37
38	33,5	17,9	33,5	17,9	33,2	18,4	32,9	19,0	32,5	19,5	32,6	19,5	38
39	34,4	18,3	34,4	18,4	34,1	18,9	33,8	19,5	33,4	20,0	33,4	20,1	39
40	35,3	18,8	35,3	18,9	35,0	19,4	34,6	20,0	34,3	20,6	34,3	20,6	40
41	36,2	19,1	36,1	19,3	35,8	19,9	35,5	20,5	35,2	21,1	35,1	21,1	41
42	37,1	19,7	37,0	19,8	36,7	20,4	36,4	21,0	36,0	21,6	36,0	21,6	42
43	38,0	20,1	37,9	20,3	37,6	20,8	37,2	21,5	36,9	22,1	36,9	22,1	43
44	38,8	20,6	38,8	20,7	38,5	21,3	38,1	22,0	37,7	22,6	37,7	22,6	44
45	39,7	21,1	39,7	21,2	39,3	21,8	39,0	22,5	38,6	23,1	38,6	23,1	45
46	40,6	21,6	40,6	21,7	40,2	22,3	39,8	23,0	39,5	23,6	39,4	23,7	46
47	41,5	22,1	41,4	22,2	41,1	22,8	40,7	23,5	40,3	24,2	40,3	24,2	47
48	42,4	22,5	42,3	22,6	42,0	23,3	41,6	24,0	41,3	24,7	41,1	24,7	48
49	43,3	23,0	43,2	23,2	42,8	23,7	42,4	24,5	42,0	25,2	42,0	25,2	49
50	44,1	23,5	44,1	23,6	43,7	24,2	43,3	25,0	42,9	25,7	42,9	25,7	50
E	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dif.
F	52 Deg.	$\frac{1}{2}$ Point	51 Deg.	60 Deg.	$\frac{1}{4}$ Point	59 Deg.							Dif.

	28 Deg		2½ Points		29 Deg		30 Deg		2¾ Points		31 Deg		Dif.
Dif.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Dif.
• 51	+5.0	23.9	45.0	24.0	44.6	24.7	44.2	25.5	43.8	26.2	43.7	26.3	51
52	+5.9	24.4	45.9	24.5	45.5	25.0	45.0	26.1	44.6	26.7	44.6	26.8	52
53	+6.8	24.9	46.7	25.0	46.0	25.7	45.9	26.5	45.5	27.2	45.4	27.3	53
54	+7.7	25.3	47.6	25.5	47.2	26.2	46.8	27.0	46.3	27.8	46.2	27.9	54
55	+8.6	25.8	48.5	25.9	48.1	26.7	47.6	27.5	47.1	28.3	47.1	28.3	55
56	+9.4	26.3	49.4	26.4	49.0	27.1	48.5	28.0	48.0	28.8	48.0	28.8	56
57	+0.3	26.8	50.3	+6.9	49.8	27.6	49.4	28.5	49.9	29.3	48.9	29.4	57
58	-1.2	27.2	51.2	27.3	50.7	28.1	50.2	29.0	49.7	29.8	49.7	29.9	58
59	-2.1	27.7	52.0	27.8	51.6	28.6	51.1	29.5	50.6	30.3	50.6	30.4	59
60	-3.0	28.2	52.9	28.1	52.5	29.1	52.0	30.0	51.5	30.8	51.4	30.9	60
61	-3.9	28.6	53.8	28.7	53.3	29.6	52.8	30.5	52.3	31.4	52.3	31.4	61
62	-4.7	29.1	54.7	29.2	54.2	30.1	53.7	31.0	53.2	31.9	53.1	31.9	62
63	-5.6	29.6	55.6	29.7	55.1	30.5	54.6	31.5	54.0	32.4	54.0	32.4	63
64	-6.5	30.0	56.4	30.2	56.0	31.0	55.4	32.0	54.9	32.9	54.9	33.0	64
65	-7.4	30.5	57.3	30.6	56.8	31.5	56.3	32.5	55.7	33.4	55.7	33.5	65
66	-8.3	31.0	58.2	31.1	57.7	32.0	57.2	33.0	56.6	33.9	56.6	34.0	66
67	-9.2	31.4	59.1	31.6	58.6	32.5	58.0	33.5	57.5	34.4	57.4	34.5	67
68	-0.0	31.9	60.0	32.0	59.5	33.0	58.5	34.0	58.3	35.0	58.3	35.0	68
69	-0.9	32.4	60.8	32.5	60.3	33.4	59.7	34.5	59.2	35.5	59.1	35.5	69
70	-1.8	32.9	61.7	33.0	61.2	33.9	60.6	35.0	60.0	36.0	60.0	36.0	70
71	-2.7	33.3	62.6	33.5	62.1	34.4	61.5	35.5	60.9	36.5	60.9	36.6	71
72	-3.6	33.8	63.5	33.9	63.0	34.9	62.3	36.0	61.8	37.0	61.7	37.2	72
73	-4.4	34.3	64.4	34.4	63.8	35.4	63.2	36.5	62.6	37.5	62.6	37.6	73
74	-5.3	34.7	65.3	34.9	64.7	35.9	64.1	37.0	63.5	38.0	63.4	38.1	74
75	-6.2	35.2	66.1	35.4	65.6	36.4	64.9	37.5	64.3	38.6	64.3	38.6	75
76	-7.1	35.7	67.0	35.8	66.4	36.8	65.8	38.0	65.2	39.1	65.1	39.1	76
77	-8.0	36.1	67.9	36.3	67.3	37.3	66.7	38.1	66.0	39.6	66.0	39.7	77
78	-8.9	36.6	68.8	36.5	68.2	37.8	67.5	39.0	66.9	40.1	66.9	40.1	78
79	-9.7	37.1	69.7	37.2	69.1	38.3	68.4	39.5	67.8	40.6	67.7	40.7	79
80	-10.6	37.6	70.5	37.7	70.0	38.8	69.3	40.0	68.6	41.1	68.6	41.2	80
81	-11.5	38.1	71.4	38.2	70.8	39.8	70.7	40.0	69.4	41.6	69.4	41.7	81
82	-12.4	38.5	72.3	38.6	71.7	39.7	70.9	41.0	70.3	42.2	70.3	42.2	82
83	-13.3	39.1	73.2	39.1	72.6	40.2	71.8	41.5	71.2	42.7	71.1	42.7	83
84	-14.2	39.4	74.1	39.6	73.5	40.7	72.7	42.0	72.1	43.2	72.0	43.3	84
85	-15.0	39.9	75.0	40.1	74.3	41.2	73.6	42.5	72.9	43.7	72.9	43.8	85
86	-15.9	40.4	75.8	40.5	75.2	42.7	74.5	43.0	73.8	44.2	73.7	44.3	86
87	-16.8	40.8	76.7	41.0	76.1	42.2	75.3	43.5	74.6	44.7	74.6	44.8	87
88	-17.7	41.3	77.6	41.5	77.0	42.7	76.2	44.0	75.5	45.2	75.4	45.3	88
89	-18.6	41.7	78.5	41.9	77.8	43.1	77.1	44.5	76.3	45.7	76.3	45.8	89
90	-19.5	42.2	79.4	42.4	78.7	43.6	77.9	45.0	77.2	46.3	77.1	46.3	90
91	-20.3	42.7	80.2	42.9	79.6	44.1	78.8	45.5	78.1	46.8	78.0	46.9	91
92	-21.2	43.2	81.1	43.4	80.5	44.6	79.7	46.0	78.9	47.3	78.9	47.4	92
93	-22.1	43.6	82.0	43.8	81.3	45.1	80.5	46.5	79.8	47.8	79.7	47.9	93
94	-23.0	44.1	82.9	44.3	82.2	45.6	81.4	47.0	80.6	48.3	80.6	48.4	94
95	-23.9	44.6	83.8	44.8	83.1	46.1	82.3	47.5	81.5	48.8	81.4	48.9	95
96	-24.8	45.1	84.7	45.2	84.0	46.5	83.1	48.0	82.3	49.3	82.3	49.4	96
97	-25.6	45.5	85.5	45.7	84.8	47.0	84.0	49.5	83.2	49.9	83.1	50.0	97
98	-26.5	46.0	86.4	46.2	85.7	47.5	84.9	49.0	84.1	50.4	84.0	50.5	98
99	-27.4	46.5	87.3	46.7	86.6	48.0	85.7	49.5	84.9	50.9	84.9	51.0	99
100	-28.3	46.9	88.2	47.1	87.5	48.5	86.6	50.0	85.8	51.4	85.7	51.3	100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dif.
	62 Deg.	5½ Points	61 Deg.	60 Deg.	5½ Points	59 Deg.							

Diff.	31 Deg.		33 Deg.		3 Points		34 Deg.		35 Deg.		36 Deg.		Diff.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	00,8	00,5	00,8	00,5	00,8	00,6	00,8	00,6	00,8	00,6	00,8	00,6	1
2	01,7	01,1	01,7	01,1	01,7	01,1	01,7	01,1	01,6	01,1	01,6	01,1	2
3	02,5	01,6	02,5	01,6	02,5	01,7	02,5	01,7	02,5	01,7	02,4	01,8	3
4	03,4	02,1	03,4	02,2	03,3	02,2	03,3	02,1	03,3	02,3	03,2	02,3	4
5	04,2	02,6	04,2	02,7	04,2	02,8	04,1	02,8	04,1	02,9	04,0	02,9	5
6	05,1	03,2	05,0	03,3	05,0	03,3	05,0	03,4	04,9	03,4	04,8	03,5	6
7	05,9	03,7	05,9	03,8	05,8	03,9	05,8	03,9	05,7	04,0	05,7	04,1	7
8	06,8	04,2	06,7	04,4	06,6	04,4	06,6	04,5	06,5	04,6	06,5	04,7	8
9	07,6	04,8	07,5	04,9	07,5	05,0	07,5	05,0	07,4	05,2	07,3	05,3	9
10	08,5	05,3	08,4	05,4	08,3	05,6	08,3	05,6	08,2	05,7	08,1	05,9	10
11	09,3	05,8	09,2	06,0	09,1	06,1	09,1	06,1	09,0	06,3	08,9	06,5	11
12	10,2	06,4	10,1	06,5	10,0	06,7	09,9	06,7	09,8	06,9	09,7	07,0	12
13	11,0	06,9	10,9	07,1	10,8	07,2	10,8	07,3	10,6	07,5	10,5	07,6	13
14	11,9	07,4	11,7	07,6	11,6	07,8	11,6	07,8	11,5	07,9	11,5	07,9	14
15	12,7	07,9	12,6	08,1	12,5	08,3	12,5	08,4	12,2	08,6	12,1	08,8	15
16	13,6	08,5	13,4	08,7	13,3	08,9	13,3	08,9	13,1	09,2	12,9	09,4	16
17	14,4	09,0	14,3	09,3	14,1	09,4	14,1	09,5	13,9	09,8	13,7	10,0	17
18	15,3	09,5	15,1	09,8	15,0	10,0	14,9	10,1	14,8	10,3	14,6	10,6	18
19	16,1	10,1	15,9	10,3	15,8	10,6	15,7	10,6	15,7	10,9	15,4	11,2	19
20	17,0	10,6	16,8	10,9	16,6	11,1	16,6	11,2	16,4	11,5	16,2	11,8	20
21	17,8	11,1	17,6	11,4	17,5	11,7	17,4	11,7	17,2	12,0	17,0	12,3	21
22	18,6	11,7	18,5	12,0	18,3	12,2	18,2	12,3	18,0	12,5	17,8	12,9	22
23	19,5	12,2	19,3	12,5	19,1	12,8	19,0	12,8	18,8	13,2	18,6	13,5	23
24	20,3	12,7	20,1	13,1	20,0	13,3	19,9	13,4	19,7	13,8	19,4	14,1	24
25	21,2	13,2	21,0	13,6	20,7	13,9	20,7	14,0	20,5	14,3	20,1	14,7	25
26	22,0	13,8	21,8	14,2	21,6	14,4	21,5	14,5	21,3	14,9	21,0	15,3	26
27	22,9	14,3	22,6	14,7	22,4	15,0	22,4	15,1	22,1	15,5	21,8	15,9	27
28	23,7	14,8	23,5	15,2	23,3	15,5	23,2	15,6	22,9	16,1	22,6	16,5	28
29	24,6	15,4	24,3	15,8	24,1	16,1	24,0	16,2	23,8	16,6	23,5	17,0	29
30	25,4	15,9	25,2	16,3	24,9	16,7	24,9	16,8	24,6	17,2	24,3	17,6	30
31	26,3	16,4	26,0	16,9	25,3	17,2	25,7	17,3	25,4	17,8	25,1	18,0	31
32	27,1	17,0	26,8	17,4	26,6	17,8	26,5	17,9	26,2	18,3	25,9	18,6	32
33	28,0	17,5	27,7	18,0	27,4	18,3	27,4	18,4	27,0	18,9	26,7	19,4	33
34	28,8	18,0	28,5	18,5	28,3	18,9	28,2	19,0	27,9	19,5	27,5	20,0	34
35	29,7	18,5	29,4	19,1	29,1	19,4	29,0	19,6	28,7	20,1	28,3	20,6	35
36	30,5	19,1	30,2	19,6	29,9	20,0	29,8	20,1	29,5	20,6	29,1	21,2	36
37	31,4	19,6	31,0	20,1	30,8	20,6	30,7	20,7	30,3	21,1	29,9	21,7	37
38	32,2	20,1	31,9	20,7	31,6	21,1	31,5	21,1	31,1	21,8	30,7	21,3	38
39	33,1	20,7	32,7	21,2	32,5	21,7	32,3	21,8	32,0	21,3	31,5	22,9	39
40	33,9	21,2	33,6	21,8	33,3	22,2	33,2	22,2	32,8	21,9	32,4	23,5	40
41	34,8	21,7	34,4	22,3	34,1	22,8	34,0	22,8	33,6	23,5	33,2	24,5	41
42	35,6	22,3	35,2	22,9	34,9	23,3	34,8	23,5	34,4	24,1	34,0	24,7	42
43	36,5	22,8	36,1	23,4	35,7	23,9	35,6	24,0	35,2	24,6	34,8	25,3	43
44	37,3	23,3	36,9	24,0	36,6	24,4	36,5	24,9	36,0	25,2	35,6	25,9	44
45	38,1	23,8	37,7	24,5	37,4	25,0	37,2	25,2	36,9	25,8	36,4	26,4	45
46	39,0	24,4	38,6	25,0	38,2	25,5	38,1	25,7	37,7	26,4	37,1	27,0	46
47	39,9	24,9	39,4	25,6	39,1	26,1	39,0	26,3	38,5	26,9	38,0	27,6	47
48	40,7	25,4	40,3	26,1	39,9	26,7	39,8	26,8	39,3	27,5	38,8	28,1	48
49	41,5	26,0	41,1	26,7	40,7	27,2	40,6	27,4	40,1	28,1	39,6	28,8	49
50	42,4	26,5	41,9	27,2	41,6	27,8	41,4	28,0	41,0	28,7	40,4	29,4	50
D	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	D
58	Deg.	57	Deg.	5 Points	56	Deg.	55	Deg.	54	Deg.	53	Deg.	57

## of Latitude and Departure.

195

D	32 Deg		33 Deg		3 Points		34 Deg		35 Deg		36 Deg.		Diff.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	43.2	17.0	42.1	17.8	42.4	18.3	41.3	18.5	41.8	19.2	41.3	19.0	51
52	44.1	27.6	43.6	28.3	43.2	28.9	43.1	29.1	43.6	29.8	42.1	30.6	52
53	44.9	28.1	44.5	28.9	44.1	29.6	43.9	29.4	43.4	30.4	42.9	31.2	53
54	45.8	28.6	45.3	29.4	44.9	30.0	44.5	30.2	44.2	31.0	43.7	31.7	54
55	46.6	29.1	46.1	30.0	45.7	30.6	45.6	30.7	45.1	31.5	44.5	32.3	55
56	47.5	29.7	47.0	30.5	46.6	31.1	46.4	31.3	45.9	32.1	45.3	32.9	56
57	48.3	30.2	47.8	31.0	47.4	31.7	47.3	31.9	46.7	32.7	46.1	33.5	57
58	49.2	30.7	48.7	31.6	48.2	32.2	48.1	32.4	47.5	33.3	46.5	34.1	58
59	50.0	31.3	49.5	32.1	49.0	32.8	48.9	33.0	48.3	33.8	47.7	34.7	59
60	50.9	31.8	50.3	32.7	49.9	33.3	49.7	33.5	49.1	34.4	48.5	35.3	60
61	51.7	32.2	51.2	33.2	50.7	33.9	50.6	34.1	50.0	34.9	49.3	35.9	61
62	52.6	32.9	52.0	33.8	51.5	34.4	51.4	34.7	50.8	35.6	50.2	36.3	62
63	53.4	33.4	52.9	34.3	52.4	35.0	52.2	35.2	51.6	36.1	51.0	37.0	63
64	54.3	34.2	53.7	34.9	53.2	35.5	53.1	35.5	52.4	36.7	51.8	37.6	64
65	55.1	34.4	54.5	54.4	54.0	55.1	53.9	56.3	53.2	57.3	52.6	58.2	65
66	56.0	35.0	55.3	35.9	54.9	56.7	54.7	56.9	54.1	57.9	53.4	58.8	66
67	56.8	35.5	56.2	36.5	55.7	57.2	55.5	57.5	54.0	58.4	54.2	59.4	67
68	57.7	36.0	57.0	37.0	56.5	57.8	56.4	58.0	55.7	59.0	55.0	40.0	68
69	58.5	36.6	57.9	37.6	57.4	38.3	57.2	38.1	56.5	39.6	55.8	40.6	69
70	59.4	37.1	58.7	38.1	58.2	38.9	58.0	39.1	57.3	40.1	56.6	41.1	70
71	60.2	37.6	59.6	38.7	59.0	39.4	58.9	39.7	58.2	40.7	57.4	41.7	71
72	61.0	38.1	60.4	39.2	59.8	40.0	59.7	40.3	59.0	41.3	58.2	42.3	72
73	61.9	38.7	61.2	39.8	60.7	40.6	60.5	40.8	59.8	41.9	59.0	42.9	73
74	62.7	39.2	62.1	40.3	61.5	41.1	61.3	41.4	60.6	42.4	59.9	43.5	74
75	63.6	39.7	62.9	40.8	62.4	41.7	62.2	41.9	61.4	43.0	60.7	44.1	75
76	64.4	40.3	63.8	41.5	63.2	42.1	63.0	42.5	62.3	43.6	61.5	44.7	76
77	65.3	40.8	64.6	41.9	64.0	42.8	63.8	43.0	63.1	44.2	62.3	45.3	77
78	66.1	41.3	65.4	42.5	64.8	43.3	64.7	43.6	63.9	44.7	63.1	45.8	78
79	67.0	41.9	66.3	43.0	65.7	44.9	65.5	44.2	64.7	45.3	63.9	46.4	79
80	67.8	42.4	67.1	43.6	66.5	44.4	66.3	44.7	65.5	45.9	64.7	47.0	80
81	68.7	42.9	68.0	44.1	67.3	45.0	67.1	45.3	66.4	46.5	65.5	47.6	81
82	69.5	43.4	68.8	44.7	68.1	45.5	68.0	45.8	67.2	47.0	66.3	48.1	82
83	70.4	44.0	69.6	45.2	69.0	46.1	68.8	46.4	68.0	47.6	67.1	48.8	83
84	71.2	44.5	70.5	45.8	69.8	46.7	69.6	47.0	68.8	48.2	68.0	49.4	84
85	72.1	45.0	71.3	46.3	70.7	47.2	70.5	47.5	69.6	48.8	68.8	50.0	85
86	72.9	45.6	72.1	46.8	71.5	47.7	71.3	48.1	70.5	49.3	69.6	50.5	86
87	73.8	46.1	73.0	47.3	72.3	48.3	72.1	48.6	71.3	49.9	70.4	51.1	87
88	74.6	46.5	73.8	47.9	73.3	48.9	72.9	49.2	72.1	50.5	71.2	51.7	88
89	75.5	47.2	74.7	48.5	74.0	49.4	73.8	49.8	72.9	51.0	72.0	52.3	89
90	76.3	47.7	75.5	49.0	74.8	50.0	74.6	50.3	73.7	51.6	72.8	52.9	90
91	77.2	48.2	76.3	49.6	75.7	50.6	75.4	50.9	74.5	52.2	73.6	53.5	91
92	78.0	48.7	77.2	50.1	76.5	51.1	76.3	51.4	75.4	52.8	74.4	54.1	92
93	78.9	49.3	78.0	50.6	77.3	51.7	77.1	52.0	76.2	53.3	75.2	54.7	93
94	79.7	49.8	78.9	51.2	78.2	52.2	77.9	52.6	77.0	53.9	76.0	55.2	94
95	80.6	50.3	79.7	51.7	79.0	52.7	78.7	53.1	77.8	54.5	76.9	55.8	95
96	81.4	50.9	80.5	52.3	79.8	53.3	79.5	53.7	78.6	55.1	77.7	56.4	96
97	82.3	51.4	81.4	52.8	80.6	53.9	80.4	54.2	79.5	55.6	78.5	57.0	97
98	83.1	51.9	82.2	53.4	81.5	54.4	81.2	54.8	80.3	56.2	79.3	57.6	98
99	84.0	52.5	83.1	53.9	82.3	55.0	81.0	55.4	81.1	56.8	80.1	58.2	99
100	84.8	53.0	83.9	54.5	83.1	55.5	82.9	55.9	81.9	57.4	80.9	58.8	100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Diff.
	58	Deg.	57	Deg.	5 Points.	56	Deg.	55	Deg.	54	Deg.	54	Deg.

Dif.	34 <sup>1</sup> Point.	37 Deg.	38 Deg.	39 Deg.	32 <sup>1</sup> Point.	40 Deg.	Dif.						
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.						
1	00.8	00.6	00.5	00.6	00.8	00.6	00.7	00.8	00.6	00.8	00.6	1	
2	01.6	01.2	01.6	01.2	01.6	01.2	01.5	01.3	01.2	01.3	01.5	2	
3	02.4	01.8	02.4	01.8	02.4	01.8	02.3	01.9	02.3	01.9	02.3	3	
4	03.2	02.0	03.2	02.4	03.1	02.5	03.5	02.5	03.1	02.5	03.1	4	
5	04.0	03.0	04.0	03.0	03.9	03.1	03.9	03.1	03.9	03.1	03.2	5	
6	04.8	03.6	04.8	03.6	04.7	03.7	04.6	03.9	04.6	03.8	04.6	6	
7	05.6	04.1	05.6	04.2	05.5	04.3	05.4	04.4	05.4	04.4	05.4	7	
8	06.4	04.8	06.4	04.8	06.3	04.9	06.2	05.0	05.2	05.1	05.1	8	
9	07.2	05.4	07.2	05.4	07.1	05.5	07.0	05.7	05.7	05.9	05.8	9	
10	08.0	06.0	08.0	06.0	07.9	06.2	07.8	06.3	07.7	06.3	07.7	10	
11	08.8	06.6	08.8	06.6	08.7	06.8	08.5	06.9	08.5	07.0	08.4	11	
12	09.6	07.1	09.5	07.2	09.4	07.4	09.3	07.5	09.3	07.6	09.2	12	
13	10.4	07.7	10.4	07.8	10.2	08.1	10.1	08.2	10.0	08.2	10.0	13	
14	11.2	08.3	11.2	08.4	11.0	08.7	10.9	08.8	10.8	08.9	10.7	14	
15	12.0	08.9	12.0	09.0	11.8	09.0	11.6	09.4	11.6	09.5	11.5	15	
16	12.8	09.5	12.8	09.6	12.6	09.6	12.4	10.1	12.3	10.3	12.3	16	
17	13.6	10.1	13.6	10.2	13.4	10.5	13.2	10.7	13.1	10.8	13.0	17	
18	14.5	10.7	14.4	10.8	14.2	11.1	13.5	11.3	13.9	11.4	13.2	18	
19	15.3	11.3	15.2	11.4	15.0	11.7	14.8	12.0	14.7	12.0	14.5	19	
20	16.1	11.9	16.0	12.0	15.8	12.3	15.5	12.5	15.5	12.7	15.3	20	
21	16.9	12.5	16.8	12.6	16.5	12.9	16.3	13.2	16.2	13.3	16.1	21	
22	17.7	13.1	17.6	13.2	17.3	13.5	17.1	13.8	17.0	14.0	16.8	22	
23	18.5	13.7	18.4	13.8	18.3	14.2	17.9	14.5	17.8	14.6	17.6	23	
24	19.3	14.3	19.2	14.4	18.9	14.8	18.6	15.1	18.5	15.2	18.4	24	
25	20.1	14.9	20.0	15.0	19.7	15.4	19.4	15.7	19.3	15.9	19.1	25	
26	20.9	15.5	20.8	15.6	20.5	16.0	20.2	16.4	20.1	16.5	19.9	26	
27	21.7	16.1	21.6	16.2	21.3	16.6	21.0	17.0	20.9	17.1	20.7	27	
28	22.5	16.7	22.4	16.8	22.1	17.1	21.8	17.6	21.6	17.8	21.4	28	
29	23.3	17.3	23.2	17.4	22.8	17.8	22.6	18.3	22.4	18.4	22.2	29	
30	24.1	17.9	24.0	18.0	23.6	18.5	23.3	18.9	23.2	19.0	23.0	30	
31	24.9	18.5	24.8	18.6	24.4	19.1	24.1	19.5	24.0	19.7	23.7	31	
32	25.7	19.1	25.6	19.3	25.2	19.7	24.9	20.1	24.7	20.3	24.5	20.6	32
33	26.5	19.7	26.4	19.9	26.0	20.5	25.6	20.8	25.5	20.9	25.3	21.2	33
34	27.3	20.1	27.1	20.5	26.8	20.9	26.4	21.4	26.1	21.6	26.0	21.9	34
35	28.1	20.8	28.9	21.1	27.6	21.5	27.2	22.0	27.0	22.2	26.8	22.5	35
36	28.9	21.4	28.7	21.7	28.4	22.2	27.9	22.7	27.8	22.8	27.6	23.1	36
37	29.7	22.0	29.5	22.3	29.2	22.8	28.8	23.3	28.6	23.5	28.1	23.8	37
38	30.5	22.6	30.3	22.9	29.9	23.4	29.5	23.9	29.4	24.1	29.1	24.4	38
39	31.3	23.2	31.1	23.5	30.7	24.0	30.3	24.5	30.1	24.7	29.9	25.1	39
40	32.1	23.8	31.8	24.1	31.5	24.6	31.1	25.2	30.9	25.4	30.0	25.7	40
41	32.9	24.4	32.7	24.7	32.3	25.2	31.9	25.5	31.7	26.0	31.4	26.4	41
42	33.7	25.0	33.5	25.3	33.1	25.9	32.6	26.4	32.5	26.6	32.2	27.0	42
43	34.1	25.6	34.3	25.9	33.9	26.7	33.4	27.1	33.2	27.3	32.9	27.6	43
44	35.3	26.2	35.1	26.5	34.7	27.1	34.2	27.7	34.0	27.5	33.7	28.3	44
45	36.1	26.8	36.9	27.1	35.5	27.7	35.0	28.3	34.8	28.5	34.5	28.9	45
46	36.9	27.4	36.7	27.7	36.2	28.3	35.9	29.0	35.6	29.2	35.2	29.6	46
47	37.7	28.0	37.5	28.3	37.0	28.9	36.8	29.6	36.3	29.8	36.0	30.2	47
48	38.5	28.6	38.3	28.9	37.8	29.5	37.6	30.2	37.1	30.4	36.8	30.9	48
49	39.3	29.2	39.1	29.5	38.6	30.2	38.1	30.8	37.9	31.1	37.5	31.5	49
50	40.1	29.8	39.9	30.1	39.4	30.8	38.9	31.9	38.6	31.7	38.3	31.7	50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
	44 Point.	53 Deg.	52 Deg.	51 Deg.	42 Point.	50 Deg.							

Dif.	3 1/2 Point		37 Deg.		38 Deg.		39 Deg.		3 1/2 Point		40 Deg.		Dif.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	41.0	30.4	40.7	30.7	40.1	31.4	49.0	32.1	39.4	32.3	39.1	32.8	51
52	42.8	31.0	41.5	31.3	41.9	32.0	40.4	31.7	40.2	33.0	39.8	33.4	52
53	42.6	31.6	41.3	31.9	41.8	32.6	41.2	33.3	41.0	33.6	40.6	34.1	53
54	43.4	32.2	43.1	32.5	42.5	33.2	42.0	34.0	41.8	34.4	42.7	34.7	54
55	44.2	32.8	43.9	33.1	43.3	33.9	42.7	34.6	42.5	34.9	42.1	35.4	55
56	45.0	33.3	44.7	33.7	44.1	34.5	43.5	35.2	43.3	35.5	42.9	36.0	56
57	45.8	33.9	45.5	34.2	44.9	35.1	44.3	35.9	44.1	36.2	43.7	36.6	57
58	46.6	34.5	46.3	34.9	45.1	35.8	45.1	36.5	44.8	36.8	44.4	37.3	58
59	47.4	35.1	47.1	35.5	46.5	36.3	45.8	37.1	45.6	37.4	45.2	37.9	59
60	48.2	35.7	47.9	36.1	47.3	36.9	46.6	37.8	46.4	38.1	46.0	38.6	60
61	49.0	36.3	48.7	36.7	48.1	37.5	47.4	38.4	47.1	38.7	46.7	39.3	61
62	49.8	36.9	49.5	37.3	48.9	38.3	48.2	39.0	47.9	39.3	47.5	39.9	62
63	50.6	37.5	50.3	37.9	49.6	38.8	49.0	39.6	48.7	40.0	48.3	40.5	63
64	51.4	38.1	51.1	38.5	50.5	39.1	49.7	40.3	49.5	40.6	49.0	41.2	64
65	52.2	38.7	51.9	39.1	51.2	40.0	50.5	40.9	50.2	41.2	49.8	41.8	65
66	53.0	39.3	52.7	39.7	52.0	40.4	51.3	41.5	51.0	41.9	50.5	42.4	66
67	53.8	39.9	53.5	40.3	52.8	41.2	52.1	42.2	51.8	42.5	51.3	43.1	67
68	54.6	40.6	54.3	40.9	53.6	41.9	52.8	42.8	52.6	43.1	52.1	43.7	68
69	55.4	41.1	55.1	41.5	54.4	42.5	53.6	43.4	53.3	43.8	52.9	44.4	69
70	56.2	41.7	55.9	43.1	55.2	43.1	54.4	44.0	54.1	44.4	53.6	45.0	70
71	57.0	42.3	56.7	42.7	55.9	43.7	55.2	44.7	54.9	45.0	54.4	45.6	71
72	57.8	42.9	57.5	43.3	56.7	44.3	55.9	45.3	55.7	45.7	55.1	46.3	72
73	58.6	43.5	58.2	43.9	57.5	44.9	56.7	45.9	56.4	46.3	55.9	46.9	73
74	59.4	44.1	59.1	44.5	58.3	45.5	57.5	46.6	57.2	46.9	56.7	47.6	74
75	60.2	44.7	59.9	45.1	59.2	46.2	58.3	47.2	58.0	47.6	57.4	48.2	75
76	61.0	45.3	60.7	45.7	60.0	46.8	59.1	47.8	58.7	48.2	58.2	48.9	76
77	61.8	45.9	61.5	46.3	60.7	47.4	59.8	48.5	59.5	48.8	59.0	49.5	77
78	62.7	46.5	62.3	46.9	61.5	48.0	60.6	49.1	60.3	49.5	59.7	50.1	78
79	63.5	47.1	63.1	47.5	62.1	48.6	61.4	49.7	61.1	50.1	60.5	50.8	79
80	64.3	47.7	63.9	48.1	63.0	49.3	62.2	50.3	61.8	50.7	61.3	51.4	80
81	65.1	48.3	64.7	48.7	63.8	49.9	62.9	51.0	62.6	51.4	62.0	52.1	81
82	65.9	48.8	65.5	49.3	64.6	50.5	63.1	51.5	63.5	52.0	62.8	52.7	82
83	66.7	49.4	66.3	49.9	65.4	51.1	64.5	52.2	64.2	52.6	63.6	53.4	83
84	67.5	50.0	67.1	50.5	66.2	51.7	65.3	52.9	64.9	53.3	64.3	54.0	84
85	68.3	50.6	67.9	51.1	67.0	52.1	66.1	53.5	65.7	53.9	65.1	54.6	85
86	69.1	51.2	68.7	51.7	67.8	52.9	66.8	54.1	66.5	54.6	65.9	55.3	86
87	69.9	51.8	69.5	52.4	68.6	53.6	67.6	54.8	67.2	55.2	66.6	55.9	87
88	70.7	52.4	70.3	53.0	69.3	54.2	68.4	55.6	68.0	55.8	67.4	56.6	88
89	71.5	53.0	71.1	53.5	70.1	54.8	69.1	56.0	68.8	56.5	68.2	57.2	89
90	72.3	53.6	71.9	54.2	70.9	55.4	69.9	56.6	69.6	57.1	68.9	57.8	90
91	73.1	54.2	72.7	54.8	71.7	56.0	70.7	57.2	70.3	57.7	69.7	58.5	91
92	73.9	54.8	73.5	55.4	72.5	56.6	71.5	57.9	71.1	58.4	70.5	59.1	92
93	74.7	55.4	74.3	56.0	73.3	57.3	72.3	58.5	71.9	59.0	71.2	59.8	93
94	75.5	56.0	75.1	56.6	74.1	57.9	73.0	59.2	72.7	59.6	72.0	60.4	94
95	76.3	56.6	75.9	57.2	74.9	58.5	73.8	59.8	73.4	60.3	72.8	61.1	95
96	77.1	57.2	76.7	57.8	75.6	59.1	74.6	60.4	74.2	60.9	73.5	61.7	96
97	77.9	57.8	77.5	58.4	76.4	59.7	75.4	61.0	75.0	61.5	74.3	62.1	97
98	78.7	58.4	78.3	59.0	77.2	60.3	76.2	61.7	75.7	62.2	75.5	63.0	98
99	79.5	59.0	79.1	59.6	78.0	60.9	76.9	62.3	76.5	62.8	75.8	63.6	99
100	80.3	59.6	79.9	60.2	78.8	61.6	77.7	64.9	77.8	63.4	76.6	64.3	100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dif.
	3 1/2 Point	53 Deg.	52 Deg.	51 Deg.	50 Deg.	4 1/2 Point	50 Deg.						

Diff.	41 Deg.	42 Deg.	3 $\frac{1}{4}$ Point.	43 Deg.	44 Deg.	+ Point.	Diff.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	00.7	00.7	00.7	00.7	00.7	00.7	00.7	00.7
2	01.5	01.3	01.5	01.2	01.5	01.3	01.5	01.4
3	02.3	02.0	02.1	02.0	02.2	02.0	02.2	02.1
4	03.0	02.6	03.0	02.7	03.0	02.7	02.9	02.8
5	03.8	03.3	03.7	03.3	03.7	03.4	03.6	03.5
6	04.5	03.9	04.5	04.0	04.4	04.0	04.4	04.2
7	05.3	04.6	05.2	04.7	05.2	04.7	05.1	04.9
8	06.0	05.5	05.2	05.3	05.9	05.4	05.8	05.6
9	06.8	05.9	06.7	06.0	06.7	06.0	06.5	06.7
10	07.5	06.6	07.4	06.7	07.4	06.7	07.3	06.9
11	08.3	07.2	08.2	07.4	08.1	07.4	08.0	07.5
12	09.1	07.9	08.9	08.0	08.9	08.1	08.8	08.6
13	09.8	08.5	09.7	08.5	09.6	08.7	09.5	09.3
14	10.6	09.2	10.4	09.4	10.4	09.4	10.3	09.7
15	11.3	09.8	11.1	10.0	11.0	10.2	10.8	10.4
16	12.1	10.5	11.5	10.7	11.9	11.7	11.9	11.3
17	12.8	11.1	12.7	11.4	12.6	11.4	12.2	11.8
18	13.6	11.9	13.4	12.0	13.3	12.1	13.1	12.5
19	14.3	12.5	14.1	12.7	14.1	12.8	13.3	13.7
20	15.1	13.1	14.9	13.4	14.8	13.4	14.4	13.0
21	15.8	13.8	15.6	14.0	15.6	14.1	15.4	14.3
22	16.6	14.4	16.3	14.7	16.3	14.8	16.1	15.0
23	17.4	15.1	17.1	15.4	17.0	15.4	16.5	15.7
24	18.1	15.7	17.3	16.1	17.8	16.1	17.5	16.4
25	18.9	16.4	18.6	16.7	18.5	16.8	18.3	17.1
26	19.6	17.1	19.3	17.5	19.3	17.4	19.0	17.7
27	20.4	17.7	20.1	18.1	20.0	18.1	19.7	18.4
28	21.1	18.4	20.8	18.7	20.7	18.8	20.5	19.1
29	21.9	19.0	21.5	19.4	21.5	19.5	21.1	19.8
30	22.6	19.7	21.3	20.1	22.2	20.1	21.9	20.5
31	23.4	20.3	23.0	20.7	23.0	20.8	22.6	21.1
32	24.1	21.0	23.8	21.4	23.7	21.5	23.4	21.8
33	24.9	21.6	24.5	22.1	24.4	22.2	23.7	22.2
34	25.7	22.3	25.3	22.7	25.2	22.8	24.9	23.2
35	26.4	23.0	26.0	23.4	25.9	23.5	25.6	23.9
36	27.2	23.6	26.7	24.1	26.7	24.2	26.3	24.5
37	27.9	24.3	27.5	24.7	27.4	24.6	27.0	25.2
38	28.7	24.9	28.2	25.4	28.2	25.5	27.8	25.9
39	29.4	25.6	29.0	26.1	28.5	26.1	28.5	27.1
40	30.2	26.2	29.7	26.8	29.6	26.9	29.2	27.3
41	31.0	26.9	30.5	27.4	30.4	27.5	30.0	28.5
42	31.7	27.5	31.2	28.1	31.1	28.2	30.7	28.6
43	32.5	28.2	31.9	28.8	31.9	28.9	31.4	29.3
44	33.2	28.9	32.7	29.4	31.9	29.5	32.2	30.0
45	34.0	29.5	33.4	30.1	33.3	30.2	32.9	30.7
46	34.7	30.2	34.2	30.8	34.1	30.9	33.6	31.4
47	35.5	30.8	34.9	31.4	34.8	31.6	34.4	32.1
48	36.3	31.5	35.7	32.1	35.6	32.1	35.1	32.7
49	37.0	32.1	36.1	32.8	36.3	32.9	35.8	33.4
50	37.7	32.8	37.8	33.5	37.0	33.6	36.6	34.1
D	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
F	49 Deg	48 Deg	47 Point	+6 Deg	46 Deg	+6 Deg	45 Point	Diff.

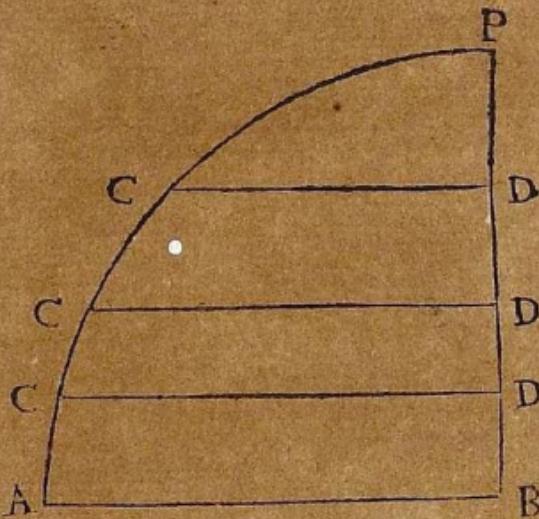
B \*

D	41 Deg	42. Deg.	3 $\frac{3}{4}$ Point	43 Deg.	44 Deg	4 Points	Dif
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
51	38.5	33.5	37.9	34.1	37.8	34.2	37.3
52	39.2	34.1	38.6	34.8	38.5	34.9	38.0
53	40.0	34.8	39.4	35.5	39.3	35.6	38.8
54	40.8	35.4	40.1	36.1	40.0	36.3	39.5
55	41.5	36.0	40.9	36.8	40.7	36.9	40.2
56	42.3	36.7	41.6	37.5	41.5	37.6	41.0
57	43.0	37.4	42.4	38.3	42.2	38.3	41.7
58	43.8	38.1	43.1	38.8	43.0	38.9	42.4
59	44.5	38.8	43.8	39.5	43.7	38.6	43.1
60	45.3	39.5	44.6	40.1	44.5	40.3	43.8
61	46.0	40.0	45.3	40.8	45.2	41.0	44.6
62	46.8	40.7	45.0	41.5	46.0	41.6	45.3
63	47.5	41.3	45.8	42.2	46.7	42.3	46.7
64	48.3	42.0	47.5	42.8	47.0	42.9	47.0
65	49.1	42.6	48.3	43.5	48.2	43.7	47.5
66	49.8	43.3	49.0	44.2	48.9	44.3	47.5
67	50.6	44.0	49.8	44.8	49.6	45.0	45.7
68	51.3	44.8	50.5	45.5	50.4	45.9	49.7
69	52.1	45.3	51.3	46.2	51.1	46.3	49.5
70	52.8	45.9	52.0	46.8	52.0	47.0	51.2
71	53.6	46.6	52.8	47.5	52.6	47.7	51.9
72	54.3	47.2	53.5	48.2	53.3	48.3	52.7
73	55.1	47.9	54.2	48.8	54.1	49.0	53.4
74	55.9	48.5	55.0	49.5	54.8	49.7	54.1
75	56.8	49.2	55.7	50.2	55.6	50.4	54.8
76	57.4	49.9	56.5	50.9	56.3	51.0	55.0
77	58.1	50.5	57.2	51.5	57.1	51.7	55.7
78	58.9	51.2	58.0	52.1	57.8	52.4	55.3
79	59.6	51.8	58.7	52.8	58.5	53.0	57.8
80	60.4	52.5	59.4	53.5	59.3	53.7	58.5
81	61.1	53.1	60.2	54.2	60.0	54.4	59.2
82	61.9	53.8	60.9	54.9	60.8	55.1	60.0
83	62.6	54.5	61.7	55.5	61.5	55.7	60.7
84	63.4	55.1	62.4	56.2	62.2	56.4	61.4
85	64.2	55.9	63.2	56.9	63.0	57.1	62.1
86	64.9	56.4	63.9	57.5	63.7	57.7	62.8
87	65.7	57.1	64.7	58.2	64.5	58.4	63.5
88	66.4	57.7	65.5	58.9	65.2	59.1	64.4
89	67.2	58.4	66.1	59.6	65.9	60.7	65.0
90	67.9	59.0	66.9	60.2	66.7	60.4	64.7
91	68.7	59.7	67.6	60.9	67.4	61.1	65.5
92	69.4	60.4	68.4	61.6	68.2	61.8	66.2
93	70.1	61.0	69.1	62.2	68.9	62.4	66.0
94	71.0	61.7	69.9	62.9	69.6	63.1	66.7
95	71.7	62.3	70.6	63.6	70.4	63.8	67.2
96	72.5	63.0	71.3	64.2	71.1	64.5	67.9
97	73.2	63.6	67.2	64.9	71.9	65.1	67.4
98	74.0	64.3	72.8	65.6	72.6	65.8	71.7
99	74.7	65.0	73.6	66.2	73.4	66.5	72.4
100	75.5	65.6	74.3	66.9	74.1	67.2	73.1
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
Dif	41 Deg	48 Deg	4 $\frac{1}{4}$ Point	47 Deg	46 Deg	4 Points	Dif

## S E C T. VIII.

## Of Parallel Sailing.

1. SINCE the *Parallels of Latitude* do always decrease, the nearer they approach the *Pole*, it is plain, a Degree on any of them must be less than a Degree upon the *Equator*. Now, in order to know the Length of a Degree on any of them; let *PB* represent half the Earth's Axis, *PA*, a Quadrant of a *Meridian*, and consequently *A*,



Point on the *Equator*, *C*, a Point on the *Meridian*, and *CD* a Perpendicular from that Point upon the Axis, which plainly will be the Sine of *CP*, the Distance of that Point from the Pole, or the Co-sine of *CA*, its Distance from the Equator, and *CD* will be to *AB*, as the Sine of *CP*, or Co-sine of *CA*, is to the Radius. Again, if the Quadrant *PAB* be turn'd round upon the Axis *PB*, 'tis plain,

the Point A will describe the Circumference of the Equator, whose Radius is A B, and any other Point S upon the Meridian will describe the Circumference of a Parallel, whose Radius is C D.

*Cor. 1.* Hence (because the Circumferences of Circles are as their Radii) it follows, that the Circumference of any Parallel is to the Circumference of the Equator, as the Co-sine of its Latitude is to Radius.

*Cor. 2.* And since the Wholes are as their similar Parts, it will be, as the Length of a Degree on any Parallel, is to the Length of a Degree upon the Equator, so is the Co-sine of the Latitude of that Parallel to Radius.

*Cor. 3.* Hence, as Radius is to the Co-sine of any Latitude, so is the Minutes of Difference of Longitude between two Meridians, or their Distance in Miles upon the Equator, to the Distance of these two Meridians on the Parallel in Miles.

*Cor. 4.* And as the Co-sine of any Parallel is to Radius, so is the Length of any Arch on that Parallel (intercepted between two Meridians) in Miles, to the Length of a similar Arch on the Equator, or Minutes of Difference of Longitude.

*Cor. 5.* Also as the Co-sine of any one Parallel, is to the Co-sine of any other Parallel, so is the Length of any Arch on the first, in Miles, to the Length of the same Arch on the other in Miles.

2. From what has been said, arises the Solution of the several Cases of Parallel Sailing, which are as follow.

### C A S E I.

Given the Difference of Longitude between two Places, both lying on the same Parallel, to find the Distance between those Places.

*Example 1.*

## Example 1.

Suppose a Ship in the Latitude of  $54^{\circ}, 20'$  North, sails directly West on that Parallel, till she has differ'd Longitude  $12^{\circ}, 45'$ . Required the Distance sail'd on that Parallel.

First, The Difference of Longitude reduced into Minutes, or nautical Miles, is 765', which is the Distance between the Meridian sail'd from, and the Meridian come to, up in the Equator; then, to find the Distance between those Meridians on the Parallel of  $54^{\circ}, 20'$ , or the Distance sail'd, it will be, by Cor. 3. of the last Article.

As Radius	- - - - -	10.00000
is to the Co-sine of the Lat.	$54^{\circ}, 20'$	9.76572
so is the Min. of Diff. of Long.	765	- 2.88366
to the Distance on the Parallel	446.1	- 2.64938

## Example 2.

A Degree on the Equator being 60 Minutes, or nautical Miles. Required the Length of a Degree on the Parallel of  $51^{\circ}, 32'$ .

By Cor. 3. of the last Article, it will be

As Radius	- - - - -	10.00000
is to the Co-sine of the Lat.	$51^{\circ}, 32'$	9.79383
so is the Min. in 1 Deg. on the Eq.	60.	- 1.77815
to	37.32	- 1.57198
the Miles answering to a Degree on the Parallel of	$51^{\circ}, 32'$	

By this Problem the following Table is constructed, shewing the Geographic Miles answering to a Degree on any Parallel of Latitude; in which you may observe, that the Columns mark'd at the Top with D. L. contain the Degrees of Latitude belonging to each Parallel; and the adjacent Columns mark'd at the Top, Miles, contain the Miles answering to a Degree upon these Parallels.

A Table shewing how many Miles answer to a Degree of Longitude, in every Degree of Latitude.

D. L.	Miles								
I	59.99	19	56.73	37	47.92	55	34.41	73	17.54
2	59.97	20	56.38	38	47.28	56	33.55	74	16.53
3	59.92	21	56.01	39	46.62	57	32.68	75	15.52
4	59.86	22	55.63	40	45.96	58	31.79	76	14.51
5	59.77	23	55.23	41	45.28	59	30.90	77	13.50
6	59.67	24	54.81	42	44.95	60	30.00	78	12.48
7	59.56	25	54.38	43	43.88	61	29.09	79	11.45
8	59.42	26	53.93	44	43.16	62	28.17	80	10.42
9	59.26	27	53.46	45	42.43	63	27.24	81	9.38
10	59.08	28	52.97	46	41.68	64	26.30	82	8.35
11	58.89	29	52.47	47	40.92	65	25.36	83	7.32
12	58.68	30	51.96	48	40.15	66	24.41	84	6.28
13	58.46	31	51.43	49	39.36	67	23.45	85	5.23
14	58.22	32	50.88	50	38.57	68	22.48	86	4.18
15	57.95	33	50.32	51	37.76	69	21.50	87	3.14
16	57.67	34	49.74	52	36.94	70	20.52	88	2.09
17	57.37	35	49.15	53	36.11	71	19.54	89	1.05
18	57.06	36	48.54	54	35.26	72	18.55	90	0.00

Tho' this Table does only shew the Miles answering to a Degree of any Parallel, whose Latitude consists of a whole Number of Degrees; yet it may be made to serve for any Parallel, whose Latitude is some Number of Degrees and Minutes, by making the following Proportion, viz.

As 1 Degree, or 60 Minutes, is to the Difference between the Miles answering to a Degree in the next greater and next less Tabular Latitude than that

that proposed, so is the Excess of the proposed Latitude above the next less Tabular Latitude, to a proportional Part; which, subtracted from the Miles answering to a Degree of Longitude in the next less Tabular Latitude, will give the Miles answering to a Degree in the proposed Latitude.

### *Example.*

Required to find the Miles answering to a Degree on the Parallel  $56^{\circ} 44'$ .

First, The next less Parallel of Latitude in the Table, than that proposed, is that of  $56^{\circ}$ , a Degree of which (by the Table) is equal to 33.55 Miles; and the next greater Parallel of Latitude in the Table, than that proposed, is that of  $57^{\circ}$ , a Degree of which is (by the Table) equal to 32.68 Miles; the Difference of these is .87, and the Distance between these Parallels is 1 Degree or 60 Minutes; also the Distance between the Parallel of  $56^{\circ}$ , and the proposed Parallel of  $56^{\circ}, 44'$  is 44 Minutes; then by the preceding Proportion it will be: As 60 is to .87, so is 44 to .638, the Difference between a Degree on the Parallel of  $56^{\circ}$ , and a Degree on the Parallel of  $56^{\circ}, 44'$ , which therefore taken from 33.55, the Miles answering to a Degree on the Parallel of  $56^{\circ}$ , leaves 32.912, the Miles answering to a Degree on the Parallel of  $56^{\circ}, 44'$ , as was required.

### C A S E 2.

*The Distance sail'd in any Parallel of Latitude, or the Distance between any two Places on that Parallel being given, to find the Difference of Longitude.*

*Example.*

## Example.

Suppose a Ship in the Latitude of  $55^{\circ} 36'$  North, sails directly East 685.6 Miles. Required how much she has differ'd her Longitude.

By Cor. 4. Art. 1. of this Section, it will be,

As the Co-sine of the Lat.	$55^{\circ}, 36'$	-	9.75202
is to Radius	- - -	-	10.00000
so is the Distance sail'd	685.6	-	2.83607
to Min. of Diff. of Lg. git.	1213.	-	3.80405

which reduc'd into Degrees, by dividing by 60, makes  $20^{\circ}, 13'$  the Difference of Longitude the Ship has made.

This may also be solv'd by Help of the foregoing Table, viz. by finding from it, the Miles answering to a Degree on the proposed Parallel, and dividing with this the given Number of Miles, the Quotient will be the Degrees and Minutes of Difference of Longitude required.

Thus, in the last Example; I find, from the foregoing Table, that a Degree on the Parallel of  $55^{\circ}$ ,  $36'$  is equal to 33.89 Miles; by this I divide the proposed Number of Miles 685.6 and the Quotient is  $20.23$  Degrees, i. e.  $20^{\circ}, 13'$ , the Difference of Longitude required.

## C A S E 3.

The Difference of Longitude between two Places on the same Parallel, and the Distance between them being given, to find the Latitude of that Parallel.

Example.

## Example.

Suppose a Ship sails on a certain *Parallel* directly West 624 Miles, and then has differ'd her Longitude  $10^{\circ}, 46'$ , or 1126 Miles. Required the Latitude of the *Parallel* she sail'd upon.

By Cor. 3. Art. 1. of this *Section*, it will be,

As the Min. of Diff. of Long. 1126. - 3.05154  
 is to the Distance sail'd - 624. - 2.79518  
 so is Radius - - - - - 10.00000  
 to the Co-sine of the Lat. -  $56^{\circ}, 21'$  9.74264  
 consequently the Latitude of the Ship, or *Parallel*  
 she sail'd upon, was  $56^{\circ}, 21'$ .

From what has been said, may be solv'd the following Problems.

## Problem 1.

Suppose two Ships in the Latitude of  $46^{\circ}, 30'$  North, distant asunder 654 Miles, sail both directly North 256, and consequently are come to the Latitude of  $50^{\circ}, 46'$  North. Required their Distance on that *Parallel*.

By Cor. 5. of Art. 1. of this *Section*, it will be,

As the Co-sine of - -  $46^{\circ}, 30'$  - 9.83781  
 is to the Co-sine of - -  $50^{\circ}, 46'$  - 9.80105  
 so is - - - - - 654. - - - 2.81558  
 to - - - - - 601. - - - 2.77882

the Distance between the Ships, when on the *Parallel* of  $50^{\circ}, 46'$ .

## Problem

## Problem 2.

Suppose two Ships in the Latitude of  $45^{\circ}, 48'$  North, distant asunder 846 Miles, sail directly North, till the Distance between them is 624 Miles. Required the Latitude come to, and the Distance sail'd.

By Cor. 5. of Art. 1. of this Section, it will be,

As their first Distance - - - - -	846	- - - - -	2.92737
is to their second Distance - - - - -	624	- - - - -	2.79518
so is the Co-sine of - - - - -	$45^{\circ}, 48'$	- - - - -	9.84334
to the Co-sine of - - - - -	$59^{\circ}, 04'$	- - - - -	9.71115
the Latitude of the Parallel the Ships are come to.			

Consequently to find their Distance sail'd,

From the Latitude come to - - - - -	$59^{\circ}, 04'$
subtract the Latitude sail'd from - - - - -	$45^{\circ}, 48'$
and there remains - - - - -	$13^{\circ}, 16'$
equal to 796 Miles, the Difference of Latitude or Distance sail'd.	

3. Tho' in solving the Problems in this Section, we supposed the Earth to be really spherical, yet it is not so, but rather an *Oblate Spheroid*, having the Diameter of the Equator about 34 Miles longer than the Axis, which makes the Length of a Degree on the Meridian, near the Pole, about a Mile longer than the Length of a Degree near the Equator; and the Radii of the Parallels, instead of being Sines in a Circle, will be *Ordinates* to the lesser Axe of an *Ellipse*. Consequently, the true Length of a Degree on any Parallel, will somewhat differ from its Length on the Supposition of the Earth's being a Sphere; but this Difference is so small, that in all *nautical Cases* it may safely be neglected.

## SECT. IX.

## Of Middle Latitude Sailing.

WHEN two Places lie both on the same Parallel, we shew'd, in the last Section, how from the Difference of Longitude given, to find the Miles of Easting or Westing between them, & e contra; but when two Places lie not on the same Parallel, then their Difference of Longitude cannot be reduced to Miles of Easting or Westing on the Parallel of either Place; for if counted on the Parallel of that Place that has the greatest Latitude it would be too small, and if on the Parallel of that Place having the least Latitude it would be too great. Hence the common Way of reducing the Difference of Longitude between two Places lying on different Parallels, to Miles of Easting or Westing, & e contra, is by counting it on the middle Parallel between the Places, which is found by adding the Latitudes of the two Places together, and taking half the Sum, which will be the Latitude of the middle Parallel required. And hence arises the Solution of the following Cases.

## CASE I.

The Latitudes of two Places, and their Difference of Longitude given, to find the direct Course and Distance.

## Example.

Requir'd the direct Course and Distance between the Lizard in the Latitude of  $50^{\circ}$ ,  $00'$  N. and E. e Longi-

210 Middle Latitude Sailing.

Longitude of  $5^{\circ}$ ,  $14'$  W. and St. Vincent in the Latitude of  $17^{\circ}$ ,  $10'$  N. and Longitude of  $24^{\circ}$   $20'$  W.

First, To the Latitude of the Lizard -  $5^{\circ} 00'$  N  
add the Latitude of St. Vincent -  $17^{\circ} 10'$   
 $\underline{-----}$   
 The Sum is - - - - -  $67^{\circ} 10'$

Half the Sum, or Latitude of the middle Parallel is -  $\frac{1}{2} 33^{\circ} 35'$

Also the Difference of Latitude is -  $12^{\circ} 50'$   
equal to 1970 Miles of Southing. Again,

From the Long. of St. Vincent -  $24^{\circ} 20' W$   
take the Long. of the Lizard -  $05^{\circ} 14' W$   
there remains - - - - -  $19^{\circ} 06'$   
equal to 1146 Min. of Diff. of Long. West.

Then for the Miles of Westing, or Departure, it will be, by Case 1. of Parallel Sailing,

As Radius - - - - - - - - -  $10.00000$   
is to the Co-sine of the middle Parallel -  $\frac{1}{2} 33^{\circ} 35' \quad 9.92069$   
so is Min. Diff. of Long. -  $1146 \quad 3.05918$ ,  
to the Miles of Westing -  $954.7 \quad 2.97987$

And for the Course it will be, by Case 4. of Plain Sailing,

As the Diff. of Lat. -  $1970 \quad 3.29447$   
is to Radius - - - - - - - - -  $10.00000$   
so is the Departure -  $954.7 \quad 2.97987$   
to the Tang. of the Course  $25^{\circ} 51' \quad 9.68510$   
which because it is between South and West will be SSW $\frac{1}{2}$  West nearly.

For the Distance it will be, by the same Case,

As Radius - - - - - - - - -  $10.00000$   
is to the Diff. of Lat. -  $1970 \quad 3.29447$   
so

so is the Secant of the Course  $25^{\circ} 51'$  - 10.04579  
 to the Distance - - - - 2189 - 3.34026  
 whence the direct Course and Distance from the  
 Island to St. Vincent is SSW  $\frac{1}{4}$  W, 2189 Miles.

## C A S E . 2.

*One Latitude, Course and Distance sail'd, being given, to find the other Latitude, and Difference of Longitude.*

## Example.

Suppose a Ship in the Latitude of  $50^{\circ}, 00'$  North, sails South  $50^{\circ}, 06'$  West 150 Miles. Required the Latitude the Ship has come to, and how much she has differ'd her Longitude.

*First, For the Difference of Latitude it will be, by Case 1. of Plain Sailing,*

As Radius - - - - - 10.00000  
 is to the Distance - - - 150 - 2.17609  
 so is the Co-sine of the Course  $50^{\circ}, 06'$  9.80716  
 to the Diff. of Latitude - 96.22 1.98325  
 equal to  $1^{\circ}, 36'$ , and since the Ship is sailing  
 towards the Equator. Therefore,

From the Latitude she was in - - -  $50^{\circ}, 00'$   
 take the Diff. of Latitude - - -  $1, 36$   
 and there remains - - - - -  $48, 24$

the Latitude she has come to North. Consequent-  
 ly the Latitude of the middle Parallel will be  
 $49^{\circ}, 12'$ .

Then for Departure or Westing it will be, by the  
 same Case,

As Radius - - - - - 10.00000  
 is to the Distance - - 150 - - 2.7609  
 so is the Sine of the Course  $50^{\circ} 06'$  - 0.88489  
 to the Departure - - 115.1 - - 2.06098  
 and for the Difference of Longitude, it will be by  
*Case 2. of Parallel Sailing,*

As the Co-sine of the mid. Par.  $49^{\circ} 12'$  9.81519  
 is to Radius - - - - - 0.00000  
 so is the Departure - - 115.1 - 2.06098  
 to the min. Diff of Longitude 176.1 - 2.44579  
 equal to  $2^{\circ} 56'$ , which is the Difference of Lon-  
 gitude, the Ship has made Westerly.

### C A S E 3.

*Course and Difference of Latitude given, to find  
 the Distance sail'd, and Difference of Longitude.*

#### Example.

Suppose a Ship in the Latitude of  $53^{\circ} 34'$  North, sails S E b S, till by Observation she's found to be in the Latitude of  $51^{\circ} 12'$ , and consequently has differ'd her Latitude  $2^{\circ} 22'$ , or 142 Miles. Required the Distance sail'd, and the Difference of Longitude.

*First, For the Departure, it will be (by Case 2.  
 of Plain Sailing)*

As Radius - - - - - 10.00000  
 is to the Diff. of Latitude - 142 - 2.1529  
 so is the Tang. of Course  $33^{\circ} 45'$  9.82489  
 to the Departure - - 94.88 1.97718

And for the Dist. it will be, by the same Case,

As

~~Radius = - - - - - 10,00000  
is to the Diff. of Lat. - - - 142 - 2.15229  
to find the Secant of the Course 33°, 45' 10.08015  
to the Dist. - - - - - 170.8 - 2.23244~~

Then, since the Latitude sail'd from was 53°, 34' North, and the Latitude come to 51°, 12' N. therefore the middle Parallel will be 47°, 23', and consequently for the Diff. of Longitude, it will be (by Case 2, of Parallel Sailing)

As the Co-sine of the mid. Par. 47°, 23' 9.83065  
is to the Depart. - - - - - 94.88 - 1.97718  
so is Radius - - - - - - - - - 10.00000  
to min. of Diff. of Longit. - 140 - 2.14653  
equal to 2°, 20', the Difference of Longitude  
Easterly.

#### C A S E 4.

*Difference of Latitude, and Distance sail'd given,  
to find the Course and Difference of Longitude.*

#### Example.

Suppose a Ship in the Latitude of 43°, 26' N. sails between S. and E 246 Miles, and then is found by Observation to be in the Latitude of 41°, 06' N. Required the direct Course and Difference of Longitude.

First, For the Course it will be, by Case 3. of Plain Sailing,

As the Dist. - - - 246 - - - 2.39094  
is to Radius - - - - - 10.00000  
so

so is the Diff. of Latitude 140 - - 2.1  
 to the Co-sine of the Course 55°, 19' 9.75519  
 which because the Ship sails between South and  
 East, will be South 55°, 19' East, or S E b E.  
 nearly.

Then for Departure it will be, by the same Case,

As Radius	- - - - -	10.00000
is to the Dist.	- - 2.16 - - -	2.3994
so is the Sine of the Course 55°, 19'	- - - - -	9.91504
to the Depart.	- - 202.3 - -	2.30598

Lastly, For the Difference of Longitude, it will  
 be, by Case 2. of Parallel Sailing.

As the Co-sine of the mid. Par. 42°, 16' 9.86924  
 is to the Depart. - - - 202.3 - 2.30598  
 so is Radius - - - - - 10.00000  
 to min. of Diff. of Longit. - 273.3 - 2.43674  
 equal to 4°, 33', the Difference of Longitude  
 Easterly.

### C A S E 5.

Course and Departure given, to find Difference of  
 Latitude, Difference of Longitude, and Distance  
 sail'd.

#### Example.

Suppose a Ship in the Latitude of 48°, 23' N.  
 sails SW b S. till she has made of Westing 123  
 Miles. Required the Latitude come to, the Differ-  
 ence of Longitude, and the Distance sail'd.

First, For the Distance it will be, by Case 6.  
 of Plain Sailing,

As

As the Sine of the Course	$33^{\circ} 45'$	-	9.74474
is to the Departure.	-	$123$	-
so is Radius	-	-	-
to the Distance	-	-	$221.4$

And for the Difference of Latitude it will be, by the same Case,

As the Tang. of Course	-	$33^{\circ} 45'$	-	9.82489
is to the Departure	-	-	$123$	-
so is Radius	-	-	-	-
to the Diff. of Latitude	-	-	$184$	-

equal to  $3^{\circ} 04'$ , and since the Ship is sailing towards the Equator, the Latitude come to will be  $45^{\circ} 19'$  North; and consequently the middle Parallel will be  $46^{\circ} 51'$ .

Then to find the Difference of Longitude by Case 2. of Parallel Sailing,

As the Co-sine of mid. Par.	$46^{\circ} 51'$	-	9.83500
is to the Departure	-	$123$	-
so is Radius	-	-	-
to min. of Diff. of Longit.	-	$180$	-

which is equal to  $3^{\circ} 00'$ , the Difference of Longitude Westerly.

### CASE 6.

*Difference of Latitude and Departure given, to find Course, Distance, and Difference of Longitude.*

#### Example.

Suppose a Ship in the Latitude of  $46^{\circ} 37'$  North, sails between South and East, till she has made of Easting, 146 Miles and is then found by

## 216 Middle Latitude Sailing.

by Observation to be in the Latitude of  $43^{\circ}$ , North. Required the Course, Distance and Difference of Longitude.

First, By Case 4. of Plain Sailing, it will be for the Course,

As the Diff. of Latitude	-	193	-	2.28556	
is to Departure	-	-	146	-	2.16137
so is Radius	-	-	-	-	10.00000
to the Tang. of the Course	$36^{\circ}, 55'$			9.87581	
which because the Ship is sailing between South and East, will be South $36^{\circ}, 55'$ East, or SE by S $\frac{1}{2}$ East nearly.					

For the Distance it will be by the same Case,

As Radius	-	-	-	-	10.00000
is to the Diff. of Latitude	-	193	-	2.28556	
so is the Sec. of the Course	$36^{\circ}, 55'$			10.09718	
to the Distance	-	-	241.4	-	2.38274

Then for the Difference of Longitude it will be, by Case 2. of Parallel Sailing.

As the Co-sine of the mid. Par.	$45^{\circ}, 00'$	9.84959		
is to the Departure	-	146	-	2.16137
so is Radius	-	-	-	10.00000
to min. of Diff. of Longitude	205	-	2.31188	
equal to $3^{\circ}, 25'$ , the Difference of Longitude Easterly.				

### C A S E 7.

Distance and Departure given, to find Difference of Latitude, Course, and Difference of Longitude.

Example.

## Example.

Suppose a Ship in the Latitude of  $33^{\circ}$ ,  $40'$  North, sails between South and East 165 Miles, and has then made of Easting 112.5 Miles. Required the Difference of Latitude, Course, and Difference of Longitude.

First, For the Course it will be, (by Case 5. of Plane Sailing.

As the Distance - - - - 165 - 2.11748  
 is to Radius - - - - - 10.00000  
 so is the Departure - - 102.5 - 2.05115  
 to the Sine of the Course -  $42^{\circ}, 59'$  9.83367  
 which because the Ship sails between South and  
 East, will be South  $42^{\circ}, 59'$  East, or SE by S,  
 $\frac{1}{2}$  East, nearly.

And for the Difference of Latitude it will be, by  
 the same Case,

As Radius - - - - - 10.00000  
 is to the Distance - - 165 - 2.11748  
 so is the Co-sine of the Course  $42^{\circ}, 59'$  9.86436  
 to the Difference of Latitude 120.7 - 2.08184

equal to  $2^{\circ}, 00'$ . Consequently the Latitude come  
 to will be  $31^{\circ}, 40'$  North, and the Latitude of the  
 middle Parallel will be  $32^{\circ}, 40'$ . Hence to find  
 the Difference of Longitude it will be, by Case 2. of  
 Parallel Sailing.

As the Co-Sine of the mid. Par.  $32^{\circ}, 40'$  9.92522  
 is to the Departure - - 112.5 - 2.05115  
 so is Radius - - - - - 10.00000  
 to the Min. of Diff. of Long. 133.6 - 2.12593

F f

equal

218 Middle-Latitude Sailing.  
equal to  $2^{\circ} 13'$  nearly, the Difference of Longitude Easterly.

### C A S E 8.

Difference of Longitude and Departure given, to find the Difference of Latitude, Course, and Distance sail'd.

#### Example.

Suppose a Ship in the Latitude of  $50^{\circ} 46'$  North, sails between South and West, till her Difference of Longitude is  $3^{\circ} 12'$ , and is then found to have departed from her former Meridian 126 Miles. Required the Difference of Latitude, Course, and Distance sail'd.

First, For the Latitude she has come to it will be, by Case 3. of Parallel Sailing,

As the Min. of Diff. of Long.	192	-	2.28330	
is to the Departure	- - -	126	-	2.10037
so is Radius	- - -	- - -	-	10.00000
to the Co-sine of the mid. Par.	$48^{\circ} 59'$	9.81707		

Now, since the Middle-Latitude is equal to half the Sum of the two Latitudes (by Art. 1. of this Sect.) and so the Sum of the two Latitudes equal to double the middle Latitude; it follows, that if from double the middle Latitude we subtract any one of the Latitudes, the Remainder will be the other. Hence from twice  $48^{\circ} 59'$ , viz.  $97^{\circ} 58'$ , taking  $50^{\circ} 46'$ , the Latitude sail'd from, there remains  $47^{\circ} 12'$ , the Latitude come to. Consequently the Difference of Latitude is  $3^{\circ} 34'$ , or 214 Minutes.

Then,

Then, for the Course it will be, by Case 4. of  
Plane Sailing.

As the Difference of Lat. - 214 - 2.33041  
 is to Radius - - - - 10.00000  
 so is the Diff. of Long. - 126 - 2.10037  
 to the Tang. of the Course -  $30^{\circ}, 29'$  9.76996  
 which, because it is between South and West, will  
 be South  $30^{\circ}, 29'$  West, or SSW  $\frac{1}{4}$  West,  
 nearly.

And for the Distance it will be, (by the same Case,

As Radius - - - - 10.00000  
 is to the Difference of Lat. 214 - 2.33041  
 so is the Sec. of the Course -  $30^{\circ}, 29'$  10.06461  
 to the Distance - - - 248.4 - 2.39502

2. From what has been said, it will be easy to  
 solve a *Traverse*, by the Rules of *Middle-Latitude  
 Sailing*.

### Example.

Suppose a Ship in the Latitude of  $43^{\circ}, 25'$  North, sails upon the following Courses, viz. SW by S 63 Miles, SSW  $\frac{1}{2}$  West 45 Miles, S by E 54 Miles, and SW by W 74 Miles. Required the Latitude the Ship has come to, and how far she has differ'd her Longitude.

*First*, By Case 2. of this Sect. find the Difference  
 of Latitude, and Difference of Longitude belong-  
 ing to each Course and Distance, and they will  
 stand as in the following Table.

Course	Diff.	Diff. of Lat.		Diff. of Longit.		W.
		N.	S.	E.		
SW by S	63	—	52.4	—	47.85	
SSW $\frac{1}{2}$ W	45	—	39.7	—	28.62	
S by E	54	—	53.0	13.75	—	81.08
SW by W	74	—	41.1	—	—	
<i>Diff. of Lat.</i>		186.2		157.55 13.75		
<i>Diff. of Long.</i> 143.80						

Hence it is plain, the Ship has differ'd her Latitude 186.2 Minutes, or  $3^{\circ} 06'$ , and so has come to the Latitude of  $40^{\circ} 19'$  North, and has made of Difference of Longitude 143.8 Minutes, or  $2^{\circ} 23' 48''$  Westerly.

3. This Method of Sailing, tho' it be not strictly true, yet it comes very near the Truth, as will be evident, by comparing an Example wrought by this Method, with the same wrought by the Method deliver'd in the next Section, which is strictly true; and it serves without any considerable Error, in Runnings of 450 Miles between the Equator and Parallel of 30 Degrees; of 300 Miles between that and the Parallel of 60 Degrees; and of 150 Miles, as far as there is any Occasion, and consequently must be sufficiently exact for 24 Hours Run.

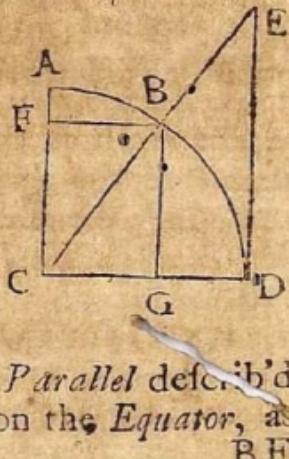
## S E C T. X. Of Mercator's Sailing.

I. **T**HO' the Meridians do all meet at the Pole, and the Parallels to the Equator do continually decrease, and that in Proportion to the Co-  
fines

sines of their Latitudes; yet, in old Sea-Charts the Meridians were drawn parallel to one another, and consequently the Parallels of Latitude, made equal to the Equator, and so a Degree of Longitude on any Parallel, as large as a Degree on the Equator; also in these Charts the Degrees of Latitude were still represented (as they are in themselves) equal to each other, and to those of the Equator. By these Means Places were very erroneously mark'd down upon the Chart; thus, for Instance, an Island on the Parallel of 50, would in this Chart be represented in a double Proportion, as to its Length, in *Easting* and *Westing*, but the same as to its Breadth in *Northing* and *Southing*; whereas in order to its being truly drawn upon the Chart, it ought to be lengthened, as to its *Southing* and *Northing*, in the same Proportion as it is in its *Easting* and *Westing*, so as the whole may be represented on the Chart proportionally as it is on the Globe itself.

3. To remedy this Inconvenience, so as still to keep the Meridians parallel, 'tis plain we must protract, or lengthen the Degrees of Latitude in the same Proportion as those of Longitude are, that so the Proportion in *Easting* and *Westing*, may be the same with that of *Southing* and *Northing*.

3. In the annex'd Scheme let ABD be a Quadrant of a Meridian, BF or CG, the Radius of the Parallel describ'd by the Point B and CD the Radius of the Equator; draw the Tangent DE and Secant CE, also the right Sine BG. Then it has been demonstrated, in *Sect. 8.* that a Degree upon any Parallel, is to a Degree on the Equator, as the Co-sine of its Latitude, is to Radius. Thus, a Degree on the Parallel describ'd by the Point B, is to a Degree on the Equator, as



BF or CG is to CD the Radius; but (by Art. 74. Sect. 1.)  $CG : CD :: CB : CE$ ; therefore a Degree on any Parallel, is to a Degree on the Equator, as Radius is to the Secant of the Latitude; and since in this Projection the Meridians are suppos'd to be parallel, and consequently each of the Parallels equal to the Equator, 'tis plain, the Radius of any Parallel will become equal to the Radius of the Equator, and so CG will every where become equal to CD; but when CG becomes equal to CD, 'tis plain, CB will become equal to CE. Consequently in this Projection, the Radius of the Meridian at any Parallel, will be equal to the Secant of the Latitude of that Parallel. Also since a Degree, or any small Arch upon the Equator, is equal to a Degree, or the like Arch upon the Meridian; therefore as the Secant of any Parallel, is to Radius, so is the Length of a Degree, or any small Arch on the Meridian, to the Length of a Degree, or like Arch on that Parallel. Hence 'tis evident that, in this Projection, where the Meridians are parallel, a Degree on any Parallel will be increas'd beyond its just Proportion, at such Rate as the Secant of the Latitude is greater than Radius; and consequently the Degrees on the Meridian must every where be increas'd in the same Rate; that so the Proportion in *Northing* and *Southing* may be the same with that of *Easting* and *Westing*, that is, the Length of a Degree, or any small Arch on the enlarrg'd Meridian, must every where be to a Degree, or like Arch of the Meridian on the Globe, as the Secant of the Latitude is to Radius. Hence, by supposing the Length of any small Arch of the Meridian Radius, it follows, from what has been said.

*Cor. 1.* That the Length of a Degree, or any small Arch on the enlarrg'd Meridian, is every where equal to the Secant of the Arch contain'd between it and the Equator.

*2.* The

2. The Distance of any Point upon the enlarg'd Meridian from the Equator, is equal to the Sum of all the Secants contain'd between it and the Equator.

3. The Distance between any two Parallels on the same Side of the Equator, is equal to the Difference of the Sums of all the Secants contain'd between the Equator and each of the Parallels.

4. The Distance between any two Parallels on contrary Sides of the Equator, is equal to the Sum of the Sums of all the Secants contain'd between the Equator and each Parallel.

5. Now, since it has been shewn, that in this Projection the Distance of each Point of the Meridian from the Equator, is equal to the Sum of all the Secants contain'd between it and the Equator; 'tis plain, that by a continual Addition of the Secants, beginning at the Equator, we shall have the Distance of every particular Point in the Meridian from the Equator, which Distances collected together from the Table, commonly call'd, *A Table of Meridional Parts*, which is annex'd to the End of this Section, and in which you may observe that the Top-Column contains the Degrees, and the Left-hand Side Column the Minutes; the other Columns contain the Meridional Parts answering to these Degrees and Minutes. There is also upon Gunter's Scale, a Line of Meridional Parts, mark'd Mer. which shews the Distance of each Point of the Meridian from the Equator.

6. By either of these, viz. the Table of Meridional Parts, or the Meridian Line upon Gunter's Scale, may a Mercator's Chart be constructed. Thus for Example, let it be required to make a Chart that shall commence at the Equator, and reach to the Parallel of 60 Degrees, and shall contain 80 Degrees of Longitude.

Draw the Line  $EQ$  presenting the Equator; (see Plate I.) then take from any convenient Line, of equal Parts, 4800 (the Number of Minutes contain'd in 80 Degrees) which set off from  $E$  to  $Q$ , and this will determine the Breadth of the Chart.

Divide the Line  $EQ$  into eight equal Parts, in the Points 10, 20, 30, &c. each containing 10 Degrees, and each of these divided into 10 equal Parts, will give the single Degrees upon the Equator; then thro' the Points  $E$ , 10, 20, &c. drawing Lines perpendicular to  $EQ$ , these shall be the Meridians.

From the Scale of equal Parts take 4527.4 (the Meridional Parts answering to 60 Degrees) and set that off from  $E$  to  $A$ , and from  $Q$  to  $B$ , and join  $AB$ ; then this Line will represent the Parallel of 60, and will determine the Length of the Chart.

Again, from the Scale of equal Parts take 603.1, (the Meridional Parts answering to 10 Degrees) and set that off from  $E$  to 10, on the Line  $EA$ , and through the Point 10 draw 10, 10, parallel to  $EQ$ , and this will be the Parallel of 10 Degrees. The same Way setting off from  $E$  on the Line  $EA$ , the Meridional Parts answering to each Degree, &c. of Latitude, and thro' the several Points drawing Lines parallel to  $EQ$ , we shall have the several Parallels of Latitude.

If the Chart does not commence from the Equator, but is only to serve for a certain Distance on the Meridian, between two given Parallels on the same Side of the Equator; then the Meridians are to be drawn, as in the last Example; and for the Parallels of Latitude you are to proceed thus; viz. from the Meridional Parts answering to each Point of Latitude in your Chart, subtract the Meridional Parts answering to the least Latitude, and set off the Differences severally, from the Parallel of the least Latitude, upon the two extreme Meridians, and the

Lines.

Lines joining these Points of the Meridians shall represent the several *Parallels* upon your *Chart*.

Thus let it be required to draw a *Chart* that shall serve from the Latitude of 20 Degrees North to 60 Degrees North, and that shall contain 80 Degrees of Longitude.

Having drawn the Line DC to represent the Parallel of 20 Degrees (see *Plate 1.*) and the *Meridians* to it, as in the foregoing Example; set off 663.3 (the Difference between the Meridional Parts answering to 30 Degrees, and those of 20 Degrees) from D to 30, and from C to 30; then join the Points 30 and 30 with a Right Line, and that shall be the Parallel of 30. Also set off 1397.6 (the Difference between the Meridional Parts answering to 40 Degrees, and those of 20 Degrees) from D to 40, and from C to 40; and joining the Points 40, and 40 with a Right Line, that shall be the Parallel of 40. And proceeding after the same Way, we may draw as many of the intermediate Parallels as we shall have occasion for.

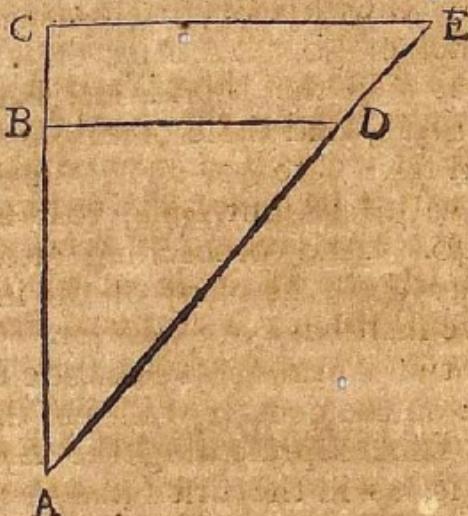
But if the two *Parallels* of Latitude that bounds the *Chart*, are on the contrary Sides of the *Equator*; then draw a Line representing the *Equator*, and *Meridians* to it, as in the first *Example*; and from the *Equator* set off on each Side of it the several Parallels contained between it and the given Parallels, as above, and your *Chart* is finished.

*N. B.* Here you must Notice; that in all *Charts*, the upper Part is the *North* Side, and the lower Part, or Bottom, is the *South* Side; also that Part of it towards the Right-hand is the *East*, and that towards the Left-hand, the *West* Side of the *Chart*.

6. Since, according to this Projection, the *Meridians* are parallel Right Lines, 'tis plain, that the *Rumbs*, which form always equal Angles with the *Meridians*, will be strait Lines; which Property renders this Projection of the Earth's Surface much more easy and proper for Use, than any other.

7. This Method of projecting the Earth's Surface upon a Plane, was first invented by Mr. Edward Wright, but first published by Mercator; and hence the Sailing by the Chart, was called Mercator's Sailing.

8. In the annexed Scheme, let A and D represent two Places upon the Surface of the Globe, AC the Meridian of A, and AD the Rhumb Line between the two Places; thro' D draw BD perpendicular to AC, and this will be the Parallel of Latitude of the Place D; from A set off upon the



Meridian, the Length AC, equal to the *Meridional or enlarg'd Difference of Latitude*; and thro' C draw CE parallel to BD meeting AD produced in E; then AB will be the *proper Difference of Latitude*, and AC the *enlarg'd Difference of Latitude*, or the Difference of Latitude, according to Mercator's Chart, between the Places A and D: CE will be the *Difference of Longitude*, and BD the *Def.<sup>n</sup>ture*; also AD will be the *proper Distance*, and AE the *enlarg'd*, or according to Mercator's Chart, and the Angle BAD will be the *Course*.

9. Now since in the Triangle ACE, BD is parallel to one of its Sides CE; 'tis plain, the Triangles ACE, ABD will be similar, and consequently the Sides proportional (by Art. 74. Sect. 1.) Hence arise the Solutions of the several Cases in this Sailing, which are as follow.

### C A S E I.

*The Latitudes of two Places given, to find the Meridional or enlarg'd Difference of Latitude between them.*

Of this Case there are three Varieties, viz. either one of the Places lies on the Equator, or both on the same Side of it; or Lastly, on different Sides.

1. If one of the proposed Places lies on the Equator, then the Meridional Difference of Latitude is the same with the Latitude of the other Place, taken from the Table of Meridional Parts.

### Example.

Required the Meridional Difference of Latitude between St. Thomas, lying on the Equator, and St. Antonio, in the Latitude of  $17^{\circ} 20'$  North. I look in the following Table for the Meridional Parts answering to  $17^{\circ} 20'$ , and find it to be 1056.2; the enlarg'd Difference of Latitude required.

2. If the two proposed Places be on the same Side of the Equator, then the Meridional Difference of Latitude is found by subtracting the Meridional Parts answering to the least Latitude, from those answering to the greatest, and the Difference is that required.

**Example.**

Required the Meridional Difference of Latitude between the *Lizard*, in the Latitude of  $50^{\circ}, 00'$  North, and *Antegoa*, in the Latitude of  $17^{\circ}, 30'$  North.

From the Meridional Parts of  $- 50^{\circ}, 00' = 3474.5$   
 subtract the Merid. Parts of  $- 17^{\circ}, 30' = 1066.7$

there remains - - - - -  $2407.8$   
 the Meridional Difference of Latitude required.

3. If the Places lie on different Sides of the Equator, then the Meridional Difference of Latitude is found by adding together the Meridional Parts answering to each Latitude, and the Sum is that required.

**Example.**

Required the Meridional Difference of Latitude between *Antegoa*, in the Latitude of  $17^{\circ}, 30'$  North, and *Lima*, in *Peru*, in the Latitude of  $12^{\circ}, 30'$  South.

To the Merid. Parts answering to  $17^{\circ}, 30' = 1066.7$   
 add these answering to - -  $12^{\circ}, 30' = 756.1$

the Sum is - - - - -  $1822.8$   
 the Meridional Difference of Latitude required.

**C A S E 2.**

*The Latitudes and Longitudes of two Places given, to find the direct Course and Distance between them.*

**Example.**

## Example.

Required to find the direct Course and Distance between the *Lizard*, in the Latitude of  $50^{\circ}, 00'$  North, and *Port-Royal* in *Jamaica*, in the Latitude of  $17^{\circ}, 40'$ ; differing in Longitude  $70^{\circ}, 46'$ , *Port-Royal* lying so far to the Westward of the *Lizard*.

## Preparation.

From the Latitude of the *Lizard* - -  $50^{\circ}, 00'$   
 subtract the Latitude of *Port-Royal* - -  $17, 40$

and there remain - - - - -  $32, 20$

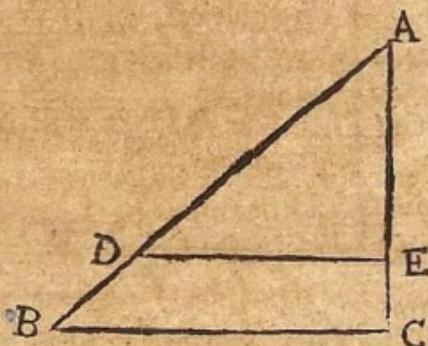
equal to 1940 Minutes, the proper Difference of Latitude.

Then from the Merid. Parts of  $50^{\circ}, 00'$  -  $3474.5$   
 subtract those of - - -  $17, 40$  -  $1077.2$

and there remain - - - - -  $2397.3$   
 the Meridional or enlarg'd Difference of Latitude.

## Geometrically.

Draw the Line AC representing the Meridian of



the *Lizard* at A, and set off from A, upon that Line,

Line, AE equal to 1940 (from any Scale of equal Parts) the proper Difference of Latitude, also AC equal to 2397.3 (from the same Scale) the Meridional or enlarg'd Difference of Latitude. Upon the Point C raise CB perpendicular to AC, and make CB equal to 4246, the Minutes of Differences of Longitude,

Join AB, and thro' E draw ED parallel to BC; so the Case is constructed, and AD applied to the same Scale of equal Parts the other Legs were taken from, will give the direct Distance, and the Angle DAE, measured by the Line of Chords, will give the Course.

### *By Calculation.*

For the Angle of the Course EAD it will be,  
(by Case 4. of Rectangular Trigonometry.)

$$AC : CB :: R : T, \text{ BAC, i. e.}$$

As the Meridional Diff. of Lat. 2397.3 = 3.37970  
is to the Difference of Long. 4246.0 = 3.62798  
so is Radius - - - - - 10.00000  
to the Tang. of the dir. Course  $60^\circ, 33'$  10.34828  
which because Port-Royal is Southward of the Lizard, and the Difference of Longitude Westerly, will be South  $60^\circ, 33'$  West, or SW by W  $\frac{1}{2}$  West, nearly.

Then for the Distance AD, it will be, by Case 2. of Rectangular Trigonometry.

$$R : AE :: \text{Sec. A} : AD, \text{ i. e.}$$

As the Radius - - - - - 10.00000  
is to the proper Diff. of Lat. 1940 - 3.28780  
so is the Sec. of the Course.  $60^\circ, 33'$  10.30833  
to the Distance - - - 3945.6 - 3.59613  
conse-

consequently the direct Course and Distance between the Lizard and Port-Royal in Jamaica, is South  $60^{\circ}$ ,  $33'$  West, 3945.6 Miles.

## CASE 3.

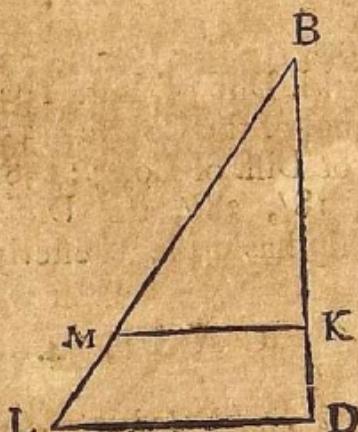
*Course and Distance sail'd given, to find the Difference of Latitude and Difference of Longitude.*

## Example.

Suppose a Ship from the Lizard in the Latitude of  $50^{\circ}$ ,  $00'$  North, sails South  $35^{\circ}$ ,  $40'$  West 156 Miles. Required the Latitude come to, and how much she has alter'd her Longitude.

## Geometrically.

1. Draw the Line BK representing the Meridian of the Lizard at B; from B draw the Line BM,



making with BK an Angle equal to  $35^{\circ}, 40'$ , and upon this Line set off BM equal to 156, the given Distance,

Distance, and from M let fall the Perpendicular MK upon BK.

Then for BK, the proper Difference of Latitude, it will be, by Case 3. of Rectangular Trigonometry.

$$R : MB :: S, BMK : BK.$$

i. e. As Radius - - - - - 10.00000  
 is to the Distance - - - - - 193.4 - 2.19312  
 so is the Co-sine of the Course  $35^{\circ}, 40'$  9.90978  
 to the proper Diff. of Latitude 127 - 2.10290  
 equal to  $2^{\circ}, 07'$ , and since the Ship is sailing from a North Latitude towards the South, therefore the Latitude come to will be  $47^{\circ}, 53'$  North. Hence the Meridional Difference of Latitude will be 193.4.

2. Produce BK to D, till BD be equal to 193.4; thro' D draw DL parallel to MK, meeting DM produced in L; then DL will be the Difference of Longitude: to find which by Calculation; it will be, (by Case 1. of Rectangular Trigonometry.)

$$R : BD :: T, LBD : DL.$$

i. e. As Radius - - - - - 10.00000  
 is to the Merid. Diff. of Lat. 193.4 - 2.28646  
 so is the Tang. of the Course  $35^{\circ}, 40'$  9.85594  
 to the Min. of Diff. of Long. 138.8 - 2.14240  
 equal to  $2^{\circ}, 18', 38''$ , the Difference of Longitude the Ship has made Westerly.

#### C A S E 4.

*Given, Course and both Latitudes, viz. the Latitude sail'd from, and the Latitude come to, to find the Distance sail'd, and the Difference of Longitude.*

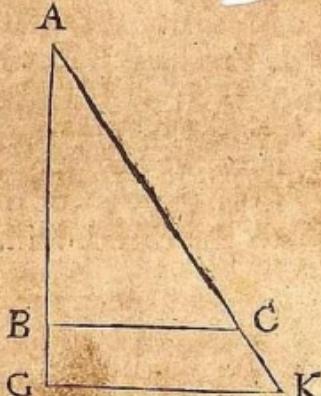
Example.

## Example.

Suppose a Ship in the Latitude of  $54^{\circ} 20'$  N.E. sails South  $33^{\circ} 45'$  East, until by Observation she's found to be in the Latitude of  $51^{\circ} 45'$  North. Required the Distance sail'd, and the Difference of Longitude.

## Geometrically.

Draw A B, to represent the Meridian of the Ship in the first Latitude, and set off from A to B 155, the Minutes of the proper Difference of Latitude, also A G equal to 257.9 the Minutes of the enlarg'd Difference of Latitude. Thro' B and G draw the Lines B C and G K perpendicular to A G; also draw A K making with A G an Angle of  $33^{\circ} 45'$  which will meet the two former Lines in the Points C and K; so the Case is constructed, and A C and GK may be found from the Line of equal Parts, to find which



## By Calculation.

First, For the Difference of Longitude it will be, by Case I. of Rectangular Trigonometry.

$$\text{R : A G} :: \text{T}, \text{G A K} : \text{G K}.$$

i. e. As Radius is to the enlarg'd Diff. of Lat.  $\frac{10.00000}{257.9 - 2.41145}$   
 $\text{H h}$

so is the Tang. of the Course  $33^{\circ} 45'$  - .9.82489  
to the Min. of Diff. of Longit. - 172.3 - 2.23634

equal to  $2^{\circ} 52' 18''$ , the Difference of Longitude  
the Ship has made Easterly.

This might also have been found, by first finding  
the Departure BC (by Case 2. of Plane Sailing.) and  
then (by Art. 74. Sect. 1.) it would

$AB : BC :: AG : GK$ . The Difference of  
Longitude required.

Then for the direct Distance A C, it will be, by  
*Case 2. of Rectangular Trigonometry.*

$$R : AB :: \text{Sec. } A : AC.$$

i. e. As Radius - - - - - 10.00000  
is to the proper Diff. of Lat. 155 - - - 2.19033  
so is the Secant of the Course  $33^{\circ}, 45'$  10.08015  
to the direct Distance - - 186.4 - - 2.27048

consequently the Ship has sail'd South  $33^{\circ}, 45'$   
East, 186.4 Miles, and has differ'd her Longitude  
 $2^{\circ}, 52' 18''$  Easterly.

### C A S E 5.

*Both Latitudes, and Distance sail'd, given, to find  
the direct Course, and Difference of Longitude.*

### Example.

Suppose a Ship from the Latitude of  $45^{\circ}, 26'$  North, sails between North and East 195 Miles, and then by Observation she's found to be in the Latitude of  $48^{\circ}, 06'$  North. Required the direct Course and Difference of Longitude.

*Geometrically.*

## Geometrically.

Draw A B equal to 160 the proper Difference of Latitude, and from the Point B raise the perpendicular B D; then take 195 in your Compasses, and setting one Foot of them in A, with the other cross the Line B D in D. Produce A B till A C be equal to 233.6 the enlarg'd Difference of Latitude. Thro' C draw C K parallel to B D, meeting A D produc'd in K; so the Case is constructed, and the Angle A may be measured by the Line of Chords, and C K by the Line of equal Parts. To find which

## By Calculation.

*First,* For the Angle of the Course B A D it will be, (by Case 5. of Rectangular Trigonometry.)

$$A B : R :: A D : \text{Sec. A. i. e.}$$

As the proper Diff. of Lat.	160.	- - -	2.20412
is to Radius	- - -	- - -	10.00000
so is the Distance	- - -	- - -	195. - - .2.29003
to the Sec. of the Course		34°, 52'	- 10.08591

which because the Ship is sailing between North and East, will be North 34°, 52' East, or S E b S 1°, 07' Easterly:

*Then for the Difference of Longitude it will be,*  
(by Case 1. of Rectangular Trigonometry.)

R: AC:: T, A: CK.

i. e. As Radius - - - - - 1.00000  
 is to the Merid. Diff. of Lat. - 233. - 2.36847  
 so is the Tangent of the Course  $34^{\circ}$  - 9.84307  
 to the Min. Diff. of Long. - 162.8 - 2.21134  
 equal to  $2^{\circ} 42' 48''$ , the Difference of Longitude  
 Easterly.

## C A S E . 6.

*One Latitude, Course, and Difference of Longitude, given, to find the other Latitude, and Distance sail'd.*

## Example.

Suppose a Ship from the Latitude of  $48^{\circ}$ ,  $50'$  North, sails South  $34^{\circ}, 40'$  West, till her Difference of Longitude is  $2^{\circ}, 44'$ . Required the Latitude come to, and the Distance sail'd.

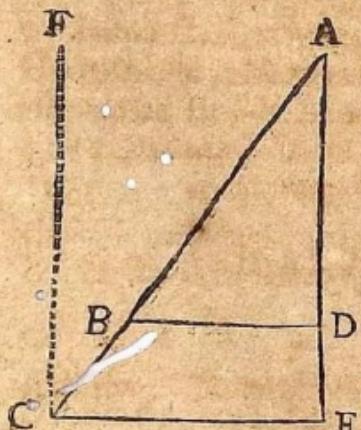
## Geometrically.

1. Draw A E to represent the Meridian of the Ship in the first Latitude, and make the Angle E A C equal to  $34^{\circ}, 40'$ ; the Angle of the Course; then draw F C parallel to A E, at the Distance of 164 the Minutes of Difference of Longitude,

which will meet A C in the Point C. From C let fall upon A E the perpendicular C E; then A E will be the enlarg'd Difference of Latitude. To find which, by Calculation it will be, by Case 1.

of Rectangular Trigonometry.

T,



T, A; R:: CE: A E.

i.e. As the Tang. of the Course  $34^\circ, 40'$  - 9.83984  
is to the Radius - - - - - 10.00000  
so are the Min. of Diff. Long. - 164. -- 2.21484  
to the enlarg'd Diff. of Lat. - 237.2 - - 2.37500

and because the Ship is sailing from a North Latitude Southerly. Therefore,

From the Merid. Parts of the Latitude sail'd from  $48^\circ, 50'$  - 3366.9  
take the Merid. Diff. of Lat. - - - - - 237.2

and there remains - - - - - 5129.7

the Meridional Parts of the Latitude come to, viz.  
 $46^\circ, 09'$ .

Hence for the proper Difference of Latitude,

From the Latitude sail'd from -  $48^\circ, 50'$  N  
take the Latitude come to - - -  $46, 09$  N

and there remain - - - - - 2, 40

equal to 161, the Minutes of Difference of Latitude.

2. Set off upon A E the Length A D equal to 161 the proper Difference of Latitude, and thro' D draw D B parallel to C E; then A B will be the direct Distance. To find which, by Calculation, it will be, by Case 2. of Rectangular Trigonometry.

R: A D:: Sec. A: A B.

i.e. As Radius - - - - - 10.00000  
is to the proper Diff. of Lat. 161 - - - 2.20683  
so is the Sec. of the Course  $34^\circ, 40'$  10.08488  
to the direct Distance - - - 195.8 - - 2.29171

CASE 7

## CASE 7.

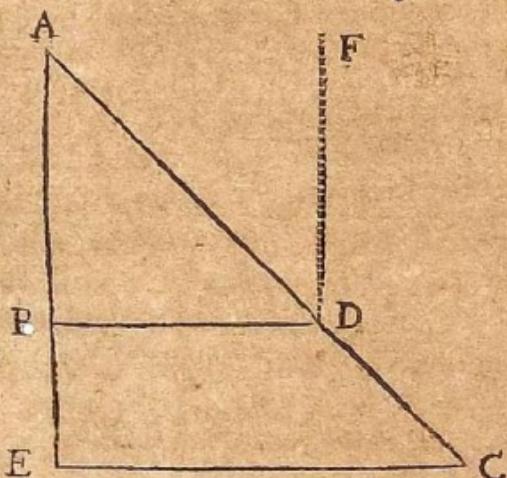
*One Latitude, Course and Departure given, to find the other Latitude, Distance sail'd, and Difference of Longitude.*

*Example.*

Suppose a Ship sails from the Latitude of  $54^{\circ}$ ,  $36'$  North, South  $42^{\circ}, 33'$  East, until she has made of Departure 116 Miles. Required the Latitude she is in, her direct Distance sail'd, and how much she has alter'd her Longitude.

*Geometrically.*

I. Having drawn the Meridian A B, make the Angle B A D equal to  $42^{\circ}, 33'$ . Draw F D pa-



rallel to A B at the Distance of 116, which will meet A D in D. Let fall upon A B the perpendicular D B. Then A B will be the proper Difference

rence of Latitude, and A D the direct Distance, to find which, *by Calculation*; first, for the Distance A D it will be, by *Case 2. Rectangular Trigonometry*.

$$S, A : BD :: R : A D.$$

i. e. As the Sine of the Course	$42^\circ, 33'$	9.83010
is to the Departure	- - - 116.	- - 2.06446
so is Radius	- - - - -	10.00000
to the direct Distance	- - 171.5	- - 2.23436

Then for the proper Difference of Latitude it will be, by *Case 1. of Rectangular Trigonometry*,

$$T, A : BD :: R : AB.$$

i. e. As the Tang. of the Course	$42^\circ, 33'$	9.96281
is to the Departure	- - - 116.	- - 2.06446
so is Radius	- - - - -	10.00000
to the proper Diff. of Lat.	- - 126.4	- - 2.10165

equal to  $2^\circ, 6'$ , consequently the Ship has come to the Latitude of  $52^\circ, 30'$  North, and so the Meridional Difference of Latitude will be 212.2.

2. Produce A B to E, till A E be equal to 212.2; and thro' E draw E C parallel to B D, meeting A D produc'd in C; then E C will be the Difference of Longitude, to find which, *by Calculation*, it will be, by *Case 1. of Rectangular Trigonometry*.

$$R : AE : T, A : EC.$$

i. e. As Radius	- - - - -	10.00000
is to the Meridian Diff. of Lat.	- 212.2	- 2.32675
so is the Tang. of the Course	$42^\circ, 33'$	9.96281
to the Min. of Diff. of Long.	- 194.8	- 2.28956

equal to  $3^\circ, 14', 48''$ , the Difference of Longitude Easterly.

This might have been found otherwise; thus, because the Triangles A C E, A D B are similar, therefore (by Art. 74. Sect. 1.) it will be

$$AB : BD :: AE : EC:$$

i. e. As the proper Diff. of Lat. - 126.4 = 210105  
is to the Departure - - - - 116. - 2.06446  
so is the enlarged Diff. of Lat. - - 212.2 = 2.32675  
to the Min. of Diff. of Long. -- 194.8 - 2.28956

### C A S E 8.

*Both Latitudes and Departure given, to find the Course, Distance and Difference of Longitude.*

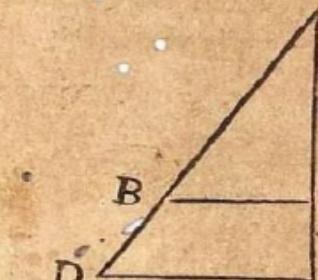
#### Example.

Suppose a Ship from the Latitude of  $46^{\circ} 20'$  North, sails between South and West, till she has made of Departure 126.4 Miles; and is then found by Observation to be in the Latitude of  $43^{\circ} 35'$  North. Required the Course and Distance sail'd, and Difference of Longitude.

#### Geometrically.

Draw AK to represent the Meridian of the Ship

A in her first Latitude, set off upon it A C, equal to 165, the proper Difference of Latitude. Draw BC perpendicular to C, equal to 126.4 the Departure, and join AB. Set off from A, AK equal to 232.3, the enlarg'd Difference of Latitude, and through K draw KD parallel to BC, meeting A B produc'd in D; so the Case is construct-ed,



structed, and D K will be the Difference of Longitude, A B the Distance, and the Angle A the Course to find which.

### By Calculation.

First, For D K, the Difference of Longitude, it will be (by Art. 7. Sect. 1.)

$$AC : CB :: AK : KD.$$

i.e. As the proper Diff. of Lat. 165 - 2.21748  
 is to the Departure - - 126.4 - 2.10175  
 so is the enlarr'd Diff. of Lat. 233.3 - 2.36791  
 to the Minutes of Diff. of Long. 178.7 - 2.25218  
 equal to  $2^{\circ} 58' 42''$ , the Difference of Longitude Westerly.

Then for the Course it will be, (by Case 4. of Rectangular Trigonometry.

$$AC : BC :: R : T, A.$$

i.e. As the proper Diff. of Lat. 165 - 2.21748  
 is to the Departure - - 126.4 - 2.10175  
 so is Radius - - - - - 10.00000  
 to the Tang. of the Course -  $37^{\circ} 27' 9.88427$   
 which, because the Ship sails between South and West, will be South  $37^{\circ} 27'$  West, or SW by S  
 $6^{\circ}, 30'$  Westerly.

Last, For the Distance A B, it will be, (by Case 2. of Rectangular Trigonometry.

$$S, A : BC :: R : AB.$$

i.e. As the Sine of the Course	$37^\circ, 27'$	-	9.8395
is to the Departure	- -	126.4	- 2.10175
so is Radius	- - -	-	10.00000
to the direct Distance	-	207.9	- 2.31780

## C A S E 9.

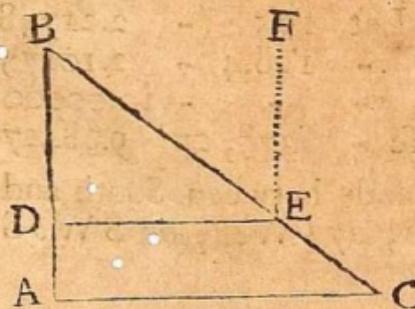
One Latitude, Distance sail'd, and Departure given, to find the other Latitude, Difference of Longitude and Course.

## Example.

Suppose a Ship in the Latitude of  $48^\circ, 33'$  North, sails between South and East 138 Miles, and has then made of Departure 112.6. Required the Latitude come to, the direct Course and Difference of Longitude.

## Geometrically.

1. Draw BD for the Meridian of the Ship at B,



and parallel to it draw FE, at the Distance of 112.6, the Departure. Take 138, the Distance, in your Compasses, and fixing one Point of them in B, with the other cross the Line FE in the point E; then join B and E,

and from E let fall upon BD the Perpendicular ED; so BD will be the proper Difference of Latitude, and the Angle B will be the Course; to find which, by Calculation.

First, For the Course it will be, (by Case 5. of Rectangular Trigonometry.)

$$BE : R :: DE : S, B.$$

i. e. As the Distance - - .138 - - 2.13988  
 is to Radius - - - - - 10.00000  
 so is the Departure - - - - 112.6 - - 2.05154  
 to the Sine of the Course - 54°, 41' 9.91166  
 which because the Ship sails between South and  
 East, will be South 54°, 41' East, or SE 9°, 41'  
 Easterly.

Then for the Difference of Latitude it will be, (by Case 3. of Rectangular Trigonometry.)

$$R : BE :: Co-S, B : BD.$$

i. e. As Radius - - - - - 10.00000  
 is to the Distance - - .138 - - 2.13988  
 so is the Co-sine of the Course 54°, 41' 9.76200  
 to the Difference of Latitude 79.8 - - 1.90188

equal to 1°, 19'. Consequently the Ship has come  
 to the Latitude of 47°, 13'. Hence the Meridional  
 Difference of Latitude will be 117.7.

2. Produce B to A, till BA be equal to 117.7,  
 and through A draw AC parallel to DE, meeting  
 BE produc'd in C; then AC will be the Difference  
 of Longitude, to find which, by Calculation it will  
 be (by Art. 74. Sect. I.)

$$BD : DE :: BA : AC.$$

i. e. As the proper Diff. of Lat. 79.8 - - 1.90188  
 is to the Departure - - - - 112.6 - - 2.05154  
 so is the enlarg'd Diff. of Lat. 117.7 - - 2.07078  
 to the Difference of Longitude 166.1 - - 2.22044  
 I i 2 equal

equal to  $2^{\circ} 46' 06''$ , the Difference of Longitude Easterly.

9. From what has been said, it will be easy to solve a Traverse according to the Rules of Mercator's Sailing.

### Example.

Suppose a Ship at the *Lizard* in the Latitude of  $50^{\circ} 00'$  North, is bound to the *Madera*, in the Latitude of  $32^{\circ} 20'$  North, the Difference of Longitude between them, being  $11^{\circ} 40'$  the West End of the *Madera*, lying so much to the Westward of the *Lizard*, and consequently the direct Course and Distance (by Case 2. of this Sett.) is South  $26^{\circ} 15'$  West 1181.9 Miles; but by reason of the Winds she is forced to sail on the following Courses (Allowance being made for Lee-way and Variation, &c.) SSW 44 Miles, Sb W  $\frac{1}{2}$  West 36 Miles, SWbS 56 Miles, and Sb E 28 Miles. Required the Latitude the Ship is in, her Bearing and Distance from the *Lizard*, and her direct Course and Distance from the *Madera*, at the End of these Courses.

The Geometrical Construction of this Traverse is perform'd by laying down the two Ports, according to the Construction of Case 2. of this Sett. and the several Courses and Distances according to Case 3. by which we have the following Solution by Calculation.

i. Course SSW, Distance 44 Miles.  
For Difference of Latitude,

As Radius	- - - - -	10.00000
is to the Distance	- - - 44 -	1.64345
so is the Co-sine of the Course	$22^{\circ} 30'$	9.96562
to the Difference of Latitude	40.65 -	1.60907

and

and since the Course is Southerly, therefore the Latitude come to will be  $49^{\circ} 20'$  North, and consequently the Meridional Difference of Latitude will be 61.8. Then,

### For the Difference of Longitude.

As Radius - - - - - 10.00000  
 is to the enlarg'd Diff. of Lat. 61.8 - 1.79099  
 so is the Tang. of the Course  $22^{\circ}, 30'$  9.61722  
 to the Minutes of Diff. of Long. 25.6 - 1.40821

### 2. Course S $\frac{1}{2}$ W $\frac{1}{2}$ West, Distance 36 Miles.

#### For Difference of Latitude.

As Radius - - - - - 10.00000  
 is to the Distance - - 36 - 1.55630  
 so is the Co-sine of the Course  $16^{\circ}, 52'$  9.98090  
 to the Difference of Latitude 34.46 - 1.53720

and since the Course is Southerly, therefore the Latitude come to will be  $48^{\circ} 45'$ . Hence the Meridional Difference of Latitude will be 53.4  
 Then,

### For the Difference of Longitude.

As Radius - - - - - 10.00000  
 is to the enlarg'd Diff. of Lat. 53.4 - 1.72754  
 so is the Tang. of the Course  $16^{\circ}, 52'$  9.48171  
 to the Difference of Longitude 16.19 - 1.20925

### 3. Course S W $\frac{1}{2}$ S, Distance 56 Miles.

#### For Difference of Latitude.

As Radius - - - - - 10.00000  
 is to the Distance - - 56 - 1.74819  
 so is the Co-sine of the Course  $33^{\circ}, 45'$  9.91985  
 to the Difference of Latitude 46.56 - 1.66804  
 conse-

consequently the Latitude come to is  $47^{\circ} 59'$ ;  
and therefore the enlarg'd Difference of Latitude  
will be 69.2. Then,

### For the Difference of Longitude.

As Radius - - - - -	10.00000
is to the enlarg'd Diff. of Lat. 69.2 -	1.84011
so is the Tang. of the Course $33^{\circ}, 45'$	9.82489
to the Difference of Long. - 46.24 -	1.66500

### 4. Course S by E, Distance 28 Miles.

#### For Difference of Latitude.

As Radius - - - - -	10.00000
is to the Distance - - 28 -	1.44716
so is the Co-sine of the Course $11^{\circ}, 15'$	9.99157
to the Difference of Latitude 27.46 -	1.43873

consequently the Latitude come to will be  $47^{\circ}$ ,  
 $31'$ , and hence the Meridional Difference of La-  
titude will be 43.2. Then,

#### For the Difference of Longitude.

As Radius - - - - -	10.00000
is to the enlarg'd Diff. of Lat. 43.2 -	1.63548
so is the Tang. of the Course $11^{\circ}, 15'$	9.29866
to the Difference of Long. - 8.59 -	0.92414

Now these several Courses and Distances, toge-  
ther with the Difference of Latitude and Longi-  
tude, belong to each of them, being set down in  
their proper Columns in the *Traverse Table*, will  
stand as follows.

Course	Dist.	Diff. of Lat.		Longit.	
		N.	S.	E.	W.
SSW	44	—	40.65	—	25.00
Sb W b W	36	—	34.46	—	16.19
SW b S	56	—	46.56	—	46.24
Sb E	8	—	27.46	3.59	—
		Diff. of Lat.	149.13	8.59	88.03 8.59
				Diff. of Long.	79.44

Hence it is plain, that the Ship has made of Southing 149.13 Minutes, and consequently has come to the Latitude of  $47^{\circ} 31'$  North, and so the Meridional Difference of Latitude between that and her first Latitude will be 226.1; and since she has made of Difference of Longitude 79.44 Minutes Westerly; therefore for the direct Course and Distance between the *Lizard* and the Ship, it will be, (by Case 2. of this Section.)

#### For the direct Course.

As the Merid. Diff. of Lat. 226.1 - - 2.3543°  
 is to Radius - - - - - 10.00000  
 so is the Diff. of Long. - 79.44 - 1.90004  
 to the Tang. of the Course  $19^{\circ}, 22'$  - 9.54574  
 which because the Difference of Latitude is Southerly, and the Difference of Longitude Westerly,  
 will be South  $19^{\circ}, 22'$  West, or Sb W  $8^{\circ}, 07'$  Westerly. Then,

#### For the direct Distance.

As Radius - - - - - 10.00000  
 is to the proper Diff. of Lat. 149.13 - 2.17349  
 so is the Sec. of the Course -  $19^{\circ}, 22'$  10.02530  
 to the direct Distance - 158 - - 2.19879  
From

From the Latitude the Ship is in -  $47^{\circ}, 51' \text{ N}$   
 subtract Lat. of the Madera -  $32, 20 \text{ N}$

---

and there remains - - - -  $15, 11$   
 equal to 91 Minutes, the proper Difference of  
 Latitude between the Ship and the Madera

Again, from the Merid. Parts answering to the Latitude the Ship is in  $\frac{1}{2} - 3248.4$   
 Take the Meridional Parts answering to the Latitude of the Madera  $\frac{1}{2} - 2052.0$

---

and there remains - - - - -  $1196.4$   
 the enlarr'd Difference of Latitude between the  
 Ship and the Madera.

Also, from the Diff. of Long. between the Lizard and the Madera  $\frac{1}{2} 11^{\circ}, 40' \text{ W}$   
 Take the Difference of Long. between the Lizard and the Ship  $\frac{1}{2} 1, 19 \frac{44}{60} \text{ W}$

---

and there remains - - - -  $10, 20 \frac{56}{60} \text{ W}$   
 equal to 620.56 Min. of Difference of Longitude  
 between the Ship and the Madera Westerly.

Then, for the direct Course and Distance between  
 the Ship and the Madera, it will be

#### For the direct Course.

As the Merid. Diff. of Lat.	$1196.4$	-	$3.07788$
is to Radius	- - - - -	-	$10.00000$
so is the Diff. of Long.	$620.56$	-	$2.79278$
to the Tang. of the Course	$27^{\circ}, 25'$	-	$9.71490$

#### For the direct Distance.

As Radius	- - - - -	-	$10.00000$
is to the proper Diff. of Lat.	$911$	-	$2.95952$
		-	$10$

so is the Sec. of the Course  $27^{\circ}$ , &  $0.05174$   
to the direct Distance - -  $102$ ,  $3.01126$

10. It is very common in working a Day's Reckoning at Sea, to find the Difference of Latitude and Departure to each Course and Distance, and adding all the Departures together, and all the Differences of Latitudes for the whole Departure and Difference of Latitude made good that Day; from thence (by Case 8. of this Section) to find the Difference of Longitude, &c. made good that Day. Now that this Method is false, will evidently appear, if we consider that the same Departure reckon'd on two different Parallels will give unequal Differences of Longitude; and consequently when several Departures are compounded together and reckon'd on the same Parallel, the Difference of Longitude resulting from that, cannot be the same with the Sum of the Differences of Longitude resulting from the several Departures on different Parallels; and therefore, I have chosen in the last Example of a Traverse, to find the Difference of Longitude answering to each particular Course and Distance, the Sum of which must be the true Difference of Longitude made good by the Ship on these several Courses and Distances.

11. We shew'd at Art. 5. of this Section, how to construct a Mercator's Chart, and now we shall proceed to its several Uses; contain'd in the following Problems.

Prob. 1. Let it be required to lay down a Place upon the Chart, its Latitude, and the Difference of Longitude between it, and some known Place upon the Chart being given.

Example. Let the known Place be the Lizard, lying on the Parallel of  $50^{\circ}, 00'$  N. and the Place to be laid down St. Katharines, on the East Coast of America, differing in Longitude from the Lizard  $42^{\circ}, 36'$ , lying so much to the Westward of it.

Let L represent the *Lizard* on the Chart, (see Plate I.) lying on the Parallel of  $50^{\circ}, 00'$  North, its Meridian A E. Set off from E upon the Equator EQ $^{\circ} 45^{\prime}$ ,  $36^{\prime}$ , towards Q, which will reach from E to F. Thro' F draw the Meridian FG, and this will be the Meridian of St. Katharines; then set off from Q,  $0^{\circ} H$  upon the graduated Meridian Q B,  $28$  Degrees; and thro' H draw the Parallel of Latitude HM, which will meet the former Meridian in K the Place upon the Chart required.

*Prob. 2.* Given two Places upon the Chart, to find their Difference of Latitude and Difference of Longitude.

Thro' the two Places draw Parallels of Latitude; then the Distance between these Parallels number'd in Degrees and Minutes upon the graduated Meridian, will be the Difference of Latitude required; and thro' the two Places drawing Meridians, the Distance between these counted in Degrees and Minutes on the Equator, or any graduated Parallel, will be the Difference of Longitude required.

*Prob. 3.* To find the Bearing of one Place from another upon the Chart.

*Example.* Required the Bearing of St. Katharines at K, (see Plate I.) from the *Lizard* at L.

Draw the Meridian of the *Lizard* A E, and join K and L with the right Line KL, then by the Line of Chords measuring the Angle K L E, and with that entering the Table at Page 156, we shall have the Thing required.

This may also be done, by having Compasses drawn on the Chart (suppose at two of its Corners) then lay the Edge of a Ruler over the two Places and let fall a Perpendicular, or take the nearest Distance from the Center of the Compass next the first Place, to the Ruler's Edge; then with this Distance in your Compasses slide them along by the Ruler's Edge, keeping one Foot of them close to the

the Ruler, and the other as near as you can judge perpendicular to it, which will determine the Radius required.

*Prob. 4.* To find the Distance between two given Places upon the Chart.

This Problem admits of four Cases according to the Situation of the two Places, with Respect to one another.

*Case 1.* When the given Places lie both upon the Equator.

In this Case their Distance is found by converting the Degrees of Difference of Longitude intercepted between them into Minutes.

*Case 2.* When the two Places lie both on the same Meridian.

Draw the Parallels of those Places, and the Degrees upon the graduated Meridian, intercepted between those Parallels reduced to Minutes, give the Distance required.

*Case 3.* When the two Places lie on the same Parallel.

*Example.* Required to find the Distance between the Points K and N, (see Plate 1.) both lying on the Parallel of  $28^{\circ}$ , or North. Take from your Scale the Chord of  $60^{\circ}$ , or Radius in your Compasses, and with that Extent on KN as a Base, make the Isosceles Triangle KPN; then take from the Line of Sines the Co-sine of the Latitude, or Sine of  $62^{\circ}$ , and set that off from P to S and T. Join S and T with the right Line ST, and that applied to the graduated Equator will give the Degrees and Minutes upon it equal to the Distance; which, converted into Minutes, will be the Distance required.

The Reason of this is evident from *Sect. 8.* for it has been there demonstrated, that Radius is to the Co-sine of any Parallel, as the Length of any Arch on the Equator, to the Length of the same Arch on

that Parallel now in this Chart KN is the Distance of the Meridians of the two Places K and N upon the Equator, and since in the Triangle PNK, ST is parallel to KN, therefore  $PN : PT :: NK : TS$ . Consequently TS will be the Distance of the two Places K and N upon the Parallel of  $28^{\circ}$ .

If the Parallel of the two Places lies on be not far from the Equator, and they not far asunder; then their Distance may be found thus. Take the Distance between them in your Compasses, and apply that to the graduated Meridian, so as the one Foot may be as many Minutes above, as the other is below the given Parallel, and the Degrees and Minutes intercepted, reduced to Minutes, will give the Distance.

Or it may also be found thus. Take the Length of a Degree on the Meridian at the given Parallel, half a Deg. above, and half a Deg. below the Parallel, and turn that over on the Parallel from the one Place to the other, as oft as you can; then as oft as that Extent is contain'd between the Places, so many times 60 Miles will be contain'd in the Distance between them.

*Case 4.* When the Places differ both in Longitude and Latitude.

*Example.* Suppose it were required to find the Distance between the two Places *a* and *e* upon the Chart. By,

*Prob. 2.* Find the Difference of Latitude between them, and take that in your Compasses from the graduated Equator, which set off on the Meridian of *a*, from *a* to *b*; then thro' *b* draw *b c* parallel to *d e*, and taking *a c* in your Compasses, apply it to the graduated Equator and it will show the Degrees and Minutes contain'd in the Dist. required, which multiplied by 60 will give the Miles of Distance.

The Reason of this is evident from Art. 8. of this Sect. for 'tis plain *a d* is the enlarg'd Difference of

of Latitude and  $a b$  the proper; consequently  $a c$  the enlarg'd Distance and  $a c$  the place.

*Prob. 5.* To lay down a Place upon a Chart, its Latitude and Bearing from some known Place upon the Chart being known; or (which is the same) having the Course and Difference of Latitude that a Ship has made, to lay down the Running of the Ship, and find her Place upon the Chart.

*Example.* A Ship from the *Lizard* in the Latitude of  $50^{\circ}, 00'$  North, sails SSW till she has differ'd her Latitude  $36^{\circ}, 40'$ . Required her Place upon the Chart.

Count from the *Lizard* at *L*, on the graduated Meridian downwards (because the Course is Southly)  $36^{\circ}, 40'$  to *g*; thro' which draw a Parallel of Latitude, which will be the Parallel the Ship is in; then from *L* draw a SSW Line *Lf*, cutting the former Parallel in *f*, and this will be the Ship's Place upon the Chart.

*Prob. 6.* One Latitude, Course and Distance sail'd, given to lay down the Running of the Ship, and find her Place upon the Chart.

*Example.* Suppose a Ship at *a* in the Latitude of  $20^{\circ}, 00'$  North, sails North  $37^{\circ}, 20'$  East,  $191$  Miles. Required the Ship's Place upon the Chart.

Having drawn the Meridian and Parallel of the Place *a*, set off the Rhumb-Line *ae*, making with *ab* an Angle of  $37^{\circ}, 20'$ , and upon it set off  $191$  from *a* to *c*; thro' *c* draw the Parallel *cb*, and taking *ab* in your Compasses, apply it to the graduated Equator, and observe the Number of Degrees it contains; then count the same Number of Degrees on the graduated Meridian from *C* to *b*, and thro' *b* draw the Parallel *be*, which will cut *ac* produc'd in the Point *e*, the Ship's Place requir'd.

*Prob. 7.* Both Latitudes, and Distance sail'd given, to find the Ship's Place upon the Chart.

*Example.* Suppose a Ship sails from  $a$  in the Latitude of  $20^{\circ}, 00'$  North, between North and E. 191 Miles and is then in the Latitude of  $45^{\circ}, 00'$  N. Required the Ship's Place upon the Chart.

Draw  $de$  the Parallel of  $45^{\circ}$ , and set off upon the Meridian of  $a$  upwards,  $ab$  equal to the proper Difference of Latitude taken from the Equator or graduated Parallel. Thro'  $b$  draw  $bc$  parallel to  $de$ ; then with 191 in your Compasses taken as before from the Equator or graduated Parallel, fixing one Foot of them in  $a$  with the other cross  $bc$  in  $c$ . Join  $a$  and  $c$  with the right Line  $ac$ , which produc'd will meet  $de$  in  $e$  the Ship's Place required.

*Prob. 8.* One Latitude, Course and Difference of Longitude, given to find the Ship's Place upon the Chart.

*Example.* Suppose a Ship from the Lizard in the Latitude of  $50^{\circ}, 00'$  North, sails SW by W, till her Difference of Longitude is  $42^{\circ}, 36'$ . Requir'd the Ship's Place upon the Chart.

Having drawn AF the Meridian of the Lizard at L, count from E to F upon the Equator  $42^{\circ}, 36'$ , and thro' F draw the Meridian FG; then from L draw the SW by W Line LK and where this meets FG, as at K, will be the Ship's Place requir'd.

*Prob. 9.* One Latitude, Course, and Departure, given, to find the Ship's Place upon the Chart.

*Example.* Suppose a Ship at  $a$  in the Latitude of  $20^{\circ}, 00'$  North, sails North  $37^{\circ}, 20'$  East, till she has made of Departure 116 Miles. Requir'd the Ship's Place upon the Chart.

Having drawn the Meridian of  $a$ , at the Distance of 116, draw Parallel to it the Meridian  $kl$ . Draw the Rumb Line  $ac$ , which will meet  $kl$  in some Point  $c$ ; then thro'  $c$  draw the Parallel  $cb$ , and  $ab$

$a b$  will be the proper Difference of Latitude, and  $b c$  the Departure. Take  $a b$  in your Compasses and apply it to the Equator or graduated Parallel; then observe the Number of Degrees it contains, and count so many on the graduated Meridian from C towards to  $b$ . Thro'  $b$  draw the Parallel  $b c$ , which will meet  $a c$  produc'd in some Point as  $e$ , which is the Ship's Place upon the Chart.

Prob. 10. One Latitude, Distance, and Departure, given, to find the Ship's Place upon the Chart.

Example. Suppose a Ship at  $a$  in the Latitude of  $20^{\circ}$ ,  $00'$  North, sails 191 Miles between North and East, and then is found to have made of Departure 116 Miles. Requir'd the Ship's Place upon the Chart.

Having drawn the Meridian and Parallel of the Place  $a$ , set off upon the Parallel  $a m$  equal to 116, and thro'  $m$  draw the Meridian  $k l$ . Take the given Distance 191 in your Compasses setting one Foot of them in  $a$ , with the other cross  $k l$  in  $c$ , join  $a c$ , and thro'  $c$  draw the Parallel  $c b$ ; so  $c b$  will be the Departure, and  $a b$  the proper Difference of Latitude; then proceeding with this as in the foregoing Problem, you'll find the Ship's Place to be  $e$ .

Prob. 11. The Latitude sail'd from, Difference of Latitude and Departure given, to find the Ship's Place upon the Chart.

Example. Suppose a Ship from  $a$  in the Latitude of  $20^{\circ}$ ,  $00'$  North, sails between North and East, till she be in the Latitude of  $45^{\circ}$ ,  $00'$  North, and is then found to have made of Departure 116 Miles. Requir'd the Ship's Place upon the Chart.

Having drawn the Meridian of  $a$ , set off upon it from  $a$  to  $b$ , 25 Degrees, (taken from the Equator or graduated Parallel) the proper Difference of Latitude; then thro'  $b$  draw the Parallel  $b c$ , and make  $b c$  equal to 116 the Departure, and join  $a c$ . Count from the Parallel of  $a$  on the graduated Meridian

Mefidians upwards to  $\text{b}$  25 Degrees, and thro'  $\text{b}$  draw the parallel  $\text{b} e$ , which will meet  $ac$  produc'd in some Part of  $c$ , and this will be the Place of the Ship required.

12. In Sect. 1. 'tis plain that the Terms *Meridional Distance*, *Departure*, and *Difference of Longitude* were synonymous, constantly signifying the same Thing; which evidently follow'd from the Supposition of the Earth's Surface being projected on a Plane, in which the Meridians were made parallel and the Degrees of Latitude equal to one another and to those of the Equator. But since it has been demonstrated (in this *Section*) that, if in the Projection of the Earth's Surface upon a Plane, the Meridians be made parallel, the Degrees of Latitude must be unequal, still increasing the nearer they come to the Pole. It follows that these Terms must denote Lines really different from one another. *Difference of Longitude* is defin'd at Art. 14. Sect. 3. *Meridional Distance* at Art. 3. Sect. 7. and *Departure* at Art. 8. of this *Section*.



TABLE  
OF  
*MERIDIONAL PARTS.*

LI

## 358 A Table of Meridional Part

L.	O	1	2	3	4	5	6	7	8
M.	Mni.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.
0	0.0	60.0	120.0	180.1	240.2	300.3	360.7	420.4	480.1
1	1.0	61.0	121.0	181.1	241.2	301.4	361.7	421.1	482.6
2	2.0	62.0	122.0	182.1	242.2	302.4	362.7	423.1	483.6
3	3.0	63.0	123.0	182.1	243.2	303.4	363.7	424.1	484.6
4	4.0	64.0	124.0	184.1	244.2	304.4	364.7	425.1	485.6
5	5.0	65.0	125.0	185.1	245.2	305.4	365.7	426.1	486.6
6	6.0	66.0	126.0	186.1	246.2	306.4	366.7	427.1	487.6
7	7.0	67.0	127.0	187.1	247.2	307.4	367.7	428.1	488.6
8	8.0	68.0	128.0	188.1	248.2	308.4	368.7	429.1	489.6
9	9.0	69.0	129.0	189.1	249.2	309.4	369.7	430.1	490.7
10	10.0	70.0	130.0	190.1	250.2	310.4	370.7	431.1	491.7
11	11.0	71.0	131.0	191.1	251.2	311.4	371.7	432.1	492.7
12	12.0	72.0	132.0	192.1	252.2	312.4	372.7	433.1	493.7
13	13.0	73.0	133.0	193.1	253.2	313.4	373.7	434.2	494.7
14	14.0	74.0	134.0	194.1	254.2	314.4	374.7	435.2	495.7
15	15.0	75.0	135.0	195.1	255.2	315.5	375.8	436.2	496.7
16	16.0	76.0	136.0	196.1	256.2	316.5	376.8	437.2	497.7
17	17.0	77.0	137.0	197.1	257.2	317.5	377.8	438.2	498.7
18	18.0	78.0	138.0	198.1	258.2	318.5	378.8	439.2	499.8
19	19.0	79.0	139.0	199.1	259.2	319.5	379.8	440.2	500.8
20	20.0	80.0	140.0	200.1	260.3	320.5	380.8	441.2	501.8
21	21.0	81.0	141.0	201.1	261.3	321.5	381.8	442.2	502.8
22	22.0	82.0	142.0	202.1	262.3	322.5	382.8	443.2	503.8
23	23.0	83.0	143.0	203.1	263.3	323.5	383.8	444.2	504.8
24	24.0	84.0	144.0	204.1	264.3	324.5	384.8	445.2	505.8
25	25.0	85.0	145.0	205.1	265.3	325.5	385.8	446.3	506.8
26	26.0	86.0	146.0	206.1	266.3	326.5	386.8	447.3	507.8
27	27.0	87.0	147.0	207.1	267.3	327.5	387.8	448.3	508.9
28	28.0	88.0	148.0	208.1	268.3	328.5	388.8	449.2	509.9
29	29.0	89.0	149.0	209.1	269.3	329.5	389.8	450.0	510.0
M.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	No
L.	O	I	2	3	4	5	6	7	8

Table of Meridional Parts. 25

L.	C.	I	2	3	4	5	6	7	8
M.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.
30.	0.0	150.	2	270.3	330.5	390.8	451.3	511.5	
31.	0	1	211.	271.3	331.5	391.9	452.3	512.5	
32.	32.0	6	152.1	212.	272.3	332.5	392.9	453.3	513.5
33.	33.0	5	153.1	213.	273.	333.5	393.9	454.3	514.5
34.	34.0	94.0	154.1	214.1	274.	334.	394.9	455.3	515.9
35.	35.0	95.0	155.1	215.1	275.	335.5	395.3	456.3	516.9
36.	36.0	96.0	156.1	216.1	276.	336.5	396.5	457.3	518.8
37.	37.0	97.0	157.1	217.1	277.	337.5	397.9	458.4	519.0
38.	38.0	98.0	158.1	218.2	278.	338.6	398.9	459.4	520.0
39.	39.0	99.0	159.1	219.2	279.3	339.5	399.9	460.4	521.0
40.	40.0	100.0	160.1	220.2	280.3	340.6	400.9	461.4	522.0
41.	41.0	101.0	161.1	221.2	281.3	341.6	401.9	462.4	523.0
42.	42.0	102.0	162.1	222.2	282.3	342.6	402.9	463.4	524.0
43.	43.0	103.0	163.1	223.2	283.3	343.6	403.9	464.4	525.0
44.	44.0	104.0	164.1	224.2	284.3	344.6	404.9	465.4	526.0
45.	45.0	105.0	165.1	225.2	285.3	345.6	405.9	466.4	527.1
46.	46.0	106.0	166.1	226.2	286.3	346.6	407.0	467.4	528.1
47.	47.0	107.0	167.1	227.2	287.3	347.6	408.0	468.4	529.1
48.	48.0	108.0	168.1	228.2	288.3	348.6	409.0	469.5	530.1
49.	49.0	109.0	169.1	229.2	289.3	349.6	410.0	470.5	531.1
50.	50.0	110.0	170.1	230.2	290.3	350.6	411.0	471.5	532.1
51.	51.0	111.0	171.1	231.2	291.4	351.6	412.0	472.5	533.1
52.	52.0	112.0	172.1	232.2	292.4	352.6	413.0	473.5	534.1
53.	53.0	113.0	173.1	233.2	293.4	353.6	414.0	474.5	535.1
54.	54.0	114.0	174.1	234.2	294.4	354.6	415.0	475.5	536.2
55.	55.0	115.0	175.1	235.2	295.4	355.6	416.0	476.5	537.2
56.	56.0	116.0	176.1	236.2	296.4	356.6	417.0	477.5	538.2
57.	57.0	117.0	177.1	237.2	297.4	357.6	418.0	478.5	539.2
58.	58.0	118.0	178.1	238.2	298.4	358.7	419.0	479.6	540.2
59.	59.0	119.0	179.1	239.2	299.4	359.7	420.0	480.6	541.2
	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.
L.	Q	I	2	3	4	5	6	7	8

560 A Table of Meridional Part

L.	9	10	11	12	13	14	15	16
M.	Min.	in.						
0	542,2	603,1	664,1	725,3	786,9	848,5	910,	92,8
1	543,3	604,1	665,1	726,4	787,9	849,9	911,	973,8
2	544,3	605,1	666,1	727,4	788,9	850,6	912,	974,8
3	545,3	606,1	667,1	728,4	789,9	851,6	913,	975,9
4	546,3	607,1	668,1	729,	790,9	852,6	914,6	976,9
5	547,3	608,	669,2	730,	791,	853,7	915,7	978,0
6	548,3	609,2	670,2	731,	793,0	854,7	916,9	979,0
7	549,3	610,2	671,2	732,	794,0	855,7	917,7	980,0
8	550,3	611,2	672,2	733,	795,0	856,8	918,8	981,1
9	551,4	612,2	673,2	734,6	796,1	857,8	919,8	982,1
10	552,4	613,2	674,3	735,6	797,1	858,9	920,8	983,2
11	553,4	614,2	675,3	736,6	798,1	859,9	921,8	984,2
12	554,4	615,3	676,3	737,6	799,1	860,0	922,9	985,2
13	555,4	616,3	677,3	738,7	800,2	862,0	923,9	986,3
14	556,4	617,3	678,3	739,7	801,2	863,0	925,0	987,3
15	557,4	618,3	679,4	740,7	802,2	864,1	926,0	988,4
16	558,4	619,3	680,4	741,7	803,2	865,0	927,0	989,4
17	559,4	620,3	681,4	742,8	804,3	866,1	928,1	990,4
18	560,5	621,3	682,4	743,8	805,3	867,2	929,1	991,5
19	561,5	622,4	683,4	744,8	806,3	868,2	930,1	992,5
20	562,5	623,4	684,5	745,8	807,3	869,2	931,2	993,6
21	563,5	624,4	685,5	746,9	808,4	870,3	932,2	994,6
22	564,5	625,4	686,5	747,9	809,4	871,3	933,2	995,6
23	565,5	626,6	687,5	748,9	810,4	872,3	934,3	996,7
24	566,6	627,4	688,5	749,9	811,4	873,4	935,3	997,7
25	567,6	628,5	689,6	751,0	812,5	874,4	936,3	998,8
26	568,6	629,5	690,6	752,0	813,5	875,4	937,4	999,8
27	569,6	630,5	691,6	753,0	814,5	876,5	938,4	1000,3
28	570,6	631,5	692,6	754,0	815,5	877,5	939,4	1001,1
29	571,6	632,5	693,6	755,1	816,6	878,5	940,5	1002,1
M.	Min.							
L.	9	10	11	12	13	14	15	16

# Table of Meridional Parts, 261

	9	10	11	12	13	14	15	16
M.	Min.	Min.						
L.	9	10	11	12	13	14	15	16
30	633.5	69.7	756.1	817.6	879.6	941.5	1004.0	
31	57	634.5	695.7	757.1	818.6	880.6	942.5	1005.0
32	57	635.6	696.7	758.1	819.7	881.6	943.6	1006.1
33	57	626.6	697.7	759.1	820.7	882.7	944.6	1007.1
34	576.7	67.6	759.7	821.7	883.7	945.6	1008.1	
35	577.7	63.6	690.0	760	822.7	884.7	946.7	1009.2
36	578.7	639.6	700.8	762	823.7	885	947.7	1010.2
37	579.7	640.6	701.8	763	824.8	886.8	948.7	1011.3
38	580.8	641.7	702.8	764	825.8	887.8	949.8	1012.3
39	581.8	642.7	703.8	765.3	826.8	888.9	950.8	1013.4
40	582.8	643.7	704.9	766.3	827.9	889.9	951.9	1014.4
41	583.8	644.5	705.9	767.4	828.9	890.9	952.9	1015.4
42	584.8	645.7	706.9	768.4	829.9	892.0	953.9	1016.5
43	585.8	646.7	707.9	769.4	831.9	893.0	955.0	1017.5
44	586.8	647.7	709.0	770.4	832.0	894.0	956.0	1018.6
45	587.9	648.8	710.0	771.5	833.0	895.1	957.1	1019.6
46	588.9	649.8	711.0	772.5	834.1	896.1	958.1	1020.6
47	589.9	650.8	712.0	773.5	835.1	897.1	959.2	1021.7
48	590.9	651.8	713.0	774.5	836.1	898.2	960.2	1022.7
49	591.9	652.8	714.1	775.6	837.2	899.2	961.3	1023.8
50	592.9	653.9	715.1	776.6	838.2	900.2	962.3	1024.8
51	593.9	654.9	716.1	777.6	839.2	901.2	963.4	1025.9
52	595.0	655.9	717.1	778.6	840.3	902.3	964.4	1026.9
53	596.0	656.9	718.1	779.7	841.3	903.3	965.5	1028.0
54	597.0	657.9	719.2	780.7	842.3	904.3	966.5	1029.0
55	598.0	659.0	720.2	781.7	843.4	905.4	967.6	1030.1
56	599.0	660.0	721.2	782.7	844.4	906.4	968.6	1031.1
57	600.0	661.0	722.3	783.8	845.4	907.4	969.6	1032.2
58	601.0	662.0	723.3	784.8	846.5	908.4	970.7	1033.2
59	602.1	663.0	724.3	785.8	847.5	909.5	971.7	1034.3
M.	Min.	Min.						
L.	9	10	11	12	13	14	15	16

262 A Table of Meridional Pa

L.	17	18	cF9	20	21	22	23
M.	Min.						
0	1035-3	1098.2	1461.5	1225.1	1239.2	1353.7	1428.7
1	1036.3	1099.3	1162.5	1226.2	1290.2	1354.1	1419.7
2	1037.4	1100.3	163.6	1227.	1291.3	1355.4	1420.8
3	1038.	1101.4	1164.7	1228.	1292.4	1356.1	1421.9
4	1039.5	1102.4	115.7	1229.	1293.5	1357.1	1423.0
5	1040.5	1103.5	1166.8	1230.	1294.5	1358.0	1424.1
6	1041.6	1104.5	1167.8	1231.	1295.6	1360.1	1425.1
7	1042.6	1105.6	1168.9	1232.6	1296.7	1361.2	1426.2
8	1043.7	1106.6	1169.0	1233.6	1297.8	1362.3	1427.3
9	1044.7	1107.7	1171.0	1234.7	1298.8	1363.3	1428.4
10	1045.8	1108.7	1172.1	1235.8	1299.9	1364.4	1429.5
11	1046.8	1109.8	1173.1	1236.8	1301.0	1365.5	1430.6
12	1047.9	1110.8	1174.2	1237.9	1302.0	1366.6	1431.7
13	1048.9	1111.9	1175.2	1239.0	1303.1	1367.6	1432.8
14	1049.9	1112.9	1176.3	1240.0	1304.2	1368.7	1433.9
15	1051.0	1114.0	1177.4	1241.1	1305.3	1369.8	1434.9
16	1052.0	1115.0	1178.4	1242.2	1306.3	1370.9	1436.0
17	1053.1	1116.0	1179.5	1243.2	1307.4	1372.0	1437.1
18	1054.1	1117.1	1180.5	1244.3	1308.5	1373.1	1438.3
19	1055.2	1118.2	1181.6	1245.4	1309.6	1374.2	1439.3
20	1056.2	1119.2	1182.7	1246.4	1310.6	1375.3	1440.4
21	1057.3	1120.3	1183.7	1247.5	1311.7	1376.4	1441.5
22	1058.3	1121.3	1184.8	1248.6	1312.8	1377.4	1442.6
23	1059.3	1122.4	1185.8	1249.6	1313.8	1378.5	1443.7
24	1060.4	1123.4	1186.9	1250.7	1314.8	1379.6	1444.8
25	1061.4	1124.5	1188.0	1251.8	1316.0	1380.7	1445.8
26	1062.5	1125.5	1189.0	1252.8	1317.1	1381.8	1446.9
27	1063.5	1126.6	1190.1	1253.9	1318.1	1382.0	1448.0
28	1064.6	1127.6	1191.1	1255.0	1319.2	1383.9	1449.1
29	1065.6	1128.7	1192.2	1256.0	1320.3	1385.0	1450.2
M.	Min.						
L.	17	18	19	20	21	22	23

Table of Meridional Parts. 26

M.	7	18	19	20	21	22	23
	Min.						
30	I	1129.7	1133.2	1257.1	1321.4	1386.1	1451.3
31	1067	1130.8	1194.2	1258.2	1322.4	1387.2	1452.4
32	1069	1131.0	1195.1	1259.2	1323.5	1388.3	1453.6
33	1069	1132.9	1195.6	1260.3	1324.6	1389.4	1454.6
34	1070	1134.0	1197.9	1261.4	1325.7	1390.4	1455.7
35	1072.0	1135.1	1198.5	1262.4	1326.7	1391.5	1456.8
36	1073.0	1136.1	1199.6	1263.5	1327.8	1392.6	1457.9
37	1074.1	1137.2	1200.7	1264.6	1328.9	1393.7	1458.9
38	1075.1	1138.2	1201.7	1265.6	1330.0	1394.8	1460.0
39	1076.2	1139.3	1202.8	1266.7	1331.0	1395.9	1461.1
40	1077.2	1140.3	1203.9	1267.8	1332.1	1396.9	1462.2
41	1078.3	1141.3	1204.9	1268.8	1333.2	1398.0	1463.3
42	1079.3	1142.4	1205.9	1269.9	1334.2	1399.1	1464.4
43	1080.4	1143.5	1207.1	1271.0	1335.2	1400.2	1465.5
44	1081.4	1144.6	1208.1	1272.1	1336.4	1401.3	1466.6
45	1082.5	1145.6	1209.2	1273.1	1337.5	1402.4	1467.7
46	1083.5	1146.6	1210.2	1274.2	1338.6	1403.4	1468.8
47	1084.6	1147.7	1211.3	1275.3	1339.7	1404.5	1469.8
48	1085.6	1148.8	1212.4	1276.3	1340.7	1405.6	1470.9
49	1086.7	1149.8	1213.4	1277.4	1341.8	1406.7	1472.0
50	1087.7	1150.9	1214.5	1278.5	1342.9	1407.8	1473.1
51	1088.8	1152.0	1215.5	1279.5	1344.0	1408.8	1474.2
52	1089.8	1153.0	1216.6	1280.6	1345.0	1409.9	1475.3
53	1090.9	1154.1	1217.6	1281.7	1346.1	1411.0	1476.5
54	1091.9	1155.1	1218.7	1282.7	1347.2	1412.1	1477.5
55	1093.0	1156.2	1219.8	1283.8	1348.3	1413.2	1478.6
56	1094.0	1157.2	1220.9	1284.9	1349.4	1414.3	1479.6
57	1095.1	1158.3	1221.9	1286.0	1350.4	1415.4	1480.8
58	1096.1	1159.4	1223.0	1287.0	1351.5	1416.5	1481.9
59	97.2	1160.4	1224.1	1288.1	1352.6	1417.6	1483.0
M.	Min.						
VL	17	18	19	20	21	22	23

## 264 A Table of Meridional Parts

L.	24	25	26	27	28	29	30
M.	Min.						
L.	24	25	26	27	28	29	30
0	1484.1	1550.0	1616.5	1683.6	1751.2	1819.5	1889.4
1	1485.2	1551.1	1617.6	1684.7	1752.3	1820.0	1890.5
2	1486.3	1552.2	1618.7	1685.8	1753.4	1821.1	1890.7
3	1487.3	1553.3	1619.8	1686.9	1754.6	1822.2	1891.9
4	1488.4	1554.1	1620.9	1688.0	1755.7	1823.0	1893.0
5	1489.5	1555.5	1622.0	1689.1	1756.8	1823.8	1894.2
6	1490.6	1556.5	1623.2	1690.3	1758.0	1826.3	1895.3
7	1491.7	1557.7	1624.3	1691.4	1759.1	1827.6	1896.5
8	1492.8	1558.8	1625.4	1692.5	1760.2	1828.6	1897.6
9	1493.9	1559.9	1626.5	1693.6	1761.4	1829.7	1898.8
10	1495.0	1561.0	1627.6	1694.8	1762.5	1830.9	1899.9
11	1496.1	1562.2	1628.7	1695.9	1763.6	1832.0	1901.1
12	1497.2	1563.2	1629.8	1697.0	1764.8	1833.2	1902.3
13	1498.3	1564.3	1631.0	1698.1	1765.9	1834.3	1903.4
14	1499.4	1565.4	1632.3	1699.2	1767.0	1835.5	1904.6
15	1500.5	1566.5	1633.2	1700.4	1768.2	1836.6	1905.7
16	1501.6	1567.6	1634.3	1701.5	1769.3	1837.8	1906.9
17	1502.7	1568.7	1635.3	1702.6	1770.5	1838.9	1908.1
18	1503.8	1569.8	1636.5	1703.8	1771.6	1840.1	1909.2
19	1504.9	1571.0	1637.7	1704.9	1772.7	1841.2	1910.4
20	1506.0	1572.1	1638.8	1706.0	1773.9	1842.4	1911.5
21	1507.1	1573.2	1639.9	1707.1	1775.0	1843.5	1912.7
22	1508.2	1574.3	1641.0	1708.3	1776.1	1844.6	1913.8
23	1509.3	1575.4	1642.1	1709.4	1777.2	1845.8	1915.0
24	1510.4	1576.5	1643.2	1710.5	1778.4	1846.9	1916.2
25	1511.5	1577.6	1644.3	1711.6	1779.5	1848.1	1917.3
26	1512.6	1578.7	1645.5	1712.8	1780.6	1849.2	1918.5
27	1513.7	1579.8	1646.7	1713.9	1781.8	1850.4	1919.6
28	1514.8	1580.9	1647.8	1715.0	1783.0	1851.5	1920.8
29	1515.9	1582.0	1648.8	1716.1	1784.1	1852.7	1921.9
M.	Min.						
L.	24	25	26	27	28	29	30

A Table of Meridional Parts. 265

L.	24	25	26	27	28	29	30
M.	Min.						
30	1527.2	1583.2	1649.9	1717.3	1785.2	1853.8	1923.1
31	1518.1	1584.3	1651.0	1718.4	1786.4	1855.0	1924.3
32	1519.1	1585.4	1652.2	1719.5	1787.5	1856.1	1925.4
33	1520.3	1586.5	1653.0	1720.7	1788.6	1857.2	1926.6
34	1521.4	1587.6	1654.4	1721.8	1789.8	1858.4	1927.8
35	1522.5	1588.7	1655.5	1722.9	1790.9	1859.6	1928.9
36	1523.5	1589.8	1656.6	1723.0	1792.1	1860.7	1930.1
37	1524.7	1590.9	1657.8	1724.2	1793.2	1861.9	1931.3
38	1525.8	1592.0	1658.9	1725.3	1794.3	1863.0	1932.4
39	1526.9	1593.2	1660.0	1726.4	1795.5	1864.2	1933.6
40	1528.0	1594.3	1661.1	1728.6	1796.6	1865.3	1934.7
41	1529.1	1595.4	1662.2	1729.6	1797.8	1866.5	1935.9
42	1530.1	1596.5	1663.4	1730.7	1798.9	1867.6	1937.1
43	1531.3	1597.5	1664.5	1731.1	1800.0	1868.8	1938.2
44	1532.4	1598.7	1665.6	1733.1	1801.2	1869.9	1939.4
45	1533.5	1599.8	1666.7	1734.2	1802.3	1871.1	1940.5
46	1534.6	1600.9	1667.8	1735.3	1803.5	1872.2	1941.7
47	1535.7	1602.0	1669.0	1736.5	1804.6	1873.4	1942.9
48	1536.8	1603.1	1670.1	1737.6	1805.7	1874.5	1944.0
49	1537.9	1604.3	1671.2	1738.7	1806.9	1875.7	1945.2
50	1539.0	1605.4	1672.3	1739.9	1808.0	1876.8	1946.4
51	1540.1	1606.5	1673.4	1741.0	1809.2	1878.0	1947.5
52	1541.2	1607.6	1674.6	1742.1	1810.3	1879.2	1948.7
53	1542.3	1608.7	1675.7	1743.2	1811.4	1880.3	1949.9
54	1543.4	1609.8	1676.9	1744.4	1812.6	1881.5	1951.0
55	1544.5	1610.9	1678.0	1745.5	1813.7	1882.6	1952.2
56	1545.6	1612.0	1679.1	1746.6	1814.9	1883.8	1953.4
57	1546.7	1613.1	1680.2	1747.8	1816.0	1884.9	1954.5
58	1547.8	1614.2	1681.3	1748.9	1817.2	1886.1	1955.7
59	1548.9	1615.4	1682.4	1750.0	1818.3	1887.2	1956.9
	Min.						
	24	25	26	27	28	29	30

M m

266 A Table of Meridional Parts.

L. M.	31 Min.	32 Min.	33 Min.	34 Min.	35 Min.	36 Min.	37 Min.
0	1950.1	2028.4	2099.6	2171.5	2244.2	2310.0	2392.8
1	1959.2	2029.6	2100.7	2172.7	2245.5	2311.3	2393.9
2	1960.4	2030.7	2101.9	2173.8	2246.8	2312.5	2395.2
3	1961.5	2031.9	2103.1	2175.1	2248.0	2313.7	2396.4
4	1962.7	2033.1	2104.3	2176.3	2249.2	2313.0	2397.7
5	1963.9	2034.3	2105.5	2177.5	2250.4	2324.2	2398.9
6	1965.0	2035.5	2106.7	2178.7	2251.6	2325.4	2400.2
7	1966.2	2036.7	2107.9	2180.0	2252.9	2326.7	2401.4
8	1967.4	2037.8	2109.1	2181.2	2254.1	2327.9	2402.7
9	1968.5	2039.0	2110.3	2182.4	2255.3	2329.2	2403.9
10	1969.7	2040.2	2111.5	2183.6	2256.5	2330.4	2405.2
11	1970.9	2041.4	2112.7	2184.8	2257.8	2331.6	2406.4
12	1972.0	2042.6	2113.9	2186.0	2259.0	2332.9	2407.8
13	1973.2	2043.8	2115.1	2187.2	2260.2	2334.1	2409.0
14	1974.4	2044.9	2116.3	2188.4	2261.4	2335.3	2410.2
15	1975.6	2046.1	2117.5	2189.6	2262.7	2336.6	2411.5
16	1976.8	2047.3	2118.7	2190.8	2263.9	2337.8	2412.7
17	1977.9	2048.5	2119.8	2192.0	2265.1	2339.0	2414.0
18	1979.1	2049.7	2121.0	2193.3	2266.2	2340.3	2415.2
19	1980.3	2050.8	2122.2	2194.5	2267.6	2341.5	2416.5
20	1981.4	2052.0	2123.4	2195.7	2268.8	2342.8	2417.8
21	1982.6	2053.2	2124.6	2196.9	2270.0	2344.0	2419.0
22	1983.7	2054.4	2125.8	2198.1	2271.2	2345.3	2420.3
23	1984.9	2055.6	2127.0	2199.3	2272.5	2346.5	2421.5
24	1986.1	2056.8	2128.2	2200.5	2273.7	2347.9	2422.8
25	1987.3	2058.0	2129.4	2201.7	2274.9	2349.0	2424.0
26	1988.4	2059.1	2130.6	2203.0	2276.1	2350.2	2425.3
27	1989.6	2060.3	2131.8	2204.2	2277.4	2351.5	2426.5
28	1990.8	2061.5	2133.0	2205.4	2278.6	2352.7	2427.8
29	1992.0	2062.7	2134.2	2206.6	2279.8	2354.0	2429.1
M.	Min.						
L.	31	32	33	34	35	36	39

A Table of Meridional Parts. 26

L.	31	32	33	34	35	36	37
M.	Min.	Min.	Min.	Min.	Min.	Min.	Min.
30	1993, 1	2062.9	2135.4	2207.8	2281.0	2355.2	2430.3
31	1994 31	2065.1	2136.6	2209.0	2282.3	2356.5	2431.6
32	1995, 1	2066.2	2137.8	2210.2	2283.5	2357.7	2432.9
33	1996, 1	2077.4	2139.0	2211.4	2284.7	2358.0	2434.1
34	1997, 8	2068.6	2140.2	2212.7	2286.9	2360.0	2435.0
35	1999, 0	2069.8	2141.4	2213.9	2287.2	2361.4	2436.7
36	2000, 2	2071.0	2142.6	2215.1	2288.4	2362.7	2437.9
37	2001, 3	2072.2	2143.8	2216.3	2289.7	2363.9	2439.2
38	2002, 5	2073.4	2145.0	2217.5	2290.9	2365.2	2440.4
39	2003, 7	2074.6	2146.2	2218.7	2292.1	2366.4	2441.7
40	2004, 9	2075.7	2147.4	2219.9	2293.3	2367.7	2443.0
41	2006, 0	2076.9	2148.6	2221.2	2294.6	2368.9	2444.2
42	2007, 2	2078.1	2149.8	2222.4	2295.8	2370.2	2445.5
43	2008, 4	2079.3	2151.0	2223.6	2297.0	2371.4	2446.8
44	2009, 6	2080.5	2152.2	2224.8	2298.3	2372.7	2448.0
45	2010, 7	2081.7	2153.4	2226.0	2299.5	2373.9	2449.3
46	2011, 9	2082.9	2154.6	2227.2	2300.7	2375.2	2450.6
47	2013, 1	2084.1	2155.8	2228.5	2302.0	2376.4	2451.8
48	2014, 3	2085.3	2157.0	2229.7	2303.2	2377.7	2453.1
49	2015, 4	2086.5	2158.2	2230.9	2304.4	2378.9	2454.3
50	2016, 6	2087.7	2159.4	2232.1	2305.7	2380.1	2455.5
51	2017, 8	2088.9	2160.7	2233.3	2306.9	2381.4	2456.9
52	2019, 0	2090.1	2161.9	2234.6	2308.1	2382.6	2458.1
53	2020, 2	2091.3	2163.1	2235.8	2309.4	2383.9	2459.4
54	2021, 4	2092.5	2164.3	2237.0	2310.6	2385.1	2460.7
55	2022, 5	2093.7	2165.5	2238.2	2311.8	2386.4	2461.9
56	2023, 7	2094.9	2166.7	2239.4	2313.1	2387.6	2463.2
57	2024, 9	2096.2	2167.9	2240.7	2314.3	2388.9	2464.5
58	2026, 0	2097.3	2169.1	2241.9	2315.5	2390.2	2465.8
59	2027, 2	2098.5	2170.3	2243.1	2316.7	2391.4	2467.0
M.	Min.	Min.	Min.	Min.	Min.	Min.	Min.
L.	31	32	33	34	35	36	37

## 268 A Table of Meridional Parts.

L.	38	39	40	41	42	43	44
M.	Min.						
0	2468.3	2545.0	2622.7	2701.6	2781.7	2863.1	2945.7
1	2469.6	2546.2	2624.0	2702.9	2783.1	2864.5	2947.2
2	2470.8	2547.5	2625.3	2704.2	2784.4	2865.8	2948.6
3	2472.1	2548.8	2626.6	2705.6	2785.8	2867.2	2950.0
4	2473.4	2550.1	2627.9	2706.9	2787.1	2868.5	2951.4
5	2474.6	2551.4	2629.2	2708.2	2788.5	2870.0	2952.8
6	2475.9	2552.7	2630.5	2709.6	2789.8	2871.3	2954.2
7	2477.1	2554.0	2631.9	2710.9	2791.2	2872.7	2955.6
8	2478.5	2555.3	2633.2	2712.2	2792.5	2874.1	2957.0
9	2479.7	2556.6	2634.5	2713.6	2793.8	2875.4	2958.4
10	2481.0	2557.8	2635.8	2714.9	2795.1	2876.8	2959.9
11	2482.3	2559.1	2637.1	2716.2	2796.5	2878.2	2961.1
12	2483.5	2560.4	2638.4	2717.5	2797.9	2879.6	2962.5
13	2484.8	2561.7	2639.7	2718.9	2799.3	2880.9	2963.9
14	2486.1	2563.0	2641.0	2720.2	2800.6	2882.3	2965.3
15	2487.4	2564.3	2642.3	2721.5	2802.0	2883.7	2966.7
16	2488.6	2565.6	2643.6	2722.9	2803.3	2885.0	2968.1
17	2489.9	2566.9	2644.9	2724.2	2804.7	2886.4	2969.5
18	2491.2	2568.2	2646.3	2725.5	2806.0	2887.8	2970.8
19	2492.5	2569.5	2647.6	2726.9	2807.4	2889.2	2972.3
20	2493.8	2570.7	2648.8	2728.2	2808.7	2890.5	2973.7
21	2495.0	2572.0	2650.2	2729.5	2810.1	2891.9	2975.1
22	2496.3	2573.3	2651.5	2730.8	2811.4	2893.3	2976.5
23	2497.6	2574.6	2652.8	2732.2	2812.8	2894.7	2977.9
24	2498.8	2575.9	2654.1	2733.5	2814.1	2896.0	2979.3
25	2500.1	2577.2	2655.4	2734.8	2815.5	2897.4	2980.7
26	2501.4	2578.5	2656.8	2736.2	2816.8	2898.8	2982.1
27	2502.7	2579.8	2658.7	2737.5	2818.2	2900.2	2983.5
28	2503.4	2581.1	2659.4	2738.8	2819.5	2901.5	2984.9
29	2505.2	2582.4	2660.7	2740.2	2820.9	2902.9	2986.3
M.	Min.						
L.	38	39	40	41	42	43	44

A Table of Meridional Parts. 26

L.	38	39	40	41	42	43	44
M.	Min.						
30	2506.5	2583.7	2662.0	2741.5	2822.	2904.3	2987.7
31	2507.8	2585.0	2663.3	2742.9	2823.6	2905.7	2989.1
32	2509.0	2586.3	2664.6	2744.2	2825.0	2907.1	2990.5
33	2510.3	2587.6	2666.0	2745.5	2826.3	2908.4	2991.9
34	2511.6	2588.9	2667.3	2746.9	2827.7	2909.7	2993.3
35	2512.9	2590.2	2668.6	2748.2	2829.0	2911.2	2994.7
36	2514.2	2591.5	2669.9	2749.5	2830.3	2912.6	2996.5
37	2515.4	2592.9	2671.2	2750.9	2831.8	2914.0	2997.5
38	2516.7	2594.1	2672.5	2752.2	2833.1	2915.3	2998.9
39	2518.0	2595.4	2673.1	2753.5	2834.5	2916.7	3000.1
40	2519.3	2596.7	2675.1	2754.4	2835.8	2918.1	3001.3
41	2520.6	2598.0	2676.5	2756.2	2837.2	2919.5	3003.2
42	2521.8	2599.3	2677.8	2757.6	2838.6	2920.9	3004.6
43	2523.1	2600.6	2679.1	2758.9	2839.9	2922.3	3006.0
44	2524.4	2601.9	2680.5	2760.2	2841.3	2923.6	3007.4
45	2525.7	2603.2	2681.8	2761.5	2842.6	2925.0	3008.8
46	2527.0	2604.5	2683.1	2762.9	2844.0	2926.4	3010.2
47	2528.3	2605.8	2684.4	2764.3	2845.4	2927.8	3011.6
48	2529.5	2607.1	2685.7	2765.6	2846.7	2929.2	3013.0
49	2530.8	2608.4	2687.1	2766.9	2848.1	2930.6	3014.4
50	2532.1	2609.7	2688.4	2768.3	2849.5	2932.0	3015.8
51	2533.4	2611.0	2689.7	2769.6	2850.8	2933.3	3017.2
52	2534.7	2612.3	2691.9	2771.0	2852.2	2934.7	3018.7
53	2536.0	2613.6	2692.3	2772.3	2853.6	2936.1	3020.1
54	2537.2	2614.9	2693.7	2773.7	2854.9	2937.5	3021.5
55	2538.5	2616.2	2695.0	2775.0	2856.3	2938.9	3022.9
56	2539.8	2617.5	2696.3	2776.4	2857.7	2940.3	3024.3
57	2541.1	2618.8	2697.6	2777.7	2859.1	2941.8	3025.7
58	2542.4	2620.1	2699.0	2779.0	2860.5	2943.1	3027.1
59	2543.7	2621.4	2700.3	2780.4	2861.8	2944.4	3028.5
M.	Min.						
L.	38	39	40	41	42	43	44

270 A Table of Meridional Parts.

L.	45	46	47	48	49	50	51
M.	Min.						
0	3030.0	3115.6	3202.8	3291.5	3382.1	3474.5	3568.8
1	3031.4	3117.0	3204.2	3293.1	3383.6	3476.1	3570.4
2	3032.8	3118.5	3205.7	3294.5	3385.2	3477.6	3572.0
3	3034.2	3120.0	3207.2	3296.1	3386.7	3479.1	3573.6
4	3035.6	3121.4	3208.6	3297.5	3388.2	3480.7	3575.2
5	3037.0	3122.9	3210.1	3299.0	3389.7	3482.3	3576.8
6	3038.4	3124.2	3211.6	3300.5	3391.3	3483.9	3578.4
7	3039.8	3125.9	3213.0	3302.0	3392.8	3485.4	3580.0
8	3041.3	3127.1	3214.5	3303.5	3394.3	3487.0	3581.6
9	3042.7	3128.6	3216.0	3305.0	3395.9	3488.5	3583.2
10	3044.1	3130.0	3217.4	3306.5	3397.4	3490.1	3584.9
11	3045.5	3131.5	3218.9	3308.0	3398.9	3491.7	3586.4
12	3047.0	3132.9	3220.4	3309.5	3400.4	3493.2	3588.0
13	3048.4	3134.3	3221.9	3311.1	3402.0	3494.8	3589.5
14	3049.8	3135.8	3223.3	3312.5	3403.5	3496.3	3591.1
15	3051.2	3137.2	3224.8	3314.0	3405.0	3497.9	3592.7
16	3052.6	3138.7	3226.3	3315.5	3406.6	3499.5	3594.2
17	3054.1	3140.1	3227.7	3317.0	3408.1	3501.0	3595.9
18	3055.5	3141.6	3229.1	3318.0	3409.6	3502.6	3597.5
19	3056.9	3143.0	3230.7	3320.0	3411.2	3504.2	3599.1
20	3058.3	3144.5	3232.7	3321.5	3412.7	3505.7	3600.7
21	3059.7	3145.9	3233.6	3323.1	3414.2	3507.3	3602.2
22	3061.2	3147.4	3235.1	3324.6	3415.8	3508.9	3603.9
23	3062.6	3148.8	3236.6	3326.1	3417.5	3510.5	3605.5
24	3064.0	3150.3	3238.1	3327.6	3418.8	3512.0	3607.1
25	3065.4	3151.7	3239.5	3329.6	3420.4	3513.6	3608.7
26	3066.9	3153.2	3241.0	3330.6	3421.9	3515.1	3610.3
27	3068.3	3154.6	3242.5	3332.1	3423.5	3516.7	3611.9
28	3069.7	3156.1	3244.0	3333.6	3425.0	3518.3	3613.6
29	3071.1	3157.5	3245.7	3335.1	3426.5	3519.8	3615.2
M.	Min.						
L.	45	46	47	48	49	50	51

A Table of Meridional Parts. 27

L.	45	46	47	48	49	50	51
M.	Min.						
30	3072,6	3159,0	3246,9	3336,6	3428,1	3521,4	3616,8
31	3074,0	3160,4	3248,4	3338,1	3429,6	3523,0	3618,4
32	3075,4	3161,9	3249,9	3339,6	3431,2	3524,6	3620,0
33	3076,9	3163,3	3251,4	3341,1	3432,7	3526,1	3621,6
34	3078,3	3164,8	3252,9	3342,7	3434,2	3527,8	3623,0
35	3079,7	3166,2	3254,4	3344,2	3435,8	3529,3	3624,8
36	3081,1	3167,7	3255,8	3345,7	3437,3	3530,9	3626,4
37	3082,6	3169,1	3257,3	3347,2	3438,9	3532,4	3628,0
38	3084,0	3170,6	3258,4	3348,7	3440,4	3534,0	3629,6
39	3085,4	3172,1	3260,3	3350,1	3442,0	3535,6	3631,3
40	3086,9	3173,5	3261,8	3351,7	3443,5	3537,2	3632,9
41	3088,3	3175,0	3263,3	3353,2	3445,9	3538,8	3634,5
42	3089,7	3176,4	3264,7	3354,8	3446,6	3540,3	3636,1
43	3091,2	3177,9	3266,2	3356,3	3448,1	3541,9	3637,7
44	3092,6	3179,3	3267,7	3357,8	3449,7	3542,5	3639,3
45	3094,9	3180,8	3269,2	3359,3	3451,2	3545,1	3640,9
46	3095,3	3182,3	3270,7	3360,8	3452,8	3546,7	3642,5
47	3096,9	3183,7	3272,2	3362,3	3454,3	3548,2	3644,2
48	3098,3	3185,2	3273,7	3363,9	3455,9	3549,8	3645,8
49	3099,8	3186,6	3275,2	3365,4	3457,4	3551,4	3647,4
50	3101,2	3188,1	3276,6	3366,9	3459,0	3553,0	3649,0
51	3102,6	3189,6	3278,1	3368,4	3460,5	3554,6	3650,6
52	3104,1	3191,0	3279,5	3369,9	3462,1	3556,1	3652,3
53	3105,6	3192,5	3281,1	3371,5	3463,6	3557,7	3653,9
54	3107,0	3194,1	3282,6	3373,0	3465,2	3559,3	3655,5
55	3108,4	3195,4	3284,1	3374,5	3466,7	3560,9	3657,1
56	3109,9	3196,9	3285,6	3376,0	3468,3	3562,5	3658,7
57	3111,2	3198,4	3287,1	3377,6	3469,8	3564,1	3660,4
58	3112,7	3199,8	3288,6	3379,1	3471,4	3565,7	3662,0
59	3114,1	3201,1	3290,1	3380,6	3473,0	3567,3	3663,6
M.	Min.						
L.	45	46	47	48	49	50	51

272 A Table of Meridional Parts.

L.	52	53	54	55	56	57	58
M.	Min.						
0	3665.2	3763.8	3864.7	3968.0	4073.9	4182.7	4294.3
1	3666.9	3765.3	3866.4	3969.7	4075.7	4184.5	4296.2
2	3668.5	3767.1	3868.1	3971.5	4077.5	4186.3	4298.1
3	3670.1	3768.8	3869.8	3973.2	4079.3	4188.2	4300.9
4	3671.7	3770.4	3871.5	3975.0	4081.1	4190.0	4301.9
5	3673.4	3772.1	3873.2	3976.7	4083.5	4191.8	4303.8
6	3675.0	3773.8	3874.9	3978.5	4084.7	4193.7	4305.7
7	3676.6	3775.4	3876.6	3980.2	4086.5	4195.5	4307.6
8	3678.2	3777.1	3878.3	3982.0	4088.3	4197.4	4309.5
9	3679.9	3778.8	3880.0	3983.7	4090.1	4199.2	4311.4
10	3681.5	3780.4	3881.7	3985.5	4091.9	4201.3	4313.2
11	3683.1	3782.1	3883.4	3987.2	4093.7	4202.9	4315.1
12	3684.8	3783.8	3885.1	3989.0	4095.5	4204.7	4317.0
13	3686.4	3785.5	3886.8	3990.7	4097.3	4206.6	4318.9
14	3688.0	3787.1	3888.6	3992.5	4099.1	4208.4	4320.8
15	3689.7	3788.8	3890.3	3994.2	4100.9	4210.3	4322.7
16	3691.3	3790.5	3892.0	3996.0	4102.7	4212.1	4324.6
17	3692.9	3792.1	3893.7	3997.7	4104.5	4214.0	4326.5
18	3694.6	3793.8	3895.8	3999.5	4106.3	4215.8	4328.4
19	3696.2	3795.5	3907.1	4001.3	4108.1	4217.7	4330.3
20	3697.8	3797.2	3908.8	4003.0	4109.9	4219.5	4332.2
21	3699.5	3798.8	3900.5	4004.8	4111.7	4221.4	4334.2
22	3701.1	3800.5	3902.4	4006.5	4113.5	4223.2	4336.1
23	3702.7	3802.2	3904.0	4008.3	4115.3	4225.1	4338.0
24	3704.4	3803.9	3905.7	4010.0	4117.1	4227.0	4339.9
25	3706.0	3805.5	3907.4	4011.8	4118.5	4228.8	4341.8
26	3707.7	3807.2	3909.1	4013.6	4120.5	4230.7	4343.7
27	3709.9	3808.9	3910.9	4015.3	4122.5	4232.5	4345.6
28	3710.5	3810.6	3912.6	4017.1	4124.3	4234.4	4347.5
29	3712.6	3812.3	3914.7	4018.9	4126.1	4236.2	4349.4
M.	Min.						
L.	52	53	54	55	56	57	58

A Table of Meridional Parts. 273

	52	53	54	55	56	57	58
M.	Min.						
30	3714.2	3813.9	3916.0	4020.6	4127.9	4238.1	+351.2
31	3715.9	3815.6	3917.7	4022.4	4129.7	4240.0	4353.3
32	3717.5	3817.3	3919.5	4024.2	4131.6	4241.8	4355.2
33	3719.2	3819.0	3921.2	4025.9	4133.4	4243.7	4357.1
34	3720.7	3820.7	3922.5	4027.7	4135.2	4245.6	4359.0
35	3722.4	3822.2	3924.6	4029.5	4137.0	4247.4	4360.9
36	3724.1	3824.0	3924.4	4031.2	4138.8	4249.3	4362.8
37	3725.7	3825.7	3928.1	4033.0	4140.6	4251.2	4364.8
38	3727.4	3827.4	3929.8	4034.8	4142.5	4253.0	4366.7
39	3729.0	3829.1	3931.5	4036.6	4144.3	4254.9	4368.6
40	3730.7	3830.8	3933.3	4038.3	4146.1	4256.8	4370.5
41	3732.3	3832.5	3935.9	4040.1	4147.9	4258.6	4372.5
42	3734.0	3834.2	3936.7	4041.9	4149.7	4260.5	4374.4
43	3735.6	3835.8	3938.5	4043.6	4151.6	4262.4	4376.4
44	3737.3	3837.5	3940.2	4045.4	4153.4	4264.3	4378.2
45	3738.9	3839.2	3941.9	4047.2	4155.2	4266.1	4380.2
46	3740.6	3840.9	3943.7	4049.0	4157.0	4268.0	4382.1
47	3742.2	3842.6	3945.4	4050.7	4158.8	4269.9	4384.0
48	3743.9	3844.3	3947.1	4052.5	4160.7	4271.8	4385.9
49	3745.6	3846.0	3948.9	4054.3	4162.5	4272.6	4387.9
50	3747.2	3847.7	3950.6	4056.1	4164.3	4275.5	4389.8
51	3748.9	3849.4	3952.3	4057.9	4166.2	4277.4	4391.7
52	3750.5	3851.1	3954.1	4059.7	4168.0	4279.3	4393.7
53	3752.2	3852.8	3955.8	4061.4	4169.8	4281.1	4395.6
54	3753.8	3854.5	3957.6	4063.2	4171.7	4283.0	4397.5
55	3755.5	3856.2	3959.3	4065.0	4173.5	4284.9	4399.5
56	3757.2	3857.9	3961.0	4066.8	4175.3	4286.8	4401.4
57	3758.8	3859.6	3962.8	4068.6	4177.2	4288.7	4403.4
58	3760.5	3861.3	3964.5	4070.4	4179.0	4290.6	4405.3
59	3762.2	3863.0	3966.3	4072.2	4180.8	4292.5	4407.2
M.	Min.						
L.	52	53	54	55	56	57	58

## 274 A Table of Meridional Parts.

L.	59	60	61	62	63	64	65
M.	Min.						
0	4409.2	4527.4	4649.3	4775.0	4905.0	5039.5	5178.5
1	4411.0	4529.4	4651.3	4777.1	4907.2	5041.7	5181.2
2	4413.1	4531.4	4653.4	4779.3	4909.4	5044.0	5183.6
3	4415.0	4533.4	4655.5	4781.4	4911.6	5046.3	5186.0
4	4417.0	4535.4	4657.5	4783.5	4913.8	5048.6	5188.3
5	4418.9	4537.4	4659.6	4785.7	4915.9	5050.9	5190.7
6	4420.8	4539.4	4661.7	4787.3	4918.2	5053.2	5193.1
7	4422.8	4541.4	4663.7	4790.0	4920.4	5055.5	5195.4
8	4424.7	4543.4	4665.8	4792.1	4922.5	5057.7	5197.8
9	4426.7	4545.4	4667.9	4794.2	4924.8	5060.0	5200.2
10	4428.6	4547.5	4669.9	4796.4	4927.1	5062.3	5202.6
11	4430.6	4549.5	4672.0	4798.5	4929.3	5064.6	5205.0
12	4432.5	4551.5	4674.1	4800.7	4931.6	5066.9	5207.3
13	4434.5	4553.5	4676.2	4802.8	4933.7	5069.2	5209.7
14	4436.4	4555.6	4678.2	4804.9	4936.9	5071.5	5212.1
15	4438.4	4557.5	4680.3	4807.1	4938.1	5073.9	5214.5
16	4440.4	4559.5	4682.4	4809.2	4940.4	5076.1	5216.9
17	4442.3	4561.5	4684.5	4811.4	4942.6	5078.4	5219.3
18	4444.3	4563.6	4686.6	4813.5	4944.8	5080.7	5221.7
19	4446.2	4565.6	4688.6	4815.7	4947.0	5083.0	5224.1
20	4448.2	4567.6	4690.7	4817.8	4949.3	5085.3	5226.5
21	4450.2	4569.6	4692.8	4820.0	4951.5	5087.7	5228.9
22	4452.1	4571.6	4694.9	4822.2	4953.7	5090.0	5231.3
23	4454.1	4573.7	4697.0	4824.3	4956.0	5092.3	5233.7
24	4456.0	4575.7	4699.1	4826.5	4958.2	5094.6	5236.1
25	4458.0	4577.7	4701.2	4828.6	4960.4	5096.9	5238.5
26	4460.0	4579.6	4703.2	4830.8	4962.7	5099.2	5240.9
27	4461.9	4581.8	4705.3	4832.9	4964.9	5102.5	5243.3
28	4463.9	4583.8	4707.4	4835.1	4967.1	5103.9	5245.7
29	4466.9	4585.8	4709.6	4837.3	4969.4	5106.2	5248.1
M.	Min.						
L	59	60	61	62	63	64	65

A Table of Meridional Parts. 275

L.	59	60	61	62	63	64	65
M.	Min.	Min.	Min.	Min.	Min.	Min.	Min.
30	4467.8	+ 87.8	4711.6	4839.4	4971.6	5108.5	5250.5
31	4469.8	+ 95.9	4713.7	4841.6	4973.5	5110.8	5252.9
32	4471.8	+ 91.9	4715.8	4843.8	4976.1	5113.1	5255.3
33	4473.8	+ 93.9	4717.9	4845.9	4978.3	5115.5	5257.7
34	4475.7	+ 96.0	4720.0	4848.1	4980.6	5117.8	5260.1
35	4477.7	+ 98.0	4722.6	4850.3	4982.8	5120.1	5262.6
36	4479.7	+ 600.1	4724.2	4852.5	4985.1	5122.5	5265.0
37	4481.7	+ 602.1	4726.3	4854.6	4987.3	5124.8	5267.4
38	4483.6	+ 604.1	4728.4	4856.8	4989.6	5127.1	5269.8
39	4485.6	+ 606.2	4730.5	4859.0	4991.8	5129.5	5272.3
40	4487.6	+ 608.2	4732.6	4861.2	4994.1	5131.8	5274.7
41	4489.6	+ 610.3	4734.7	4863.3	4996.3	5134.1	5277.1
42	4491.6	+ 612.3	4736.9	4865.5	4998.6	5136.5	5279.5
43	4493.5	+ 614.3	4739.0	4867.7	5000.9	5138.8	5282.0
44	4495.5	+ 616.4	4741.1	4869.9	5003.1	5141.2	5284.4
45	4497.5	+ 618.4	4743.2	4872.1	5005.4	5143.5	5286.8
46	4499.5	+ 620.5	4745.3	4874.3	5007.6	5145.9	5289.3
47	4501.5	+ 622.5	4747.4	4876.4	5009.9	5148.2	5291.7
48	4503.5	+ 624.6	4749.5	4878.6	5012.2	5150.6	5294.2
49	4505.5	+ 626.6	4751.7	4880.8	5014.4	5152.9	5296.6
50	4507.5	+ 628.7	4753.8	4882.0	5016.7	5155.3	5299.0
51	4509.4	+ 630.7	4755.9	4885.2	5019.0	5157.6	5301.5
52	4511.4	+ 632.8	4758.0	4887.4	5021.2	5160.0	5303.9
53	4513.4	+ 634.8	4760.1	4889.6	5023.5	5162.3	5306.4
54	4515.4	+ 636.9	4762.3	4891.8	5025.8	5164.7	5308.8
55	4517.4	+ 639.0	4764.4	4894.0	5028.1	5167.0	5311.3
56	4519.4	+ 641.0	4766.5	4896.2	5030.3	5169.4	5313.7
57	4521.4	+ 643.1	4768.6	4898.4	5032.7	5171.8	5316.2
58	4523.4	+ 645.1	4770.8	4900.6	5034.9	5174.1	5318.6
59	4525.4	+ 647.2	4772.9	4902.8	5037.2	5176.5	5321.1
L.	Min.	Min.	Min.	Min.	Min.	Min.	Min.
M.	59	60	61	62	63	64	65

## 276 A Table of Meridional Parts.

L.	66	67	68	69	70	71	72
M.	Min.						
0	5323.6	5474.0	5630.9	5794.6	5966.0	6145.7	6334.1
1	5326.0	5476.6	5633.5	5797.4	5968.9	6148.8	6338.1
2	5328.5	5479.2	5636.2	5800.2	5971.8	6151.9	6341.4
3	5330.9	5481.7	5638.9	5803.0	5974.7	6155.0	6344.6
4	5333.4	5484.3	5641.6	5805.8	5977.7	6158.0	6347.8
5	5335.9	5486.9	5644.2	5808.6	5980.4	6161.1	6351.1
6	5338.3	5489.4	5646.9	5811.1	5983.5	6164.2	6354.3
7	5340.8	5492.0	5649.0	5814.2	5986.5	6167.3	6357.6
8	5343.3	5494.6	5652.3	5817.0	5989.4	6170.4	6360.9
9	5345.7	5497.1	5655.0	5819.8	5992.4	6173.5	6364.1
10	5348.2	5499.7	5657.6	5822.6	5995.3	6176.6	6367.4
11	5350.7	5502.3	5660.3	5825.4	5998.3	6179.7	6370.6
12	5353.2	5504.9	5663.0	5828.2	6001.2	6182.8	6373.9
13	5355.7	5507.5	5665.7	5831.0	6004.2	6185.9	6377.2
14	5358.1	5510.2	5668.4	5833.9	6007.1	6189.0	6380.5
15	5360.6	5512.6	5671.1	5836.7	6010.1	6192.1	6383.7
16	5363.1	5515.2	5673.8	5839.5	6013.0	6195.2	6387.0
17	5365.6	5517.8	5676.5	5842.7	6016.0	6198.3	6390.3
18	5368.1	5520.4	5679.2	5845.5	6019.0	6201.4	6393.6
19	5370.5	5523.0	5681.9	5848.0	6021.9	6204.6	6396.9
20	5373.0	5525.0	5684.6	5850.8	6024.9	6207.7	6400.2
21	5375.5	5528.3	5687.3	5853.7	6027.9	6210.8	6403.6
22	5378.0	5530.8	5690.0	5856.5	6030.8	6213.8	6406.8
23	5380.5	5533.4	5692.8	5859.3	6033.8	6217.1	6410.1
24	5383.0	5536.0	5695.5	5862.2	6036.8	6220.2	6413.4
25	5385.5	5538.6	5698.2	5865.0	6039.8	6223.3	6416.7
26	5388.0	5541.2	5700.9	5867.7	6042.7	6226.5	6420.0
27	5390.5	5543.8	5703.6	5870.9	6045.7	6229.6	6423.3
28	5393.0	5546.4	5706.3	5873.5	6048.7	6232.7	6426.6
29	5395.5	5549.0	5709.1	5876.4	6051.7	6235.9	6429.9
M.	Min.						
L.	66	67	68	69	70	71	72

A Table of Meridional Parts, 277

M.	66	67	68	69	70	71	72
M.	Min.						
30	5398.0	551.6	5711.8	5879.3	6054.7	6239.0	6433.2
31	5400.5	5554.2	5714.5	5882.1	6057.7	6242.2	6436.6
32	5403.0	5556.8	5717.3	5885.0	6060.7	6245.3	6439.9
33	5405.6	5559.5	5720.0	5887.8	6063.7	6248.5	6443.2
34	5408.1	5562.1	5722.7	5890.7	6066.7	6251.7	6446.6
35	5410.6	5564.7	5725.5	5893.6	6069.7	6254.8	6449.9
36	5413.1	5567.3	5728.2	5896.4	6072.7	6258.0	6453.3
37	5415.6	5569.9	5731.0	5899.3	6075.7	6261.2	6456.6
38	5418.1	5572.6	5733.7	5902.2	6078.8	6264.4	6460.0
39	5420.7	5575.2	5736.4	5905.1	6081.8	6267.5	6463.3
40	5423.2	5577.8	5739.2	5907.9	6084.8	6270.7	6466.7
41	5425.7	5580.5	5741.9	5910.8	6087.7	6273.9	6470.0
42	5428.2	5583.1	5744.7	5913.7	6090.8	6277.1	6473.4
43	5430.8	5585.7	5747.5	5916.6	6093.9	6280.3	6476.8
44	5433.3	5588.4	5750.2	5919.5	6096.9	6283.5	6480.1
45	5435.8	5591.0	5753.0	5922.4	6099.9	6286.6	6483.5
46	5438.4	5593.7	5755.7	5925.2	6103.0	6289.8	6486.9
47	5440.9	5596.3	5758.5	5928.1	6106.0	6293.0	6490.3
48	5443.5	5599.0	5761.3	5931.0	6109.1	6296.2	6493.6
49	5446.0	5601.6	5764.0	5933.9	6112.1	6299.4	6497.0
50	5448.5	5604.3	5766.8	5936.8	6115.1	6302.7	6500.0
51	5451.1	5606.9	5769.6	5939.7	6118.2	6305.9	6503.9
52	5453.6	5609.6	5772.3	5942.6	6121.2	6309.1	6507.2
53	5456.2	5612.2	5775.1	5945.5	6124.3	6312.3	6510.6
54	5458.7	5614.9	5777.9	5948.5	6127.4	6315.5	6514.0
55	5461.3	5617.5	5780.7	5951.4	6130.0	6318.7	6517.4
56	5463.8	5620.2	5783.5	5954.3	6133.5	6322.0	6520.8
57	5466.4	5622.9	5786.2	5957.2	6136.5	6325.2	6524.2
58	5468.9	5625.5	5789.0	5960.1	6139.6	6328.4	6527.6
59	5471.5	5628.2	5791.8	5963.0	6142.7	6331.7	6531.0
M.	Min.						
L.	66	67	68	69	70	71	72

## 278 A Table of Meridional Parts.

L.	73	74	75	76	77	78	79
M.	Min.						
0	6534.5	6745.7	6970.3	7210.1	7467.7	774.6	8045.7
1	6537.9	6749.4	6974.2	7214.2	7471.7	7749.4	8051.0
2	6541.3	6753.0	6978.1	7218.3	7476.1	7754.2	8056.2
3	6544.7	6756.6	6980.9	7222.5	7480.5	7759.0	8061.5
4	6548.2	6760.3	6985.8	7226.6	7485.0	7763.9	8066.8
5	6551.6	6763.9	6989.7	7230.9	7488.5	7768.7	8072.0
6	6555.0	6767.6	6993.6	7234.9	7494.0	7773.5	8077.3
7	6558.5	6771.2	6997.1	7239.1	7498.5	7778.4	8082.6
8	6561.9	6774.9	7001.4	7243.3	7502.9	783.2	8087.9
9	6565.4	6778.5	7005.3	7247.5	7507.4	7788.1	8093.2
10	6568.8	6782.2	7009.2	7251.6	7511.9	7793.0	8098.5
11	6572.3	6785.8	7013.1	7255.8	7516.4	7797.8	8103.8
12	6575.7	6789.5	7017.0	7260.0	7520.9	7802.7	8109.2
13	6579.2	6793.2	7020.9	7264.2	7525.4	7807.6	8114.5
14	6582.6	6796.9	7024.8	7268.4	7530.0	7812.5	8119.8
15	6586.1	6800.5	7028.7	7272.6	7534.5	7817.4	8125.2
16	6589.5	6804.2	7032.7	7276.8	7539.0	7822.3	8130.6
17	6593.0	6807.9	7036.6	7281.0	7543.6	7827.2	8135.9
18	6596.5	6811.6	7040.5	7285.2	7548.1	7832.2	8141.3
19	6600.0	6815.8	7044.5	7289.4	7552.7	7837.1	8146.7
20	6603.4	6819.0	7048.4	7293.7	7557.2	7842.0	8152.1
21	6606.9	6822.7	7052.4	7297.9	7561.8	7847.0	8157.5
22	6610.4	6826.4	7056.3	7302.1	7566.3	7851.9	8162.9
23	6613.9	6830.1	7060.3	7306.4	7570.9	7856.9	8168.3
24	6617.4	6833.8	7064.2	7310.6	7575.5	7861.9	8173.7
25	6620.9	6837.6	7068.2	7314.9	7580.1	7866.8	8179.2
26	6624.4	6841.3	7072.2	7319.1	7584.7	7871.7	8184.6
27	6627.9	6845.0	7076.2	7323.4	7589.3	7876.8	8190.1
28	6631.4	6848.7	7080.1	7327.7	7593.9	7881.8	8195.5
29	6635.0	6852.5	7084.1	7332.0	7598.3	7886.8	8201.0
M.	Min.						
L.	73	74	75	76	77	78	79

Table of Meridional Parts. 279

M.	73	74	75	76	77	78	79
M.	Min.						
30	6638.5	6856.2	7088.1	7336.2	7603.1	7891.8	8206.5
31	6642.0	6860.0	7092.1	7340.5	7607.7	7896.8	8212.0
32	6645.5	6863.7	7096.1	7344.8	7612.3	7901.9	8217.5
33	6649.1	6867.5	7100.1	7349.1	7617.0	7906.6	8223.0
34	6652.6	6871.2	7104.1	7353.4	7621.6	7911.9	8229.5
35	6656.1	6875.0	7108.2	7357.7	7626.3	7917.0	8234.1
36	6659.7	6878.7	7112.2	7362.0	7630.9	7922.1	8239.6
37	6663.2	6882.5	7116.2	7366.4	7635.6	7927.1	8245.1
38	6666.8	6886.3	7120.2	7370.7	7640.2	7932.2	8250.7
39	6670.3	6890.1	7124.3	7375.0	7644.9	7937.3	8256.3
40	6673.9	6893.8	7128.3	7379.4	7649.6	7942.4	8261.8
41	6677.4	6897.6	7132.3	7383.7	7654.3	7947.5	8267.4
42	6681.0	6901.4	7136.3	7388.0	7659.0	7952.6	8273.0
43	6684.6	6905.2	7140.4	7392.4	7663.7	7957.7	8278.6
44	6688.1	6909.0	7144.5	7396.8	7668.0	7962.8	8284.2
45	6691.7	6912.8	7148.6	7401.1	7673.1	7968.0	8289.9
46	6695.3	6916.6	7152.6	7405.5	7677.8	7973.1	8295.5
47	6698.9	6920.4	7156.7	7409.9	7682.6	7978.2	8301.1
48	6702.4	6924.2	7160.8	7414.2	7687.3	7983.4	8306.8
49	6706.0	6928.1	7164.9	7418.6	7692.0	7988.5	8312.4
50	6709.6	6931.9	7169.0	7423.0	7696.8	7993.7	8318.1
51	6713.2	6935.7	7173.0	7427.1	7701.5	7998.9	8323.8
52	6716.8	6939.5	7177.1	7431.8	7706.3	8004.0	8329.4
53	6720.4	6943.4	7181.2	7436.2	7711.0	8009.2	8335.1
54	6724.0	6947.2	7185.3	7440.6	7715.8	8014.4	8340.8
55	6727.6	6951.1	7189.5	7445.0	7720.6	8019.6	8346.6
56	6731.2	6954.9	7193.6	7449.5	7725.4	8024.8	8352.3
57	6734.9	6958.8	7197.7	7453.9	7730.2	8030.0	8358.0
58	6738.5	6962.6	7201.8	7458.3	7735.0	8035.3	8363.7
59	6742.1	6966.5	7205.0	7462.8	7739.8	8040.5	8369.5
M.	Min.						
L.	73	74	75	76	77	78	79

## 280 A Table of Medicinal Parts.

L.	80	81	82	83	84
M.	Min.	Min.	Min.	Min.	Min.
L.	80	81	82	83	84
0	8375.3	8739.1	9145.5	9605.9	10137.0
I	8381.0	8745.5	9152.7	9614.1	10146.6
2	8386.8	8751.9	9159.9	9622.4	10156.2
3	8392.6	8758.2	9167.2	9630.6	10165.8
4	8398.3	8764.9	9174.4	9638.9	10175.4
5	8404.1	8771.2	9181.6	9647.2	10185.1
6	8409.9	8777.7	9188.9	9655.5	10194.8
7	8415.8	8784.1	9195.2	9663.8	10204.6
8	8421.6	8790.6	9203.5	9672.2	10214.4
9	8427.4	8797.1	9210.8	9680.6	10224.2
10	8433.3	8803.6	9218.1	9689.0	10234.0
11	8439.1	8810.1	9225.4	9697.4	10243.8
12	8445.0	8816.6	9232.8	9705.8	10253.7
13	8450.9	8823.2	9240.2	9714.2	10263.6
14	8456.8	8829.7	9247.6	9722.7	10273.5
15	8462.6	8836.3	9255.0	9731.2	10283.5
16	8468.6	8842.8	9262.4	9739.7	10293.5
17	8473.5	8849.4	9269.9	9748.3	10303.5
18	8480.4	8856.0	9277.3	9756.8	10313.6
19	8486.3	8862.6	9284.8	9765.4	10323.7
20	8492.3	8869.3	9292.3	9774.0	10333.8
21	8498.2	8875.9	9299.8	9782.7	10344.0
22	8504.2	8882.6	9307.3	9791.3	10354.1
23	8510.2	8889.2	9314.8	9800.0	10364.3
24	8516.2	8895.9	9322.4	9808.6	10374.5
25	8522.2	8902.6	9330.0	9817.3	10384.8
26	8528.2	8909.3	9337.7	9826.1	10395.1
27	8534.2	8916.0	9345.2	9834.8	10405.4
28	8540.2	8922.7	9352.8	9843.6	10415.8
29	8546.2	8929.5	9360.4	9852.4	10426.2
M.	Min.	Min.	Min.	Min.	Min.
L.	80	81	82	83	84

A Table of Meridional Parts. [277]

L.	80	81	82	83	84
M.	Min.	Min.	Min.	Min.	Min.
30	85 2.3	8936.2	9368.1	9861.3	10436.6
31	85 58.4	8943.0	9375.8	9870.1	10447.1
32	85 64.4	8949.8	9383.5	9879.0	10457.5
33	85 70.5	8956.6	9391.2	9887.8	10468.0
34	85 76.6	8963.4	9398.9	9896.7	10478.5
35	85 82.7	8970.8	9406.6	9905.8	10489.1
36	85 88.9	8977.1	9414.4	9914.6	10499.7
37	85 95.0	8983.9	9422.1	9923.6	10510.4
38	86 01.1	8990.8	9429.9	9932.7	10521.1
39	86 07.3	8997.7	9437.3	9941.7	10531.8
40	86 13.5	9004.6	9445.6	9950.0	10542.6
41	86 19.6	9011.5	9453.3	9959.8	10553.3
42	86 25.8	9018.4	9461.3	9968.9	10564.1
43	86 32.0	9025.4	9469.1	9978.0	10574.9
44	86 38.2	9032.3	9477.0	9987.2	10585.8
45	86 44.5	9039.3	9484.9	9996.3	10596.7
46	86 50.7	9046.3	9492.9	10005.5	10607.7
47	86 56.9	9053.3	9500.8	10014.8	10618.7
48	86 63.2	9060.3	9508.8	10024.0	10629.7
49	86 70.5	9067.3	9516.8	10033.3	10640.8
50	86 75.7	9074.4	9524.8	10042.6	10651.9
51	86 82.0	9081.4	9532.9	10051.9	10663.0
52	86 88.3	9088.4	9540.9	10061.3	10674.1
53	86 94.6	9095.5	9548.9	10070.6	10685.3
54	87 01.0	9102.7	9557.0	10080.0	10696.5
55	87 07.3	9109.8	9565.1	10089.4	10707.7
56	87 13.6	9116.9	9573.2	10098.9	10719.1
57	87 20.0	9124.0	9581.4	10108.4	10730.4
58	87 26.4	9131.2	9589.5	10117.9	10741.8
59	87 32.7	9138.4	9597.7	10127.4	10753.3
M.	Min.	Min.	Min.	Min.	Min.
L.	80	81	82	83	84

[278] A Table of Meridional Parts.

L.	85	86	87	88	89
M.	Min.	Min.	Min.	Min.	Min.
0	10764.7	11532.6	12522.4	13916.	16299.8
1	10776.2	11547.0	12541.4	13945.4	16357.5
2	10787.7	11561.4	12560.7	13974.4	16416.3
3	10799.3	11575.9	12580.0	14003.7	16476.1
4	10810.9	11590.5	12599.5	14033.2	16537.0
5	10822.5	11605.0	12619.1	14063.0	16594.9
6	10834.2	11619.8	12638.9	14093.0	16662.0
7	10845.9	11634.5	12658.6	14123.3	16726.2
8	10857.7	11649.3	12678.6	14153.9	16791.7
9	10869.6	11664.1	12698.6	14184.7	16858.5
10	10881.4	11679.1	12718.8	14215.8	16926.5
11	10893.3	11694.0	12739.1	14247.2	16990.6
12	10905.2	11709.1	12759.5	14278.9	17066.9
13	10917.2	11724.2	12780.0	14310.9	17130.3
14	10929.1	11739.4	12800.7	14343.2	17213.3
15	10941.2	11754.7	12821.5	14375.8	17288.0
16	10953.3	11770.0	12842.5	14408.7	17366.7
17	10965.5	11785.4	12863.5	14441.9	17445.0
18	10977.7	11800.9	12884.7	14475.4	17525.9
19	10989.9	11816.4	12906.0	14509.3	17608.7
20	11002.2	11832.0	12927.4	14543.5	17693.6
21	11014.5	11847.6	12948.9	14578.1	17780.7
22	11026.9	11863.4	12970.6	14613.0	17869.9
23	11039.3	11879.2	12992.5	14648.3	17961.6
24	11051.7	11895.1	13014.4	14683.9	18055.8
25	11064.2	11911.0	13036.6	14719.9	18152.6
26	11076.8	11927.1	13058.8	14756.3	18252.3
27	11089.3	11943.1	13081.2	14793.0	18354.9
28	11102.0	11959.4	13103.8	14830.2	18460.7
29	11114.6	11975.6	13126.5	14867.8	18569.8
M.	Min.	Min.	Min.	Min.	..
L.	85	86	87	88	89

A Table of Meridional Parts. [279]

L.	85	86	87	88	89
M.	Min.	Min.	Min.	Min.	Min.
30	II 127.4	I 1992.0	I 3149.3	I 4905.8	I 8682.5
31	II 140.1	I 2008.4	I 3172.3	I 4944.2	I 8792.1
32	II 152.9	I 2024.9	I 3195.5	I 4983.0	I 919.7
33	II 165.8	I 2041.5	I 3218.8	I 5022.9	I 944.7
34	II 178.7	I 2058.2	I 3242.4	I 5062.1	I 174.4
35	II 191.7	I 2074.9	I 3265.9	I 5102.3	I 309.2
36	II 204.7	I 2091.7	I 3289.7	I 5143.0	I 449.5
37	II 217.7	I 2108.6	I 3313.7	I 5184.2	I 595.8
38	II 230.9	I 2125.6	I 3337.8	I 5225.8	I 748.5
39	II 244.0	I 2142.7	I 3362.1	I 5268.0	I 908.6
40	II 257.2	I 2159.9	I 3386.6	I 5310.7	I 075.2
41	II 270.5	I 2177.1	I 3411.2	I 5354.0	I 252.5
42	II 283.8	I 2194.4	I 3436.1	I 5397.8	I 438.3
43	II 297.1	I 2211.8	I 3461.1	I 5442.1	I 634.8
44	II 310.6	I 2229.3	I 3486.3	I 5487.0	I 843.1
45	II 324.0	I 2246.9	I 3511.6	I 5532.6	I 064.9
46	II 337.6	I 2264.6	I 3537.2	I 5578.7	I 302.0
47	II 351.1	I 2282.4	I 3563.0	I 5625.5	I 556.6
48	II 364.8	I 2300.2	I 3588.9	I 5673.0	I 831.7
49	II 378.4	I 2318.2	I 3615.1	I 5721.0	I 130.6
50	II 392.2	I 2336.3	I 3641.4	I 5769.8	I 458.0
51	II 406.0	I 2354.4	I 3668.0	I 5819.3	I 819.9
52	II 419.8	I 2372.7	I 3694.7	I 5869.5	I 324.3
53	II 433.7	I 2391.0	I 3721.7	I 5920.4	I 582.6
54	II 447.7	I 2409.5	I 3748.9	I 5972.1	I 211.8
55	II 461.7	I 2428.0	I 3776.3	I 6024.6	I 436.9
56	II 475.8	I 2446.7	I 3803.9	I 6077.9	I 600.8
57	II 489.9	I 2465.3	I 3831.7	I 6132.0	I 582.9
58	II 504.1	I 2484.2	I 3859.8	I 6187.0	I 7958.0
59	II 518.3	I 2503.1	I 3888.1	I 6242.9	I 364.3
M.	Mnin.	Min.	Min.	Min.	Min.
L.	85	86	87	88	89

## S E C T. XI.

## Of Oblique Sailing.

**T**H E Questions that may be propos'd on this Head being innumerable, I shall only give a few of the most useful.

## Problem 1.

Coasting along the Shore I saw a Cape bear from me N N E, then I stood away N W b V 20 Miles, and I observ'd the same Cape to bear from me N E b E. Required the Distance of the Ship from the Cape at each Station.

## Geometrically.

Draw the Circle N W S E to represent the Compass, N S the Meridian, and E W the East and West Line, and let C be the Place of the Ship in her first



Station; then from C set off upon the NW b W Line, C A 20 Miles, and A will be the Place of the Ship in her second Station.

From C draw the N N E Line C B and from A draw A B parallel to the N E b E Line C D, which will meet C B in B the Place of the Cape, and C B will be the

Distance of it from the Ship in its first Station, and A B the Distance in the Second, to find which

By

## By Calculation.

In the Triangle  $ACB$  are given  $AC$ , equal to 20 Miles, the Angle  $ACB$  equal to  $78^\circ, 45'$ ; the Distance between the NNE and NW by W Lines; also the Angle  $A$ , equal to  $BCD$  (by Art. 36 Sect. 1.) equal to  $33^\circ, 45'$ , the Distance between the NNE and NE by E Lines; and consequently the Angle  $A$  equal to  $67^\circ, 30'$ , (by Cor. 1. Art. 61 Sect. 1.)

Hence for  $CB$ , the Distance of the Cape from the Ship in her first Station, it will be (by Case 2. of Oblique Trigonometry.)

$$S, ABC : AC :: S, BAC : CB.$$

i. e. As the Sine of the Angle  $B$   $33^\circ, 45'$  9.74474  
is to the Distance run  $AC$  20. - - 1.30103  
so is the Sine of  $BAC$  - -  $67, 30$  - 9.96562  
to  $CB$  - - - - 33.26 - 1.52191  
the Distance of the Cape from the Ship at the first Station. Then for  $AB$  it will be by the same Case.

$$S, ABC : AC :: S, ACB : AB.$$

i. e. As the Sine of  $B$  - -  $33^\circ, 45'$  - 9.74474  
is to  $AC$  - - - - 20. - - - 1.30103  
so is the Sine of  $C$  - -  $78, 45$  - 9.99157  
to  $AB$  - - - - 35.31 - 1.54786  
the Distance of the Ship from the Cape at her second Station.

## Problem 2.

Coasting along the Shore I saw two Headlands, the first bore from me NE by E 17 Miles, the other SSW 20 Miles. Required the Bearing and Distance of these Headlands from one another.

## Geometrically.

Having drawn the Compass N W S E, let C represent the Place of the Ship, set off upon the N E b E Line CA 17 miles, from C to A, and upon the S S W Line CB, 20 Miles from C to B, and join A B, then A will be the first Headland, and B the second; also A B will be their Distance, and the Angle A will be the Bearing from the N E b E Line, to find which,

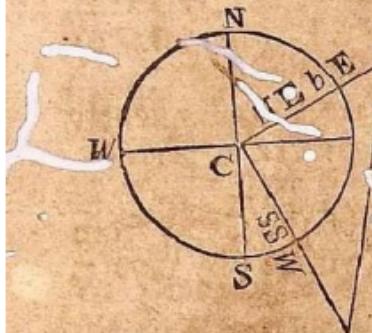
## By Calculation.

In the Triangle A C B are given, A C 17, C B 20, and the Angle A C B equal to  $101^{\circ} 15'$ , the Distance between the N E b E and S S W Lines. Hence, by Case 4. of Oblique-Angular Trigonometry, it will be,

As the Sum of the Sides A C and C B 37. 1.56820  
is to their Difference - - - 3. 0.47712  
so is the Tang. of  $\frac{1}{2}$  the Sum of the Angles A and B  $\{ 39^{\circ}, 22\frac{1}{2}' \}$  9.91417  
to the Tang. of half their Diff. 3 , 49. 8.82309  
consequently the Angle A will be  $43^{\circ}, 11'$ , and the Angle B  $35^{\circ}, 34'$ ; also the Bearing of B from A will be S b W  $1^{\circ}, 49'$ , Westerly, and the Bearing of A from B will be N b E  $1^{\circ}, 49'$  Easterly.

Then for the Distance A B it will be, by Case 2. of Oblique-Angular Trigonometry.)

S, A :



S, A : CB :: S, C : AB.

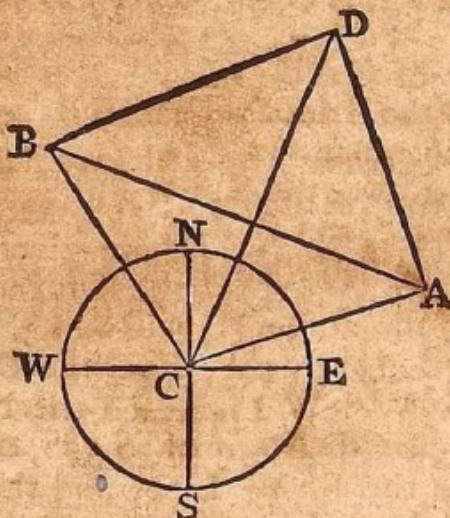
i. e. As the Sine of A  $\cdot 43^\circ$ , 11' - - 9:8327  
 is to CB - - 20. - - 1.30103  
 so is the Sine of C - 101,15 - - 9.99157  
 to AB - - 28.67 - - 1.45733  
 the Distance between the two Headlands.

### Problem 3.

Coasting along the Shore I saw two Headlands, the first bore from me N.W. by N., and the second N.N.E.; then standing away E. by N.  $\frac{1}{4}$  Northerly 20 Miles, I found the first bore from me W.N.W.  $\frac{1}{2}$  Westerly, and the second N. by W.  $\frac{1}{2}$  Westerly. Required the Bearing and Distance of these two Headlands.

### Geometrically.

Having drawn the Compass N.W.S.E., let C represent the first Place of the Ship, from which



draw the N.W. by N. Line CB, and the N.N.E. Line CD, also the E. by N.  $\frac{1}{4}$  N. Line CA, which make equal

equal to 20. From A draw AB parallel to the NW  $\frac{1}{2}$  W Line, and AD parallel to the NbW  $\frac{1}{2}$  W meeting the two first Lines in the Points B and D; then B will be the first, and D the second Headland. Join the Points B and D, and BD will be the Distance between them, and the Angle CDB the Bearing from the NNE Line, to find which

### By Calculation.

1. In the Triangle ABC is given the Angle BCA, equal to  $104^{\circ}, 04'$ , the Distance between the NWbN Line, and the ENE  $\frac{1}{4}$  E Line, the Angle BAC equal to  $36^{\circ}, 34'$ , the Distance between the WSW  $\frac{1}{4}$  W Line and the WN $\frac{1}{2}$  W Line, the Angle ABC equal to  $39^{\circ}, 22'$ , the Distance between the ESE  $\frac{1}{2}$  E Line, and the SWbS Line, also the Side CA equal to 20 Miles, whence for CB it will be, (by Case 2. of Oblique Trigonometry.)

As the Sine of CBA -	$39^{\circ}, 22'$	-	9.80228
is to AC -	20.	-	1.30103
so is the Sine of CAB -	$36^{\circ}, 34'$	-	9.77507
to CB -	18.79	-	1.27382

the Distance between the first Headland and the Ship in her first Station.

2. In the Triangle ACD, are given the Angle ACD, equal to  $47^{\circ}, 49'$ , the Distance between the ENE  $\frac{1}{4}$  E Line, and the NNE Line; the Angle CAD, equal to  $92^{\circ}, 49'$ , the Distance between the WSW  $\frac{1}{4}$  W Line, and the NbW  $\frac{1}{2}$  W Line, the Angle CDA, equal to  $39^{\circ}, 22'$ , the Distance between the SSW Line, and the SbE  $\frac{1}{2}$  E Line, also the Leg CA equal to 20.

Hence for CD it will be, (by the 2. Case of Oblique Trigonometry.)

As

As the Sine CDA - -  $39^\circ, 22'$  - 9.80228  
 is to AC - -  $20.$  - - 1.30103  
 so is the Sine of CAD  $92^\circ, 34'$  - 9.99960  
 to CD - -  $31.5$  - - 1.41835  
 the Distance between the second Headland, and  
 the Ship : her first Station.

3. In the triangle BCD are given BC 18.79,  
 CD 31.5, and the Angle BCD, equal to  $56^\circ, 15'$   
 the Distance between the NW by N Line, and the  
 NNE Line.

Hence, for the Angle CBD, it will be, (by Case  
 4. of Oblique Trigonometry.)

As the Sum of the Sides - - 50.29 - 1.70148  
 is to the Diff. of the Sides 12.71 - 1.10415  
 so is the Tang. of  $\frac{1}{2}$  the Sum  $61^\circ, 52'$  - 10.27189  
 of the unknown Angles  $36^\circ, 35'$  to the Tang. of half their diff.  $25^\circ, 18'$  - 9.67456  
 consequently the Angle CBD is  $87^\circ, 10'$ , and  
 the Angle CDB  $36^\circ, 35'$ . Hence the Bearing  
 of the first Headland from the second will be  
 $859^\circ, 08'$ , W or SW by W  $\frac{1}{2}$  W nearly, and  
 and for the Distance between them it will be

As the Sine of BDC - -  $36^\circ, 35'$  - 9.77525  
 is to BC - - - 18.79 - 1.27382  
 so is the Sine of BCD - -  $56^\circ, 15'$  - 9.91085  
 to BD - - - 26.21 - 1.41843  
 the Distance between the two Headlands.

This, and the first Problem, are of great Use in  
 drawing the Plot of any Harbour, or laying down  
 any Sea-Coast.

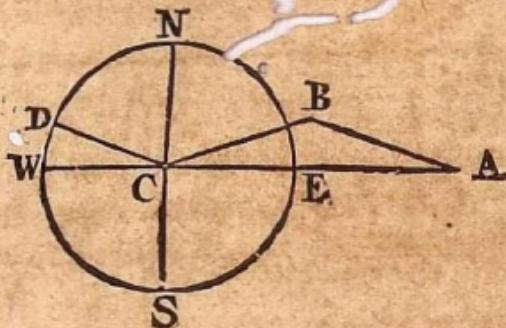
### Problem 4.

Suppose a Ship that makes her Way good within  
 $6\frac{1}{2}$  Points of the Wind, at North, is bound to a  
 Port bearing East 86 Miles distance from her. Re-  
 quir'd

quir'd the Course and Distance upon each Tack, to gain the intended Port.

### Geometrically.

Having drawn the Compass N E  $\frac{1}{2}$  E, let C represent the Ship's Place, and set off on the East, Line CA 86 Miles, so A will be the intended Port. Draw CD and CB on each Side of the North Line, at  $\frac{1}{2}$  Points Distance from it, and thro' A draw AB



parallel to CD meeting CB in B; then the ENE  $\frac{1}{2}$  E Line CB will be the Course of the Ship upon the Starboard Tack, and CB its Distance on that Tack; also the ESE  $\frac{1}{2}$  E Line AB will be the Course on the Larboard Tack, and BA the Distance on that Tack, to find which

### By Calculation.

In the Triangle ABC are given the Angle ACB equal to  $16^{\circ} 53'$ , the Distance between the East and ENE  $\frac{1}{2}$  E Line, the Angle CBA equal to  $146^{\circ} 14'$ , the Distance between the ENE  $\frac{1}{2}$  E and the NW  $\frac{1}{2}$  W Lines, the Angle BAC equal to  $16^{\circ} 53'$ , the Distance between the East, and ESE  $\frac{1}{2}$  E Lines, also AC 86 Miles.

Hence, since the Angle at A and C are equal, the Legs CB and BA will likewise be equal; to find

find either of which (Suppose CB) it will be (by Case 2. of Oblique-Angle Trigonometry.)

As the Sine pf B - - -	146°, 14'	- - -	9.7 493
is to A C - - - -	86.	- - -	1.92450
So is the Sine of A - -	16,53	- - -	9.7503
to CB - - - -	44.94	- - -	1.65260

the Distan<sup>c</sup>ce the Ship must sail on each Tack.

There is a great Variety of useful Questions of this Nature that may be propos'd, but the Nature of them being better understand by Practice at Sea, we shall leave them, and go on to Current Sailing.

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## S E C T. XII.

### Concerning Currents, and how to make proper Allowances for them.

I. **C U R R E N T S** are certain Settings of the Stream, by which all Bodies (as Ships, &c.) moving therein, are compell'd to alter their Course or Velocity, or both; and submit to the Motion impressed upon them by the Current.

#### C A S E I.

If the Current sets just with the Course of the Ship, (*i. e.*) moves on the same Rumb with it; then the Motion of the Ship is encreas'd, by as much as is the Drift or Velocity of the Current.

#### Example.

Suppose a Ship sails SE b S at the Rate of 6 Miles an Hour, in a Current that sets SE b S 2 Miles an Hour. Requir'd her true Rate of Sailing.

Here it is evident, that the Ship's true Rate of Sailing, will be 8 Miles an Hour.

#### •C A S E

## C A S E 2.

If the Current sets directly against the Ship's Course, then the Motion of the Ship is lessen'd by as much as is the Velocity of the Current.

## Example.

Suppose a Ship sails S<sup>E</sup>W<sup>N</sup> at the Rate of 10 Miles an Hour, in a Current that sets NNE 6 Miles an Hour. Requir'd the Ship's true Rate of Sailing.

Here it is evident, that the Ship's true Rate of Sailing will be 4 Miles an Hour. Hence it is plain,

*Cor. 1.* If the Velocity of the Current be less than the Velocity of the Ship, then the Ship will get so much *a-Head* as is the Difference of these Velocities.

*Cor. 2.* If the Velocity of the Current be greater than that of the Ship, then the Ship will fall so much *a-Stern* as is the Difference of these Velocities.

*Cor. 3.* Lastly, If the Velocity of the Current be equal to that of the Ship, then the Ship will stand still; the one Velocity destroying the other.

## C A S E 3.

If the Current thwarts the Course of the Ship, then it not only lessens or augments her Velocity, but gives her a new Direction compounded of the Course she steers, and the setting of the Current, as is manifest from the following

## Lemma.

If a Body at A be impell'd by two Forces at the same Time, the one in the Direction AB, capable

pable to carry that Body from A to B in a certain Space of Time, and the other in the Direction AD capable to carry it from A to D in the same Time: Complete the Parallelogram ABCD, and draw the Diagonal AC; then the Body at A, agitated by these two Forces together will move along the Line AC, & I will be in the Point C at the End of the Time, in which it would have mov'd a long AD or AB with the Forces separately applied.

Hence the Solution of the following Examples will be evident.

### Example 1.

Suppose a Ship sails (by the Compas) directly South 96 Miles in 24 Hours, in a Current that sets East 45 Miles in the same Time. Requir'd the Ship's true Course and Distance.

### Geometrically.

Draw AD (see the last Scheme) to represent the South and North Line of the Ship at A, which make equal to 96; from D draw DC perpendicular to AD equal to 45, and join AC. Then C will be the Ship's true Place, AC her true Distance, and the Angle CAD the true Course. To find which,

### By Calculation

First, For the true Course DAC, it will be (by Case 4. of Rectangular Trigonometry.)

As the apparent Distance AD -	96.	-	1.98227
is to the Current's Motion DC -	45.	-	1.65321

so is Radius - - - - - 10.00000  
 to the Tangent of the true Course  $\{ 25^\circ, 07' - 9.67094$   
 Course DAC - - - - -  
 consequently the Ship's true Course is S  $25^\circ, 07'$  E  
 or SSE  $2^\circ, 37'$  Easterly.

Then for the true Distance AC, it will be, (by  
 Case 2. of Rectangular Trigonometry)

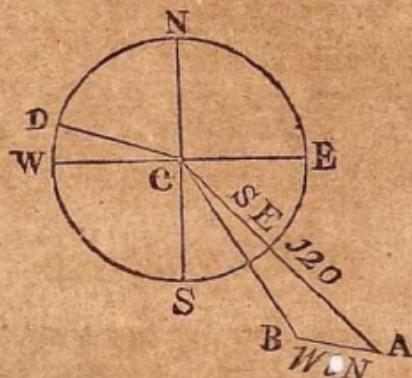
As the Sine of the Course A  $25^\circ, 07'$  - 9.62784  
 is to the Curr. Motion DC 45° - - - - - 1.03321  
 so is Radius - - - - - 10.00000  
 to the true Distance AC - - - - - 2.02537

### Example 2.

Suppose a Ship sails SE 120 Miles in 20 Hours, in a Current that sets W b N, at the Rate of 2 Miles an Hour. Requir'd the Ship's true Course and Distance sail'd in that Time.

### Geometrically.

Having drawn the Compass N E S W, let C represent the Place the Ship sail'd from; draw the



SE Line CA, which make equal to 120; then will A be the Place the Ship caped at.

From

From A draw AB parallel to the W b N Line CD, equal to 20, the Motion of the Current in 20 Hours, and join CB; then B will be the Ship's true Place at the End of 20 Hours, CB her true Distance, and the Angle SCB her true Course. To find which,

### By Calculation.

In the Triangle ABC are given CA 120, AB 40, and the Angle C A B equal to  $33^{\circ} 45'$ , the Distance between the E. S. and SE Lines, to find the Angles B and C, and the Side CB.

First, For the Angles C and B it will be, (by Case 4. of Oblique Trigonometry,)

As the Sum of the Sides CA and AB 160. 2.20412  
is to their Difference - - - 80. 1.90309  
so is the Tang. of half the  $\angle$  73 $^{\circ}$ , 07' - 10.51783

Sum of the Angles B and C  $\angle$  73 $^{\circ}$ , 07' - 10.51783  
to the Tang. of half their Diff. 58 $^{\circ}$ , 45' - 10.21680  
consequently the Angle B will be 131 $^{\circ}$ , 52', and the Angle A C B 14 $^{\circ}$ , 23'. Hence the true Course is S 30 $^{\circ}$ , 37' E, or SSE 8 $^{\circ}$ , 07' Easterly.

Then, for the true Distance CB, it will be, (by Case 2. of Oblique Trigonometry,)

As the Sine of B	- - -	131 $^{\circ}$ , 52'	-	9.87198
is to AC	- - -	120.	- - -	2.07918
so is the Sine of A	- - -	33 $^{\circ}$ , 45'	-	9.74474
to the true Distance CB	-	89.53	-	1.95194

### Example 3.

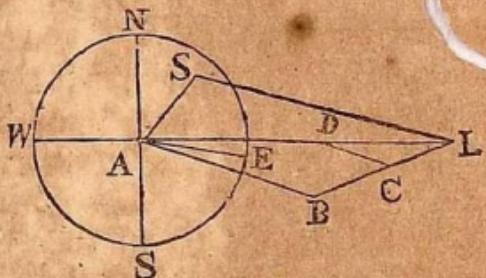
Suppose a Ship coming out from Sea in the Night, has Sight of Scilly Light, bearing N E b N Distance 4 Leagues, it being then Flood-Tide, setting E N E 2 Miles an Hour, and the Ship running after the Rate of 5 Miles an Hour. Requir'd upon what

Course, and how far she must sail to hit the Lizard which bears from Scilly E  $\frac{1}{2}$  S Distance 17 Miles.

### Geometrically.

Having drawn the Compass N E S W, let A represent the Ship's Place at Sea, and draw the N E  $\frac{1}{2}$  N Line A S, which make equal to 12 Miles, so S will represent Scilly.

From S draw S L, equal to 51 Miles, and parallel to the E  $\frac{1}{2}$  S Line; then L will represent the Lizard.



From L draw L C parallel to the E N E Line, equal to 2 Miles, and from C draw C D equal to 3 Miles, meeting A L in D; then from A draw A B parallel to C D, meeting L C produc'd in B, and A B will be the requir'd Distance, and S A B the true Course. To find which,

### By Calculation.

In the Triangle A S L are given the Side A S, equal to 12 Miles, the side S L, equal to 51, and the Angle A S L equal to  $118^{\circ} 07'$ , the Distance between the N E  $\frac{1}{2}$  N and W  $\frac{1}{2}$  N Lines, to find the Angles S A L and S L A. Consequently, (by Case 4. of Oblique Trigonometry, it will be

As the Sum of the Sides AS and SL 63. 1.79934  
 is to their Difference - - - 39. 1.59106  
 so is the Tang. of half the Sum } 30°, 56' 9.77763  
 of the Angles SAL and SLA } 30°, 56' 9.77763  
 to the Tang. of half their Diff. 20°, 21' 9.56955  
 consequently the Angle SAL, will be 51°, 17',  
 and so the direct Bearing of the Lizard from the  
 Ship, will be N 85°, 02' E, or E by N 6°, 17' E,  
 and for the Distance AL, it will be, (by Case 2. of  
 Oblique Trigonometry,)

As the Sine of SAL - - 51°, 17' - 9.89223  
 is to SL - - - - 51. - - - 1.70757  
 so is the Sine of ASL 118°, 07' : 9.94546  
 to AL - - - - 57.65 - - 1.76080  
 the Distance between the Ship and the Lizard.

Again, in the Triangle DLC, are given the  
 Angle L, equal to 17°, 32', the Distance between  
 the ENE and N 85°, 02' E Lines, the Side LC  
 equal to 2 Miles, the Current's Drift in an Hour,  
 and the Side CD equal to 5 Miles the Ship's Run  
 in the same Time. Hence, for the Angle D, it will  
 be, (by Case 1. of Oblique Trigonometry,)

As the Ship's Run in 1 Hour DC 5. - 0.69897  
 is to the Sine of L - - - 17°, 32' 9.47894  
 so is the Current's Drift LC - 2. - 0.30103  
 to the Sine of D - - - 6°, 55' 9.08100

consequently, since by Construction the Angle  
 LAB is equal to the Angle LDC, the Course  
 the Ship must steer is S 88°, 03' E. .

Then for the Distance AB, it will be, (by Case  
 2. of Oblique Trigonometry,)

As the Sine of B - - 155°, 33' - - 9.61689  
 is to AL - - - - 57.65 - - 1.76080  
 so is the Sine of L - 17,32 - - 9.47894  
 to AB - - - - 41.96 - - 1.62285.  
 consequently,

consequently, since the Ship is sailing at the Rate of 5 Miles an Hour, it follows, that in sailing 8 Hours, 24 Min. S.  $8^{\circ}$ ,  $103'$  E, she will arrive at the Lizard.

## Example 4.

A Ship from a certain Headland in the Latitude of  $34^{\circ}$ ,  $00'$  North, sails S E b S 12 Miles in three Hours, in a Current that sets between North and East, and then the same Headland is found to bear W N W, and the Ship to be in the Latitude of  $33^{\circ}$ ,  $52'$  North. Requir'd the Setting and Drift of the Current.

## Geometrically.

Having drawn the Compas NESW, let A represent the Place of the Ship, and draw the S E b S

Line A B equal to 12 Miles, also the E S E Line A C.

Set off from A upon the Meridian, A D, equal to 8 Miles, the Difference of Latitude, and thro' D draw DC parallel to the East and West Line W E, meeting AC in C. Join C and B with the Right Line BC; then C will be the Ship's Place, the Angle ABC the setting of the Current from the S E b S Line, and the Line BC will be the Drift of the Current in 3 Hours. To find which,

## By Calculation.

In the Triangle ABC, Right-angled at D, are given the Difference of Latitude A D equal to 8 Miles, the Angle DAC equal to  $67^{\circ}, 30'$ . Whence for AC, the Distance the Ship has sail'd, it will be,

As

As Radius	- - -	10.00000
is to the Difference of Lat at AD	8. -	0.00300
so is the Sec. or the Course	{ 67°, 30' -	10.41716
DAC	- - -	
to the Distance run AC	* 20.9 - -	1.32025

Again, in the Triangle ABC are given AB equal to 12 Miles, AC equal to 20.9, and the Angle BAC equal to  $33^{\circ}, 45'$ , the Distance between the SE & S and ESE Lines. Whence, for the Argle at B, it will be,

As the Sum of the Sides AC and AB	32.9	1.51720
is to their Difference	- - -	8.9 0.94939
so is the Tang. of half the	{ 73°, 07'	10.51806
Sum of the Angles B and C	- - -	
to the Tang. of $\frac{1}{2}$ their Diff.	$41^{\circ}, 43' \frac{1}{2}$	9.95025

consequently the Angle B is  $114^{\circ}, 51'$ , and so the Setting of the Current will be N  $81^{\circ}, 06'$  E or Eb N  $2^{\circ}, 21'$  E. Then for BC, the Current's Drift in three Hours, it will be,

As the Sine of B	- - -	$114^{\circ}, 51'$	-	9.95025
is to the Distance run AC	20.9	- - -	-	1.32025
so is the Sine of A	- - -	$33^{\circ}, 45'$	-	9.74474
to BC	- - - -	12.8	- - -	1.10719

the Current's Drift in 3 Hours, and consequently the Current sets Eb N  $2^{\circ}, 21'$  E 4.266 Miles an Hour.

## SECT. XII.

Concerning the Variation of the Compass,  
and how to find it from the true and  
observ'd Amplitudes or Azimuths of  
the Sun.

1. THE Variation of the Compass is how far  
the North or South Point of the Needle  
stands from the true South or North Point of the  
Horizon towards the East or West; or 'tis an Arch  
of the Horizon intercepted between the Meridian  
of the Place of Observation and the Magnetic Me-  
ridian.

2. It is absolutely necessary to know the Variation  
of the Compass at Sea, in order to correct the  
Ship's Course; for since the Ship's Course is directed  
by the Compass, 'tis evident, that if the Com-  
pass be wrong, the true Course will differ from the  
observed, and consequently the whole Reckoning  
differ from the Truth.

3. The Sun's true Amplitude is an Arch of the  
Horizon, comprehended between the true East or  
West Point thereof, and the Center of the Sun at  
Rising or Setting; or it is the Number of Degrees,  
&c. that the Center of the Sun is distant from the  
true East or West Point of the Horizon, towards  
the South or North.

4. The Sun's Magnetic Amplitude is the Number  
of Degrees that the Center of the Sun is from the  
East or West Point of the Compass, towards the  
South or North Point of the same at Rising or Setting.

5. Having the Declination of the Sun, together  
with the Latitude of the Place of Observation, we  
may from thence find the Sun's true Amplitude, by  
the following Astronomic Proposition, viz.

As the Co-sine of the Latitude  
is to the Radius

so is the Sine of the Sun's Declination  
to the Sine of the Sun's true Amplitude.

which will be North or South according as the Declination is North or South.

### Example.

Requir'd the Sun's true Amplitude in the Latitude of  $41^{\circ} 50'$  North, on the 23 Day of April 1731.

First, I find from the third Table at the End of this Book, that the Sun's Declination the 23d of April 1731, is  $15^{\circ} 54'$  North, then for the true Amplitude, it will be, by the former Analogy.

As the Co-Sine of the Lat. . .  $41^{\circ}, 50'$  . 9.87221  
is to Radius . . . . . 10.00000

so is the Sine of the Declination  $15^{\circ}, 54'$  . 9.43769  
to the Sine of the Amplitude  $21, 35'$  . 9.56548

which is North, because the Declination is North at that Time; and consequently in the Latitude of  $41^{\circ}, 50'$  North, the Sun rises on the 23d of April 1731,  $21^{\circ}, 35'$ , from the East-Part of the Horizon towards the North, and sets so much from the West the same Way.

6. The Sun's true *Azimuth* is the Arch of the Horizon intercepted between the Meridian and the Vertical Circle passing thro' the Center of the Sun at the Time of Observation.

7. The Sun's *Magnetic Azimuth* is the Arch of the Horizon intercepted between the Magnetic Meridian and the Vertical, passing thro' the Sun.

8. Having the Latitude of the Place of Observation, together with the Sun's Declination and Altitude at the Time of Observation, we may find his true Azimuth after the following Method, viz.

Make it,

*As the Tangent of half the Complement of the Latitude  
is to the Tangent of half the Sum of the Distance of  
the Sun from the Pole and Complement of the Altitude,  
so is the Tangent of half the Difference between the  
Distance of the Sun from the Pole and Complement of  
the Altitude  
to the Tangent of a fourth Arch.*

which fourth Arch added to half the Complement  
of the Latitude, will give a fifth Arch, and this  
fifth Arch lessened by the Complement of the La-  
titude will give a sixth Arch; then make it

*As the Radius  
is to the Tangent of the Altitude  
so is the Tangent of the sixth Arch  
to the Co-Sine of the Sun's Azimuth,*

which is to be counted from the South or North, to  
the East or West, according as the Sun is situated  
with respect to the Place of Observation.

If the Latitude of the Place and Declination of  
the Sun be both North or both South, then the De-  
clination taken from  $90^\circ$ , will give the Sun's Dis-  
tance from the Pole; but if the Latitude and Decli-  
nation be on contrary Sides of the Equator, then  
the Declination added to  $90^\circ$ , will give the Sun's Dis-  
tance from the nearest Pole to the Place of Obser-  
vation.

### Example.

In the Latitude of  $51^\circ$ ,  $32'$  North, the Sun hav-  
ing  $19^\circ$ ,  $39'$  North Declination, his Altitude was  
found by Observation to be  $38^\circ$ ,  $18'$ . Requir'd the  
Azimuth.

By

By the first of the foregoing Analogies it will be

As the Tangent of $\frac{1}{2}$ the Com-	$\frac{1}{2}$	Latitude	$\{ 19^\circ, 14'$	9.54269
plement of the Latitude				10.25655
is to the Quotient of $\frac{1}{2}$ the	$\frac{1}{2}$	Sum of the Distance of the	$\{ 61,,01$	
Sun from the Pole; and Com-				
plement of the Altitude	$\frac{1}{2}$	So is the Tangent of half their	$\{ 9,,19$	9.21499
Difference				to the Tang. of a fourth Arch
			$\{ 40,,20$	9.92885

which fourth Arch  $40^\circ, 20'$ , added to  $19^\circ, 14'$  half the Complement of the Latitude gives a fifth Arch  $59^\circ, 34'$ , and this fifth Arch lessened by  $38^\circ, 28'$ , the Complement of the Latitude gives the sixth Arch  $21^\circ, 06'$ ; then for the Azimuth it will be by the second of the preceding Analogies,

As Radius		10.00000
is to the Tang. of the Altitude	$38^\circ, 18'$	9.89749
so is the Tang. of the sixth Arch	$21, 06'$	9.58644
to the Co-Sine of the Azimuth	$72,,15$	9.48393

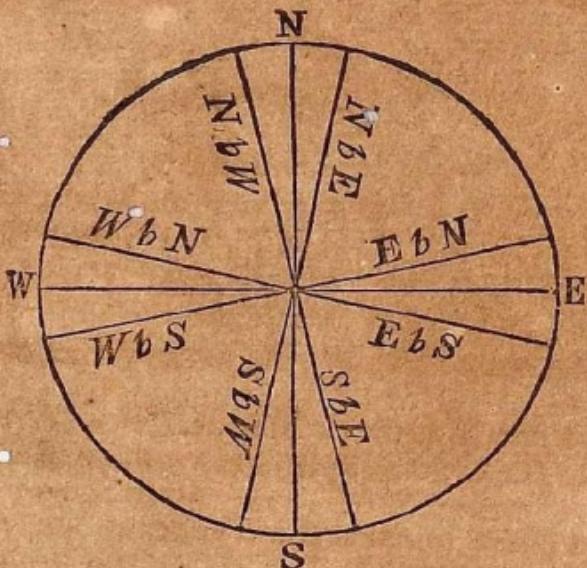
which, because the Latitude is North, and the Sun South off the Place of Observation, must be counted from the South towards the East or West; and consequently if the Altitude of the Sun was taken in the Morning, the Azimuth will be S  $72^\circ, 15'$  E, or E S E  $4^\circ, 45'$  E; but if the Altitude was taken in the Afternoon, the Azimuth will be S  $72^\circ, 15'$  W, or W S W  $4^\circ, 45'$  Westerly.

9. Having found the Sun's true Amplitude or Azimuth by the preceding Analogies, and his Magnetic Amplitude or Azimuth by Observation, 'tis evident if they agree there is no Variation; but if they disagree, then if the true and observ'd Amplitudes at the Rising or Setting of the Sun, be both of the same

same Name, i. e. either both North, or both South, their Difference is the *Variation*. But if they be of different Names, i. e. one North, and the other South, their Sum is the *Variation*: Again, if the true and observ'd Azimuths be both of the same Name, i. e. either both East or both West, their Difference is the *Variation*; but if they be of different Names their Sum is the *Variation*: And to know whether the *Variation* is Easterly or Westerly, observe this general Rule, viz.

Let the Observer's Face be turn'd to the Sun, then if the true Amplitude or Azimuth be to the Right-Hand of the observ'd, the *Variation* is Easterly; but if to the Left, Westerly.

To explain which, let N E S W represent a Compass, and suppose the Sun is really E b S at the Time of Observation, but the Observer sees him off



the East-Point of the Compass, and so the true Amplitude or Azimuth of the Sun, is to the Right of the Magnetic, or observ'd; here 'tis evident that the

the E. b S Point of the Compass ought to lie where the East-Point is, and so the North where the N. b W. is; consequently the North-Point of the Compass is a Point too far East, i. e. the Variation in this Case is Easterly. The same will hold when the Amplitude or Azimuth is taken on the West-side of the Meridian.

Again, let the true Amplitude or Azimuth be to the Left-Hand of the observ'd; thus suppose the Sun is really E. b N at the Time of Observation, but the Observer sees him off the East-Point of the Compass, and so the true Amplitude or Azimuth to the Left of the observ'd: Here it is evident that the E. b N Point of the Compass ought to stand where the East-Point is, and so the North where the N. b E Point is; consequently the North-Point of the Compass lies a Point too far Westerly, so in this Case the Variation is West. The same will hold when the Sun is observ'd on the West-side of the Meridian.

### *Example I.*

Suppose the Sun's true Amplitude at Rising is found to be E  $14^{\circ}$ ,  $20'$  N, but by the Compass it is found to be E  $26^{\circ}$ ,  $12'$  North. Required the Variation, and which Way it is.

Since they are both the same Way; therefore,

From the Magnetic Amplitude - E  $26^{\circ}$ ;  $12'$  N.  
take the true Amplitude - - - E  $14^{\circ}$ ,  $20'$  N.

and there remains the Variation - II, 52 E.

which is Easterly, because in this Case the true Amplitude is to the Right of the observ'd.

### *Example*

## Example 2.

Suppose the Sun's true Amplitude at Setting is W  $34^{\circ}$ ,  $26'$  S, and his Magnetic Amplitude W  $23^{\circ}$ ,  $13'$  S. Requir'd the Variation, and which Way it is. Since they lie both the same Way, therefore,

From the Sun's true Amplitude W  $34^{\circ}$ ,  $26'$  S.  
take the Magnetic Amplitude W  $23^{\circ}$ ,  $13'$  S.

there remains the Variation - - II,  $13'$  W.  
which is Westerly, because the true Amplitude in  
this Case is to the Left-Hand of the observ'd.

## Example 3.

Suppose the Sun's true Amplitude at Rising is found to be E  $13^{\circ}$ ,  $24'$  N, and his Magnetic E  $12^{\circ}$ ,  $32'$  S. Requir'd the Variation, and which Way it lies.

Since the true and observ'd Amplitudes lie different Ways, therefore,

To the true Amplitude - - - E  $13^{\circ}$ ,  $24'$  N.  
add the Magnetic Amplitude E  $12^{\circ}$ ,  $32'$  S.  
the Sum is the Variation - - - 25,  $56'$  W.

which is Westerly, because the true Amplitude is,  
in this Case, to the Left of the observ'd.

## Example 4.

Suppose the Sun's true Amplitude at Setting is found to be W  $8^{\circ}$ ,  $24'$  N, but his Magnetic Amplitude is W  $10^{\circ}$ ,  $13'$  S. Requir'd the Variation.

## Variation of the Compass. 303

To the true Amplitude : . W  $8^{\circ}$ ,  $24'$  N.  
add the Magnetic : . W  $10$ ,  $13'$  S.

the Sum is the Variation : .  $18$ ,  $37'$  E.  
which is Easterly, because the true Amplitude is to  
the Right of the observ'd.

### Example 5.

Suppose the Sun's true Azimuth at the Time of Observation, is found to be N  $86^{\circ}$ ,  $40'$  E, but by the Compass it is N  $73^{\circ}$ ,  $24'$  E. Requir'd the Variation, and which Way it lies.

From the Sun's true Azimuth, N  $86^{\circ}$ ,  $40'$  E.  
take the Magnetical, - - - N  $73$ ,  $24$  E.

There remains the Variation, . . .  $13$ ,  $16$  E.

which is Easterly, because the true Azimuth is to the Right of the observ'd.

### Example 6.

Suppose the Sun's true Azimuth is S.  $3^{\circ}$ ,  $24'$  E. and the Magnetical S.  $4^{\circ}$ ,  $36'$  W. Requir'd the Variation, and which Way it lies.

To the true Azimuth - - S.  $3^{\circ}$ ,  $24'$  E.  
add the Magnetical Azimuth. - S.  $4$ ,  $36$  W.

The Sum is the Variation. - -  $8$ ,  $00$  W.

which is Westerly, because the true Azimuth is (in this Case) to the Left of the observ'd.

10. The Variation of the Compass was first observ'd at *London*, in the Year 1580, to be  $11^{\circ}$ ,  $15'$  Easterly, and in the Year 1622 it was  $6^{\circ}$ ,  $0'$  E. also in the Year 1634, it was  $4^{\circ}$ ,  $05'$  E. still decreasing, and the Needle approaching the true Meridian, till it coincided with it, and then there

there was no Variation; after which, the Variation began to be Westerly, and in the Year 1672, it was observ'd to be  $2^{\circ}$ ,  $30'$  W, also in the Year 1683, it was  $4^{\circ}$ ,  $30'$  W, and since that Time the Variation still continues at London to increase Westerly; but how far it will go that Way, Time and Observations will probably be the only Means to discover.

Again, at Paris, in the Year 1640, the Variation was  $3^{\circ}$ ,  $30'$  E, and in the Year 1666, there was no Variation; but in the Year 1681, it was  $2^{\circ}$ ,  $30'$  W, and still continues to go Westerly.

In short, from Observations made in different Parts of the World, it appears, that in different Places the Variation differs both as to its Quantity and Denomination, it being East in one Place, and West in another; the true Cause and Theory of which, for Want of a sufficient Number of Observations, has not yet been fully explain'd.

## S E C T. XIV.

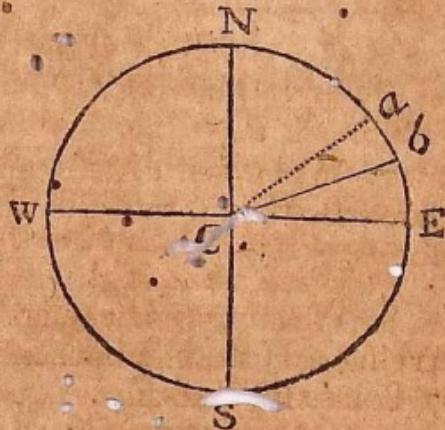
*The Method of keeping a Journal at Sea, and how to Correct it, by making proper Allowances for the Lee-way, Variation, &c.*

**L**EE-WAY is the Angle that the Rumb-line upon which the Ship endeavours to sail, makes with the Rumb she really sails upon. This is occasion'd by the Force of the Wind, or Surge of the Sea; when she lies to the Windward, or is close-haul'd, which causes her to fall off and glide

glide side-ways from the Point of the Compafs she capes at. Thus let NESW represent the Compafs and suppose a Ship at C capes at, or endeavours to sail upon the Rumb Ca; but by the Force of the Wind and Surge of the Sea, she's oblig'd to fall off, and make her Way good upon the Rumb Cb; then the Angle  $\alpha Cb$  is the *Lee-way*, and if that Angle be equal to one Point, the Ship is said to make one Point *Leeway*; and if equal to two Points, the Ship is said to make two Points *Leeway*, &c.

2. The Quantity of this Angle is very uncertain, because some Ships, with the same Quantity of Sail, and with the same Gale, will make more *Lee-way* than others; it depending much upon the Mould and Trim of the Ship, and the Quantity of Water that she draws. The common Allowances that are generally made for the *Lee-way*, are as follows:

1. If a Ship be close haul'd, has all her Sails set, the Water smooth, and a moderate Gale of Wind, she is then suppos'd to make little or no *Lee-way*.
2. If it blow so fresh as to cause the small Sails to be handed, 'tis usual to allow one Point.
3. If it blow so hard that the Top-sails must be close reefed, then the common Allowance is two Points for *Lee-way*.
4. If one Top-sail must be handed, then the Ship is suppos'd to make between two and three Points *Lee-way*.



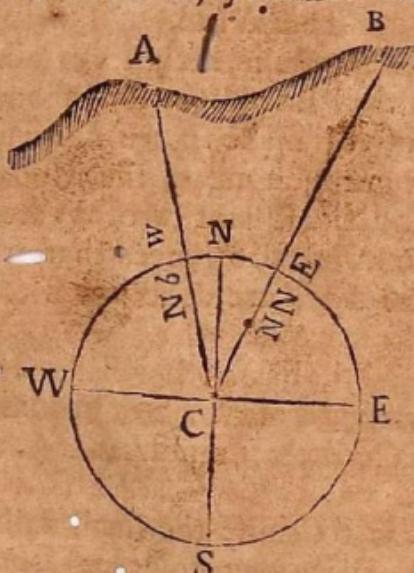
5. When both Top-sails must be handed, then the Allowance is about four Points for *Lee-way*.

6. If it blows so hard, as to occasion the Fore-Course to be handed, the Allowance is between  $5\frac{1}{2}$  and 6 Points.

7. When both Main and Fore-Courses must be handed, then 6 or  $6\frac{1}{2}$  Points are commonly allow'd for *Lee-way*.

8. When the *Mizen* is handed, and the Ship is trying a Hull, she is then commonly allow'd about 7 Points for *Lee-way*.

3. Though these Rules are such as are generally made use of, yet since the *Lee-way* depers much



upon the Mould and Trim of the Ship, 'tis evident that they can't exactly serve to every Ship; and therefore the best Way is to find it by Observation: Thus, let the Ship's *Wake* be set by a *Compass* in the *Poop*, and the opposite *Rumb* is the true *Course* made good by the Ship; then the Difference between this and the *Course* given by the *Compass* in the

*Bittack*, is the *Lee-way* required. If the Ship be within Sight of Land; then the *Lee-way* may be exactly found by observing a Point on the Land which continues to bear the same Way, and the Distance between the Point of the *Compass* it lies upon, and the Point the Ship capes at, will be the *Lee-way*. Thus, suppose a Ship at Sea is lying up

N b W

N<sub>b</sub>W towards A; but instead of keeping that Course, she is carried, in the NNE Line CB, and consequently the Point B continues to bear the same Way from the Ship: Here 'tis evident, that the Angle ACB, or the Distance between the N<sub>b</sub>W Line in't the Ship capes at, and the NNE Line that the Ship really sails upon, will be the *Lee-way*.

4. Having the Course steer'd, and the *Lee-way* given, we may from thence find the true Course by the following Method, *viz.* Let your Face be turn'd directly to the Windward, and if the Ship have her Larboard Tacks on Board, count the *Lee-way* from the Course steer'd towards the Right-hand; but if the Starboard Tacks be on Board, then count it from the Course steer'd towards the Left-hand. Thus, suppose the Wind at North, and the Ship lies up within 6 Points of the Wind, with her Larboard Tacks on Board, making one Point *Lee-way*; here 'tis plain, that the Course steer'd is ENE, and the true Course EbN; also, suppose the Wind is at NNW, and the Ship lies up within 6½ Points of the Wind with her Scarboard Tacks on Board, making 1½ Point *Lee-way*; 'tis evident that the true Course, in this Case, is WSW.

5. We have shew'd, in the last Section, how to find the Variation of the Compas; and from what has been said there, we have this general Rule for finding the Ship's true Course, having the Course steer'd and the Variation given, *viz.* Let your Face be turn'd towards the Point of the Compas upon which the Ship is steer'd; and if the Variation be Easterly, count the Quantity of it from the Course steer'd, towards the Right-hand; but if Westerly, towards the Left-hand; and the Course thus found, is the true Course steer'd. Thus, suppose the Course steer'd is N<sub>b</sub>E, and the Varia-

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tion one Point Easterly; then the true Course  
steer'd, will be NNE; And suppose the Course  
steer'd is NE & E, and the Variation one Point  
Westerly; then in this Case, the true Course will  
be NE; and so of others.

Hence, by knowing the *Lee-way*, *Variation*, and  
*Course* steer'd, we may from thence find the Ship's  
true Course; but if there be a Current under  
Foot, then that must be try'd, and proper Allow-  
ances made for it, as has been shewn at Sect 12.  
from thence to find the true Course.

6. After making all the proper Allowances for  
finding the Ship's true Course, and making as just  
an Estimate of the Distance as we can; yet by  
reason of the many Accidents that attend a Ship in  
a Days Running, such as different Rates of sailing  
between the times of heaving the Log, the Want  
of due Care at the Helm, by not keeping her stea-  
dy, but suffering her to yaw and fall off, sudden  
Storms, when no Account can be kept, &c. the  
Latitude by Account, frequently differs from the  
Latitude by Observation, and when that happens,  
'tis evident there must be some Error in the Reck-  
oning; to discover which and where it lies, and  
also how to correct the Reckoning, you may ob-  
serve the following Rules.

1. If the Ship sail near the Meridian, or within  
2 or  $2\frac{1}{2}$  Points thereof; then, if the Latitude  
by Account, disagrees with the Latitude by Ob-  
servation, 'tis most likely that the Error lies in  
the Distance run; for it is plain, that in this Case it  
will require a very sensible Error in the Course to  
make any considerable Error in the Difference of  
Latitude, whith can't well happen, if due Care be  
taken at the Helm, and proper Allowances be  
made for the *Lee-way*, *Variation*, and *Currents*.  
Consequently, if the Course be pretty near the  
Truth, and the Error in the Distance run regu-  
larly

Larly through the whole, we may from the Latitude obtain'd by Observation, correct the Distance and Departure by Account, by the following Analogies, viz.

*As the Difference of Latitude by Account  
is to the true Difference of Latitude,  
so is the Departure by Account  
to the true Departure,  
and so is the direct Distance by Account  
to the true direct Distance.*

The Reason of this is plain; for let A B denote the Meridian of the Ship at A, and suppose the Ship sails upon the Rumb A E, near the Meridian till, by Account, she is found in C, and consequently her Difference of Latitude by Account is A B; but by Observation she's found in the Parallel E D, and so her true Difference of Latitude is A D, her true Distance A E, and her true Departure D E; then since the Triangles A B C, A D E are similar, it will be  $AB : AD :: BC : DE$  and  $AB : AD :: AC : AE$ .



### Example.

Suppose a Ship from the Latitude of  $45^{\circ} 20'$  North, after having sail'd upon several Courses near the Meridian for 24 Hours, her Difference of Latitude is computed to be upon the whole, 95 Miles Southerly, and her Departure 34 Miles Easterly; but by Observation she is found to be in Latitude  $43^{\circ} 10'$  North, and consequently her true Difference of Latitude is 130 Miles Southerly; then for the true Departure it will be. As the Difference of Latitude by Account 95, is to the true Difference

rence of Latitude 130, so is the Departure by Account 34, to the true Departure 46.52, and so is the Distance by Account 139, to the true Distance 138.

2. If the Courses are for the most Part near the Parallel of East and West, and the Direct Course be not less than 6 Points off the Meridian, then, if the Latitude by Account differs from the observ'd Latitude, it is next probable that the Error lies in the Course, or Distance, or perhaps both; for in this Case 'tis evident, the Departure by Account will be very nearly true; and thence, by the Help of this, and the true Difference of Latitude, may the true Course and direct Distance be readily found by Case 4th of *Plane Sailing*.

### Example.

Suppose a Ship from the Latitude of  $43^{\circ} 50'$  North, after having sail'd upon several Courses near the Parallel of East and West, for the Space of 24 Hours, is found by dead Reckoning to be in the Latitude of  $42^{\circ} 45'$  North, and to have made 160 Miles of Westing; but by a good Observation the Ship is found to be in the Latitude of  $42^{\circ} 35'$  North. Requir'd the true Course, and direct Distance sail'd.

With the true Difference of Latitude 75 Miles, and Departure 160 Miles, we shall find (by Case 4th of *Plane Sailing*) the true Course to be S.  $64^{\circ} 53'$  W, and the direct Distance 176.7 Miles.

3. If the Courses are for the most Part near the Middle of the Quadrant, and the direct Course within 2 and 6 Points of the Meridian; then the Error may be either in the Course, or in the Distance, or in both, which will cause an Error both in the Difference of Latitude and Departure, to correct

correct which, having found the true Difference of Latitude by Observation; with this, and the direct Distance by dead Reckoning, find a new Departure (*by Case 3d of Plane Sailing*) then half the Sum of this Departure, and that by dead Reckoning, will be nearly equal to the true Departure; and consequently with this, and the true Difference of Latitude, we may (*by Case 4th of Plane Sailing*) find the true Course and Distance.

### Example.

Suppose a Ship from the Latitude of  $44^{\circ} 38'$  North, sails between South and East upon several Courses, near the middle of the Quadrant, for the Space of 24 Hours, and is then found, by dead Reckoning, to be in the Latitude of  $42^{\circ} 15'$  North, and to have made of Easting 136 Miles; but by Observation she's found to be in the Latitude of  $42^{\circ} 04'$  North. Requir'd her true Course and Distance.

With the true Difference of Latitude 154 Miles, and the direct Distance, by dead Reckoning, 197.4 you'll find (*by Case 3d of Plane Sailing*) the new Departure to be 123.4, and half the Sum of this and the Departure, by dead Reckoning, will be 124.7 the true Departure; then with this, and the true Difference of Latitude, you'll find (*by Case 4th of Plane Sailing*) the true Course to be  $S\ 39^{\circ} 00'$  E, and the direct Distance 198.2 Miles.

7. In keeping a Ship's Reckoning at Sea, the common Method is to take from the Log-board the several Courses and Distances stemm'd by the Ship last 24 Hours, and to transfer these, together with the most remarkable Occurrences into the Log-Book, in which also are inserted the Courses corrected, and the Difference of Latitude and Difference of Longitude

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Longitude made good upon each ; then the whole  
Days Work being finish'd in the Log-Book, if the  
Latitude by Account agree with the Latitude by  
Observation, the Ship's Place will be truly deter-  
min'd ; if not, then the Reckoning must be cor-  
rected according to the preceding Rules, and plac'd  
in the Journal.

The Form of the Log-Book and Journal, toge-  
ther with an Example of 2 Days Work, you have  
here subjoin'd.

Note, To express the Days of the Week, they  
commonly use the Characters by which the Sun  
and Planets are express'd, viz. ☐ denotes Sunday,  
☽ Monday, ☉ Tuesday, ☂ Wednesday, ☄ Thursday,  
♀ Friday, and ☎ denotes Saturday.

T H E

*Correcting a Journal at SEA.* 313

The FORM of the  
**LOG-BOOK,**

With the Manner of working Days  
Works at *SEA.*

S f

The

## The Log-Book.

H.	K.	$\frac{1}{2}$ K.	Courses.	Winds.	Observations and Accidents. Day of —
1					Fair Weather, at
2				North	four this Afternoon
3					I took my Departure from the <i>Lizard</i> ,
4					in the Latitude of $50^{\circ}, 00'$
5	7		S $\frac{1}{2}$ S	N b E	North, it bearing
6	7				N N E, Distance
7	7	I			five Leagues.
8	7	I			
9	6				
10	6				
11	6		S S W	E b S	The Gale increas-
12	6	I			ing and being un-
1	6	I			der all our Sails.
2	6	I	S W b W	N N E	After three this
3	6	I			Morning, frequent
4	7				Showers with thick
5	7	I			Weather, till near
6	8				Noon.
7	8				
8	8		S W	E N E	The Variation I
9	8	I			reckon to be one
10	9				Point Westerly.
11	8	I	S W $\frac{1}{2}$ W	N E b E	
12	8				

## The Log-Book.

Courses Correct.	Dist.	Diff.		Lat.		Diff.		Long.	
		N	S	E	W	E	W	E	W
S S W	50		46 <sup>2</sup>					29.4	
S b W	19		18 <sup>5</sup>					5.5	
S W	49		20 <sup>7</sup>					45.5	
S W b S	24.5		2 <sup>2</sup>					20.0	
S W $\frac{1}{2}$ S	25.5		19 <sup>1</sup>					24.6	
				134				125.0	

Hence the Ship, by Account, has come to the Latitude of  $47^{\circ} 46'$  North, and has differ'd her Longitude  $2^{\circ} 5'$  westerly; so this Day I have made my Way good S  $51^{\circ} 31'$  W. Distance 157.4 Miles.

At Noon the *Lizard* bore from me N.  $51^{\circ} 31'$  E. Distance 157.4 Miles, and having observ'd the Latitude, I found it agreed with the Latitude by Account,

## The Log Book.

H.	K.	$\frac{1}{2}$ K.	Courses.	Winds.	Observations and Accidents &c Day of —————
1	2		S S W	W	This 24 Hours,
2	1	I	Hauled the Main		strong Gale of
3	1	I	and Fore Courses		Wind and Vari-
4	1	I	Lee-way 6 Points.		able.
5	I	I			
6	I				
7	I				
8	I	I	The Wind increa-		
9	I		ing, we try'd a		The Variation I
10	I		Hull, Lee-way 7		judge to be 1 Point
11	I		Points.		West.
12	I	I			
I	2		S W b W N W b W		
2	I	I	Set Main-sail Lee-		
3	I		way 4 $\frac{1}{2}$ Points.		
4	I				
5	I				
6	I	I			
7	I				
8	4		S b E S W b W		
9	4	I	Set Fore-sail, Lee-		Lat. by Observa-
10	4	I	way 3 Points.		tion, 47°, 06' N.
11	5				
12	4	I			

## The Log-Book.

Courses Correct.	Dist.	Diff.		Lat.		Diff.		Long.	
		N	S	E	W	E	W	E	W
S E b E	32.5		17.5	37.7					
E S E	6		2.5	10.6					
S $\frac{1}{2}$ E	9		8.9	1.3					
			20.0	49.6					

Hence the Ship, by Account, has come to the Latitude of  $47^{\circ} 17'$  North, and has differ'd her Longitude  $49'$  Easterly; consequently, she has got  $1^{\circ} 16'$  to the Westward of the *Lizard*, and has made her Way good the last 24 Hours, S.  $49^{\circ}, 08'$  E. Distance 44.3 Miles.

At Noon the *Lizard* bore from me North,  $17^{\circ}, 07'$  East, Distance 170.6 Miles.

This Day I had an Observation, and found the Latitude, by Account, to disagree with the Latitude by Observation by 11 Minutes, I being so much further to the Southward than by dead Reckoning, which by the third of the preceding Rules, I correct as in the *Journal*.

A JOUR-

A JOURNAL from the Lizard towards Jamaica, in the Ship  
Neptune, F.M. Commander.

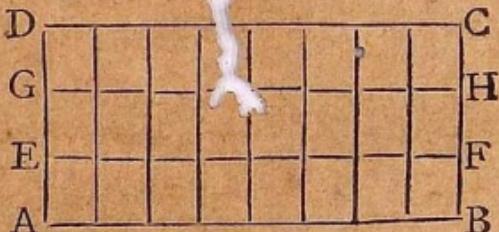
Week	Months	Days.	Winds.	Direct Course	Dift. Miles.	Latitude	Whole Diff.	Bearing and Drift	Remarkable Ob.
Years.						Correct.	Lat. from the Isd.	from the Isd.	Serv. & Accidents.
5			N b E	S 31, 31 W	157.4	47°, 46'	2°, 03' W	At Noon the	Fair Weather all
			E b S					Lizard bore	four P.M. I took
			N N E			N 31°	31 E.		my Depart. from
			E N E						the Island, it bear-
			N E b E						ing N N E Drift.
			West	S 34, 31 E	48.2	47°, 06'	1°, 35' W		5 Leagues.
			N W b W						
			S W b W						
5									Strong Gales
									of Wind and
									V. Variable.
									Dist. 18 3 Miles

## SECT. XV.

## Of MENSURATION.

*Def.* THE Area of any plane Surface in Inches, Feet, or any other Measure, is the Number of Square Inches, Feet, &c that the Surface contains.

i. Let ABCD represent a rectangular Parallelogram, and suppose the Side AB, or DC contains Six equal Parts, and the Side AD or BC three of the same Parts; then let the Line AB be moved along in the Direction of AD, till it has come to EF, where AE or FB (the Distance of it from its first Situation) may be equal to one of the equal Parts: Here 'tis evident, that the generated Parallelogram ABFE will contain as many Squares as the Side AB contains equal Parts (in this Case, six) each Square having for its Side one of the equal Parts, into which AB or AD is divided. Again, let AB move on till it comes to GH, so as GE or HF may be equal to AE or BF; then 'tis plain, that the Parallelogram AGHB will contain twice as many Squares as the Side AB contains equal Parts, each Square having one of the equal Parts, into which AB or AD is divided, for its Side; and by the same Way of Reasoning it will appear, that the Parallelogram ADCB will contain three times as many Squares as the Side AB contains equal Parts, and in general, that every rectangular Parallelogram contains



contains as many Squares, as the Product of the Number of equal Parts in the Base, multiply'd into the Number of the same equal Parts in the Height, contains Units, each Square having for its Side one of the equal Parts.

Hence arises the Solution of the following Problems.

### *Problem 1.*

To find the Area of a Rectangular Parallelogram.

*Rule.* Multiply the Base into the Perpendicular Height, and the Product is the Area requir'd.

### *Example.*

Suppose the Base AB (see the preceding Figure) of the Rectangular Parallelogram ABCD, is six Inches in Length; and the Perpendicular AD three Inches, requir'd the Area of that Parallelogram in Inches.

6 the Base AB,

3 the Perpendicular AD,

Product 18, the Area of the Parallelogram ABCD in Inches.

### *Problem 2.*

To find the Area of an Oblique-Angular Parallelogram.

*Rule.* Multiply the Base into the perpendicular Height, and the Product is the Area. The Reason of this Rule is evident from Art. 69. Sect. I.

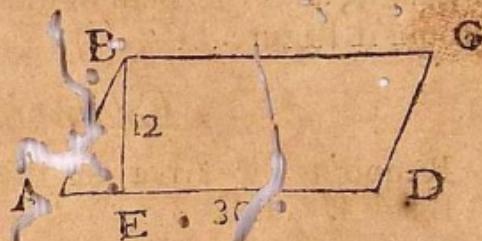
### *Example.*

*Example.*

Suppose the Base AD, of the Oblique-Angular Parallelogram ADCB is 30 Inches, and the Perpendicular BE,

12 Inches. Requir'd the Area in Inches.

Multiplying 30, the Base, into 12, the Perpendicular Height, the Product 360, is the Area or Number of square Inches contain'd in the propos'd Figure.

*Problem 3.*

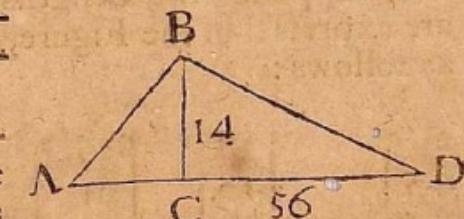
To find the Area of a Triangle:

*Rule.* Multiply the Base into half the Perpendicular Height, and the Product is the Area requir'd. The Reason of this Rule is plain from Cor. 3. Art. 68. Sect. I.

*Example.*

In the Triangle ABD, suppose the Base AD is 56 Feet, and the Perpendicular BC 14. Requir'd the Area.

The Base 56, multiply'd into  $\frac{1}{2}$ , half the Perpendicular, gives



392, the Area or square Feet contained in the given Triangle.

*Problem 4.*

To find the Area of any irregular Figure.

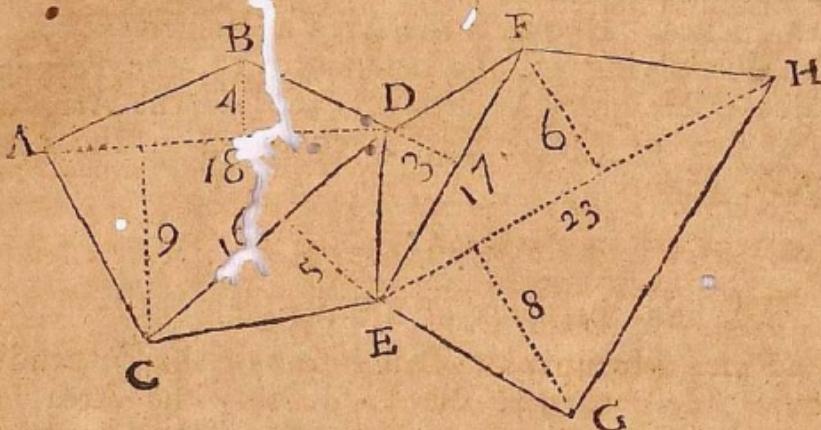
T t

*Rule.*

*Rule.* Reduce the Figure to Triangles by drawing Diagonals therein; then find the Area of each Triangle, and the Sum of these is the Area of the propos'd Figure.

*Example.*

Requir'd the Area of this Irregular Figure, A B D F H G E C.



Draw the Diagonals E H, E F, E D, D C and D A, which will divide the Figure into six Triangles, in each of which let fall from any one of its Angles a Perpendicular to the opposite Side; then supposing the Lengths of these to be, as they are express'd in the Figure, the Operation will stand as follows:

$\frac{2}{4.5}$	$\frac{18}{18}$	$\frac{36}{81}$	The Area of the	ABD
$\frac{2.5}{1.5}$	$\frac{16}{17}$	$\frac{40}{25.5}$	Triangle	ACD
$\frac{3}{4}$	$\frac{23}{23}$	$\frac{69}{92}$		CED
				EDF
				EFH
				EGH

343.5 the Area of the whole Figure.

*Problem*

## Problem 5.

To find the Area of any regular Polygon.

*Rule.* Thro' any three of the Angular Points draw a Circle (by *Pr<sup>b</sup>*, *Set<sup>t</sup>*. I.) which will pass thro' the rest also; then from the Center of this Circle let fall, upon any of the Sides, a Perpendicular, and half this Perpendicular multiply'd into the Sum of the Sides, will give the Area requir'd.

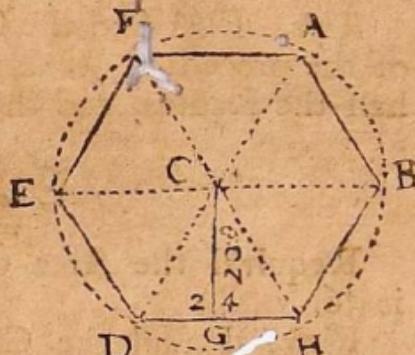
## Example.

Requir'd the Area of the Hexagon ABHDEF, the Center of whose circumscrib'd Circle is C, and the Perpendicular CG from the Center upon one of the Sides is 20.8, each Side of the Polygon being 24.

The Sum of the Sides is 144, which multiply'd by 10.4, half the Perpendicular, gives 1497.6, the Area of the propos'd Hexagon.

2. It has been found by Calculation, that if the Diameter of a Circle be 1, the Circumference of the same will be 3.1416 nearly; and consequently the Diameter of any Circle will be to its Circumference as 1 to 3.1416, & *e contra*.

*Cor.* 1. Hence, multiplying the Diameter of any Circle by 3.1416, the Product will be the Circumference. Thus, let the Diameter of a Circle be 36; then 36 multiply'd by 3.1416, will give 113.0976, the Circumference of the propos'd Circle.



## 324. Of MENSURATION.

*Cor. 2.* Hence, dividing the Circumference of a Circle by 3.1416, the Quotient will be the Diameter. So if the Circumference of a Circle be 75.3984 then this divided by 3.1416 will give 24 the Diameter of the propos'd Circle.

Now a Circle being a Polygon of an infinite Number of Sides, the Sum of all which is the Circumference, and the Perpendicular on any of them, the Radius; therefore

### Problem 6.

Given the Diameter of a Circle, to find its Area.

*Rule.* First find the Circumference (by the first of the preceding Corollaries) then multiply that by half the Radius, and the Product is the Area.

### Example.

Requir'd the Area of a Circle whose Diameter is 36.

First, I find the Circumference is 113.0976, which multiply'd by 9 half the Radius, gives 1017.8784 the Area requir'd.

### Problem 7.

The Circumference of a Circle given, to find its Area.

*Rule.* Find the Diameter by *Cor. 2*; then multiply the Circumference by half the Radius, and the Product is the Area.

### Example.

Requir'd the Area of a Circle, whose Circumference is 75.3984.

*First,*

*First,* I find the Diameter to be 14; then multiplying the Circumference 75.3984 by half the Radius, viz. 6, the Product 452.3904 is the Area requir'd.

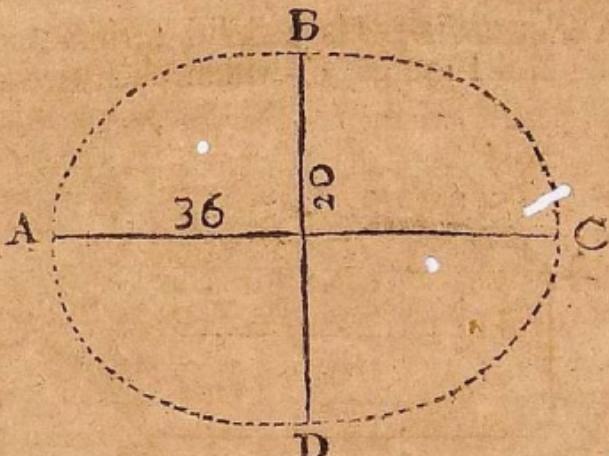
### Problem 8.

To find the Area of an Ellipse.

*Rule.* Multiply the greatest Diameter into the least, and the Product into .7854; this last Product is the Area.

### Example.

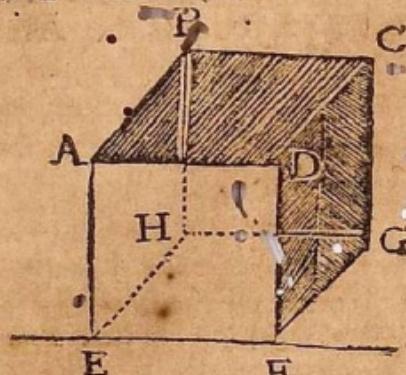
Suppose in the Ellipse ABCD the greatest Dia-



meter AC is 36, and the least Diameter BD 20. Requir'd the Area of that Ellipse.

Multiplying 36 into 20, the Product is 720, which multiply'd into .7854, gives 565.488 the Area of the propos'd Ellipse.

3. A Solid is that which has Length, Breadth, and Thickness.



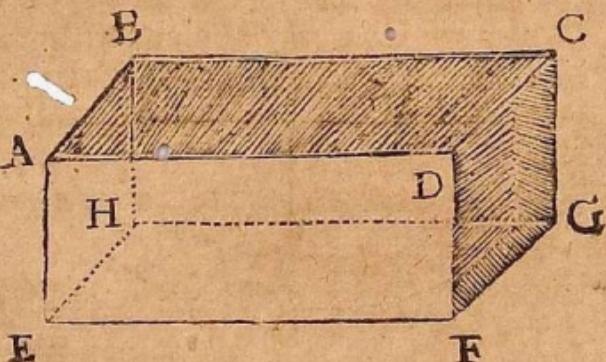
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4. A Cube is a Solid bounded by Six equal Squares. Thus the Solid ABCGFEDH, bounded by the Six equal Squares ABCD, CDFG, ADFE, ABHE, BCGH, and HGFE, is a Cube.

If the terminating Squares be square Inches, then the Solid is call'd a Cubic Inch; if square Feet, a Cubic Foot, &c.

5. The Solidity of any Body in Inches, Feet, &c. is the Number of Cubic Inches, Feet, &c. the Body contains.

6. A Parallelipiped is a Solid terminated by six Quadrilateral Figures, of which each two opposite



to one another are equal and parallel, as ABCG, FDHE.

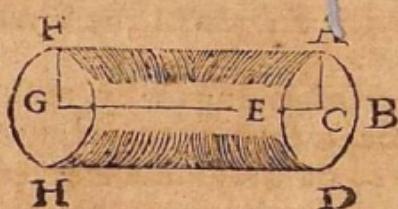
The Solidity of this Body is found by multiplying the Length, Breadth, and Thickness, into one another; and the Product is that requir'd.

*Example.* Suppose in the Parallelipiped ABCDFGHE, the Length EF is 36 Feet, the Breadth DF 16, and the Thickness FG 12; then these

these three multiply'd into one another will give 6912 for the Solidity, or Number of Cubic Feet the propos'd Body contains.

The Area of the Surface, or superficial Content of that Body, is found by taking the Sum of the Areas of the Quadrilateral Figures that terminate it.

7. If in a rectangular Parallelogram ACGF, one of the Sides GC remain fix'd, and the Paralle-

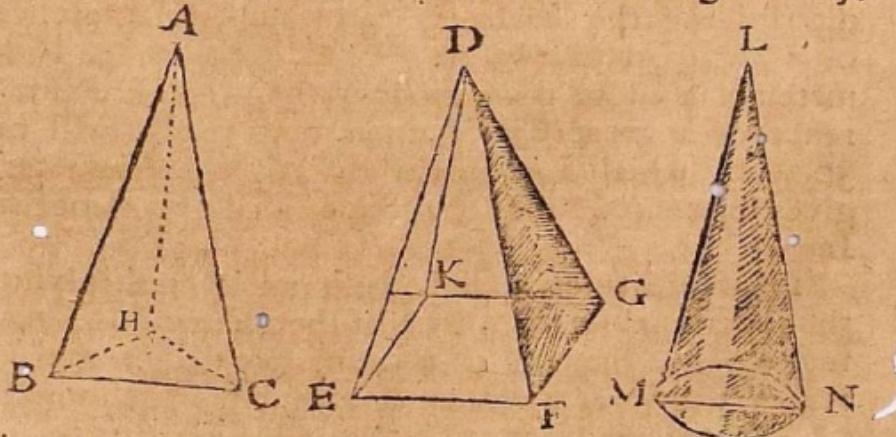


logram move quite round to its first Place; then the generated Solid ADHF is call'd a Cylinder.

The Solidity of this Body is found by multiplying the Area of one of its circular Bases into the Length. Thus let the Radius AC of one of the Bases of the Cylinder be 6 Inches, and the Length AF 36; then the Area of the Base ABDF will be 113.0976 (by Problem 6.) which multiply'd into the Length 36, gives 4071.5136 for the Solidity.

The superficial Content is found by multiplying the Circumference of one of the Bases into the Length, and to the Product adding the Areas of the two Bases.

8. Solids that decrease from the Base gradually,



till they come to a Point, are in general call'd Pyramids,

ramids, and are of different Kinds, according to the Figure of their Bases. Thus a *Pyramid*, having a *Triangular Base*, is called a *Triangular Pyramid*, as ABCH; and if the Base be a *Parallelogram*, it's call'd a *Paralllogrammic Pyramid*, as DEFGK, and if a *Circle*, it's call'd a *Circular Pyramid*, or simply a *Cone*; as LMN, &c. The Point in which the Pyramids ends, is call'd, the *Vertex*, and a Line drawn from the Vertex, perpendicular to the Base, is call'd, the *Height* of the *Pyramid*.

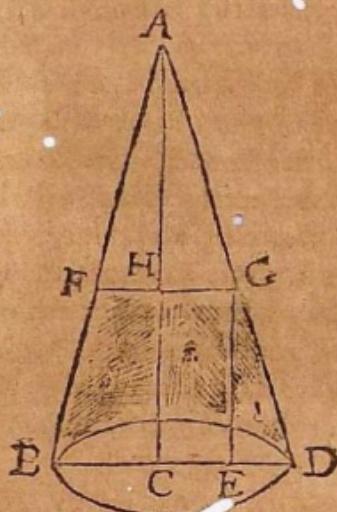
The Solidity of a *Pyramid* is found by multiplying the Area of the Base into  $\frac{1}{3}$  of the Height. Thus, suppose the Diameter of the Base of a *Cone* is 24 Inches, and the Height 51; then the Area of the Base will be 452.3904, which multiply'd by 17, the third Part of the Height, gives 7690.6368. The superficial Content of a *Cone* is found by multiplying the Circumference of the Base into half the Line joining the Vertex, and any Point in that Circumference, and to that Product adding the Area of the Base.

9. If a Semicircle be turn'd quite round upon its Diameter as an Axis, it will generate a Solid call'd a *Globe* or *Sphere*.

The Area of the Surface of a *Globe* is found by multiplying the Diameter into the Circumference of a great Circle upon it. Thus, suppose the Diameter of a *Globe* is 16 Inches; then the Circumference of a great Circle upon that *Globe* will be 50.2656, which multiply'd by 16, the Diameter, gives 804.2496 for the Superficial Content in Inches.

The Solidity of a *Globe* is found by multiplying the superficial Content by  $\frac{1}{3}$  of the Diameter. Thus, suppose the Diameter of a *Globe* is 18, then the Area of the Surface will be 1017.8784, which multiply'd by 3, gives 3053.6352 for the Solidity.

10. We have shewn how to find the Solidity of a Cone, having the Diameter of the Base, and the Height given, and thence we have a Method of finding the Solidity of a *Frustum* of a Cone, having the Diameter of the two Bases and the Height of the *Frustum* given. Let FBDG denote a *Frustum* of the Cone ABL; BD the greatest, and FG the least Diameter of the *Frustum*. Join the Vertex of the Cone A, and the Center of the Base C, with the Right Line AC, which will pass thro' H, the Center of the least Base of the *Frustum*; and thro' G draw GE parallel to AC, which will be equal to HC, the Height of the *Frustum*; then 'tis evident, that ED will be the Difference between the greatest and least Semidiameters of the *Frustum*; and since the Triangles ACD and GED are similar, therefore (by Art. 74. Sect. I.)  $DE : DC :: EG : CA$ , i. e. as the Difference between the greatest and least Semidiameters of the *Frustum*, is to the greatest Semidiameter, so is the Height of the *Frustum* to the Height of the whole Cone. Consequently, having the Diameter of the Base, and Height of the whole Cone, we can find its Solidity; and from AC, the Height of the whole Cone, taking CH, the Height of the *Frustum*, we have AH, the Height of the Cone cut off, with which, and the Base FG, which is given, we may find the Solidity of the Cone cut off, AFG. Consequently, from the Solidity of the whole Cone ABD, taking the Solidity of the small Cone AFG, there will remain the Solidity of the *Frustum* FBDG.



### 330 Of MENSURATION.

*Example.* Suppose the greatest Diameter of the Frustum of Cone is 20, and the least 12, and the Height 12, then the Difference between the two Semidiameters will be 4, and making it as 4 : 10 :: 12 : 30; we have 30 for the Height of the whole Cone, and from 30 taking 12, there remains 18, the Height of the least Cone; so the Solidity of the whole Cone is 3141.6, and the Solidity of the least Cone is 678.5856, the Difference of these is 2463.0144, which is the Solidity of the propos'd Frustum.

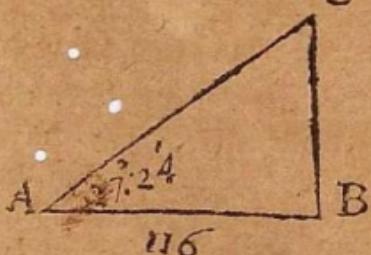
The Superficial Content of the Frustum of a Cone is found by adding to the Superficial Content of the whole Cone, twice the Area of the Base of the small Cone, and from that Sum taking the Superficial Content of the small Cone.

II. We have (in the preceding Part of this Book) shewn the Use of *Plane Trigonometry* in solving Problems of *Navigation*; and now we shall apply in the following Problems, to the Measuring the Heights of accessible and inacessible Objects.

#### Problem I.

To find the Height of any accessible Object.

Let BC be the Object to be observ'd, and from any Point A in the Level, upon which the Object



C stands, let the Angle of Altitude CAB be observed, and measure the Distance AB; then in the Right-Angled Triangle ABC are given the two oblique Angles A and C, and the Side AB, whence

to find BC it will be, by Case I. of Rectangular Trigonometry.

$$R:T, A::AB:BC.$$

*Example.*

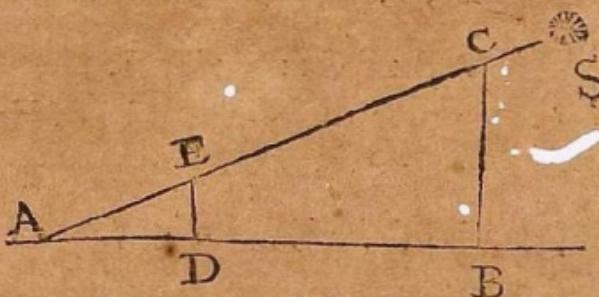
# Of MENSURATION. 331.

*Example.* Suppose the Angle of Altitude CAB is  $37^{\circ} 24'$ , and the Length AB 116. Then for BC it will be

As Radius - - - - - 10.00000  
 is to the Tang. of Altitude -  $37^{\circ} 24'$  - 9.88341  
 so is AB - - - - - 116 - - - 2.06446  
 to the Height of the Object BC 88.69 - 1.94787

*Note,* In taking the Height of any Object, if the Eye be not in the Level upon which the Object stands; then to or from the Height found, you must add or subtract the Distance of the Eye from the Level, according as it is placed above or below it, and the Sum, or Difference, is the true Height of the Object.

The Height of an accessible Object may also be found by Means of its Shadow. Thus, suppose CB is the Object, and BA its Shadow, caus'd by

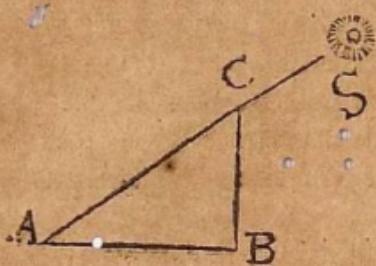


the Sun at S, and let DE be a Stick of a known Length, plac'd perpendicular to the Line of the Shadow, and in some Point of it D, so as the Extremity of the Shadows of the Object and Stick may coincide at A. Measure AD and AB, the Lengths of the Shadows; and then, since ED and CB are both perpendicular to AB, it will be; as AD, the Stick's Shadow, is to DE, the Length of the Stick, so is AB, the Object's Shadow, to CB the Height of the Object.

## Problem 2.

To find the Altitude of the Sun by the Length of the Shadow of an accessible Object, whose Measure is also known.

Let CB represent a Stick, or any other accessible Object of a known Length, standing perpendicular to the Horizontal Plane A B, and let A B be



its Shadow made by the Sun at S. Measure, the Length of the Shadow AB, and then in the Right-Angled Triangle A B C are given the two Sides

A B and B C, whence to find the Angle CAB, or the Altitude of the Sun at the Time of Observation, it will be, by Case 4th of Rectangular Trigonometry,

$$AB : BC :: R : T, A.$$

*Example.* Suppose the Stick BC is 4 Feet, and the Shadow of it AB 5, then for the Sun's Altitude it will be

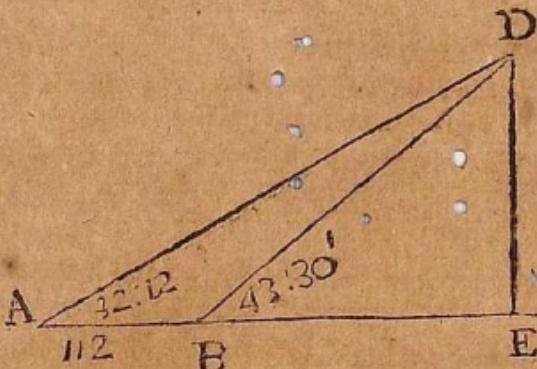
As the Length of the Shadow - 5 - 0.69897  
is to the Length of the Stick - 4 - 0.60206  
so is Radius - - - - - 10.00000  
to the Tang. of the Sun's Altitude  $38^{\circ} 39' 9.90309$

## Problem 3.

To find the Height and Distance of an inaccessible Object.

Let DE represent an inaccessible Object, and B a Point in the Horizontal Plane on which it stands, and from whence we can observe the Angle of Altitude DB E. At any other Point in the same Plane, as A, observe the Angle of Altitude D A E, and measure

measure the Length of AB, the Distance between the two Stations A and B; then in the Triangle



ABD, having the external Angle DBE, together with the internal opposite one A, we have the Angle ADB (by Art 60. Sect. 1.) and also the Side AB; whence for BD, the Hypotenuse of the Right-angled Triangle DBE, it will be, by Case 2. of Oblique-angled Trigonometry,

$$S, ADB : AB :: S, A : BD.$$

Then in the Right-angled Triangle BDE are given the Hypotenuse BD and the Oblique Angles; whence for DE, the Height of the Object, it will be, by Case 3d of Rectangular Trigonometry,

$$R : S, DBE :: BD : DE.$$

And for BE, the Distance of the Object from the nearest Situation, it will be, by the same,

$$R : S, BDE :: BD : BE.$$

*Example.* Suppose the Angle of Altitude at B is  $43^\circ, 30'$ , and at A  $32^\circ, 12'$ , and the Distance AB between the two Stations is 112 Feet; then the Angle ADB will be  $11^\circ, 18'$ , and the Angle BDE will be  $46^\circ, 30'$ . Hence for BD it will be -

As the Sine of ADB -	$11^\circ, 18'$	-	9.29214
is to AB - - - - -	112	- - - - -	2.04922
so is the Sine of A - -	$32^\circ, 12'$	-	9.72663
to BD - - - - -	304.6	- - - - -	2.48371

Then

Then for D F, the Height of the Object, it will be,

As Radius - - - - -	10.00000
is to the Sine of DBE - -	43°, 30' - 9.83781
so is BD - - - - -	304.6 - - 2.48371
to DE - - - - -	209.7 - - 2.32152

Lastly, For BE, the Distance of the Object from the nearest Station, it will be,

As Radius - - - - -	10.00000
is to the Sine of BDE - -	46°, 30' - 9.86056
so is BD - - - - -	304.6 - - 2.48371
to BE - - - - -	221 - - 2.34427

If the Object stands upon a Rising Ground, then find the Height of the Object above the Plane on which you stand (*by the last Problem*) as also the Height of some Point on the Rising Ground near the Foot of the Object, and this last Height taken from the former, will give the true Height of the Object.

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## S E C T. XVI.

### Of SURVEYING.

1. THE Instruments chiefly in Use for taking Angles in the Field are, the *Plane-Table*, *Theodolite*, *Compass*, *Semicircle*, &c. The Nature and Use of which is much easier obtain'd by viewing the Instruments themselves, than by a Description of them, from their Draughts upon Paper.

2. To measure Distances upon the Field, they commonly use Mr. Gunter's Chain, which contains 22 Yards in Length, the fourth Part of which is  $5\frac{1}{2}$  Yards, or \*  $16\frac{1}{2}$  Feet, is call'd a *Perch* or *Pole*; confe-

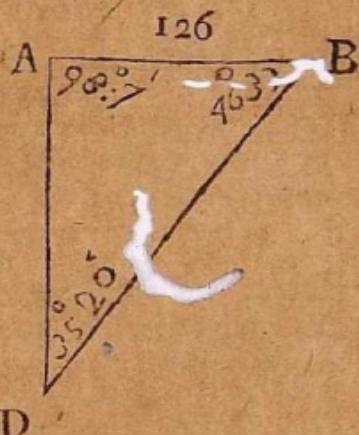
\* But in Ireland there are 21 Feet to a Perch, *Plantation Measure*.

consequently a Square Chain contains 16 Square Poles; and since an Acre contains 16 Square Chains, therefore 160 Square Poles is equal to one Acre. This Chain is commonly divided into 100 equal Parts, called *Links*, and is sometimes mark'd at every 10 Links, for the Conveniency of working by Decimals.

*Problem I.*

To find the Distance of any Object from a given Point.

Let the Object be D, and the given Point A; then let the Distance between A and any other Point B (from whence we can see the Object) be measur'd, and with a Semicircle, or any other proper Instrument, take the Angles  $DAB$  and  $ABD$ ; then in the Triangles  $ABD$  are given the Angles and the Side  $AB$ , whence to find the Side  $AD$  it will be, by *Cafe 2d of Oblique Angled Trigonometry*,



$$S, D : AB :: S, B : AD.$$

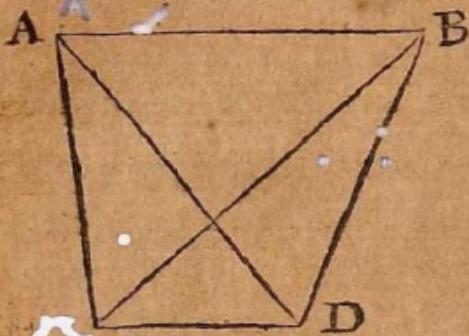
*Example.* Suppose BA is 126 Feet; the Angle A  $98^{\circ}, 7'$ , the Angle B  $46^{\circ}, 33'$ , and consequently the Angle D  $35^{\circ}, 20'$ ; then for AD it will be

As the Sine of D - - -  $35^{\circ}, 20'$  - 9.76218  
is to the Distance AB - - - 126 - - - 2.10037  
so is the Sine of B - - -  $46^{\circ}, 33'$  - 9.86392  
to the Dist. between A and D 158.2 - - - 2.1911

## Problem 2.

To find the Distance between two inaccessible Objects.

Let the two Objects be A and B, to which we cannot approach, being hinder'd by a River, &c.



assume in some convenient Place two Points C and D, from each of which you can see the two Objects; and measure the Distance between them; then at the Point C observe

serve the Angles ACD and DCB, and at D observe the Angles CDB and CDA; so in the Triangle CDB are given the two Angles BCD and CDB (and consequently the Angle CBD) and the Side CD; whence to find CB it will be S, CBD : S, CDB :: CD : CB. Again, in the Triangle ACD are given the two Angles ACD and ADC (and consequently the Angle CAD) and the Side CD; whence to find AC it will be S, CAD : S, CDA :: CD : CA. Lastly, from the Angle ACD take the Angle DCB, and there will remain the Angle ACB; then in the Triangle ACB are given the two Sides AC and CB, and the included Angle ACB; whence AB, the Distance between the two Objects, is found by Case 5th of Oblique Trigonometry.

Example.

# Of SURVEYING. 337

*Example.* Suppose the Angle ACD is  $94^\circ, 55'$ , the Angle BCD  $41^\circ, 25'$ , the Angle CDB  $103^\circ$ , the Angle ADC  $46^\circ, 44'$ , and the Side CD 144 Feet: Then 1st, for CB it will be

As the Sine of CBD =  $35^\circ, 21' \approx 9.76236$   
 is to the Sine of CDB =  $103, 14 \approx 9.98831$   
 so is CD - - - - - 144 - - - - - 2.15836  
 to CB - - - - - 242.3 - - - - - 2.98431

2dly, For CA it will be

As the Sine of CAD =  $38^\circ, 21' \approx 9.79256$   
 is to the Sine of CDA =  $46, 44 \approx 9.86223$   
 so is CD - - - - - 144 - - - - - 2.15836  
 to CA - - - - - 169.1 - - - - - 2.22803

Lastly, For AB it will be

As the Sum of the Sides  
 AC and CB - - - - - 411.4 - - - - - 2.61426  
 is to their Difference - - - 73.2 - - - - - 0.90451  
 so is the Tang: of  $\frac{1}{2}$  the Sum  
 of the Ang. CAB and CBA - - -  $63^\circ, 15' \approx 10.29753$   
 to the Tang. of  $\frac{1}{2}$  their Diff. 19, 25 - - - - - 9.54778

Then,

As the Sine of CBA =  $43^\circ, 49 \approx 9.84033$   
 is to the Sine of ACB =  $53, 30 \approx 9.90518$   
 so is AC - - - - - 169.1 - - - - - 2.22803  
 to AB - - - - - 196.3 - - - - - 2.29288

Consequently the Distance between the two Objects A and B is 196.3 Feet:

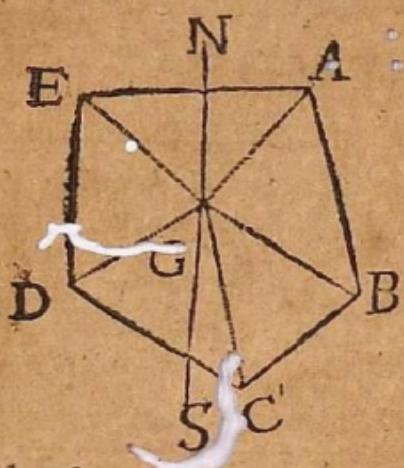
## Problem 3.

To take the Plot of a Field at one Station, in or near the Middle of it; when we can from thence see all the Angles or Corners of the Field.

This may either be done by the *Plane-Table* or *Theodolite*, or any of the other Instruments above-mentioned.

Let ABCDE represent the Field; and first suppose you are to plot it with the *Plane-Table*. Having planted the Table with a Sheet of white Paper, fix'd upon it, in or near the Middle of the Field, as at G; mark a Point upon the Paper to represent the Point of the Field on which the Table stands; and laying the Edge of your Index upon that Point, and keeping it there, turn it about so as you can, thro' the Sights, see one of the Angles, as A; then from the Point, along the Edge of the

Index, draw the Line GA, and measuring the distance on the Field from the *Plane-Table* to the Angle at A in Chains and Links, take it from any convenient Line of equal Parts, and set it off upon the Paper, from G to A, along the Line GA; then (keeping the Table still fix'd as it was) turn the Index so as it lying with its Edge upon the Point G, you may, thro' the Sights, see the Angle B; and drawing the Line GB, measure the Distance GB in the Field, which set off upon the Table from G to B; after the same Manner, drawing the Lines GC, GD and GE, and joining the Extremities of them with the Right-Lines AB, BC, CD, DE and EA, the Field is protracted, and the Lines BA, AE, &c. taken from the Scale from which you protracted the rest, will give the Lengths of them in the Field.



To perform the same with the *Theodolite*, place the Instrument in, or near, the Middle of the Field, as at G, and so as the Needle may hang directly over

over the Meridian Line of the Chart, which let NS represent; then direct your Sights from G to the Angle A, and observe the Number of Degrees it cuts, or the Bearing of A, which suppose to be N  $16^{\circ}$ ,  $24'$  E, and place this in the Field-Book, together with the Distance in Chains and Links from C to A, and proceeding the same Way with the rest of the Angles, you'll have the Bearing of each Angle from the Meridian, together with the Distance of each from the Instrument, in your Field-Book, the Form of which follows.

### *The FIELD-BOOK.*

Angles.	Bearings.	Chains.	Links.	Remarks.
A	N $16$ , $24$ E	7	20	
B	S $73$ , $35$ E	7	60	
C	S $19$ , $15$ E	7	65	
D	S $54$ , $56$ W	6	6	
E	N $59$ , $40$ W	7	26	

The Table is rul'd into five Columns; in the first are mark'd down the Angles express'd by Letters, or any other Characters at Pleasure; the second contains the Bearings of these Angles from the Meridian; the third and fourth their Distances in Chains and Links from the Place of Observation, and the fifth is for any remarkable Occurrence.

Having mark'd down the Bearings of all the Angles in the Field from the Meridian, together with their Distances in Chains from the Place of Observation in your Field-Book, you may afterwards protract it upon Paper in the following Manner, viz. Assume any convenient Point in the Paper to represent the Place of Observation, and thro'

it draw a Line representing the Meridian; then from that Point draw Lines, making Angles with the Meridian, as in the Field-Book, and from the said Point upon these Lines the several Distances express'd in the Field-Book, taken from any Scale of equal Parts; Lastly, joining the Extremities of them with Right-Lines, the Field will be præcised; and the Area of it in Chains may be found by Prob. 4. Sect. 15. which divided by 10, will give the Area in Acres.

The Method of plotting a Field by the *Semicircle*, *Circumferentor*, &c. differs so little from the Way of doing the same by the *Theodolite*, that it would be altogether needless to shew it in each of them. When the Angles of the Field are at such a Distance from you, that you can't perfectly perceive them from your Station, then put Marks of white Paper, or Pieces of Linnen at each of them, so as you may easily see them.

If it be more convenient to plot the Field at one Station, in or near some Corner of the Field; then you are to do it the same Way by the *Plane-Table*, *Theodolite*, or any other of the Instruments, as when your Station was in or near the Middle of the Field.

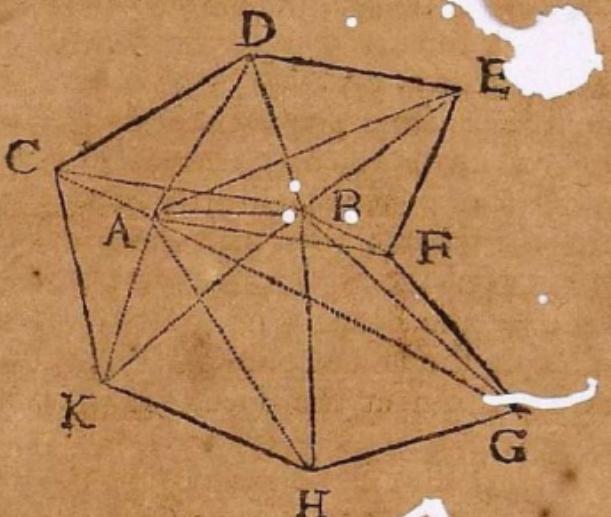
### Problem 4.

To plot a Field at two Stations near the Middle thereof, the Distance between which Stations is known, and from each of which all the Angles in the Field can be easily seen.

Let the Field to be plotted be CDEFGHK, in which chuse two convenient Points A and B near the Middle, from each of which you can perceive all the Angles, and the Distance between which you know; then if you are to plot it by the *Plane-Table*, plant the Table upon the Point A, and mark

a cer-

a certain Point upon the Table to represent it, upon which lay the Edge of the Index, and direct the Sights to the other Station B, and by the Side of the Index draw A.B; then from A, along that Line, set off a Line A.B, taken from any convenient Scale of equal Parts, equal to the Distance between your two Stations; then laying the Edge of



your Index upon the Point A, and directing your Sights to D, draw the Line A.D; the same Way keeping the Edge of the Index on A, direct the Sights to all the other Angles of the Field successively, and draw the Lines A.E, A.F, &c. then remove the Table to the other Station B, and laying the Edge of the Index along the Line A.B, turn the Table about till you can, thro' the Sights, see the other Station A, and fixing the Table. lay the Edge of the Index on B, and direct the Sights to D, and draw the Line B.D, which will intersect A.D in D; the same Way keeping the Edge of the Index still on the Point B, direct the Sights to all the other Angles of the Field, and draw the Lines B.E, B.F, &c. which will intersect the former Lines drawn from A in the Points E, F, G, &c. and joining these Points with Right Lines, you'll have

have the Plot of the Field, and the Lines D E, E F, &c. taken from the same Scale of equal Parts that A B was taken from, will give the Distances of the Angles in the Field from one another. *Lastly,* The Area of the Field being thus protracted, may be found by *Prop. 4. of the last Section.*

In plotting of a Field at two Stations, you ought to take the Stations as far asunder as conveniently you can; or the nearer they are together, the more Danger there is of contracting an Error, & *e contra.*

To plot the same by the Theodolite; having fix'd the Instrument in one of the Stations as A, turn it about till the Needle be directly over the Meridian Line of the Chart; then turn about the Index till you can, thro' the Sights, see the other Station B, and observe the Bearing of it from the Meridian, and measure the Distance in Chains and Links, both which set down at the Head of the Field-Book. Thus,

A B — S 7° 23', E — 3 Chains, 24 Links.

Then turn the Index to the Angle D, and observe its Bearing from the Meridian, and the same Way, turning the Index to all the Angles of the Field, observe the Bearing of each of them, which set down in the Field-Book in the second Column, mark'd at the Top thus, *Station A.* Then go to the Station B, and fixing your Instrument as before, turn the Sights to the Angle D, and observe the Bearing of it from the Meridian; and the same Way, turning the Sights to the rest of the Angles, observe the Bearing of each of them, which mark down in another Column of your Field-Book, mark'd at the Top with *Station B,* and your Work in the Field is finish'd; the plotting of which upon Paper is so plain and easy, that it needs no Example.

By

By this Method the principal Places in a Survey of a County, or any large Piece of Ground, may be placed in a Map, *viz.* By making Choice of two Eminences for your two Stations, the Distance between which you can measure, and from each of which you can see all the principal Objects, such as *Churches, Castles, Hills, Gentlemen's Seats,* and whatever else is remarkable in the Ground you are Surveying.

If all the Angles in the Field can't be seen at two Stations, then make Choice of a third, from whence you can see any of the former two, and the Distance between which you can measure; and if that be not sufficient, then use a 4th, 5th, &c. Station; by which Means you'll always have two Stations to proceed with thro' the Country you are to Survey, be it ever so large; and even in a Field, where you can take the Survey of it at two Stations alone; the chusing a third Station, from whence you can see one of the former ones, and also all the Angles of the Field, and thence taking the Plot of it, as before, is a sure Way of proving your former Work.

### Problem 5.

To plot a Field by going round it.

Let the Field be ABCDEFA, and suppose you are to plot it by the *Plane-Table.* Having fix'd your Instrument at any of the Angles of the Field, as A, mark a Point upon the Paper to represent it; then laying the Edge of the Index upon A, turn it about, till through the Sights you can see the adjacent Angle F, and along the Edge of the Index draw the Line AF, which measure in the Field, and taking that from any Scale of equal Parts, set it off upon the Line AF on the Table.

Table from A to F, then move your Table from A to F in the Field, and laying the Edge of the

Index on F, turn it about till, thro' the Sights, you can see E, and draw the Line F E, which measure in the Field, and taking it from the same Scale, set it off upon the Table from F to E: After the same Manner, proceeding with the

rest of the Angles, you'll have the Plot of the Field.

To plot the same by the Theodolite. Having placed ~~your~~ Instrument at the Corner of the Field, you are to begin from, as at A, set the Index at 00 Deg. 00 Min. then turn the Instrument about with that End of the Index forward (or towards F) that lies upon 00 Deg. 00 Min. till you can, thro' the Sights, see the Angle F; and there fixing the Instrument, turn the Index about till you can, through the Sights, see the Corner B, and mark the Degrees (in your Field-Book) cut by the Index, which will be the Measure of the Angle FAB, and measure AF in Chains and Links, which also mark down in your Field-Book; then remove your Instrument to F, and placing the Index upon the Beginning of the Degrees, as before, turn the Instrument about till you can, thro' the Sights, see the Corner A, and fixing the Instrument there, turn the Index about till you see, thro' the Sights, the Corner E, and mark the Degrees cut by the Index in your Field-Book, which will be the Angle AFE, then measure FE in Chains and Links, which also mark down in your Field-Book: the same



same Way, proceeding with the rest of the Angles, mark down the Quantity of each, together with the Distance from the preceding, in your Field-Book; and thence you may project it at Leisure upon Paper.

This Method of plotting a Field by going round it, is much less liable to Error than any of the two former; and is more especially useful in measuring large Fields, or Fields upon which are Woods, or other Things to obstruct the Sight, in which Case the other Methods are impracticable.

## S E C T. XVII.

*Of GAGING.*

I. WE have shewn in Section 1. how to find the Solidity of several Sorts of Bodies, in Inches or Feet, &c. which Solidity (if taken in Inches) divided by the Inches contain'd in a Gallon, Bushel, &c. will shew the Number of Gallons, Bushels, &c. contain'd in the Vessel.

The Number of solid Inches contain'd in a Gallon, Bushel, &c. as determin'd by Act of Parliament, are as follows;

A Gallon of	$\left\{ \begin{array}{l} \text{Ale or Beer} \\ \text{Wine} \\ \text{Corn} \end{array} \right\}$	contains	$\left\{ \begin{array}{l} 281. \\ 231. \\ 268.8 \end{array} \right\}$	Solid Inches.
A Bushel of	$\left\{ \begin{array}{l} \text{Malt} \\ \text{Coals} \end{array} \right\}$		$\left\{ \begin{array}{l} 2150.4 \\ 2246. \end{array} \right\}$	
A Scots Pint	—		102.3	
An Irish Gallon	—		217.6	

2. In *Gaging*. The Vessels that are not Cylindrical are commonly reduc'd to Cylinders, and their Solidities found as such;

A Cask having different Diameters at the Head and Bung, is reduc'd to a Cylinder, by taking the mean or equated Diameter between the two, for the Diameter of the Cylinder, equal in Length and Solidity to the propos'd Cask; the common Method for finding the equated Diameter, and which serves pretty justly in most Casks, is this, *viz.* Multiply the Difference between the Head and Bung Diameters by .65, and adding the Product to the Head Diameter, the Sum will be the Diameter of a Cylinder of equal Length and Solidity with the Cask.

Hence we have the following Rule for finding the Content of any Cask in *Wine, Beer, &c.* The Head and Bung Diameter, and Length of the Cask being given in Inches, *viz.* Find the equated Diameter between the Head and Bung Diameters of the Cask, and thence find the Area of the Circle belonging to that Diameter; then multiply this Area by the Length of the Cask, and the Product will be the Solidity of the Cask in Inches, which divided by the solid Inches contain'd in a Gallon of Wine, Beer, &c. will give the Content of the Cask in Wine, Beer, &c.

### Example.

Let it be requir'd to find the Content of the Cask AEDB in Wine Gallons, whose Head Diameter AE or BD, is 26 Inches, the Bung Diameter FC 34 Inches, and the Length GH 55 Inches.

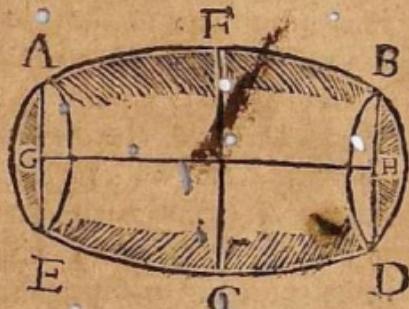
The Difference between the Head and Bung Diameters is 8, which multipliy'd by .65, gives 5.2 and this added to 26, the Head Diameter, makes

31.2. for the equated Diameter, or Diameter of the Cylinder equal in Length and Solidity with the propos'd Cask, the Area of whose Base is 764.539776, which multiply'd into 55 the Length, gives 42049.68768 for the Solidity in Inches; and this divided by 231 the solid Inches contain'd in a Gallon of Wine, gives 182.03328 for the Content of the propos'd Cask in Wine-Gallons,

3. If the propos'd Cask be standing with its Axis perpendicular to the Horizon, and is not quite full of Liquor; then, in order to find the Contents of the contain'd Liquor, you must find the equated Diameter, as above, and thence the Area of the Base of the Cylinder, the Cask is reduced to; which multiply'd into the Depth of the Liquor, will give the solid Content of the contain'd Liquor in Inches, and this divided by the Inches in a Gallon of Wine, Beer, &c. according to the Liquor contain'd, will give the Contents of the Liquor in the Cask.

This Rule more especially serves when the Cask is more than half full of Liquor; but when it is less than half full; then the Content of the contain'd Liquor is better found by subtracting the Content of the empty Part of the Cask (found as above) from the Content of the whole. and the Remainder will be the Content of the contain'd Liquor.

4. In Gaging, by the Area of any Surface in Wine, &c. Gallons is meant the Content of it at one Inch Depth. Consequently the Area of a Circle, 1 Inch Diameter, being .7854, this divided by



282 will give .002785, for the Content of that Circle, 1 Inch Depth in Ale or Beer Gallons, and the same divided by 231 will give .0034 for its Content in Wine Gallons; and since Circles are to one another as the Squares of their Diameters; therefore, as 1, the Square of 1 Diameter, is to .0034, or 002785, the Area of that Circle in Wine or Ale-Gallons, so is the Square of the Diameter of any other Circle, to the Area of that Circle in Wine or Ale-Gallons; hence, since the first Term of the Proportion is Unity, it follows, that the Area of any Circle, in Wine or Ale-Gallons, is found by multiplying the Square of the Diameter by .0034 for Wine-Gallons, and by .002785 for Ale-Gallons; and this Area, multiply'd into the Length of the Cask to which the Circle belongs, will give the Content of the Cask in Wine or Ale-Gallons; and hence the two Numbers .0034 and .002785 are called *Fix'd Multipliers*.

Again, If 1 be divided by the former Numbers .0034 and .002785, there will be produc'd their Reciprocals 294.12 and 359, with the first of which, dividing the Square of the Diameter of any Circle, the Quotient will be the Area of that Circle in Wine-Gallons; and if the same be divided by the last, the Quotient will be the Area of that Circle in Ale-Gallons; hence these two Numbers 294.12 and 359 are called *Fix'd Divisors*, and in *Practice*, are commonly made use of by the Gagers.

5. When a Cask is lying upon its Side, with the Axis parallel to the *Horizon*, and is not full; but the Surface of the contain'd Liquors cuts the Heads of the Cask; then to find the Content of the Liquor contain'd in the Cask, we must first know how to find the Area of any Segment of a given Circle. In order to which,

Let AEBH represent a Circle, whose Diameter AB is 2; then (by Cor. 1. Art. 2. Sect. 15.) the Circumference

circumference of that Circle will be 6.2832, and the Area 3.1416 (by Prob. 6. Sect. 15.) Hence 'tis evident, that if the Diameter of a Circle be two Inches or Feet, &c. the Circumference of that Circle will contain twice as many Inches or Feet, &c. in Length, as the Area of it contains square Inches or Feet, &c. i. e. the Length of the Circumference is double the Area; and since the Area of the whole Circle, is to the Area of any Sector of it, as the Length of the whole Circumference, to the

Length of the Arch of that Sector: it follows, that the Length of half the Arch of any Sector of a Circle, whose Diameter is 2, is equal to the Area of that Sector. So in the annexed Scheme the Length of D E, half the Arch of the Sector D C F E, will be the Area of that Sector.

In the annex'd Scheme, suppose G E (the versed Sine of half the Arch of the Sector D C F E) to be equal to .4; then, since the Radius C E is 1, 'tis evident C G (the Right Sine of D A, the Complement of D E half the Arch of the Sector) will be equal to .6; so making it as 1 is to .6, or (to avoid Fractions) as 100 is to 60, so is the Radius of the Tables to a fourth Number; this will be the Sine of A D, and looking in the Table we shall find it answer to 36.87 Degrees; the Complement of which, viz. 53.13 Degrees is the Arch D E; which multiply'd by .017453 the  $\frac{1}{50}$  of 6.2832, gives .92727789 for the Length of the Arch D E, which is equal to the Area of the Sector D E F C.

Again, In the Right-Angled Triangle C G D, 'tis evident, (by Cor. 1. Art. 70. Sect. 1.) if from 1, the Square of C D, we take .36, the Square of C G, there will remain .64, the Square of D G, the Square Root



Root of which, *viz.* .8 is equal to DG, and this doubled gives 1.6 equal to DF, which multiply'd into .3, the half CG produces .48 for the Area of the Triangle DCF. Then, from .92727789 for the Area of the Sector DCFE taking .48 the Area of the Triangle DCF, there will remain .44727789 for the Area of the Segment DEF D, and this taken from 3.1416, the Area of the whole Circle, there will remain 2.69432211 for the Area of the other Segment DHFD, whose versed Sine is 1.6.

After the same Manner, by dividing the Diameter of the Circle, *viz.* 2, into 100, or any other Number of equal Parts, we may find the Area of the Segment answering to each versed Sine.

Having by the foregoing Method found the Area of a Segment belonging to any versed Sine in that Circle whose Diameter is 2, and Area 3.1416; we may find the Area of the similar Segment in any other Circle by the following Analogy, *viz.*

As the Area of that Circle, whose Diameter is 2, *viz.* 3.1416, is to the Segment belonging to any Part of its Diameter, so is the Area of any other Circle, to the Segment belonging to the like Part of its Diameter.

And hence arises the Construction of the following Table,

A TABLE of the Segments of a Circle, whose Area is  $\pi$  the Diameter, (viz. 1.128378) being divided into 100 equal Parts.

V.	Segm.	V.	Segm.	V.	Segm.	V.	Segm.	V.	Segm.
I	.0017	21	.1526	41	.3860	61	.5389	81	.8677
2	.0048	22	.1631	42	.3986	62	.5514	82	.8776
3	.0087	23	.1738	43	.4112	63	.6636	83	.8873
4	.0134	24	.1845	44	.4238	64	.6759	84	.8968
5	.0187	25	.1955	45	.4365	65	.6881	85	.9059
6	.0245	26	.2066	46	.4491	66	.7002	86	.9149
7	.0308	27	.2178	47	.4618	67	.7122	87	.9236
8	.0375	28	.2292	48	.4745	68	.7241	88	.9320
9	.0446	29	.2407	49	.4873	69	.7360	89	.9402
10	.0520	30	.2523	50	.5000	70	.7477	90	.9480
II	.0598	31	.2640	51	.5127	71	.7593	91	.9554
12	.0680	32	.2759	52	.5255	72	.7708	92	.9625
13	.0764	33	.2878	53	.5382	73	.7822	93	.9692
14	.0851	34	.2998	54	.5509	74	.7934	94	.9755
15	.0941	35	.3119	55	.5635	75	.8045	95	.9813
16	.1032	36	.3241	56	.5762	76	.8155	96	.9866
17	.1127	37	.3364	57	.5888	77	.8262	97	.9913
18	.1224	38	.3486	58	.6014	78	.8369	98	.9952
19	.1323	39	.3611	59	.6140	79	.8474	99	.9983
20	.1424	40	.3735	60	.6265	80	.8576	100	1.0000

In this Table you may observe, that the Columns mark'd at the Top with V., contain the versed Sines, proceeding from 1 to 100, and the adjacent Columns contain the Areas of the Segments belonging to these versed Sines.

By this Table the Content of the Liquor contain'd in a Cask, not full, lying with its Axis parallel to the Horizon, and the contain'd Liquor cutting the Heads of the Cask, may be found after the following Manner, viz.

To the wet Inches of the Bung-Diameter add a competent Number of Cyphers, and divide this by the

the whole Diameter, then seek for the Quotient in the Columns mark'd V, at the Top in the preceding Table, and opposite to this, in the adjacent Column, you'll find the Area of a Segment, which multiply into the whole Content of the Cask, and the Product is the Content of the Liquor in the Cask. If instead of the wet Inches we had us'd the dry, then the last Product would have been the Content of the empty Part of the Cask, which is call'd the *Ullage*.

### Example.

Suppose a Cask lying with its Axis parallel to the Horizon, has a certain Quantity of Wine in it, the Bung-Diameter is 32 Inches, the Head-Diameter 28, the Length 48, and the wet Inches 20. Requir'd the Content of the Liquor.

To the wet Inches 20 I add a Number of Cyphers, and dividing it by 32, I find the Quotient 66, which I look for in the Table, and find it answer to the Segment .7002, which multiply'd by 152.8, the whole Content of the Cask in Wine-Gallons (found by Art. 2. of this Sect.) gives 107 for the Content of the Liquor in the Cask, in Wine Gallons.

6. Malt, when lying on a Floor, is gaged by taking the Depth of it in Inches, in several Places, and dividing the Sum of these Depths by the Number of them, the Quotient will be the mean Depth; which multiply'd into the Area of the Surface, gives the Solidity in Inches; and this divided by 2150.4 gives the Content in Bushels.

7. Solid Timber is measur'd by the solid Foot, each containing 1728 solid Inches, the common Way is this, viz. Girth the Tree in several Places, and take  $\frac{1}{4}$  of the mean Girth in Inches, for the Side of a Square; which Square multiply into the Length

Length of the Tree, and the Product will be the Solidity in Inches, and this divided by 1728, will give the Solidity of the Tree in Feet.

8. The Solidity of irregular Bodies may be found exactly, after the following Method, *viz.* Let the Body be immers'd in Water in a Parallelipiped, whose Sides are exactly divided into Inches, and the Solidity of the Water rais'd, will be equal to the Solidity of the immers'd Body.

9. The common Rule for finding the Tunnage of a Ship, is as follows.

Multiply the Length of the Keel by the Breadth, and the Product by half the Breadth; then divide this last Product by 95, and the Quotient will give the Tunnage.

### Example.

Suppose a Ship's Keel is 135 Feet, and her Breadth from out to out, 48 Feet. Requir'd the Tunnage of that Ship.

The Length of the Keel, *viz.* 135 multiply'd into the Breadth 48, produces 6480, and this multiply'd into 24, half the Breadth, gives 155520, which last divided by 95, the Quotient is 1637, the Tunnage of the propos'd Ship.

F I N I S.

A TABLE of the Latitudes and Longitudes of some  
of the most principal Harbours, Headlands, and  
Islands in the most frequented Parts of the World;  
the Longitude being counted from the Meridian of  
LONDON.

Places Names.	Lat.	Long.	Denom.
	D. M.	D. M.	
<i>The Coast of England.</i>			
B E R W I C K - - -	55 50	01 39	W
Newcastle - - -	54 58	01 30	W
Scarborough - - -	54 20	01 20	W
Stockton - - -	54 33	01 25	W
Flamborough-Head - - -	54 08	00 11	E
Tarmouth - - -	52 45	01 40	E
Ipswich . . . . .	52 14	01 00	E
Colchester - - -	52 04	00 58	E
L O N D O N - - -	51 32	00 00	
The Downs - - -	51 25	01 21	E
Dover - - -	51 15	01 18	E
Beachy - - -	50 48	00 25	E
Portsmouth - - -	50 48	01 00	W
Dartmouth - - -	50 27	03 36	W
Plymouth - - -	50 36	04 13	W
Lizard - - -	50 00	05 14	W
Bristol - - -	51 32	02 35	W
Liverpool - - -	53 20	03 10	W
White-Haven - - -	54 10	03 50	W
<i>The Coast of Scotland.</i>			
Glasgow - - -	55 53	04 05	W
Aberdeen - - -	57 24	01 37	W
Leith - - -	56 00	02 55	W
St. Kilda - - -	58 02	10 05	W
Cat-Ness - - -	58 47	02 06	W
Buchan-Ness - - -	57 55	01 20	W
Orkney Isles - - -	59 13	03 32	W

Places Names.	Lat.	Long.	Denom.
Coast of Ireland.	D. M.	D. M.	
London-Derry	55 05	08 00	W
Belfast	54 36	06 50	W
Cork	51 49	09 30	W
Cape-Clear	51 10	10 30	W
Lambay	53 24	07 30	W
Dublin	53 20	06 55	W
Coast of Holland and Flanders.			
Hamborough	53 41	10 25	E
Bremen	53 50	08 00	E
The Texel	53 10	04 59	E
Amsterdam	52 21	04 51	E
Roterdam	51 55	04 21	E
Dunkirk	51 14	02 20	E
Calais	50 57	01 55	E
On the Coast of France and Portugal.	Latitude North.		
Guernsey	49 36	02 40	W
Jersey	49 20	02 19	W
Rochel	46 10	01 14	W
Bourdeaux	44 50	00 24	W
Bilboa	43 30	03 00	W
Porta-Port	41 18	09 20	W
Cadiz	36 20	06 28	W
Coast on the main Continent within the Straits, and on the Coast of Spain, &c.			
Gibraltar	36 11	05 20	W
Malaga	36 50	03 17	W
Barcelona	41 26	02 26	E
Marseilles	43 20	05 27	E
Toulon	43 06	05 40	E

Places Names.	Lat.		Long.		Den.
	D.	M.	D.	M.	
Genoa	44	27	09	06	E
Leghorn	43	18	10	44	E
Rome	41	51	13	05	E
Naples	41	05	15	40	E
Gallipoli	40	08	18	42	E
Venice	45	18	12	40	E
Constantinople	41	07	31	45	E
Smyrna	38	28	27	20	E
Scanderoon	36	00	35	58	E
Tripoli	34	40	35	48	E
Alexandria	31	07	33	00	E
Algier	36	40	03	05	E

Coast of Barbary and Guinea,  
etc.

Sallee	33	43	06	30	W
Cape de Verde	14	30	16	26	W
River Gambia	13	16	15	20	W
Monserado	06	05	09	20	W
Cape Corce	04	40	03	10	E
Cape Formosa	04	40	08	00	E
River Congo	05	45	15	27	E
Angola	08	51	15	56	E
C. St. Thomas	23	10	14	23	E
Cape of Good Hope	34	15	17	00	E

Western Islands.

Corvo	40	05	31	55	W
Fyal	39	32	31	52	W
Pico	38	45	28	34	W
Gratiosa	39	30	28	15	W
St. Michael	37	50	24	52	W
St. Maries	37	00	22	17	W
Porto Sancto	32	45	16	05	W
Madera West End	32	20	17	30	W

Places Names.	Lat.		Long.		West Longitude.
	D.	M.	D.	M.	
Teneriff . . . . .	27	50	17	05	
Canary . . . . .	27	40	16	10	
St. Antonio . . . . .	17	20	24	50	
Fuego . . . . .	15	00	24	05	
Fago . . . . .	15	10	23	30	
St. Lucia . . . . .	17	20	24	00	
St. Nicholas . . . . .	17	12	23	30	
St. Vincent . . . . .	17	10	24	20	
Antegoa. . . . .	17	30	60	40	
Barbadoes . . . . .	13	30	58	10	
Berbuda . . . . .	17	58	60	40	
St. Cruz . . . . .	18	00	63	25	
Coast of Carolina, Virginia, Maryland, &c.			North Latitude.		
Charles Town on Asbly River	32	40	78	50	
Cape Henry . . . . .	37	00	74	25	
Quebeck . . . . .	47	15	68	10	
New-York . . . . .	41	00	72	05	
Boston . . . . .	42	35	68	50	
Trinity-Bay . . . . .	48	27	52	15	
Cape St. Mary . . . . .	47	10	53	20	
Placentia . . . . .	47	57	53	00	
Cape Charles . . . . .	37	14	74	15	
St. John's Harbour . . . . .	47	28	51	23	
Coast of Hudson's Bay, and the Straits.					
Cape Jones . . . . .	55	03	78	56	
Albany River . . . . .	51	16	79	44	
Shark Point . . . . .	64	27	83	16	
Button's Isle . . . . .	60	05	66	50	
Cape Charles . . . . .	62	35	74	36	
Port Nelson . . . . .	57	10	92	50	

Places Names.	Lat.		Long.		Den.
	D.	M.	D.	M.	
<i>Coast of America in the South-Sea.</i>					
C. St. Sebastian . . . . .	42	40	N.	129 40	
Panama . . . . .	08	56	Lat.	82 18	
Aquatalco . . . . .	15	27		101 03	
Cape St. Luca . . . . .	23	25		111 56	
Cape del Ajugo . . . . .	16	38		88 50	
Arica . . . . .	18	12		74 07	
Baldivia . . . . .	39	35		81 18	
Cape Victory . . . . .	52	15	South Latitude.		
Cape Horn . . . . .	57	58		82 56	
				79 44	
<i>Coast of Brazil in S. America.</i>					
River Julian . . . . .	48	40		74 32	
Cape Blanco . . . . .	46	50		72 05	
St. Katharine's Isle . . . . .	28	00		47 50	
Cape Frio . . . . .	23	10		42 56	
Cape Roque . . . . .	05	00		35 52	
					West Longitude.
<i>Coast on the main Continent in the West-Indies.</i>					
North Cape . . . . .	02	05		49 55	
Surnam . . . . .	06	00		56 44	
Cartbagena . . . . .	10	50		75 50	
Campeche . . . . .	19	20		93 05	
Portobello . . . . .	09	55		80 15	
La vera Cruz . . . . .	19	15		100 22	
Cape Florida . . . . .	24	48		81 55	
<i>Southern Islands.</i>					
Ascension . . . . .	07	40	S	14 50	
St. Helena . . . . .	16	06	S	06 30	
St. Matthew's . . . . .	01	40	S	07 50	
Princeps . . . . .	01	35	N	09 03	E
St. Thomas . . . . .	00	00		08 00	E
Annabona . . . . .	01	05	S	07 30	E

Places Names.	Lat.		Long.	
	D.	M.	D.	M.
<i>Coast of the East-Indies.</i>				
Mosambique . . . . .	15	05 S	42	30
River de Fugos . . . . .	00	00	41	15
Cape de Bassus . . . . .	04	06	44	50
Surrat . . . . .	21	08	73	25
Siam Entrance . . . . .	23	10	101	01
Goa . . . . .	15	30	Lat. North.	73 50
Fort St. George . . . . .	13	08		81 34
Dew Point . . . . .	15	50	81	50
Bengal . . . . .	22	27	91	49
Malacca . . . . .	23	32	105	05
Cambodia . . . . .	10	30	104	20
Nanquim . . . . .	32	55	129	30
<i>Islands in the East-Indies.</i>				
Abdeleur . . . . .	12	27	N	52 35
Almircant Isles, the Eastermost . . . . .	03	42 S	52	20
Bantam in Javes . . . . .	05	37 S	105	11
Batavia . . . . .	05	47 S	106	27
Babelmandel, in the Mouth of the Red Sea . . . . .	12	25	N	45 45
Borneo . . . . .	04	20 S	109	50
Good Fortune . . . . .	01	28 S	97	20
Java, East-End . . . . .	06	20 S	113	37
Japan, S. East Point . . . . .	34	30 N	135	35
S. West Point . . . . .	35	20 N	126	50
Joanna . . . . .	12	10 S	41	20
Princes Isle . . . . .	05	47 S	105	11
Zocatra . . . . .	12	28 N	54	20
Madagascar, South End of St. Sebastian . . . . .	25	32 S	74	15
<i>Coast of the Sound and Bat- tic Sea.</i>				
Gottenberg . . . . .	57	33 N	12	25
Christiana . . . . .	59	10 N	9	45

East Longitude.

## Places Names.

	Lat.	Long.	
		D.	M.
Elfinore	56 00	12	32
Copenhagen	55 40	12	30
Stockholm	59 20	18	25
Vyburgh	60 20	29	26
Petersburgh	59 24	29	50
Riga	56 50	24	50
Coningsberg	55 00	20	13
Dantzick	54 22	19	10
Seaw	57 26	10	14

## Coast from the Naze of Norway to Archangel.

		North Latitude.	East Latitude.
Naze of Norway	57 50	07 22	
Dronton	64 00	10 40	
North Cape	71 25	22 10	
Standland	62 10	04 38	
Kilduyn	69 32	30 12	
Archangel-Bar	64 30	40 30	
Cross Island	66 31	36 10	

## Coast of the Northern Islands, Nova Zembla, Iceland, and Greenland.

Bear Isle	74 35	18 12
Hope Isle	76 13	21 44
Catnose	65 44	33 13
Point Lookout	76 40	16 25
Horn Sound	77 30	13 56
Grims Island	66 43	17 45
Whales Back	65 27	10 05
Sound Royal	66 20	14 12

A  
CORRECT and CONCISE  
**T A B L E**  
OF  
**LOGARITHMS.**

For N U M B E R S increasing in their Natural  
Order from Unity to 10000.

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
1.00000	46 1.66276	91 1.95904	136 2.13354				
2.30103	47 1.67210	92 1.96379	137 2.13672				
3.047712	48 1.68124	93 1.96878	138 2.13988				
4.060206	49 1.69020	94 1.97313	139 2.14301				
5.269897	50 1.69897	95 1.97772	140 2.14613				
6.077815	51 1.70757	96 1.98227	141 2.14922				
7.084510	52 1.71600	97 1.98677	142 2.15229				
8.090309	53 1.72428	98 1.99123	143 2.15534				
9.095424	54 1.73239	99 1.99564	144 2.15836				
10.100000	55 1.74036	100 2.00000	145 2.16137				
11.1.04139	56 1.74819	101 2.00432	146 2.16435				
12.1.07918	57 1.75587	102 2.00860	147 2.16732				
13.1.11394	58 1.76343	103 2.01284	148 2.17026				
14.1.14613	59 1.77085	104 2.01703	149 2.17319				
15.1.17809	60 1.77815	105 2.02119	150 2.17609				
16.1.20413	61 1.78533	106 2.02531	151 2.17898				
17.1.23045	62 1.79239	107 2.02938	152 2.18184				
18.1.25527	63 1.79934	108 2.03342	153 2.18469				
19.1.27875	64 1.80618	109 2.03743	154 2.18752				
20.1.30103	65 1.81291	110 2.04139	155 2.19033				
21.1.32222	66 1.81954	111 2.04532	156 2.19312				
22.1.34242	67 1.82607	112 2.04922	157 2.19590				
23.1.36173	68 1.83251	113 2.05308	158 2.19866				
24.1.38021	69 1.83885	114 2.05690	159 2.20140				
25.1.39794	70 1.84510	115 2.06070	160 2.20412				
26.1.41497	71 1.85126	116 2.06446	161 2.20683				
27.1.43136	72 1.85733	117 2.06819	162 2.20952				
28.1.44716	73 1.86332	118 2.07183	163 2.21218				
29.1.46240	74 1.86923	119 2.07555	164 2.21484				
30.1.47712	75 1.87506	120 2.07918	165 2.21748				
31.1.49136	76 1.88081	121 2.08279	166 2.22011				
32.1.50515	77 1.88649	122 2.08636	167 2.22272				
33.1.51881	78 1.89209	123 2.08991	168 2.22531				
34.1.53148	79 1.89763	124 2.09342	169 2.22789				
35.1.54407	80 1.90209	125 2.09691	170 2.23045				
36.1.55630	81 1.90849	126 2.10037	171 2.23300				
37.1.56820	82 1.91381	127 2.10380	172 2.23553				
38.1.57978	83 1.91908	128 2.10721	173 2.23805				
39.1.59106	84 1.92428	129 2.11059	174 2.24155				
40.1.60206	85 1.92942	130 2.11394	175 2.24304				
41.1.61278	86 1.93450	131 2.11727	176 2.24551				
42.1.62335	87 1.93952	132 2.12057	177 2.24797				
43.1.63347	88 1.94448	133 2.12385	178 2.25042				
44.1.64345	89 1.94939	134 2.12710	179 2.25285				
45.1.65321	90 1.95424	135 2.13033	180 2.25527				

A Table of Logarithms.

3

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
181	2.25768	226	2.35411	271	2.43297	316	2.45069
182	2.26007	227	2.35603	272	2.43457	317	2.45106
183	2.26245	228	2.35793	273	2.43616	318	2.45243
184	2.26482	229	2.35984	274	2.43775	319	2.45379
185	2.26717	230	2.36173	275	2.43933	320	2.45515
186	2.26951	231	2.36361	276	2.44091	321	2.50651
187	2.27184	232	2.36549	277	2.44248	322	2.50786
188	2.27416	233	2.36736	278	2.44405	323	2.50920
189	2.27646	234	2.36922	279	2.44560	324	2.51055
190	2.27875	235	2.37107	280	2.44716	325	2.51188
191	2.28103	236	2.37291	281	2.44871	326	2.51322
192	2.28330	237	2.37475	282	2.45025	327	2.51455
193	2.28556	238	2.37658	283	2.45179	328	2.51587
194	2.28780	239	2.37840	284	2.45332	329	2.51720
195	2.29003	240	2.38021	285	2.45485	330	2.51851
196	2.29226	241	2.38202	286	2.45637	331	2.51983
197	2.29447	242	2.38382	287	2.45788	332	2.52114
198	2.29667	243	2.38561	288	2.45939	333	2.52244
199	2.29885	244	2.38739	289	2.46090	334	2.52375
200	2.30103	245	2.38917	290	2.46240	335	2.52504
201	2.30320	246	2.39094	291	2.46389	336	2.52634
202	2.30535	247	2.39270	292	2.46538	337	2.52763
203	2.30750	248	2.39445	293	2.46687	338	2.52892
204	2.30963	249	2.39620	294	2.46835	339	2.53020
205	2.31175	250	2.39794	295	2.46982	340	2.53148
206	2.31387	251	2.39967	296	2.47129	341	2.53275
207	2.31597	252	2.40140	297	2.47276	342	2.53403
208	2.31806	253	2.40312	298	2.47422	343	2.53529
209	2.32015	254	2.40483	299	2.47567	344	2.53656
210	2.32223	255	2.40654	300	2.47712	345	2.53782
211	2.32428	256	2.40824	301	2.47857	346	2.53908
212	2.32634	257	2.40993	302	2.48001	347	2.54033
213	2.32838	258	2.41162	303	2.48144	348	2.54158
214	2.33041	259	2.41330	304	2.48287	349	2.54283
215	2.33244	260	2.41497	305	2.48430	350	2.54407
216	2.33445	261	2.41664	306	2.48572	351	2.54531
217	2.33646	262	2.41830	307	2.48714	352	2.54654
218	2.33846	263	2.41996	308	2.48855	353	2.54778
219	2.34044	264	2.42160	309	2.48996	354	2.54900
220	2.34242	265	2.42325	310	2.49136	355	2.55023
221	2.34439	266	2.42488	311	2.49276	356	2.55145
222	2.34635	267	2.42651	312	2.49415	357	2.55267
223	2.34832	268	2.42813	313	2.49554	358	2.55388
224	2.35029	269	2.42975	314	2.49693	359	2.55509
225	2.35218	270	2.43136	315	2.49831	360	2.55630

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
361	2.55751	406	2.60853	451	2.65418	496	2.69548
362	2.55871	407	2.60960	452	2.65514	497	2.69636
363	2.55991	408	2.61066	453	2.65610	498	2.69723
364	2.56110	409	2.61172	454	2.65706	499	2.69810
365	2.56229	410	2.61288	455	2.65801	500	2.69897
366	2.56348	411	2.61384	456	2.65897	501	2.69984
367	2.56467	412	2.61490	457	2.65992	502	2.70070
368	2.56585	413	2.61595	458	2.66087	503	2.70157
369	2.56703	414	2.61700	459	2.66181	504	2.70243
370	2.56820	415	2.61805	460	2.66276	505	2.70329
371	2.56937	416	2.61909	461	2.66370	506	2.70415
372	2.57054	417	2.62014	462	2.66462	507	2.70501
373	2.57171	418	2.62118	463	2.66558	508	2.70586
374	2.57287	419	2.62221	464	2.66652	509	2.70672
375	2.57403	420	2.62325	465	2.66745	510	2.70757
376	2.57519	421	2.62428	466	2.66839	511	2.70842
377	2.57634	422	2.62531	467	2.66932	512	2.70927
378	2.57749	423	2.62634	468	2.67025	513	2.71012
379	2.57864	424	2.62737	469	2.67117	514	2.71096
380	2.57978	425	2.62839	470	2.67210	515	2.71181
381	2.58093	426	2.62941	471	2.67302	516	2.71265
382	2.58206	427	2.63043	472	2.67394	517	2.71349
383	2.58320	428	2.63144	473	2.67486	518	2.71433
384	2.58433	429	2.63246	474	2.67578	519	2.71517
385	2.58546	430	2.63347	475	2.67669	520	2.71600
386	2.58659	431	2.63448	476	2.67761	521	2.71684
387	2.58771	432	2.63548	477	2.67852	522	2.71767
388	2.58883	433	2.63649	478	2.67943	523	2.71850
389	2.58995	434	2.63749	479	2.68034	524	2.71933
390	2.59106	435	2.63849	480	2.68124	525	2.72016
391	2.59218	436	2.63949	481	2.68215	526	2.72099
392	2.59329	437	2.64048	482	2.68305	527	2.72181
393	2.59439	438	2.64147	483	2.68395	528	2.72263
394	2.59550	439	2.64246	484	2.68485	529	2.72346
395	2.59660	440	2.64345	485	2.68575	530	2.72428
396	2.59770	441	2.64444	486	2.68664	531	2.72509
397	2.59879	442	2.64542	487	2.68753	532	2.72591
398	2.59988	443	2.64640	488	2.68842	533	2.72673
399	2.60097	444	2.64738	489	2.68931	534	2.72754
400	2.60206	445	2.64836	490	2.69020	535	2.72835
401	2.60314	446	2.64934	491	2.69108	536	2.72916
402	2.60423	447	2.65031	492	2.69197	537	2.72997
403	2.60531	448	2.65128	493	2.69285	538	2.73078
404	2.60638	449	2.65225	494	2.69373	539	2.73159
405	2.60746	450	2.65321	495	2.69461	540	2.73239

# A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
541	2.73320	586	2.76790	631	2.80003	676	2.82995
542	2.73400	587	2.76864	632	2.80072	677	2.83059
543	2.73480	588	2.76938	633	2.80146	678	2.83123
544	2.73560	589	2.77012	634	2.80209	679	2.83187
545	2.73640	590	2.77085	635	2.80277	680	2.83251
546	2.73719	591	2.77159	636	2.80346	681	2.83315
547	2.73799	592	2.77232	637	2.80414	682	2.83378
548	2.73878	593	2.77305	638	2.80482	683	2.83442
549	2.73957	594	2.77379	639	2.80550	684	2.83506
550	2.74036	595	2.77452	640	2.80618	685	2.83569
551	2.74115	596	2.77525	641	2.80686	686	2.83632
552	2.74194	597	2.77597	642	2.80754	687	2.83696
553	2.74273	598	2.77670	643	2.80821	688	2.83759
554	2.74351	599	2.77743	644	2.80889	689	2.83822
555	2.74429	600	2.77815	645	2.80956	690	2.83885
556	2.74507	601	2.77887	646	2.81023	691	2.83948
557	2.74586	602	2.77960	647	2.81090	692	2.84011
558	2.74663	603	2.78032	648	2.81158	693	2.84073
559	2.74741	604	2.78104	649	2.81224	694	2.84136
560	2.74819	605	2.78176	650	2.81291	695	2.84198
561	2.74896	606	2.78247	651	2.81358	696	2.84261
562	2.74974	607	2.78319	652	2.81425	697	2.84323
563	2.75051	608	2.78390	653	2.81491	698	2.84386
564	2.75128	609	2.78462	654	2.81558	699	2.84448
565	2.75205	610	2.78533	655	2.81624	700	2.84510
566	2.75282	611	2.78604	656	2.81690	701	2.84572
567	2.75358	612	2.78675	657	2.81757	702	2.84634
568	2.75435	613	2.78746	658	2.81823	703	2.84696
569	2.75511	614	2.78817	659	2.81889	704	2.84757
570	2.75587	615	2.78888	660	2.81954	705	2.84819
571	2.75664	616	2.78958	661	2.82020	706	2.84880
572	2.75740	617	2.79029	662	2.82086	707	2.84942
573	2.75815	618	2.79099	663	2.82151	708	2.85003
574	2.75891	619	2.79169	664	2.82217	709	2.85065
575	2.75967	620	2.79235	665	2.82282	710	2.85126
576	2.76042	621	2.79309	666	2.82347	711	2.85187
577	2.76118	622	2.79379	667	2.82413	712	2.85248
578	2.76193	623	2.79449	668	2.82478	713	2.85309
579	2.76268	624	2.79518	669	2.82543	714	2.85370
580	2.76343	625	2.79588	670	2.82607	715	2.85431
581	2.76418	626	2.79657	671	2.82672	716	2.85491
582	2.76492	627	2.79727	672	2.82737	717	2.85552
583	2.76567	628	2.79796	673	2.82802	718	2.85612
584	2.76641	629	2.79865	674	2.82866	719	2.85673
585	2.76716	630	2.79934	675	2.82930	720	2.85733

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
721	2.85794	766	2.88423	811	2.90902	856	2.93247
722	2.85854	767	2.88480	812	2.90956	857	2.93298
723	2.85914	768	2.88536	813	2.91007	858	2.93349
724	2.85974	769	2.88593	814	2.91062	859	2.93399
725	2.86034	770	2.88649	815	2.91116	860	2.93450
726	2.86094	771	2.88705	816	2.91169	861	2.93500
727	2.86153	772	2.88762	817	2.91222	862	2.93551
728	2.86213	773	2.88818	818	2.91275	863	2.93601
729	2.86273	774	2.88874	819	2.91328	864	2.93651
730	2.86332	775	2.88930	820	2.91381	865	2.93702
731	2.86392	776	2.88986	821	2.91434	866	2.93752
732	2.86451	777	2.89042	822	2.91487	867	2.93802
733	2.86510	778	2.89098	823	2.91540	868	2.93852
734	2.86570	779	2.89154	824	2.91593	869	2.93902
735	2.86629	780	2.89209	825	2.91645	870	2.93952
736	2.86688	781	2.89265	826	2.91698	871	2.94002
737	2.86747	782	2.89321	827	2.91751	872	2.94052
738	2.86806	783	2.89376	828	2.91803	873	2.94101
739	2.86864	784	2.89432	829	2.91855	874	2.94151
740	2.86923	785	2.89487	830	2.91908	875	2.94201
741	2.86982	786	2.89542	831	2.91960	876	2.94250
742	2.87040	787	2.89597	832	2.92012	877	2.94300
743	2.87099	788	2.89653	833	2.92063	878	2.94349
744	2.87157	789	2.89708	834	2.92117	879	2.94399
745	2.87216	790	2.89763	835	2.92169	880	2.94448
746	2.87274	791	2.89818	836	2.92221	881	2.94498
747	2.87332	792	2.89873	837	2.92273	882	2.94547
748	2.87390	793	2.89927	838	2.92324	883	2.94596
749	2.87448	794	2.89982	839	2.92376	884	2.94645
750	2.87506	795	2.90037	840	2.92428	885	2.94694
751	2.87564	796	2.90091	841	2.92480	886	2.94743
752	2.87622	797	2.90146	842	2.92531	887	2.94792
753	2.87680	798	2.90200	843	2.92583	888	2.94841
754	2.87737	799	2.90255	844	2.92634	889	2.94890
755	2.87795	800	2.90309	845	2.92686	890	2.94939
756	2.87852	801	2.90363	846	2.92737	891	2.94988
757	2.87910	802	2.90417	847	2.92788	892	2.95036
758	2.87967	803	2.90472	848	2.92840	893	2.95085
759	2.88024	804	2.90526	849	2.92891	894	2.95134
760	2.88081	805	2.90580	850	2.92942	895	2.95182
761	2.88138	806	2.90634	851	2.92993	896	2.95231
762	2.88196	807	2.90687	852	2.93044	897	2.95279
763	2.88252	808	2.90741	853	2.93095	898	2.95328
764	2.88309	809	2.90795	854	2.93146	899	2.95376
765	2.88266	810	2.90849	855	2.93197	900	2.95424

# A. Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
901	2.95472	946	2.97589	991	2.99607	1036	3.01536
902	2.95521	947	2.97635	992	2.99651	1037	3.01978
903	2.95569	948	2.97681	993	2.99695	1038	3.01620
904	2.95617	949	2.97727	994	2.99739	1039	3.01662
905	2.95665	950	2.97772	995	2.99782	1040	3.01703
906	2.95713	951	2.97818	996	2.99826	1041	3.01745
907	2.95761	952	2.97864	997	2.99870	1042	3.01787
908	2.95809	953	2.97909	998	2.99913	1043	3.01828
909	2.95856	954	2.97955	999	2.99957	1044	3.01870
910	2.95904	955	2.98000	1000	3.00000	1045	3.01912
911	2.95952	956	2.98046	1001	3.00043	1046	3.01953
912	2.95999	957	2.98091	1002	3.00087	1047	3.01995
913	2.96047	958	2.98137	1003	3.00130	1048	3.02036
914	2.96095	959	2.98182	1004	3.00173	1049	3.02078
915	2.96142	960	2.98227	1005	3.00217	1050	3.02119
916	2.96190	961	2.98272	1006	3.00260	1051	3.02160
917	2.96237	962	2.98318	1007	3.00303	1052	3.02202
918	2.96284	963	2.98363	1008	3.00346	1053	3.02243
919	2.96332	964	2.98408	1009	3.00389	1054	3.02284
920	2.96379	965	2.98453	1010	3.00432	1055	3.02325
921	2.96426	966	2.98498	1011	3.00475	1056	3.02366
922	2.96473	967	2.98543	1012	3.00518	1057	3.02408
923	2.96520	968	2.98588	1013	3.00561	1058	3.02449
924	2.96567	969	2.98622	1014	3.00604	1059	3.02490
925	2.96614	970	2.98677	1015	3.00647	1060	3.02531
926	2.96661	971	2.98722	1016	3.00685	1061	3.02572
927	2.96708	972	2.98767	1017	3.00732	1062	3.02613
928	2.96755	973	2.98811	1018	3.00775	1063	3.02653
929	2.96802	974	2.98856	1019	3.00817	1064	3.02694
930	2.96848	975	2.98900	1020	3.00860	1065	3.02735
931	2.96895	976	2.98945	1021	3.00903	1066	3.02776
932	2.96942	977	2.98989	1022	3.00945	1067	3.02816
933	2.96988	978	2.99034	1023	3.00988	1068	3.02857
934	2.97035	979	2.99078	1024	3.01031	1069	3.02898
935	2.97081	980	2.99123	1025	3.01072	1070	3.02938
936	2.97128	981	2.99167	1026	3.01115	1071	3.03979
937	2.97174	982	2.99211	1027	3.01157	1072	3.03019
938	2.97220	983	2.99255	1028	3.01199	1073	3.03060
939	2.97267	984	2.99300	1029	3.01242	1074	3.03100
940	2.97313	985	2.99344	1030	3.01284	1075	3.03141
941	2.97359	986	2.99388	1031	3.01326	1076	3.03181
942	2.97405	987	2.99432	1032	3.01368	1077	3.03222
943	2.97451	988	2.99476	1033	3.01410	1078	3.03262
944	2.97497	989	2.99520	1034	3.01452	1079	3.03302
945	2.97543	990	2.99564	1035	3.01494	1080	3.03342

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
1081	3.03383	1126	3.05154	1171	3.06856	1216	3.08493
1082	3.03423	1127	3.05192	1172	3.06893	1217	3.08529
1083	3.03463	1128	3.05231	1173	3.06950	1218	3.08565
1084	3.03503	1129	3.05269	1174	3.06967	1219	3.08600
1085	3.03543	1130	3.05308	1175	3.07004	1220	3.08636
1086	3.03583	1131	3.05346	1176	3.07041	1221	3.08672
1087	3.03623	1132	3.05385	1177	3.07078	1222	3.08707
1088	3.03663	1133	3.05423	1178	3.07115	1223	3.08743
1089	3.03703	1134	3.05461	1179	3.07151	1224	3.08778
1090	3.03743	1135	3.05500	1180	3.07188	1225	3.08814
1091	3.03782	1136	3.05538	1181	3.07225	1226	3.08849
1092	3.03822	1137	3.05576	1182	3.07262	1227	3.08884
1093	3.03862	1138	3.05614	1183	3.07298	1228	3.08920
1094	3.03902	1139	3.05652	1184	3.07335	1229	3.08955
1095	3.03941	1140	3.05690	1185	3.07372	1230	3.08991
1096	3.03981	1141	3.05729	1186	3.07408	1231	3.09026
1097	3.04021	1142	3.05767	1187	3.07445	1232	3.09061
1098	3.04060	1143	3.05805	1188	3.07482	1233	3.09096
1099	3.04100	1144	3.05843	1189	3.07518	1234	3.09132
1100	3.04139	1145	3.05881	1190	3.07555	1235	3.09167
1101	3.04179	1146	3.05918	1191	3.07591	1236	3.09202
1102	3.04218	1147	3.05956	1192	3.07628	1237	3.09237
1103	3.04258	1148	3.05994	1193	3.07664	1238	3.09272
1104	3.04297	1149	3.06032	1194	3.07700	1239	3.09307
1105	3.04336	1150	3.06070	1195	3.07737	1240	3.09342
1106	3.04376	1151	3.06108	1196	3.07773	1241	3.09377
1107	3.04415	1152	3.06145	1197	3.07809	1242	3.09412
1108	3.04454	1153	3.06183	1198	3.07846	1243	3.09447
1109	3.04493	1154	3.06221	1199	3.07882	1244	3.09482
1110	3.04532	1155	3.06258	1200	3.07918	1245	3.09517
1111	3.04571	1156	3.06296	1201	3.07954	1246	3.09552
1112	3.04610	1157	3.06333	1202	3.07990	1247	3.09587
1113	3.04650	1158	3.06371	1203	3.08027	1248	3.09621
1114	3.04689	1159	3.06408	1204	3.08063	1249	3.09656
1115	3.04727	1160	3.06446	1205	3.08099	1250	3.09691
1116	3.04766	1161	3.06483	1206	3.08135	1251	3.09726
1117	3.04805	1162	3.06521	1207	3.08171	1252	3.09760
1118	3.04844	1163	3.06558	1208	3.08207	1253	3.09795
1119	3.04883	1164	3.06595	1209	3.08243	1254	3.09830
1120	3.04922	1165	3.06633	1210	3.08279	1255	3.09864
1121	3.04961	1166	3.06670	1211	3.08314	1256	3.09899
1122	3.04999	1167	3.06707	1212	3.08350	1257	3.09934
1123	3.05038	1168	3.06744	1213	3.08386	1258	3.09968
1124	3.05077	1169	3.06781	1214	3.08422	1259	3.10003
1125	3.05115	1170	3.06819	1215	3.08458	1260	3.10037

*A Table of Logarithms.*

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
1261	3.10072	1306	3.11594	1351	3.13066	1396	3.14489
1262	3.10106	1307	3.11628	1352	3.13098	1397	3.14520
1263	3.10140	1308	3.11661	1353	3.13130	1398	3.14551
1264	3.10175	1309	3.11694	1354	3.13162	1399	3.14582
1265	3.10209	1310	3.11727	1355	3.13194	1400	3.14613
1266	3.10243	1311	3.11760	1356	3.13226	1401	3.14644
1267	3.10278	1312	3.11793	1357	3.13258	1402	3.14675
1268	3.10312	1313	3.11826	1358	3.13290	1403	3.14706
1269	3.10346	1314	3.11860	1359	3.13322	1404	3.14737
1270	3.10380	1315	3.11893	1360	3.13354	1405	3.14768
1271	3.10415	1316	3.11926	1361	3.13386	1406	3.14799
1272	3.10449	1317	3.11959	1362	3.13418	1407	3.14829
1273	3.10483	1318	3.11992	1363	3.13450	1408	3.14860
1274	3.10517	1319	3.12024	1364	3.13481	1409	3.1489
1275	3.10551	1320	3.12057	1365	3.13513	1410	3.14922
1276	3.10585	1321	3.12090	1366	3.13545	1411	3.14953
1277	3.10619	1322	3.12123	1367	3.13577	1412	3.14983
1278	3.10653	1323	3.12156	1368	3.13609	1413	3.15014
1279	3.10687	1324	3.12189	1369	3.13640	1414	3.15045
1280	3.10721	1325	3.12222	1370	3.13672	1415	3.15076
1281	3.10755	1326	3.12254	1371	3.13704	1416	3.15106
1282	3.10789	1327	3.12287	1372	3.13735	1417	3.15137
1283	3.10823	1328	3.12320	1373	3.13767	1418	3.15168
1284	3.10857	1329	3.12353	1374	3.13799	1419	3.15198
1285	3.10890	1330	3.12385	1375	3.13830	1420	3.15229
1286	3.10924	1331	3.12418	1376	3.13862	1421	3.15259
1287	3.10958	1332	3.12450	1377	3.13893	1422	3.15290
1288	3.10992	1333	3.12483	1378	3.13925	1423	3.15320
1289	3.11025	1334	3.12516	1379	3.13956	1424	3.15351
1290	3.11059	1335	3.12548	1380	3.13988	1425	3.15381
1291	3.11093	1336	3.12581	1381	3.14019	1426	3.15412
1292	3.11126	1337	3.12613	1382	3.14051	1427	3.15442
1293	3.11160	1338	3.12646	1383	3.14082	1428	3.15473
1294	3.11193	1339	3.12678	1384	3.14114	1429	3.15503
1295	3.11227	1340	3.12710	1385	3.14145	1430	3.15534
1296	3.11261	1341	3.12743	1386	3.14176	1431	3.15564
1297	3.11294	1342	3.12775	1387	3.14208	1432	3.15594
1298	3.11327	1343	3.12808	1388	3.14235	1433	3.15625
1299	3.11361	1344	3.12840	1389	3.14270	1434	3.15655
1300	3.11394	1345	3.12872	1390	3.14300	1435	3.15685
1301	3.11428	1346	3.12905	1391	3.14337	1436	3.15715
1302	3.11461	1347	3.12937	1392	3.14364	1437	3.15746
1303	3.11494	1348	3.12969	1393	3.14395	1438	3.15776
1304	3.11528	1349	3.13001	1394	3.14426	1439	3.15806
1305	3.11561	1350	3.13033	1395	3.14457	1440	3.15836

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
1441	3.15866	1486	3.17202	1531	3.18498	1576	3.19796
1442	3.15897	1487	3.17231	1532	3.18526	1577	3.19783
1443	3.15927	1488	3.17260	1533	3.18554	1578	3.19811
1444	3.15957	1489	3.17289	1534	3.18583	1579	3.19838
1445	3.15987	1490	3.17319	1535	3.18611	1580	3.19866
1446	3.16017	1491	3.17348	1536	3.18639	1581	3.19893
1447	3.16047	1492	3.17377	1537	3.18667	1582	3.19921
1448	3.16077	1493	3.17406	1538	3.18696	1583	3.19948
1449	3.16107	1494	3.17435	1539	3.18724	1584	3.19976
1450	3.16137	1495	3.17464	1540	3.18752	1585	3.20003
1451	3.16167	1496	3.17493	1541	3.18780	1586	3.20030
1452	3.16197	1497	3.17522	1542	3.18808	1587	3.20058
1453	3.16227	1498	3.17551	1543	3.18837	1588	3.20085
1454	3.16256	1499	3.17580	1544	3.18865	1589	3.20112
1455	3.16286	1500	3.17609	1545	3.18893	1590	3.20140
1456	3.16316	1501	3.17638	1546	3.18921	1591	3.20167
1457	3.16346	1502	3.17667	1547	3.18949	1592	3.20194
1458	3.16376	1503	3.17696	1548	3.18977	1593	3.20222
1459	3.16405	1504	3.17725	1549	3.19005	1594	3.20249
1460	3.16435	1505	3.17754	1550	3.19033	1595	3.20276
1461	3.16465	1506	3.17783	1551	3.19061	1596	3.20303
1462	3.16495	1507	3.17811	1552	3.19089	1597	3.20330
1463	3.16524	1508	3.17840	1553	3.19117	1598	3.20358
1464	3.16554	1509	3.17869	1554	3.19145	1599	3.20385
1465	3.16584	1510	3.17898	1555	3.19173	1600	3.20412
1466	3.16613	1511	3.17926	1556	3.19201	1601	3.20439
1467	3.16643	1512	3.17955	1557	3.19229	1602	3.20466
1468	3.16673	1513	3.17984	1558	3.19257	1603	3.20493
1469	3.16702	1514	3.18013	1559	3.19285	1604	3.20520
1470	3.16732	1515	3.18041	1560	3.19312	1605	3.20548
1471	3.16761	1516	3.18070	1561	3.19340	1606	3.20575
1472	3.16791	1517	3.18099	1562	3.19368	1607	3.20602
1473	3.16820	1518	3.18127	1563	3.19396	1608	3.20629
1474	3.16850	1519	3.18156	1564	3.19424	1609	3.20656
1475	3.16879	1520	3.18184	1565	3.19451	1610	3.20683
1476	3.16909	1521	3.18213	1566	3.19479	1611	3.20710
1477	3.16938	1522	3.18241	1567	3.19507	1612	3.20737
1478	3.16967	1523	3.18270	1568	3.19535	1613	3.20763
1479	3.16997	1524	3.18299	1569	3.19562	1614	3.20790
1480	3.17026	1525	3.18327	1570	3.19590	1615	3.20817
1481	3.17056	1526	3.18355	1571	3.19618	1616	3.20844
1482	3.17085	1527	3.18384	1572	3.19645	1617	3.20871
1483	3.17114	1528	3.18412	1573	3.19673	1618	3.20898
1484	3.17143	1529	3.18441	1574	3.19700	1619	3.20925
1485	3.17173	1530	3.18469	1575	3.19728	1620	3.20952

# A Table of Logarithms.

II

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
1621	3.20978	1666	3.22168	1711	3.23325	1756	3.24452
1622	3.21005	1667	3.22194	1712	3.23350	1757	3.24477
1623	3.21032	1668	3.22220	1713	3.23376	1758	3.24502
1624	3.21059	1669	3.22245	1714	3.23401	1759	3.24527
1625	3.21085	1670	3.22272	1715	3.23426	1760	3.24551
1626	3.21112	1671	3.22298	1716	3.23452	1761	3.24576
1627	3.21139	1672	3.22324	1717	3.23477	1762	3.24601
1628	3.21165	1673	3.22350	1718	3.23502	1763	3.24625
1629	3.21192	1674	3.22376	1719	3.23528	1764	3.24650
1630	3.21219	1675	3.22401	1720	3.23553	1765	3.24674
1631	3.21245	1676	3.22427	1721	3.23578	1766	3.24699
1632	3.21272	1677	3.22453	1722	3.23603	1767	3.24724
1633	3.21299	1678	3.22479	1723	3.23629	1768	3.24748
1634	3.21325	1679	3.22505	1724	3.23654	1769	3.24772
1635	3.21352	1680	3.22531	1725	3.23679	1770	3.24797
1636	3.21378	1681	3.22557	1726	3.23704	1771	3.24822
1637	3.21405	1682	3.22583	1727	3.23729	1772	3.24847
1638	3.21431	1683	3.22608	1728	3.23754	1773	3.24871
1639	3.21458	1684	3.22634	1729	3.23780	1774	3.24895
1640	3.21484	1685	3.22660	1730	3.23805	1775	3.24920
1641	3.21511	1686	3.22686	1731	3.23830	1776	3.24944
1642	3.21537	1687	3.22712	1732	3.23855	1777	3.24969
1643	3.21564	1688	3.22737	1733	3.23880	1778	3.24993
1644	3.21590	1689	3.22763	1734	3.23905	1779	3.25018
1645	3.21617	1690	3.22789	1735	3.23930	1780	3.25042
1646	3.21643	1691	3.22814	1736	3.23955	1781	3.25066
1647	3.21669	1692	3.22840	1737	3.23980	1782	3.25091
1648	3.21696	1693	3.22866	1738	3.24000	1783	3.25115
1649	3.21722	1694	3.22891	1739	3.24030	1784	3.25139
1650	3.21748	1695	3.22917	1740	3.24055	1785	3.25164
1651	3.21775	1696	3.22943	1741	3.24080	1786	3.25188
1652	3.21801	1697	3.22968	1742	3.24105	1787	3.25212
1653	3.21827	1698	3.22994	1743	3.24130	1788	3.25237
1654	3.21854	1699	3.23019	1744	3.24155	1789	3.25261
1655	3.21880	1700	3.23045	1745	3.24180	1790	3.25285
1656	3.21906	1701	3.23070	1746	3.24204	1791	3.25310
1657	3.21932	1702	3.23096	1747	3.24229	1792	3.25334
1658	3.21958	1703	3.23121	1748	3.24254	1793	3.25358
1659	3.21985	1704	3.23147	1749	3.24279	1794	3.25382
1660	3.22011	1705	3.23172	1750	3.24304	1795	3.25406
1661	3.22037	1706	3.23198	1751	3.24329	1796	3.25431
1662	3.22063	1707	3.23223	1752	3.24353	1797	3.25455
1663	3.22089	1708	3.23249	1753	3.24378	1798	3.25479
1664	3.22115	1709	3.23274	1754	3.24403	1799	3.25503
1665	3.22141	1710	3.23300	1755	3.24428	1800	3.25527

## A Table of Logarithms.

N.	Logar.		Logar.	N.	Logar.	N.	Logar.
1801	3.25553	1846	3.26623	1891	3.27669	1936	3.28691
1802	3.25575	1847	3.26647	1892	3.27692	1937	3.28713
1803	3.25600	1848	3.26670	1893	3.2771	1938	3.28735
1804	3.25624	1849	3.26694	1894	3.27738	1939	3.28758
1805	3.25648	1850	3.26717	1895	3.27761	1940	3.28780
1806	3.25672	1851	3.26741	1896	3.27784	1941	3.28803
1807	3.25696	1852	3.26764	1897	3.27807	1942	3.28825
1808	3.25720	1853	3.26788	1898	3.27830	1943	3.28847
1809	3.25744	1854	3.26811	1899	3.27853	1944	3.28870
1810	3.25768	1855	3.26834	1900	3.27875	1945	3.28892
1811	3.25792	1856	3.26858	1901	3.27898	1946	3.28914
1812	3.25816	1857	3.26881	1902	3.27921	1947	3.28937
1813	3.25840	1858	3.26905	1903	3.27944	1948	3.28959
1814	3.25864	1859	3.26928	1904	3.27967	1949	3.28981
1815	3.25888	1860	3.26951	1905	3.27990	1950	3.29003
1816	3.25912	1861	3.26974	1906	3.28012	1951	3.29026
1817	3.25935	1862	3.26998	1907	3.28035	1952	3.29048
1818	3.2596	1863	3.27021	1908	3.28058	1952	3.29070
1819	3.2598	1864	3.27045	1909	3.28081	1954	3.29092
1820	3.2600	1865	3.27068	1910	3.28103	1955	3.29115
1821	3.26031	1866	3.27091	1911	3.28126	1956	3.29137
1822	3.26055	1867	3.27114	1912	3.28149	1957	3.29159
1823	3.26079	1868	3.27138	1913	3.28172	1958	3.29181
1824	3.26102	1869	3.27161	1914	3.28194	1959	3.29203
1825	3.26126	1870	3.27184	1915	3.28217	1960	3.29226
1826	3.26150	1871	3.27207	1916	3.28240	1961	3.29248
1827	3.26174	1872	3.27231	1917	3.28262	1962	3.29270
1828	3.26198	1873	3.27254	1918	3.28285	1963	3.29292
1829	3.26221	1874	3.27277	1919	3.28308	1964	3.29314
1830	3.26245	1875	3.27300	1920	3.28330	1965	3.29336
1831	3.26269	1876	3.27323	1921	3.28353	1966	3.29358
1832	3.26293	1877	3.27346	1922	3.28375	1967	3.29380
1833	3.26316	1878	3.27370	1923	3.28398	1968	3.29403
1834	3.26340	1879	3.27393	1924	3.28421	1969	3.29425
1835	3.26364	1880	3.27416	1925	3.28443	1970	3.29447
1836	3.26387	1881	3.27439	1926	3.28466	1971	3.29469
1837	3.26411	1882	3.27462	1927	3.28488	1972	3.29491
1838	3.26435	1883	3.27485	1928	3.28511	1973	3.29513
1839	3.26458	1884	3.27508	1929	3.28533	1974	3.29535
1840	3.26482	1885	3.27531	1930	3.28556	1975	3.29557
1841	3.26505	1886	3.27554	1931	3.28578	1976	3.29579
1842	3.26529	1887	3.27577	1932	3.28601	1977	3.29601
1843	3.26553	1888	3.27600	1933	3.28623	1978	3.29623
1844	3.26576	1889	3.27623	1934	3.28646	1979	3.29645
1845	3.26600	1890	3.27646	1935	3.28668	1980	3.29667

# A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
1981	3.29688	2026	3.30664	2071	3.31618	2116	3.32552
1982	3.29710	2027	3.30685	2072	3.31639	2117	3.32572
1983	3.29732	2028	3.30707	2073	3.31660	2118	3.32593
1984	3.29754	2029	3.30728	2074	3.31681	2119	3.32613
1985	3.29776	2030	3.30750	2075	3.31702	2120	3.32634
1986	3.29798	2031	3.30771	2076	3.31723	2121	3.32654
1987	3.29820	2032	3.30792	2077	3.31744	2122	3.32675
1988	3.29842	2033	3.30814	2078	3.31765	2123	3.32695
1989	3.29863	2034	3.30835	2079	3.31785	2124	3.32715
1990	3.29885	2035	3.30856	2080	3.31806	2125	3.32736
1991	3.29907	2036	3.30878	2081	3.31827	2126	3.32756
1992	3.29929	2037	3.30899	2082	3.31848	2127	3.32777
1993	3.29951	2038	3.30920	2083	3.31869	2128	3.32797
1994	3.29973	2039	3.30942	2084	3.31890	2129	3.32818
1995	3.29994	2040	3.30963	2085	3.31911	2130	3.32838
1996	3.30016	2041	3.30984	2086	3.31931	2131	3.32858
1997	3.30038	2042	3.31006	2087	3.31952	2132	3.32878
1998	3.30060	2043	3.31027	2088	3.31973	2133	3.32899
1999	3.30081	2044	3.31048	2089	3.31994	2134	3.32919
2000	3.30103	2045	3.31069	2090	3.32015	2135	3.32940
2001	3.30125	2046	3.31091	2091	3.32035	2136	3.32960
2002	3.30146	2047	3.31112	2092	3.32056	2137	3.32980
2003	3.30168	2048	3.31133	2093	3.32077	2138	3.33001
2004	3.30190	2049	3.31154	2094	3.32098	2139	3.33021
2005	3.30211	2050	3.31175	2095	3.32118	2140	3.33041
2006	3.30233	2051	3.31197	2096	3.32139	2141	3.33062
2007	3.30255	2052	3.31218	2097	3.32160	2142	3.33082
2008	3.30276	2053	3.31239	2098	3.32181	2143	3.33102
2009	3.30298	2054	3.31260	2099	3.32201	2144	3.33122
2010	3.30320	2055	3.31281	2100	3.32222	2145	3.33143
2011	3.30341	2056	3.31302	2101	3.32243	2146	3.33163
2012	3.30363	2057	3.31323	2102	3.32263	2147	3.33183
2013	3.30384	2058	3.31345	2103	3.32284	2148	3.33203
2014	3.30406	2059	3.31366	2104	3.32305	2149	3.33224
2015	3.30428	2060	3.31387	2105	3.32325	2150	3.33244
2016	3.30449	2061	3.31408	2106	3.32346	2151	3.33264
2017	3.30471	2062	3.31429	2107	3.32366	2152	3.33284
2018	3.30492	2063	3.31450	2108	3.32387	2153	3.33304
2019	3.30514	2064	3.31471	2109	3.32408	2154	3.33325
2020	3.30535	2065	3.31492	2110	3.32428	2155	3.33345
2021	3.30557	2066	3.31513	2111	3.32449	2156	3.33365
2022	3.30578	2067	3.31534	2112	3.32469	2157	3.33385
2023	3.30600	2068	3.31555	2113	3.32490	2158	3.33405
2024	3.30621	2069	3.31576	2114	3.32511	2159	3.33425
2025	3.30643	2070	3.31597	2115	3.32531	2160	3.33445

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
2161	3.33465	2206	3.34361	2251	3.35238	2296	3.36097
2162	3.33486	2207	3.34380	2252	3.35257	2297	3.36116
2163	3.33506	2208	3.34402	2253	3.35276	2298	3.36135
2164	3.33526	2209	3.34420	2254	3.35295	2299	3.36154
2165	3.33546	2210	3.34439	2255	3.35315	2300	3.36173
2166	3.33566	2211	3.34459	2256	3.35334	2301	3.36192
2167	3.33586	2212	3.34479	2257	3.35353	2302	3.36211
2168	3.33605	2213	3.34498	2258	3.35372	2303	3.36229
2169	3.33626	2214	3.34518	2259	3.35392	2304	3.36248
2170	3.33646	2215	3.34537	2260	3.35411	2305	3.36267
2171	3.33666	2216	3.34557	2261	3.35430	2306	3.36286
2172	3.33686	2217	3.34577	2262	3.35449	2307	3.36305
2173	3.33706	2218	3.34596	2263	3.35468	2308	3.36324
2174	3.33726	2219	3.34616	2264	3.35488	2309	3.36342
2175	3.33746	2220	3.34635	2265	3.35507	2310	3.36361
2176	3.33766	2221	3.34655	2266	3.35526	2311	3.36380
2177	3.33786	2222	3.34674	2267	3.35545	2312	3.36399
2178	3.33806	2223	3.34694	2268	3.35564	2313	3.36418
2179	3.33826	2224	3.34713	2269	3.35583	2314	3.36436
2180	3.33846	2225	3.34733	2270	3.35602	2315	3.36455
2181	3.33866	2226	3.34753	2271	3.35622	2316	3.36474
2182	3.33885	2227	3.34772	2272	3.35641	2317	3.36493
2183	3.33905	2228	3.34792	2273	3.35660	2318	3.36511
2184	3.33925	2229	3.34811	2274	3.35679	2319	3.36530
2185	3.33945	2230	3.34830	2275	3.35698	2320	3.36549
2186	3.33965	2231	3.34850	2276	3.35717	2321	3.36568
2187	3.33985	2232	3.34869	2277	3.35737	2322	3.36586
2188	3.34005	2233	3.34889	2278	3.35755	2323	3.36605
2189	3.34025	2234	3.34909	2279	3.35774	2324	3.36624
2190	3.34044	2235	3.34928	2280	3.35793	2325	3.36642
2191	3.34064	2236	3.34947	2281	3.35813	2326	3.36661
2192	3.34084	2237	3.34967	2282	3.35832	2327	3.36680
2193	3.34104	2238	3.34986	2283	3.35851	2328	3.36698
2194	3.34124	2239	3.35005	2284	3.35870	2329	3.36717
2195	3.34143	2240	3.35025	2285	3.35889	2330	3.36736
2196	3.34163	2241	3.35044	2286	3.35908	2331	3.36754
2197	3.34183	2242	3.35064	2287	3.35927	2332	3.36773
2198	3.34203	2243	3.35083	2288	3.35946	2333	3.36791
2199	3.34223	2244	3.35102	2289	3.35965	2334	3.36810
2200	3.34242	2245	3.35122	2290	3.35984	2335	3.36829
2201	3.34262	2246	3.35141	2291	3.36003	2336	3.36847
2202	3.34282	2247	3.35160	2292	3.36021	2337	3.36866
2203	3.34301	2248	3.35180	2293	3.36040	2338	3.36884
2204	3.34321	2249	3.35199	2294	3.36059	2339	3.36903
2205	3.34341	2250	3.35218	2295	3.36078	2340	3.36922

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
2341	3.36940	2386	3.37767	2431	3.38579	2476	3.39375
2342	3.36959	2387	3.37785	2432	3.38596	2477	3.39393
2343	3.36977	2388	3.37803	2433	3.38614	2478	3.39410
2344	3.36996	2389	3.37822	2434	3.38631	2479	3.39428
2345	3.37014	2390	3.37840	2435	3.38650	2480	3.39445
2346	3.37033	2391	3.37858	2436	3.38668	2481	3.39463
2347	3.37051	2392	3.37876	2437	3.38686	2482	3.39480
2348	3.37070	2393	3.37894	2438	3.38703	2483	3.39498
2349	3.37088	2394	3.37912	2439	3.38721	2484	3.39515
2350	3.37107	2395	3.37931	2440	3.38739	2485	3.39533
2351	3.37125	2396	3.37949	2441	3.38757	2486	3.39550
2352	3.37144	2397	3.37967	2442	3.38775	2487	3.39568
2353	3.37162	2398	3.38985	2443	3.38792	2488	3.39585
2354	3.37181	2399	3.38003	2444	3.38810	2489	3.39602
2355	3.37199	2400	3.38021	2445	3.38828	2490	3.39620
2356	3.37217	2401	3.38039	2446	3.38846	2491	3.39637
2357	3.37236	2402	3.38057	2447	3.38863	2492	3.39655
2358	3.37254	2403	3.38075	2448	3.38881	2493	3.39672
2359	3.37273	2404	3.38093	2449	3.38899	2494	3.39690
2360	3.37291	2405	3.38112	2450	3.38917	2495	3.39709
2361	3.37310	2406	3.38130	2451	3.38934	2496	3.39724
2362	3.37328	2407	3.38148	2452	3.38952	2497	3.39741
2363	3.37346	2408	3.38166	2453	3.38970	2498	3.39759
2364	3.37365	2409	3.38184	2454	3.38987	2499	3.39777
2365	3.37383	2410	3.38202	2455	3.39005	2500	3.39794
2366	3.37401	2411	3.38220	2456	3.39023	2501	3.39811
2367	3.37420	2412	3.38238	2457	3.39041	2502	3.39829
2368	3.37438	2413	3.38256	2458	3.39058	2503	3.39846
2369	3.37457	2414	3.38274	2459	3.39076	2504	3.39863
2370	3.37475	2415	3.38292	2460	3.39094	2505	3.39881
2371	3.37493	2416	3.38310	2461	3.39111	2506	3.39898
2372	3.37511	2417	3.38328	2462	3.39129	2507	3.39915
2373	3.37530	2418	3.38346	2463	3.39146	2508	3.39933
2374	3.37548	2419	3.38364	2464	3.39164	2509	3.39950
2375	3.37566	2420	3.38382	2465	3.39182	2510	3.39967
2376	3.37585	2421	3.38399	2466	3.39199	2511	3.39985
2377	3.37603	2422	3.38417	2467	3.39217	2512	3.40002
2378	3.37621	2423	3.38435	2468	3.39235	2513	3.40019
2379	3.37639	2424	3.38453	2469	3.39252	2514	3.40037
2380	3.37658	2425	3.38471	2470	3.39270	2515	3.40054
2381	3.37667	2426	3.38489	2471	3.39287	2516	3.40071
2382	3.37694	2427	3.38507	2472	3.39305	2517	3.40088
2383	3.37712	2428	3.38525	2473	3.39322	2518	3.40106
2384	3.37731	2429	3.38543	2474	3.39340	2519	3.40123
2385	3.37749	2430	3.38561	2475	3.39358	2520	3.40140

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
2521	3.40157	2566	3.40926	2611	3.41681	2656	3.42423
2522	3.40175	2567	3.40943	2612	3.41697	2657	3.42439
2523	3.40192	2568	3.40960	2613	3.41714	2658	3.42456
2524	3.40209	2569	3.40976	2614	3.41731	2659	3.42472
2525	3.40226	2570	3.40993	2615	3.41747	2660	3.42488
2526	3.40243	2571	3.41010	2616	3.41764	2661	3.42504
2527	3.40261	2572	3.41027	2617	3.41780	2662	3.42521
2528	3.40278	2573	3.41044	2618	3.41797	2663	3.42537
2529	3.40297	2574	3.41061	2619	3.41814	2664	3.42553
2530	3.40312	2575	3.41078	2620	3.41830	2665	3.42570
2531	3.40329	2576	3.41095	2621	3.41847	2666	3.42586
2532	3.40346	2577	3.41111	2622	3.41863	2667	3.42602
2533	3.40364	2578	3.41128	2623	3.41880	2668	3.42619
2534	3.40381	2579	3.41145	2624	3.41896	2669	3.42635
2535	3.40398	2580	3.41162	2625	3.41913	2670	3.42651
2536	3.40415	2581	3.41179	2626	3.41929	2671	3.42667
2537	3.40432	2582	3.41196	2627	3.41946	2672	3.42684
2538	3.40449	2583	3.41212	2628	3.41963	2673	3.42700
2539	3.40466	2584	3.41229	2629	3.41979	2674	3.42716
2540	3.40483	2585	3.41246	2630	3.41996	2675	3.42732
2541	3.40500	2586	3.41263	2631	3.42012	2676	3.42749
2542	3.40518	2587	3.41280	2632	3.42029	2677	3.42765
2543	3.40535	2588	3.41296	2633	3.42045	2678	3.42781
2544	3.40552	2589	3.41313	2634	3.42062	2679	3.42797
2545	3.40569	2590	3.41330	2635	3.42078	2680	3.42813
2546	3.40586	2591	3.41347	2636	3.42095	2681	3.42830
2547	3.40603	2592	3.41364	2637	3.42111	2682	3.42846
2548	3.40620	2593	3.41380	2638	3.42127	2683	3.42862
2549	3.40637	2594	3.41397	2639	3.42144	2684	3.42878
2550	3.40654	2595	3.41414	2640	3.42160	2685	3.42894
2551	3.40671	2596	3.41431	2641	3.42177	2686	3.42911
2552	3.40688	2597	3.41447	2642	3.42193	2687	3.42927
2553	3.40705	2598	3.41464	2643	3.42210	2688	3.42943
2554	3.40722	2599	3.41481	2644	3.42226	2689	3.42959
2555	3.40739	2600	3.41497	2645	3.42243	2690	3.42975
2556	3.40756	2601	3.41514	2646	3.42259	2691	3.42991
2557	3.40773	2602	3.41531	2647	3.42275	2692	3.43008
2558	3.40790	2603	3.41547	2648	3.42292	2693	3.43024
2559	3.40807	2604	3.41564	2649	3.42308	2694	3.43040
2560	3.40824	2605	3.41581	2650	3.42325	2695	3.43056
2561	3.40841	2606	3.41597	2651	3.42341	2696	3.43072
2562	3.40858	2607	3.41614	2652	3.42357	2697	3.43088
2563	3.40875	2608	3.41631	2653	3.42374	2698	3.43104
2564	3.40892	2609	3.41647	2654	3.42390	2699	3.43120
2565	3.40909	2610	3.41664	2655	3.42406	2700	3.43136

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
2701	3.43152	2746	3.43870	2791	3.44576	2836	3.45271
2702	3.43169	2747	3.43886	2792	3.44592	2837	3.45286
2703	3.43185	2748	3.43902	2793	3.44607	2838	3.45301
2704	3.43201	2749	3.43917	2794	3.44623	2839	3.45317
2705	3.43217	2750	3.43933	2795	3.44638	2840	3.45322
2706	3.43233	2751	3.43949	2796	3.44654	2841	3.45347
2707	3.43249	2752	3.43965	2797	3.44669	2842	3.45362
2708	3.43265	2753	3.43981	2798	3.44685	2843	3.45378
2709	3.43281	2754	3.43996	2799	3.44700	2844	3.45393
2710	3.43297	2755	3.44012	2800	3.44716	2845	3.45408
2711	3.43313	2756	3.44028	2801	3.44731	2846	3.45423
2712	3.43329	2757	3.44044	2802	3.44747	2847	3.45439
2713	3.43345	2758	3.44059	2803	3.44762	2848	3.45454
2714	3.43361	2759	3.44075	2804	3.44778	2849	3.45469
2715	3.43377	2760	3.44091	2805	3.44793	2850	3.45484
2716	3.43393	2761	3.44107	2806	3.44809	2851	3.45500
2717	3.43409	2762	3.44122	2807	3.44824	2852	3.45515
2718	3.43425	2763	3.44138	2808	3.44840	2853	3.45530
2719	3.43441	2764	3.44154	2809	3.44855	2854	3.45545
2720	3.43457	2765	3.44170	2810	3.44871	2855	3.45561
2721	3.43473	2766	3.44185	2811	3.44886	2856	3.45576
2722	3.43489	2767	3.44201	2812	3.44902	2857	3.45591
2723	3.43505	2768	3.44217	2813	3.44917	2858	3.45606
2724	3.43521	2769	3.44232	2814	3.44932	2859	3.45621
2725	3.43537	2770	3.44248	2815	3.44948	2860	3.45637
2726	3.43553	2771	3.44264	2816	3.44963	2861	3.45652
2727	3.43569	2772	3.44279	2817	3.44979	2862	3.45667
2728	3.43584	2773	3.44295	2818	3.44994	2863	3.45682
2729	3.43600	2774	3.44311	2819	3.45010	2864	3.45697
2730	3.43616	2775	3.44326	2820	3.45025	2865	3.45712
2731	3.43632	2776	3.44342	2821	3.45040	2866	3.45728
2732	3.43648	2777	3.44358	2822	3.45056	2867	3.45743
2733	3.43664	2778	3.44373	2823	3.45071	2868	3.45758
2734	3.43680	2779	3.44389	2824	3.45086	2869	3.45773
2735	3.43696	2780	3.44404	2825	3.45102	2870	3.45788
2736	3.43712	2781	3.44420	2826	3.45117	2871	3.45803
2737	3.43727	2782	3.44436	2827	3.45133	2872	3.45818
2738	3.43743	2783	3.44451	2828	3.45148	2873	3.45834
2739	3.43759	2784	3.44467	2829	3.45163	2874	3.45849
2740	3.43775	2785	3.44483	2830	3.45179	2875	3.45864
2741	3.43791	2786	3.44498	2831	3.45194	2876	3.45879
2742	3.43807	2787	3.44514	2832	3.45209	2877	3.45894
2743	3.43823	2788	3.44529	2833	3.45225	2878	3.45909
2744	3.43838	2789	3.44545	2834	3.45240	2879	3.45924
2745	3.43854	2790	3.44560	2835	3.45255	2880	3.45939

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
2881	3.45954	2926	3.46627	2971	3.47290	3016	3.47943
2882	3.45965	2927	3.46642	2972	3.47305	3017	3.47958
2883	3.45984	2928	3.46657	2973	3.47319	3018	3.47972
2884	3.46000	2929	3.46672	2974	3.47334	3019	3.47986
2885	3.46015	2930	3.46687	2975	3.47349	3020	3.48001
2886	3.46030	2931	3.46702	2976	3.47363	3021	3.48015
2887	3.46045	2932	3.46716	2977	3.47378	3022	3.48029
2888	3.46060	2933	3.46731	2978	3.47392	3023	3.48044
2889	3.46075	2934	3.46746	2979	3.47407	3024	3.48058
2890	3.46090	2935	3.46761	2980	3.47422	3025	3.48073
2891	3.46105	2936	3.46776	2981	3.47436	3026	3.48087
2892	3.46120	2937	3.46790	2982	3.47451	3027	3.48101
2893	3.46135	2938	3.46805	2983	3.47465	3028	3.48116
2894	3.46150	2939	3.46820	2984	3.47480	3029	3.48130
2895	3.46165	2940	3.46835	2985	3.47494	3030	3.48144
2896	3.46180	2941	3.46850	2986	3.47509	3031	3.48159
2897	3.46195	2942	3.46864	2987	3.47524	3032	3.48173
2898	3.46210	2943	3.46879	2988	3.47538	3033	3.48187
2899	3.46225	2944	3.46894	2989	3.47553	3034	3.48201
2900	3.46240	2945	3.46909	2990	3.47567	3035	3.48216
2901	3.46255	2946	3.46923	2991	3.47582	3036	3.48230
2902	3.46270	2947	3.46938	2992	3.47596	3037	3.48244
2903	3.46285	2948	3.46953	2993	3.47611	3038	3.48259
2904	3.46300	2949	3.46967	2994	3.47625	3039	3.48273
2905	3.46315	2950	3.46982	2995	3.47640	3040	3.48287
2906	3.46330	2951	3.46997	2996	3.47654	3041	3.48302
2907	3.46345	2952	3.47012	2997	3.47669	3042	3.48316
2908	3.46360	2953	3.47026	2998	3.47683	3043	3.48330
2909	3.46374	2954	3.47041	2999	3.47698	3044	3.48344
2910	3.46389	2955	3.47056	3000	3.47712	3045	3.48359
2911	3.46404	2956	3.47070	3001	3.47727	3046	3.48373
2912	3.46419	2957	3.47085	3002	3.47741	3047	3.48387
2913	3.46434	2958	3.47100	3003	3.47756	3048	3.48402
2914	3.46449	2959	3.47115	3004	3.47770	3049	3.48416
2915	3.46464	2960	3.47129	3005	3.47784	3050	3.48430
2916	3.46479	2961	3.47144	3006	3.47799	3051	3.48444
2917	3.46494	2962	3.47159	3007	3.47813	3052	3.48458
2918	3.46509	2963	3.47173	3008	3.47828	3053	3.48473
2919	3.46523	2964	3.47188	3009	3.47842	3054	3.48487
2920	3.46538	2965	3.47202	3010	3.47857	3055	3.48501
2921	3.46553	2966	3.47217	3011	3.47871	3056	3.48515
2922	3.46568	2967	3.47232	3012	3.47886	3057	3.48530
2923	3.46583	2968	3.47246	3013	3.47900	3058	3.48544
2924	3.46598	2969	3.47261	3014	3.47914	3059	3.48558
2925	3.46613	2970	3.47276	3015	3.47929	3060	3.48572

# A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
3061	3.48586	3106	3.49220	3151	3.49845	3196	3.50461
3062	3.48601	3107	3.49234	3152	3.49859	3197	3.50474
3063	3.48615	3108	3.49248	3153	3.49872	3198	3.50488
3064	3.48629	3109	3.49262	3154	3.49886	3199	3.50501
3065	3.48643	3110	3.49276	3155	3.49900	3200	3.50515
3066	3.48657	3111	3.49290	3156	3.49914	3201	3.50529
3067	3.48671	3112	3.49304	3157	3.49927	3202	3.50542
3068	3.48686	3113	3.49318	3158	3.49941	3203	3.50556
3069	3.48700	3114	3.49332	3159	3.49955	3204	3.50569
3070	3.48714	3115	3.49346	3160	3.49969	3205	3.50583
3071	3.48728	3116	3.49360	3161	3.49982	3206	3.50596
3072	3.48742	3117	3.49374	3162	3.49996	3207	3.50610
3073	3.48756	3118	3.49388	3163	3.50010	3208	3.50623
3074	3.48770	3119	3.49402	3164	3.50024	3209	3.50637
3075	3.48785	3120	3.49415	3165	3.50037	3210	3.50651
3076	3.48799	3121	3.49429	3166	3.50051	3211	3.50664
3077	3.48813	3122	3.49443	3167	3.50065	3212	3.50678
3078	3.48827	3123	3.49457	3168	3.50079	3213	3.50691
3079	3.48841	3124	3.49471	3169	3.50092	3214	3.50705
3080	3.48855	3125	3.49485	3170	3.50106	3215	3.50718
3081	3.48869	3126	3.49499	3171	3.50120	3216	3.50732
3082	3.48883	3127	3.49513	3172	3.50133	3217	3.50745
3083	3.48897	3128	3.49527	3173	3.50147	3218	3.50759
3084	3.48911	3129	3.49541	3174	3.50161	3219	3.50772
3085	3.48926	3130	3.49554	3175	3.50174	3220	3.50786
3086	3.48940	3131	3.49568	3176	3.50188	3221	3.50799
3087	3.48954	3132	3.49582	3177	3.50202	3222	3.50813
3088	3.48968	3133	3.49596	3178	3.50215	3223	3.50826
3089	3.48982	3134	3.49610	3179	3.50229	3224	3.50840
3090	3.48996	3135	3.49624	3180	3.50243	3225	3.50853
3091	3.49010	3136	3.49638	3181	3.50256	3226	3.50866
3092	3.49024	3137	3.49651	3182	3.50270	3227	3.50880
3093	3.49038	3138	3.49665	3183	3.50284	3228	3.50893
3094	3.49052	3139	3.49679	3184	3.50297	3229	3.50907
3095	3.49066	3140	3.49693	3185	3.50311	3230	3.50920
3096	3.49080	3141	3.49707	3186	3.50325	3231	3.50934
3097	3.49094	3142	3.49721	3187	3.50338	3232	3.50948
3098	3.49108	3143	3.49734	3188	3.50352	3233	3.50961
3099	3.49122	3144	3.49748	3189	3.50365	3234	3.50974
3100	3.49136	3145	3.49762	3190	3.50379	3235	3.50987
3101	3.49150	3146	3.49776	3191	3.50393	3236	3.51001
3102	3.49164	3147	3.49790	3192	3.50406	3237	3.51014
3103	3.49178	3148	3.49803	3193	3.50420	3238	3.51028
3104	3.49192	3149	3.49817	3194	3.50433	3239	3.51041
3105	3.49206	3150	3.49831	3195	3.50447	3240	3.51055

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
3241	3.51068	3286	3.51667	3331	3.52257	3376	3.52840
3242	3.51081	3287	3.51680	3332	3.52271	3377	3.52853
3243	3.51095	3288	3.51693	3333	3.52284	3378	3.52866
3244	3.51108	3289	3.51706	3334	3.52297	3379	3.52879
3245	3.51121	3290	3.51720	3335	3.52310	3380	3.52892
3246	3.51135	3291	3.51733	3336	3.52323	3381	3.52905
3247	3.51148	3292	3.51746	3337	3.52336	3382	3.52917
3248	3.51162	3293	3.51759	3338	3.52349	3383	3.52930
3249	3.51175	3294	3.51772	3339	3.52362	3384	3.52943
3250	3.51188	3295	3.51786	3340	3.52375	3385	3.52956
3251	3.51202	3296	3.51799	3341	3.52388	3386	3.52969
3252	3.51215	3297	3.51812	3342	3.52401	3387	3.52982
3253	3.51228	3298	3.51825	3343	3.52414	3388	3.52994
3254	3.51242	3299	3.51838	3344	3.52427	3389	3.53007
3255	3.51255	3300	3.51851	3345	3.52440	3390	3.53020
3256	3.51268	3301	3.51865	3346	3.52453	3391	3.53033
3257	3.51282	3302	3.51878	3347	3.52466	3392	3.53046
3258	3.51295	3303	3.51891	3348	3.52479	3393	3.53058
3259	3.51308	3304	3.51904	3349	3.52492	3394	3.53071
3260	3.51322	3305	3.51917	3350	3.52504	3395	3.53084
3261	3.51335	3306	3.51930	3351	3.52517	3396	3.53097
3262	3.51348	3307	3.51943	3352	3.52530	3397	3.53110
3263	3.51362	3308	3.51957	3353	3.52543	3398	3.53122
3264	3.51375	3309	3.51970	3354	3.52556	3399	3.53135
3265	3.51388	3310	3.51983	3355	3.52569	3400	3.53148
3266	3.51402	3311	3.51996	3356	3.52582	3401	3.53161
3267	3.51415	3312	3.52009	3357	3.52595	3402	3.53173
3268	3.51428	3313	3.52022	3358	3.52608	3403	3.53186
3269	3.51441	3314	3.52035	3359	3.52621	3404	3.53199
3270	3.51455	3315	3.52048	3360	3.52634	3405	3.53212
3271	3.51468	3316	3.52061	3361	3.52647	3406	3.53224
3272	3.51481	3317	3.52075	3362	3.52660	3407	3.53237
3273	3.51495	3318	3.52088	3363	3.52673	3408	3.53250
3274	3.51508	3319	3.52101	3364	3.52686	3409	3.53263
3275	3.51521	3320	3.52114	3365	3.52699	3410	3.53275
3276	3.51534	3321	3.52127	3366	3.52711	3411	3.53288
3277	3.51548	3322	3.52140	3367	3.52724	3412	3.53301
3278	3.51561	3323	3.52153	3368	3.52737	3413	3.53314
3279	3.51574	3324	3.52166	3369	3.52750	3414	3.53326
3280	3.51587	3325	3.52179	3370	3.52763	3415	3.53339
3281	3.51601	3326	3.52192	3371	3.52776	3416	3.53352
3282	3.51614	3327	3.52205	3372	3.52789	3417	3.53365
3283	3.51627	3328	3.52218	3373	3.52802	3418	3.53377
3284	3.51640	3329	3.52231	3374	3.52815	3419	3.53390
3285	3.51654	3330	3.52244	3375	3.52827	3420	3.53403

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
3421	3.53415	3466	3.53983	3511	3.54543	3556	3.55096
3422	3.53428	3467	3.53995	3512	3.54555	3557	3.55108
3423	3.53441	3468	3.54008	3513	3.54568	3558	3.55121
3424	3.53453	3469	3.54020	3514	3.54580	3559	3.55133
3425	3.53466	3470	3.54033	3515	3.54593	3560	3.55145
3426	3.53479	3471	3.54045	3516	3.54605	3561	3.55157
3427	3.53491	3472	3.54058	3517	3.54617	3562	3.55169
3428	3.53504	3473	3.54070	3518	3.54630	3563	3.55182
3429	3.53517	3474	3.54083	3519	3.54642	3564	3.55194
3430	3.53529	3475	3.54095	3520	3.54654	3565	3.55206
3431	3.53542	3476	3.54108	3521	3.54667	3566	3.55218
3432	3.53555	3477	3.54120	3522	3.54679	3567	3.55230
3433	3.53567	3478	3.54133	3523	3.54691	3568	3.55242
3434	3.53580	3479	3.54145	3524	3.54704	3569	3.55255
3435	3.53593	3480	3.54158	3525	3.54716	3570	3.55267
3436	3.53605	3481	3.54170	3526	3.54728	3571	3.55279
3437	3.53618	3482	3.54183	3527	3.54741	3572	3.55291
3438	3.53631	3483	3.54195	3528	3.54753	3573	3.55303
3439	3.53643	3484	3.54208	3529	3.54765	3574	3.55315
3440	3.53656	3485	3.54220	3530	3.54777	3575	3.55328
3441	3.53668	3486	3.54233	3531	3.54790	3576	3.55340
3442	3.53681	3487	3.54245	3532	3.54802	3577	3.55352
3443	3.53694	3488	3.54258	3533	3.54814	3578	3.55364
3444	3.53706	3489	3.54270	3534	3.54827	3579	3.55376
3445	3.53719	3490	3.54283	3535	3.54839	3580	3.55388
3446	3.53732	3491	3.54295	3536	3.54851	3581	3.55400
3447	3.53744	3492	3.54307	3537	3.54864	3582	3.55413
3448	3.53757	3493	3.54320	3538	3.54876	3583	3.55425
3449	3.53769	3494	3.54332	3539	3.54888	3584	3.55437
3450	3.53782	3495	3.54345	3540	3.54900	3585	3.55449
3451	3.53795	3496	3.54357	3541	3.54913	3586	3.55461
3452	3.53807	3497	3.54370	3542	3.54925	3587	3.55473
3453	3.53820	3498	3.54382	3543	3.54937	3588	3.55485
3454	3.53832	3499	3.54394	3544	3.54949	3589	3.55497
3455	3.53845	3500	3.54407	3545	3.54962	3590	3.55509
3456	3.53857	3501	3.54419	3546	3.54974	3591	3.55522
3457	3.53870	3502	3.54432	3547	3.54986	3592	3.55534
3458	3.53883	3503	3.54444	3548	3.54998	3593	3.55546
3459	3.53895	3504	3.54456	3549	3.55011	3594	3.55558
3460	3.53908	3505	3.54469	3550	3.55023	3595	3.55570
3461	3.53920	3506	3.54481	3551	3.55035	3596	3.55582
3462	3.53933	3507	3.54494	3552	3.55047	3597	3.55594
3463	3.53945	3508	3.54506	3553	3.55060	3598	3.55606
3464	3.53958	3509	3.54518	3554	3.55072	3599	3.55618
3465	3.53970	3510	3.54531	3555	3.55084	3600	3.55630

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
3601	3.55642	3646	3.56182	3691	3.56714	3736	3.57241
3602	3.55654	3647	3.56194	3692	3.56726	3737	3.57252
3603	3.55666	3648	3.56205	3693	3.56738	3738	3.57264
3604	3.55678	3649	3.56217	3694	3.56750	3739	3.57276
3605	3.55691	3650	3.56229	3695	3.56761	3740	3.57287
3606	3.55703	3651	3.56241	3696	3.56773	3741	3.57299
3607	3.55715	3652	3.56253	3697	3.56785	3742	3.57310
3608	3.55727	3653	3.56265	3698	3.56797	3743	3.57322
3609	3.55739	3654	3.56277	3699	3.56808	3744	3.57334
3610	3.55751	3655	3.56289	3700	3.56820	3745	3.57345
3611	3.55763	3656	3.56301	3701	3.56832	3746	3.57357
3612	3.55775	3657	3.56313	3702	3.56844	3747	3.57368
3613	3.55787	3658	3.56324	3703	3.56855	3748	3.57380
3614	3.55799	3659	3.56336	3704	3.56867	3749	3.57392
3615	3.55811	3660	3.56348	3705	3.56875	3750	3.57403
3616	3.55823	3661	3.56360	3706	3.56891	3751	3.57415
3617	3.55835	3662	3.56372	3707	3.56902	3752	3.57426
3618	3.55847	3663	3.56384	3708	3.56914	3753	3.57438
3619	3.55859	3664	3.56396	3709	3.56926	3754	3.57449
3620	3.55871	3665	3.56407	3710	3.56937	3755	3.57461
3621	3.55883	3666	3.56419	3711	3.56949	3756	3.57473
3622	3.55895	3667	3.56431	3712	3.56961	3757	3.57484
3623	3.55907	3668	3.56443	3713	3.56972	3758	3.57496
3624	3.55919	3669	3.56455	3714	3.56984	3759	3.57507
3625	3.55931	3670	3.56467	3715	3.56996	3760	3.57519
3626	3.55943	3671	3.56478	3716	3.57008	3761	3.57530
3627	3.55955	3672	3.56490	3717	3.57019	3762	3.57542
3628	3.55967	3673	3.56502	3718	3.57031	3763	3.57553
3629	3.55979	3674	3.56514	3719	3.57043	3764	3.57565
3630	3.55991	3675	3.56526	3720	3.57055	3765	3.57577
3631	3.56003	3676	3.56538	3721	3.57066	3766	3.57588
3632	3.56015	3677	3.56549	3722	3.57078	3767	3.57600
3633	3.56026	3678	3.56561	3723	3.57089	3768	3.57611
3634	3.56038	3679	3.56573	3724	3.57101	3769	3.57623
3635	3.56050	3680	3.56585	3725	3.57113	3770	3.57634
3636	3.56062	3681	3.56597	3726	3.57124	3771	3.57646
3637	3.56074	3682	3.56608	3727	3.57136	3772	3.57657
3638	3.56086	3683	3.56620	3728	3.57148	3773	3.57669
3639	3.56098	3684	3.56632	3729	3.57159	3774	3.57680
3640	3.56110	3685	3.56644	3730	3.57171	3775	3.57692
3641	3.56122	3686	3.56656	3731	3.57183	3776	3.57703
3642	3.56134	3687	3.56667	3732	3.57194	3777	3.57715
3643	3.56146	3688	3.56679	3733	3.57206	3778	3.57726
3644	3.56158	3689	3.56691	3734	3.57217	3779	3.57738
3645	3.56170	3690	3.56703	3735	3.57229	3780	3.57749

*A Table of Logarithms.*

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N	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
3781	3.57761	3826	3.58275	3871	3.58782	3916	3.59284
3782	3.57772	3827	3.58286	3872	3.58796	3917	3.59295
3783	3.57784	3828	3.58297	3873	3.58805	3918	3.59306
3784	3.57795	3829	3.58309	3874	3.58816	3919	3.59318
3785	3.57807	3830	3.58320	3875	3.58827	3920	3.59329
3786	3.57818	3831	3.58331	3876	3.58838	3921	3.59340
3787	3.57830	3832	3.58343	3877	3.58850	3922	3.59351
3788	3.57841	3833	3.58354	3878	3.58861	3923	3.59362
3789	3.57852	3834	3.58365	3879	3.58872	3924	3.59373
3790	3.57864	3835	3.58377	3880	3.58883	3925	3.59384
3791	3.57875	3836	3.58388	3881	3.58894	3926	3.59395
3792	3.57887	3837	3.58399	3882	3.58906	3927	3.59406
3793	3.57898	3838	3.58411	3883	3.58917	3928	3.59417
3794	3.57910	3839	3.58422	3884	3.58928	3929	3.59428
3795	3.57921	3840	3.58433	3885	3.58939	3930	3.59439
3796	3.57933	3841	3.58444	3886	3.58950	3931	3.59450
3797	3.57944	3842	3.58456	3887	3.58961	3932	3.59461
3798	3.57956	3843	3.58467	3888	3.58972	3933	3.59472
3799	3.57967	3844	3.58478	3889	3.58984	3934	3.59483
3800	3.57978	3845	3.58490	3890	3.58995	3935	3.59494
3801	3.57990	3846	3.58501	3891	3.59006	3936	3.59506
3802	3.58001	3847	3.58512	3892	3.59017	3937	3.59517
3803	3.58013	3848	3.58524	3893	3.59028	3938	3.59528
3804	3.58024	3849	3.58535	3894	3.59040	3939	3.59539
3805	3.58035	3850	3.58546	3895	3.59051	3940	3.59550
3806	3.58047	3851	3.58557	3896	3.59062	3941	3.59561
3807	3.58058	3852	3.58569	3897	3.59073	3942	3.59572
3808	3.58070	3853	3.58580	3898	3.59084	3943	3.59583
3809	3.58081	3854	3.58591	3899	3.59095	3944	3.59594
3810	3.58093	3855	3.58602	3900	3.59106	3945	3.59605
3811	3.58104	3856	3.58614	3901	3.59118	3946	3.59616
3812	3.58115	3857	3.58625	3902	3.59129	3947	3.59627
3813	3.58127	3858	3.58636	3903	3.59140	3948	3.59638
3814	3.58138	3859	3.58647	3904	3.59151	3949	3.59649
3815	3.58149	3860	3.58659	3905	3.59162	3950	3.59660
3816	3.58161	3861	3.58670	3906	3.59173	3951	3.59671
3817	3.58172	3862	3.58681	3907	3.59184	3952	3.59682
3818	3.58184	3863	3.58692	3908	3.59195	3953	3.59693
3819	3.58195	3864	3.58704	3909	3.59207	3954	3.59704
3820	3.58206	3865	3.58715	3910	3.59218	3955	3.59715
3821	3.58218	3866	3.58726	3911	3.59229	3956	3.59726
3822	3.58229	3867	3.58737	3912	3.59240	3957	3.59737
3823	3.58240	3868	3.58749	3913	3.59251	3958	3.59748
3824	3.58252	3869	3.58760	3914	3.59262	3959	3.59759
3825	3.58263	3870	3.58771	3915	3.59273	3960	3.59770

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
3961	3.59780	4006	3.60271	4051	3.60756	4096	3.61236
3962	3.59791	4007	3.60282	4052	3.60767	4097	3.61247
3963	3.59802	4008	3.60293	4053	3.60778	4098	3.61257
3964	3.59813	4009	3.60304	4054	3.60789	4099	3.61268
3965	3.59824	4010	3.60315	4055	3.60799	4100	3.61278
3966	3.59835	4011	3.60325	4056	3.60810	4101	3.61289
3967	3.59846	4012	3.60336	4057	3.60821	4102	3.61300
3968	3.59857	4013	3.60347	4058	3.60831	4103	3.61310
3969	3.59868	4014	3.60358	4059	3.60842	4104	3.61321
3970	3.59879	4015	3.60369	4060	3.60853	4105	3.61331
3971	3.59890	4016	3.60379	4061	3.60863	4106	3.61342
3972	3.59901	4017	3.60390	4062	3.60874	4107	3.61352
3973	3.59912	4018	3.60401	4063	3.60885	4108	3.61363
3974	3.59923	4019	3.60412	4064	3.60895	4109	3.61374
3975	3.59934	4020	3.60423	4065	3.60906	4110	3.61384
3976	3.59945	4021	3.60433	4066	3.60917	4111	3.61395
3977	3.59956	4022	3.60444	4067	3.60927	4112	3.61405
3978	3.59967	4023	3.60455	4068	3.60938	4113	3.61416
3979	3.59977	4024	3.60466	4069	3.60949	4114	3.61426
3980	3.59988	4025	3.60477	4070	3.60959	4115	3.61437
3981	3.59999	4026	3.60487	4071	3.60970	4116	3.61448
3982	3.60001	4027	3.60498	4072	3.60981	4117	3.61458
3983	3.60002	4028	3.60509	4073	3.60991	4118	3.61469
3984	3.60003	4029	3.60520	4074	3.61002	4119	3.61479
3985	3.60004	4030	3.60531	4075	3.61013	4120	3.61490
3986	3.60005	4031	3.60541	4076	3.61023	4121	3.61500
3987	3.60006	4032	3.60552	4077	3.61034	4122	3.61511
3988	3.60007	4033	3.60563	4078	3.61045	4123	3.61521
3989	3.60008	4034	3.60574	4079	3.61055	4124	3.61532
3990	3.60009	4035	3.60584	4080	3.61066	4125	3.61542
3991	3.60108	4036	3.60595	4081	3.61077	4126	3.61553
3992	3.60119	4037	3.60606	4082	3.61087	4127	3.61563
3993	3.60130	4038	3.60617	4083	3.61098	4128	3.61574
3994	3.60141	4039	3.60627	4084	3.61109	4129	3.61584
3995	3.60152	4040	3.60638	4085	3.61119	4130	3.61595
3996	3.60163	4041	3.60649	4086	3.61130	4131	3.61606
3997	3.60173	4042	3.60660	4087	3.61140	4132	3.61616
3998	3.60184	4043	3.60670	4088	3.61151	4133	3.61627
3999	3.60195	4044	3.60681	4089	3.61162	4134	3.61637
4000	3.60206	4045	3.60692	4090	3.61172	4135	3.61648
4001	3.60217	4046	3.60703	4091	3.61183	4136	3.61658
4002	3.60228	4047	3.60713	4092	3.61194	4137	3.61669
4003	3.60239	4048	3.60724	4093	3.61204	4138	3.61679
4004	3.60249	4049	3.60735	4094	3.61215	4139	3.61690
4005	3.60260	4050	3.60746	4095	3.61226	4140	3.61701

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
4141	3.61711	4186	3.62180	4231	3.62644	4276	3.63204
4142	3.61721	4187	3.62190	4232	3.62655	4277	3.63114
4143	3.61731	4188	3.62201	4233	3.62665	4278	3.63124
4144	3.61742	4189	3.62211	4234	3.62675	4279	3.63134
4145	3.61752	4190	3.62221	4235	3.62685	4280	3.63144
4146	3.61763	4191	3.62232	4236	3.62696	4281	3.63155
4147	3.61773	4192	3.62242	4237	3.62706	4282	3.63165
4148	3.61784	4193	3.62252	4238	3.62716	4283	3.63175
4149	3.61794	4194	3.62263	4239	3.62726	4284	3.63185
4150	3.61805	4195	3.62273	4240	3.62737	4285	3.63195
4151	3.61815	4196	3.62284	4241	3.62747	4286	3.63205
4152	3.61826	4197	3.62294	4242	3.62757	4287	3.63215
4153	3.61836	4198	3.62304	4243	3.62767	4288	3.63225
4154	3.61847	4199	3.62315	4244	3.62778	4289	3.63236
4155	3.61857	4200	3.62325	4245	3.62788	4290	3.63246
4156	3.61868	4201	3.62335	4246	3.62798	4291	3.63256
4157	3.61878	4202	3.62346	4247	3.62808	4292	3.63266
4158	3.61888	4203	3.62356	4248	3.62818	4293	3.63276
4159	3.61899	4204	3.62366	4249	3.62828	4294	3.63286
4160	3.61909	4205	3.62377	4250	3.62839	4295	3.63296
4161	3.61920	4206	3.62387	4251	3.62849	4296	3.63306
4162	3.61930	4207	3.62397	4252	3.62859	4297	3.63317
4163	3.61941	4208	3.62408	4253	3.62870	4298	3.63327
4164	3.61951	4209	3.62418	4254	3.62880	4299	3.63337
4165	3.61962	4210	3.62428	4255	3.62890	4300	3.63347
4166	3.61972	4211	3.62439	4256	3.62900	4301	3.63357
4167	3.61982	4212	3.62449	4257	3.62910	4302	3.63367
4168	3.61993	4213	3.62459	4258	3.62921	4303	3.63377
4169	3.62003	4214	3.62469	4259	3.62931	4304	3.63387
4170	3.62014	4215	3.62480	4260	3.62941	4305	3.63397
4171	3.62024	4216	3.62490	4261	3.62951	4306	3.63407
4172	3.62034	4217	3.62500	4262	3.62961	4307	3.63417
4173	3.62045	4218	3.62511	4263	3.62972	4308	3.63428
4174	3.62055	4219	3.62521	4264	3.62982	4309	3.63438
4175	3.62066	4220	3.62531	4265	3.62992	4310	3.63448
4176	3.62076	4221	3.62542	4266	3.63002	4311	3.63458
4177	3.62086	4222	3.62552	4267	3.63012	4312	3.63468
4178	3.62097	4223	3.62562	4268	3.63022	4313	3.63478
4179	3.62107	4224	3.62572	4269	3.63033	4314	3.63488
4180	3.62118	4225	3.62583	4270	3.63043	4315	3.63498
4181	3.62128	4226	3.62593	4271	3.63053	4316	3.63508
4182	3.62138	4227	3.62603	4272	3.63063	4317	3.63518
4183	3.62149	4228	3.62614	4273	3.63073	4318	3.63528
4184	3.62159	4229	3.62624	4274	3.63083	4319	3.63538
4185	3.62170	4230	3.62634	4275	3.63094	4320	3.63548

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
4321	3.63558	4366	3.64008	4411	3.64454	4456	3.64895
4322	3.63568	4367	3.64018	4412	3.64464	4457	3.64904
4323	3.63579	4368	3.64028	4413	3.64473	4458	3.64914
4324	3.63589	4369	3.64038	4414	3.64483	4459	3.64924
4325	3.63599	4370	3.64048	4415	3.64493	4460	3.64933
4326	3.63609	4371	3.64058	4416	3.64503	4461	3.64943
4327	3.63619	4372	3.64068	4417	3.64513	4462	3.64953
4328	3.63629	4373	3.64078	4418	3.64523	4463	3.64963
4329	3.63639	4374	3.64088	4419	3.64532	4464	3.64972
4330	3.63649	4375	3.64098	4420	3.64542	4465	3.64982
4331	3.63659	4376	3.64108	4421	3.64552	4466	3.64992
4332	3.63669	4377	3.64118	4422	3.64562	4467	3.65002
4333	3.63679	4378	3.64128	4423	3.64572	4468	3.65011
4334	3.63689	4379	3.64137	4424	3.64582	4469	3.65021
4335	3.63699	4380	3.64147	4425	3.64591	4470	3.65031
4336	3.63709	4381	3.64157	4426	3.64601	4471	3.65040
4337	3.63719	4382	3.64167	4427	3.64611	4472	3.65050
4338	3.63729	4383	3.64177	4428	3.64621	4473	3.65060
4339	3.63739	4384	3.64187	4429	3.64631	4474	3.65070
4340	3.63749	4385	3.64197	4430	3.64640	4475	3.65079
4341	3.63759	4386	3.64207	4431	3.64650	4476	3.65089
4342	3.63769	4387	3.64217	4432	3.64660	4477	3.65099
4343	3.63779	4388	3.64227	4433	3.64670	4478	3.65108
4344	3.63789	4389	3.64237	4434	3.64680	4479	3.65118
4345	3.63799	4390	3.64246	4435	3.64689	4480	3.65128
4346	3.63809	4391	3.64256	4436	3.64699	4481	3.65137
4347	3.63819	4392	3.64266	4437	3.64709	4482	3.65147
4348	3.63829	4393	3.64276	4438	3.64719	4483	3.65157
4349	3.63839	4394	3.64286	4439	3.64729	4484	3.65167
4350	3.63849	4395	3.64296	4440	3.64738	4485	3.65176
4351	3.63859	4396	3.64306	4441	3.64748	4486	3.65186
4352	3.63869	4397	3.64316	4442	3.64758	4487	3.65196
4353	3.63879	4398	3.64326	4443	3.64768	4488	3.65205
4354	3.63889	4399	3.64335	4444	3.64777	4489	3.65215
4355	3.63899	4400	3.64345	4445	3.64787	4490	3.65225
4356	3.63909	4401	3.64355	4446	3.64797	4491	3.65234
4357	3.63919	4402	3.64365	4447	3.64807	4492	3.65244
4358	3.63929	4403	3.64375	4448	3.64816	4493	3.65254
4359	3.63939	4404	3.64385	4449	3.64826	4494	3.65263
4360	3.63949	4405	3.64395	4450	3.64836	4495	3.65273
4361	3.63959	4406	3.64404	4451	3.64846	4496	3.65283
4362	3.63969	4407	3.64414	4452	3.64856	4497	3.65292
4363	3.63979	4408	3.64424	4453	3.64865	4498	3.65302
4364	3.63988	4409	3.64434	4454	3.64875	4499	3.65312
4365	3.63998	4410	3.64444	4455	3.64885	4500	3.65321

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
4501	3.65331	4546	3.65763	4591	3.66191	4636	3.66614
4502	3.65341	4547	3.65773	4592	3.66200	4637	3.66624
4503	3.65350	4548	3.65782	4593	3.66210	4638	3.66633
4504	3.65360	4549	3.65792	4594	3.66219	4639	3.66642
4505	3.65369	4550	3.65801	4595	3.66229	4640	3.66651
4506	3.65379	4551	3.65811	4596	3.66238	4641	3.66661
4507	3.65389	4552	3.65820	4597	3.66247	4642	3.66671
4508	3.65398	4553	3.65830	4598	3.66257	4643	3.66680
4509	3.65408	4554	3.65839	4599	3.66266	4644	3.66689
4510	3.65418	4555	3.65849	4600	3.66276	4645	3.66699
4511	3.65427	4556	3.65858	4601	3.66285	4646	3.66708
4512	3.65437	4557	3.65868	4602	3.66295	4647	3.66717
4513	3.65447	4558	3.65877	4603	3.66304	4648	3.66727
4514	3.65456	4559	3.65887	4604	3.66314	4649	3.66736
4515	3.65466	4560	3.65896	4605	3.66323	4650	3.66745
4516	3.65475	4561	3.65906	4606	3.66332	4651	3.66755
4517	3.65485	4562	3.65916	4607	3.66342	4652	3.66764
4518	3.65495	4563	3.65925	4608	3.66351	4653	3.66773
4519	3.65504	4564	3.65935	4609	3.66361	4654	3.66783
4520	3.65514	4565	3.65944	4610	3.66370	4655	3.66792
4521	3.65523	4566	3.65954	4611	3.66380	4656	3.66801
4522	3.65533	4567	3.65963	4612	3.66389	4657	3.66811
4523	3.65543	4568	3.65973	4613	3.66398	4658	3.66820
4524	3.65552	4569	3.65982	4614	3.66408	4659	3.66829
4525	3.65562	4570	3.65992	4615	3.66417	4660	3.66839
4526	3.65571	4571	3.66001	4616	3.66427	4661	3.66848
4527	3.65581	4572	3.66011	4617	3.66436	4662	3.66857
4528	3.65591	4573	3.66020	4618	3.66445	4663	3.66867
4529	3.65600	4574	3.66030	4619	3.66455	4664	3.66876
4530	3.65610	4575	3.66039	4620	3.66464	4665	3.66885
4531	3.65619	4576	3.66049	4621	3.66474	4666	3.66894
4532	3.65629	4577	3.66058	4622	3.66483	4667	3.66904
4533	3.65639	4578	3.66068	4623	3.66492	4668	3.66913
4534	3.65648	4579	3.66077	4624	3.66502	4669	3.66922
4535	3.65658	4580	3.66087	4625	3.66511	4670	3.66932
4536	3.65667	4581	3.66096	4626	3.66521	4671	3.66941
4537	3.65677	4582	3.66106	4627	3.66530	4672	3.66950
4538	3.65686	4583	3.66115	4628	3.66539	4673	3.66960
4539	3.65696	4584	3.66124	4629	3.66549	4674	3.66969
4540	3.65706	4585	3.66134	4630	3.66558	4675	3.66978
4541	3.65715	4586	3.66143	4631	3.66567	4676	3.66987
4542	3.65725	4587	3.66153	4632	3.66577	4677	3.66997
4543	3.65734	4588	3.66162	4633	3.66586	4678	3.67006
4544	3.65744	4589	3.66172	4634	3.66596	4679	3.67015
4545	3.65753	4590	3.66181	4635	3.66605	4680	3.67025

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
4681	3.67034	4726	3.67449	4771	3.67861	4816	3.68269
4682	3.67043	4727	3.67459	4772	3.67870	4817	3.68278
4683	3.67052	4728	3.67468	4773	3.67879	4818	3.68287
4684	3.67062	4729	3.67477	4774	3.67888	4819	3.68296
4685	3.67071	4730	3.67486	4775	3.67897	4820	3.68305
4686	3.67080	4731	3.67495	4776	3.67906	4821	3.68314
4687	3.67090	4732	3.67504	4777	3.67916	4822	3.68323
4688	3.67099	4733	3.67514	4778	3.67925	4823	3.68332
4689	3.67108	4734	3.67523	4779	3.67934	4824	3.68341
4690	3.67117	4735	3.67532	4780	3.67943	4825	3.68350
4691	3.67127	4736	3.67541	4781	3.67952	4826	3.68359
4692	3.67136	4737	3.67550	4782	3.67961	4827	3.68368
4693	3.67145	4738	3.67560	4783	3.67970	4828	3.68377
4694	3.67154	4739	3.67569	4784	3.67979	4829	3.68386
4695	3.67164	4740	3.67578	4785	3.67988	4830	3.68395
4696	3.67173	4741	3.67587	4786	3.67997	4831	3.68404
4697	3.67182	4742	3.67596	4787	3.68006	4832	3.68413
4698	3.67191	4743	3.67605	4788	3.68015	4833	3.68422
4699	3.67201	4744	3.67614	4789	3.68024	4834	3.68431
4700	3.67210	4745	3.67624	4790	3.68034	4835	3.68440
4701	3.67219	4746	3.67633	4791	3.68043	4836	3.68449
4702	3.67228	4747	3.67642	4792	3.68052	4837	3.68458
4703	3.67238	4748	3.67651	4793	3.68061	4838	3.68467
4704	3.67247	4749	3.67660	4794	3.68070	4839	3.68476
4705	3.67256	4750	3.67669	4795	3.68079	4840	3.68485
4706	3.67265	4751	3.67679	4796	3.68088	4841	3.68494
4707	3.67274	4752	3.67688	4797	3.68097	4842	3.68502
4708	3.67284	4753	3.67697	4798	3.68106	4843	3.68511
4709	3.67293	4754	3.67706	4799	3.68115	4844	3.68520
4710	3.67302	4755	3.67715	4800	3.68124	4845	3.68529
4711	3.67311	4756	3.67724	4801	3.68133	4846	3.68538
4712	3.67321	4757	3.67733	4802	3.68142	4847	3.68547
4713	3.67330	4758	3.67742	4803	3.68151	4848	3.68556
4714	3.67339	4759	3.67752	4804	3.68160	4849	3.68565
4715	3.67348	4760	3.67761	4805	3.68169	4850	3.68574
4716	3.67357	4761	3.67770	4806	3.68178	4851	3.68583
4717	3.67367	4762	3.67778	4807	3.68187	4852	3.68592
4718	3.67376	4763	3.67788	4808	3.68196	4853	3.68601
4719	3.67385	4764	3.67797	4809	3.68205	4854	3.68610
4720	3.67394	4765	3.67806	4810	3.68215	4855	3.68619
4721	3.67403	4766	3.67815	4811	3.68224	4856	3.68628
4722	3.67413	4767	3.67825	4812	3.68233	4857	3.68637
4723	3.67422	4768	3.67834	4813	3.68242	4858	3.68646
4724	3.67431	4769	3.67843	4814	3.68251	4859	3.68655
4725	3.67440	4770	3.67852	4815	3.68260	4860	3.68664

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
4861	3.68673	4906	3.69073	4951	3.69469	4996	3.69862
4862	3.68681	4907	3.69082	4952	3.69478	4997	3.69871
4863	3.68690	4908	3.69090	4953	3.69487	4998	3.69880
4864	3.68699	4909	3.69099	4954	3.69496	4999	3.69888
4865	3.68708	4910	3.69108	4955	3.69504	5000	3.69697
4866	3.68717	4911	3.69117	4956	3.69513	5001	3.69906
4867	3.68726	4912	3.69126	4957	3.69522	5002	3.69914
4868	3.68735	4913	3.69135	4958	3.69531	5003	3.69923
4869	3.68744	4914	3.69144	4959	3.69539	5004	3.69932
4870	3.68753	4915	3.69152	4960	3.69548	5005	3.69940
4871	3.68762	4916	3.69161	4961	3.69557	5006	3.69949
4872	3.68771	4917	3.69170	4962	3.69566	5007	3.69958
4873	3.68780	4918	3.69179	4963	3.69574	5008	3.69966
4874	3.68789	4919	3.69188	4964	3.69583	5009	3.69975
4875	3.68797	4920	3.69197	4965	3.69592	5010	3.69984
4876	3.68806	4921	3.69205	4966	3.69601	5011	3.69992
4877	3.68815	4922	3.69214	4967	3.69609	5012	3.70001
4878	3.68824	4923	3.69223	4968	3.69618	5013	3.70010
4879	3.68833	4924	3.69232	4969	3.69627	5014	3.70018
4880	3.68842	4925	3.69241	4970	3.69636	5015	3.70027
4881	3.68851	4926	3.69249	4971	3.69644	5016	3.70036
4882	3.68860	4927	3.69258	4972	3.69653	5017	3.70044
4883	3.68869	4928	3.69267	4973	3.69662	5018	3.70053
4884	3.68878	4929	3.69276	4974	3.69671	5019	3.70062
4885	3.68886	4930	3.69285	4975	3.69679	5020	3.70070
4886	3.68895	4931	3.69294	4976	3.69688	5021	3.70079
4887	3.68904	4932	3.69302	4977	3.69697	5022	3.70088
4888	3.68913	4933	3.69311	4978	3.69705	5023	3.70096
4889	3.68922	4934	3.69320	4979	3.69714	5024	3.70105
4890	3.68931	4935	3.69329	4980	3.69723	5025	3.70114
4891	3.68940	4936	3.69338	4981	3.69732	5026	3.70122
4892	3.68949	4937	3.69346	4982	3.69740	5027	3.70131
4893	3.68958	4938	3.69355	4983	3.69749	5028	3.70140
4894	3.68966	4939	3.69364	4984	3.69758	5029	3.70148
4895	3.68975	4940	3.69373	4985	3.69767	5030	3.70157
4896	3.68984	4941	3.69381	4986	3.69775	5031	3.70165
4897	3.68993	4942	3.69390	4987	3.69784	5032	3.70174
4898	3.69002	4943	3.69399	4988	3.69793	5033	3.70183
4899	3.69011	4944	3.69408	4989	3.69801	5034	3.70191
4900	3.69020	4945	3.69417	4990	3.69810	5035	3.70200
4901	3.69028	4946	3.69425	4991	3.69819	5036	3.70209
4902	3.69037	4947	3.69434	4992	3.69827	5037	3.70217
4903	3.69046	4948	3.69443	4993	3.69836	5038	3.70226
4904	3.69055	4949	3.69452	4994	3.69845	5039	3.70234
4905	3.69064	4950	3.69461	4995	3.69854	5040	3.70243

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
5041	3.70252	5086	3.70638	5131	3.71020	5176	3.71399
5042	3.70260	5087	3.70646	5132	3.71028	5177	3.71408
5043	3.70269	5088	3.70654	5133	3.71037	5178	3.71416
5044	3.70278	5089	3.70663	5134	3.71046	5179	3.71425
5045	3.70286	5090	3.70672	5135	3.71054	5180	3.71433
5046	3.70295	5091	3.70680	5136	3.71163	5181	3.71441
5047	3.70303	5092	3.70689	5137	3.71171	5182	3.71450
5048	3.70312	5093	3.70697	5138	3.71179	5183	3.71458
5049	3.70321	5094	3.70706	5139	3.71188	5184	3.71467
5050	3.70329	5095	3.70714	5140	3.71196	5185	3.71475
5051	3.70338	5096	3.70723	5141	3.71105	5186	3.71483
5052	3.70346	5097	3.70731	5142	3.71113	5187	3.71492
5053	3.70355	5098	3.70740	5143	3.71122	5188	3.71500
5054	3.70364	5099	3.70748	5144	3.71130	5189	3.71508
5055	3.70372	5100	3.70757	5145	3.71139	5190	3.71517
5056	3.70381	5101	3.70766	5146	3.71147	5191	3.71525
5057	3.70389	5102	3.70774	5147	3.71155	5192	3.71533
5058	3.70398	5103	3.70782	5148	3.71164	5193	3.71542
5059	3.70406	5104	3.70791	5149	3.71172	5194	3.71550
5060	3.70415	5105	3.70800	5150	3.71181	5195	3.71559
5061	3.70424	5106	3.70808	5151	3.71189	5196	3.71567
5062	3.70432	5107	3.70817	5152	3.71198	5197	3.71575
5063	3.70441	5108	3.70825	5153	3.71206	5198	3.71584
5064	3.70449	5109	3.70834	5154	3.71214	5199	3.71592
5065	3.70458	5110	3.70842	5155	3.71223	5200	3.71600
5066	3.70466	5111	3.70851	5156	3.71231	5201	3.71609
5067	3.70475	5112	3.70859	5157	3.71240	5202	3.71617
5068	3.70484	5113	3.70868	5158	3.71248	5203	3.71625
5069	3.70492	5114	3.70876	5159	3.71257	5204	3.71634
5070	3.70501	5115	3.70885	5160	3.71265	5205	3.71642
5071	3.70509	5116	3.70893	5161	3.71273	5206	3.71650
5072	3.70518	5117	3.70902	5162	3.71282	5207	3.71659
5073	3.70526	5118	3.70910	5163	3.71290	5208	3.71667
5074	3.70535	5119	3.70919	5164	3.71299	5209	3.71675
5075	3.70544	5120	3.70927	5165	3.71307	5210	3.71684
5076	3.70552	5121	3.70935	5166	3.71315	5211	3.71692
5077	3.70561	5122	3.70944	5167	3.71324	5212	3.71700
5078	3.70569	5123	3.70952	5168	3.71332	5213	3.71709
5079	3.70578	5124	3.70961	5169	3.71341	5214	3.71717
5080	3.70586	5125	3.70969	5170	3.71349	5215	3.71725
5081	3.70595	5126	3.70978	5171	3.71357	5216	3.71734
5082	3.70603	5127	3.70986	5172	3.71366	5217	3.71742
5083	3.70612	5128	3.70995	5173	3.71374	5218	3.71750
5084	3.70621	5129	3.71003	5174	3.71383	5219	3.71759
5085	3.70629	5130	3.71012	5175	3.71391	5220	3.71767

# A Table of Logarithms.

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N	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
5221	3.71775	5266	3.72148	5311	3.72518	5356	3.72884
5222	3.71784	5267	3.72156	5312	3.72526	5357	3.72892
5223	3.71792	5268	3.72165	5313	3.72534	5358	3.72900
5224	3.71800	5269	3.72173	5314	3.72542	5359	3.72908
5225	3.71809	5270	3.72181	5315	3.72550	5360	3.72916
5226	3.71817	5271	3.72189	5316	3.72559	5361	3.72925
5227	3.71825	5272	3.72198	5317	3.72567	5362	3.72933
5228	3.71834	5273	3.72206	5318	3.72575	5363	3.72941
5229	3.71842	5274	3.72214	5319	3.72583	5364	3.72949
5230	3.71850	5275	3.72222	5320	3.72591	5365	3.72957
5231	3.71858	5276	3.72230	5321	3.72599	5366	3.72965
5232	3.71867	5277	3.72239	5322	3.72607	5367	3.72973
5233	3.71875	5278	3.72247	5323	3.72616	5368	3.72981
5234	3.71883	5279	3.72255	5324	3.72624	5369	3.72989
5235	3.71892	5280	3.72263	5325	3.72632	5370	3.72997
5236	3.71900	5281	3.72272	5326	3.72640	5371	3.73006
5237	3.71908	5282	3.72280	5327	3.72648	5372	3.73014
5238	3.71917	5283	3.72288	5328	3.72656	5373	3.73022
5239	3.71925	5284	3.72296	5329	3.72665	5374	3.73030
5240	3.71933	5285	3.72305	5330	3.72673	5375	3.73038
5241	3.71941	5286	3.72313	5331	3.72681	5376	3.73046
5242	3.71950	5287	3.72321	5332	3.72689	5377	3.73054
5243	3.71958	5288	3.72329	5333	3.72697	5378	3.73062
5244	3.71966	5289	3.72337	5334	3.72705	5379	3.73070
5245	3.71975	5290	3.72346	5335	3.72713	5380	3.73078
5246	3.71983	5291	3.72354	5336	3.72722	5381	3.73086
5247	3.71991	5292	3.72362	5337	3.72730	5382	3.73094
5248	3.71999	5293	3.72370	5338	3.72738	5383	3.73102
5249	3.72008	5294	3.72378	5339	3.72746	5384	3.73111
5250	3.72016	5295	3.72387	5340	3.72754	5385	3.73119
5251	3.72024	5296	3.72395	5341	3.72762	5386	3.73127
5252	3.72032	5297	3.72403	5342	3.72770	5387	3.73135
5253	3.72041	5298	3.72411	5343	3.72779	5388	3.73143
5254	3.72049	5299	3.72419	5344	3.72787	5389	3.73151
5255	3.72057	5300	3.72428	5345	3.72795	5390	3.73159
5256	3.72066	5301	3.72436	5346	3.72803	5391	3.73167
5257	3.72074	5302	3.72444	5347	3.72811	5392	3.73175
5258	3.72082	5303	3.72452	5348	3.72819	5393	3.73183
5259	3.72090	5304	3.72460	5349	3.72827	5394	3.73191
5260	3.72099	5305	3.72469	5350	3.72835	5395	3.73199
5261	3.72107	5306	3.72477	5351	3.72843	5396	3.73207
5262	3.72115	5307	3.72485	5352	3.72852	5397	3.73215
5263	3.72123	5308	3.72493	5353	3.72860	5398	3.73223
5264	3.72132	5309	3.72501	5354	3.72868	5399	3.73231
5265	3.72140	5310	3.72509	5355	3.72876	5400	3.73239

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
5401	3.73247	5446	3.73608	5491	3.73965	5536	3.74320
5402	3.73255	5447	3.73616	5492	3.73973	5537	3.74327
5403	3.73264	5448	3.73624	5493	3.73981	5538	3.74331
5404	3.73272	5449	3.73632	5494	3.73989	5539	3.74335
5405	3.73280	5450	3.73640	5495	3.73997	5540	3.74331
5406	3.73288	5451	3.73648	5496	3.74005	5541	3.74339
5407	3.73296	5452	3.73656	5497	3.74013	5542	3.74337
5408	3.73304	5453	3.73664	5498	3.74020	5543	3.74334
5409	3.73312	5454	3.73672	5499	3.74028	5544	3.74382
5410	3.73320	5455	3.73679	5500	3.74036	5545	3.74390
5411	3.73328	5456	3.73687	5501	3.74044	5546	3.74398
5412	3.73336	5457	3.73695	5502	3.74052	5547	3.74406
5413	3.73344	5458	3.73703	5503	3.74060	5548	3.74414
5414	3.73352	5459	3.73711	5504	3.74068	5549	3.74421
5415	3.73360	5460	3.73719	5505	3.74076	5550	3.74429
5416	3.73368	5461	3.73727	5506	3.74084	5551	3.74437
5417	3.73376	5462	3.73735	5507	3.74092	5552	3.74445
5418	3.73384	5463	3.73743	5508	3.74099	5553	3.74453
5419	3.73392	5464	3.73751	5509	3.74107	5554	3.74461
5420	3.73400	5465	3.73759	5510	3.74115	5555	3.74468
5421	3.73408	5466	3.73767	5511	3.74123	5556	3.74476
5422	3.73416	5467	3.73775	5512	3.74131	5557	3.74484
5423	3.73424	5468	3.73783	5513	3.74139	5558	3.74492
5424	3.73432	5469	3.73791	5514	3.74147	5559	3.74500
5425	3.73440	5470	3.73799	5515	3.74156	5560	3.74507
5426	3.73448	5471	3.73807	5516	3.74162	5561	3.74515
5427	3.73456	5472	3.73815	5517	3.74170	5562	3.74523
5428	3.73464	5473	3.73823	5518	3.74178	5563	3.74531
5429	3.73472	5474	3.73830	5519	3.74186	5564	3.74539
5430	3.73480	5475	3.73838	5520	3.74194	5565	3.74547
5431	3.73488	5476	3.73846	5521	3.74202	5566	3.74554
5432	3.73496	5477	3.73854	5522	3.74210	5567	3.74562
5433	3.73504	5478	3.73862	5523	3.74218	5568	3.74570
5434	3.73512	5479	3.73870	5524	3.74225	5569	3.74578
5435	3.73520	5480	3.73878	5525	3.74233	5570	3.74586
5436	3.73528	5481	3.73886	5526	3.74241	5571	3.74593
5437	3.73536	5482	3.73894	5527	3.74249	5572	3.74601
5438	3.73544	5483	3.73902	5528	3.74257	5573	3.74609
5439	3.73552	5484	3.73909	5529	3.74265	5574	3.74617
5440	3.73560	5485	3.73918	5530	3.74273	5575	3.74624
5441	3.73568	5486	3.73926	5531	3.74280	5576	3.74632
5442	3.73576	5487	3.73934	5532	3.74288	5577	3.74640
5443	3.73584	5488	3.73941	5533	3.74296	5578	3.74648
5444	3.73592	5489	3.73949	5534	3.74304	5579	3.74656
5445	3.73600	5490	3.73957	5535	3.74312	5580	3.74663

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
5581	3.74671	5626	3.75020	5671	3.75366	5716	3.75709
5582	3.74679	5627	3.75028	5672	3.75374	5717	3.75717
5583	3.74687	5628	3.75035	5673	3.75381	5718	3.75724
5584	3.74695	5629	3.75043	5674	3.75389	5719	3.75732
5585	3.74701	5630	3.75051	5675	3.75397	5720	3.75740
5586	3.74710	5631	3.75059	5676	3.75404	5721	3.75747
5587	3.74718	5632	3.75066	5677	3.75412	5722	3.75755
5588	3.74726	5633	3.75074	5678	3.75420	5723	3.75762
5589	3.74733	5634	3.75082	5679	3.75427	5724	3.75770
5590	3.74741	5635	3.75089	5680	3.75435	5725	3.75778
5591	3.74749	5636	3.75097	5681	3.75442	5726	3.75785
5592	3.74757	5637	3.75105	5682	3.75450	5727	3.75793
5593	3.74764	5638	3.75113	5683	3.75458	5728	3.75800
5594	3.74772	5639	3.75120	5684	3.75465	5729	3.75808
5595	3.74780	5640	3.75128	5685	3.75473	5730	3.75815
5596	3.74788	5641	3.75136	5686	3.75481	5731	3.75823
5597	3.74796	5642	3.75143	5687	3.75488	5732	3.75831
5598	3.74803	5643	3.75151	5688	3.75496	5733	3.75838
5599	3.74811	5644	3.75159	5689	3.75504	5734	3.75846
5600	3.74819	5645	3.75168	5690	3.75511	5735	3.75853
5601	3.74827	5646	3.75174	5691	3.75519	5736	3.75861
5602	3.74834	5647	3.75182	5692	3.75526	5737	3.75868
5603	3.74842	5648	3.75189	5693	3.75534	5738	3.75876
5604	3.74850	5649	3.75197	5694	3.75542	5739	3.75884
5605	3.74858	5650	3.75205	5695	3.75549	5740	3.75891
5606	3.74865	5651	3.75213	5696	3.75557	5741	3.75899
5607	3.74873	5652	3.75220	5697	3.75565	5742	3.75906
5608	3.74881	5653	3.75228	5698	3.75572	5743	3.75914
5609	3.74889	5654	3.75236	5699	3.75580	5744	3.75921
5610	3.74896	5655	3.75243	5700	3.75587	5745	3.75929
5611	3.74904	5656	3.75251	5701	3.75595	5746	3.75937
5612	3.74912	5657	3.75259	5702	3.75603	5747	3.75944
5613	3.74920	5658	3.75266	5703	3.75610	5748	3.75952
5614	3.74927	5659	3.75274	5704	3.75618	5749	3.75959
5615	3.74935	5660	3.75282	5705	3.75626	5750	3.75967
5616	3.74943	5661	3.75289	5706	3.75633	5751	3.75974
5617	3.74950	5662	3.75297	5707	3.75641	5752	3.75981
5618	3.74958	5663	3.75305	5708	3.75648	5753	3.75989
5619	3.74966	5664	3.75312	5709	3.75656	5754	3.75997
5620	3.74974	5665	3.75320	5710	3.75664	5755	3.76005
5621	3.74981	5666	3.75328	5711	3.75671	5756	3.76012
5622	3.74989	5667	3.75335	5712	3.75679	5757	3.76020
5623	3.74997	5668	3.75343	5713	3.75686	5758	3.76027
5624	3.75005	5669	3.75351	5714	3.75694	5759	3.76035
5625	3.75012	5670	3.75358	5715	3.75702	5760	3.76043

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
5761	3.76050	5806	3.76388	5851	3.76723	5890	3.77056
5762	3.76057	5807	3.76395	5852	3.76730	5897	3.77063
5763	3.76065	5808	3.76403	5853	3.76738	5898	3.77060
5764	3.76072	5809	3.76410	5854	3.76745	5899	3.77067
5765	3.76080	5810	3.76418	5855	3.76753	5900	3.77064
5766	3.76087	5811	3.76425	5856	3.76760	5901	3.77093
5767	3.76095	5812	3.76433	5857	3.76768	5902	3.77100
5768	3.76103	5813	3.76440	5858	3.76775	5903	3.77107
5769	3.76110	5814	3.76448	5859	3.76782	5904	3.77115
5770	3.76118	5815	3.76455	5860	3.76790	5905	3.77122
5771	3.76125	5816	3.76462	5861	3.76797	5906	3.77129
5772	3.76133	5817	3.76470	5862	3.76805	5907	3.77137
5773	3.76140	5818	3.76477	5863	3.76812	5908	3.77144
5774	3.76148	5819	3.76485	5864	3.76819	5909	3.77151
5775	3.76155	5820	3.76492	5865	3.76827	5910	3.77159
5776	3.76163	5821	3.76500	5866	3.76834	5911	3.77166
5777	3.76170	5822	3.76507	5867	3.76842	5912	3.77173
5778	3.76178	5823	3.76515	5868	3.76849	5913	3.77181
5779	3.76185	5824	3.76522	5869	3.76856	5914	3.77188
5780	3.76193	5825	3.76530	5870	3.76864	5915	3.77195
5781	3.76200	5826	3.76537	5871	3.76871	5916	3.77203
5782	3.76208	5827	3.76545	5872	3.76879	5917	3.77210
5783	3.76215	5828	3.76552	5873	3.76886	5918	3.77218
5784	3.76223	5829	3.76558	5874	3.76893	5919	3.77225
5785	3.76230	5830	3.76567	5875	3.76901	5920	3.77232
5786	3.76238	5831	3.76574	5876	3.76908	5921	3.77240
5787	3.76245	5832	3.76582	5877	3.76916	5922	3.77247
5788	3.76253	5833	3.76589	5878	3.76923	5923	3.77254
5789	3.76260	5834	3.76597	5879	3.76930	5924	3.77262
5790	3.76268	5835	3.76604	5880	3.76938	5925	3.77269
5791	3.76275	5836	3.76612	5881	3.76945	5926	3.77276
5792	3.76283	5837	3.76619	5882	3.76953	5927	3.77283
5793	3.76290	5838	3.76626	5883	3.76960	5928	3.77291
5794	3.76298	5839	3.76634	5884	3.76967	5929	3.77298
5795	3.76305	5840	3.76641	5885	3.76975	5930	3.77305
5796	3.76313	5841	3.76649	5886	3.76982	5931	3.77313
5797	3.76320	5842	3.76656	5887	3.76989	5932	3.77320
5798	3.76328	5843	3.76664	5888	3.76997	5933	3.77327
5799	3.76335	5844	3.76671	5889	3.77004	5934	3.77335
5800	3.76343	5845	3.76678	5890	3.77012	5935	3.77342
5801	3.76350	5846	3.76686	5891	3.77019	5936	3.77349
5802	3.76358	5847	3.76693	5892	3.77026	5937	3.77357
5803	3.76365	5848	3.76701	5893	3.77034	5938	3.77364
5804	3.76373	5849	3.76708	5894	3.77041	5939	3.77371
5805	3.76380	5850	3.76716	5895	3.77048	5940	3.77379

# A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
5941	3.77386	5986	3.77714	6031	3.78039	6076	3.78362
5942	3.77393	5987	3.77721	6032	3.78046	6077	3.78369
5943	3.77401	5988	3.77728	6033	3.78053	6078	3.78376
5944	3.77408	5989	3.77735	6034	3.78061	6079	3.78383
5945	3.77415	5990	3.77743	6035	3.78068	6080	3.78390
5946	3.77422	5991	3.77750	6036	3.78075	6081	3.78398
5947	3.77430	5992	3.77757	6037	3.78082	6082	3.78405
5948	3.77437	5993	3.77764	6038	3.78089	6083	3.78412
5949	3.77444	5994	3.77772	6039	3.78097	6084	3.78419
5950	3.77452	5995	3.77779	6040	3.78104	6085	3.78426
5951	3.77459	5996	3.77786	6041	3.78110	6086	3.78433
5952	3.77466	5997	3.77793	6042	3.78118	6087	3.78440
5953	3.77474	5998	3.77801	6043	3.78125	6088	3.78447
5954	3.77481	5999	3.77808	6044	3.78132	6089	3.78455
5955	3.77488	6000	3.77815	6045	3.78140	6090	3.78462
5956	3.77495	6001	3.77822	6046	3.78147	6091	3.78469
5957	3.77503	6002	3.77830	6047	3.78154	6092	3.78476
5958	3.77510	6003	3.77837	6048	3.78161	6093	3.78483
5959	3.77517	6004	3.77844	6049	3.78168	6094	3.78490
5960	3.77525	6005	3.77851	6050	3.78176	6095	3.78497
5961	3.77532	6006	3.77859	6051	3.78183	6096	3.78505
5962	3.77539	6007	3.77866	6052	3.78190	6097	3.78512
5963	3.77546	6008	3.77873	6053	3.78197	6098	3.78519
5964	3.77554	6009	3.77880	6054	3.78204	6099	3.78526
5965	3.77561	6010	3.77887	6055	3.78211	6100	3.78533
5966	3.77568	6011	3.77895	6056	3.78219	6101	3.78540
5967	3.77576	6012	3.77902	6057	3.78226	6102	3.78547
5968	3.77583	6013	3.77909	6058	3.78233	6103	3.78554
5969	3.77590	6014	3.77916	6059	3.78240	6104	3.78561
5970	3.77597	6015	3.77924	6060	3.78247	6105	3.78569
5971	3.77605	6016	3.77931	6061	3.78254	6106	3.78576
5972	3.77612	6017	3.77938	6062	3.78262	6107	3.78583
5973	3.77619	6018	3.77945	6063	3.78269	6108	3.78590
5974	3.77627	6019	3.77952	6064	3.78276	6109	3.78597
5975	3.77634	6020	3.77960	6065	3.78283	6110	3.78604
5976	3.77641	6021	3.77967	6066	3.78290	6111	3.78611
5977	3.77648	6022	3.77974	6067	3.78297	6112	3.78618
5978	3.77656	6023	3.77981	6068	3.78305	6113	3.78625
5979	3.77663	6024	3.77989	6069	3.78312	6114	3.78633
5980	3.77670	6025	3.77996	6070	3.78319	6115	3.78640
5981	3.77677	6026	3.78003	6071	3.78326	6116	3.78647
5982	3.77685	6027	3.78010	6072	3.78333	6117	3.78654
5983	3.77692	6028	3.78017	6073	3.78340	6118	3.78661
5984	3.77699	6029	3.78025	6074	3.78347	6119	3.78668
5985	3.77706	6030	3.78032	6075	3.78355	6120	3.78675

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
6121	3.78682	6166	3.79000	6211	3.79316	6256	3.79630
6122	3.78689	6167	3.79007	6212	3.79323	6257	3.79637
6123	3.78696	6168	3.79014	6213	3.79330	6258	3.79644
6124	3.78704	6169	3.79021	6214	3.79337	6259	3.79651
6125	3.78711	6170	3.79028	6215	3.79344	6260	3.79658
6126	3.78718	6171	3.79036	6216	3.79351	6261	3.79664
6127	3.78725	6172	3.79043	6217	3.79358	6262	3.79671
6128	3.78732	6173	3.79050	6218	3.79365	6263	3.79678
6129	3.78739	6174	3.79057	6219	3.79372	6264	3.79685
6130	3.78746	6175	3.79064	6220	3.79379	6265	3.79692
6131	3.78753	6176	3.79071	6221	3.79386	6266	3.79699
6132	3.78760	6177	3.79078	6222	3.79393	6267	3.79706
6133	3.78767	6178	3.79085	6223	3.79400	6268	3.79713
6134	3.78774	6179	3.79092	6224	3.79407	6269	3.79720
6135	3.78781	6180	3.79099	6225	3.79414	6270	3.79727
6136	3.78789	6181	3.79106	6226	3.79421	6271	3.79734
6137	3.78796	6182	3.79113	6227	3.79428	6272	3.79741
6138	3.78803	6183	3.79120	6228	3.79435	6273	3.79748
6139	3.78810	6184	3.79127	6229	3.79442	6274	3.79754
6140	3.78817	6185	3.79134	6230	3.79449	6275	3.79761
6141	3.78824	6186	3.79141	6231	3.79456	6276	3.79768
6142	3.78831	6187	3.79148	6232	3.79463	6277	3.79775
6143	3.78838	6188	3.79155	6233	3.79470	6278	3.79782
6144	3.78845	6189	3.79162	6234	3.79477	6279	3.79789
6145	3.78852	6190	3.79169	6235	3.79484	6280	3.79796
6146	3.78859	6191	3.79176	6236	3.79491	6281	3.79803
6147	3.78866	6192	3.79183	6237	3.79498	6282	3.79810
6148	3.78873	6193	3.79190	6238	3.79505	6283	3.79817
6149	3.78880	6194	3.79197	6239	3.79512	6284	3.79824
6150	3.78888	6195	3.79204	6240	3.79518	6285	3.79831
6151	3.78895	6196	3.79211	6241	3.79525	6286	3.79837
6152	3.78902	6197	3.79218	6242	3.79532	6287	3.79844
6153	3.78909	6198	3.79225	6243	3.79539	6288	3.79851
6154	3.78916	6199	3.79232	6244	3.79546	6289	3.79858
6155	3.78923	6200	3.79239	6245	3.79553	6290	3.79865
6156	3.78930	6201	3.79246	6246	3.79560	6291	3.79872
6157	3.78937	6202	3.79253	6247	3.79567	6292	3.79879
6158	3.78944	6203	3.79260	6248	3.79574	6293	3.79886
6159	3.78951	6204	3.79267	6249	3.79581	6294	3.79893
6160	3.78958	6205	3.79274	6250	3.79588	6295	3.79900
6161	3.78965	6206	3.79281	6251	3.79595	6296	3.79906
6162	3.78972	6207	3.79288	6252	3.79602	6297	3.79913
6163	3.78979	6208	3.79295	6253	3.79609	6298	3.79920
6164	3.78986	6209	3.79302	6254	3.79616	6299	3.79927
6165	3.78993	6210	3.79309	6255	3.79623	6300	3.79934

# A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
6301	3.79941	6346	3.80250	6391	3.80557	6436	3.80862
6302	3.79948	6347	3.80257	6392	3.80564	6437	3.80868
6303	3.79955	6348	3.80264	6393	3.80570	6438	3.80875
6304	3.79962	6349	3.80271	6394	3.80577	6439	3.80882
6305	3.79968	6350	3.80277	6395	3.80584	6440	3.80889
6306	3.79975	6351	3.80284	6396	3.80591	6441	3.80895
6307	3.79982	6352	3.80291	6397	3.80598	6442	3.80902
6308	3.79989	6353	3.80298	6398	3.80604	6443	3.80909
6309	3.79996	6354	3.80305	6399	3.80611	6444	3.80916
6310	3.80003	6355	3.80312	6400	3.80618	6445	3.80922
6311	3.80010	6356	3.80318	6401	3.80625	6446	3.80929
6312	3.80017	6357	3.80325	6402	3.80632	6447	3.80936
6313	3.80024	6358	3.80332	6403	3.80638	6448	3.80943
6314	3.80030	6359	3.80339	6404	3.80645	6449	3.80949
6315	3.80037	6360	3.80346	6405	3.80652	6450	3.80956
6316	3.80044	6361	3.80353	6406	3.80659	6451	3.80963
6317	3.80051	6362	3.80359	6407	3.80665	6452	3.80969
6318	3.80058	6363	3.80366	6408	3.80672	6453	3.80976
6319	3.80065	6364	3.80373	6409	3.80679	6454	3.80983
6320	3.80072	6365	3.80380	6410	3.80686	6455	3.80990
6321	3.80079	6366	3.80387	6411	3.80693	6456	3.80996
6322	3.80085	6367	3.80393	6412	3.80699	6457	3.81003
6323	3.80092	6368	3.80400	6413	3.80706	6458	3.81009
6324	3.80099	6369	3.80407	6414	3.80713	6459	3.81017
6325	3.80106	6370	3.80414	6415	3.80720	6460	3.81023
6326	3.80113	6371	3.80421	6416	3.80726	6461	3.81030
6327	3.80120	6372	3.80428	6417	3.80733	6462	3.81037
6328	3.80127	6373	3.80434	6418	3.80740	6463	3.81043
6329	3.80134	6374	3.80441	6419	3.80747	6464	3.81050
6330	3.80140	6375	3.80448	6420	3.80754	6465	3.81057
6331	3.80147	6376	3.80455	6421	3.80760	6466	3.81064
6332	3.80154	6377	3.80462	6422	3.80767	6467	3.81070
6333	3.80161	6378	3.80468	6423	3.80774	6468	3.81077
6334	3.80168	6379	3.80475	6424	3.80781	6469	3.81084
6335	3.80175	6380	3.80482	6425	3.80787	6470	3.81090
6336	3.80182	6381	3.80489	6426	3.80794	6471	3.81097
6337	3.80188	6382	3.80496	6427	3.80801	6472	3.81104
6338	3.80195	6383	3.80502	6428	3.80808	6473	3.81111
6339	3.80202	6384	3.80509	6429	3.80814	6474	3.81117
6340	3.80209	6385	3.80516	6430	3.80821	6475	3.81124
6341	3.80216	6386	3.80523	6431	3.80828	6476	3.81131
6342	3.80223	6387	3.80530	6432	3.80835	6477	3.81137
6343	3.80228	6388	3.80536	6433	3.80841	6478	3.81144
6344	3.80236	6389	3.80543	6434	3.80848	6479	3.81151
6345	3.80242	6390	3.80550	6435	3.80855	6480	3.81158

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
6481	3.81164	6526	3.81465	6571	3.81763	6616	3.82060
6482	3.81171	6527	3.81471	6572	3.81770	6617	3.82066
6483	3.81178	6528	3.81478	6573	3.81776	6618	3.82073
6484	3.81184	6529	3.81485	6574	3.81783	6619	3.82079
6485	3.81191	6530	3.81491	6575	3.81790	6620	3.82086
6486	3.81198	6531	3.81498	6576	3.81796	6621	3.82093
6487	3.81204	6532	3.81505	6577	3.81803	6622	3.82099
6488	3.81211	6533	3.81511	6578	3.81809	6623	3.82105
6489	3.81218	6534	3.81518	6579	3.81816	6624	3.82112
6490	3.81224	6535	3.81525	6580	3.81823	6625	3.82119
6491	3.81231	6536	3.81531	6581	3.81829	6626	3.82125
6492	3.81238	6537	3.81538	6582	3.81836	6627	3.82132
6493	3.81245	6538	3.81544	6583	3.81842	6628	3.82138
6494	3.81251	6539	3.81550	6584	3.81849	6629	3.82145
6495	3.81258	6540	3.81558	6585	3.81856	6630	3.82151
6496	3.81265	6541	3.81564	6586	3.81862	6631	3.82158
6497	3.81271	6542	3.81571	6587	3.81869	6632	3.82164
6498	3.81278	6543	3.81578	6588	3.81875	6633	3.82171
6499	3.81285	6544	3.81584	6589	3.81882	6634	3.82178
6500	3.81291	6545	3.81591	6590	3.81889	6635	3.82184
6501	3.81298	6546	3.81598	6591	3.81895	6636	3.82191
6502	3.81305	6547	3.81604	6592	3.81902	6637	3.82197
6503	3.81311	6548	3.81611	6593	3.81908	6638	3.82204
6504	3.81318	6549	3.81618	6594	3.81915	6639	3.82210
6505	3.81325	6550	3.81624	6595	3.81921	6640	3.82217
6506	3.81331	6551	3.81631	6596	3.81928	6641	3.82223
6507	3.81338	6552	3.81637	6597	3.81935	6642	3.82230
6508	3.81345	6553	3.81644	6598	3.81941	6643	3.82236
6509	3.81351	6554	3.81651	6599	3.81948	6644	3.82243
6510	3.81358	6555	3.81657	6600	3.81954	6645	3.82250
6511	3.81365	6556	3.81664	6601	3.81961	6646	3.82256
6512	3.81371	6557	3.81671	6602	3.81968	6647	3.82263
6513	3.81378	6558	3.81677	6603	3.81974	6648	3.82269
6514	3.81385	6559	3.81684	6604	3.81981	6649	3.82276
6515	3.81391	6560	3.81690	6605	3.81987	6650	3.82282
6516	3.81398	6561	3.81697	6606	3.81994	6651	3.82289
6517	3.81405	6562	3.81701	6607	3.82000	6652	3.82295
6518	3.81411	6563	3.81710	6608	3.82007	6653	3.82302
6519	3.81418	6564	3.81717	6609	3.82014	6654	3.82308
6520	3.81425	6565	3.81723	6610	3.82020	6655	3.82315
6521	3.81431	6566	3.81730	6611	3.82027	6656	3.82321
6522	3.81438	6567	3.81737	6612	3.82033	6657	3.82328
6523	3.81445	6568	3.81743	6613	3.82040	6658	3.82334
6524	3.81451	6569	3.81750	6614	3.82046	6659	3.82341
6525	3.81458	6570	3.81757	6615	3.82053	6660	3.82347

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
6661	3.82354	6706	3.82646	6751	3.82937	6796	3.83225
6662	3.82360	6707	3.82653	6752	3.82943	6797	3.83232
6663	3.82367	6708	3.82656	6753	3.82950	6798	3.83238
6664	3.82374	6709	3.82669	6754	3.82956	6799	3.83245
6665	3.82380	6710	3.82672	6755	3.82963	6800	3.83251
6666	3.82387	6711	3.82679	6756	3.82969	6801	3.83257
6667	3.82393	6712	3.82685	6757	3.82977	6802	3.83264
6668	3.82400	6713	3.82692	6758	3.82982	6803	3.83270
6669	3.82406	6714	3.82698	6759	3.82983	6804	3.83276
6670	3.82413	6715	3.82705	6760	3.82995	6805	3.83283
6671	3.82419	6716	3.82711	6761	3.83001	6806	3.83289
6672	3.82426	6717	3.82718	6762	3.83008	6807	3.83296
6673	3.82432	6718	3.82724	6763	3.83014	6808	3.83302
6674	3.82439	6719	3.82730	6764	3.83020	6809	3.83308
6675	3.82445	6720	3.82737	6765	3.83027	6810	3.83315
6676	3.82452	6721	3.82743	6766	3.83033	6811	3.83321
6677	3.82458	6722	3.82750	6767	3.83040	6812	3.83327
6678	3.82465	6723	3.82756	6768	3.83046	6813	3.83334
6679	3.82471	6724	3.82763	6769	3.83052	6814	3.83340
6680	3.82478	6725	3.82769	6770	3.83059	6815	3.83347
6681	3.82484	6726	3.82776	6771	3.83065	6816	3.83353
6682	3.82491	6727	3.82782	6772	3.83072	6817	3.83359
6683	3.82497	6728	3.82789	6773	3.83078	6818	3.83366
6684	3.82504	6729	3.82795	6774	3.83085	6819	3.83373
6685	3.82510	6730	3.82802	6775	3.83091	6820	3.83378
6686	3.82517	6731	3.82808	6776	3.83097	6821	3.83385
6687	3.82523	6732	3.82814	6777	3.83104	6822	3.83391
6688	3.82530	6733	3.82821	6778	3.83110	6823	3.83398
6689	3.82536	6734	3.82827	6779	3.83117	6824	3.83404
6690	3.82543	6735	3.82834	6780	3.83123	6825	3.83410
6691	3.82549	6736	3.82840	6781	3.83129	6826	3.83417
6692	3.82556	6737	3.82847	6782	3.83136	6827	3.83423
6693	3.82562	6738	3.82853	6783	3.83142	6828	3.83429
6694	3.82569	6739	3.82860	6784	3.83149	6829	3.83436
6695	3.82575	6740	3.82866	6785	3.83155	6830	3.83442
6696	3.82582	6741	3.82872	6786	3.83161	6831	3.83448
6697	3.82588	6742	3.82879	6787	3.83168	6832	3.83455
6698	3.82595	6743	3.82885	6788	3.83174	6833	3.83461
6699	3.82601	6744	3.82892	6789	3.83181	6834	3.83468
6700	3.82607	6745	3.82898	6790	3.83187	6835	3.83474
6701	3.82614	6746	3.82905	6791	3.83193	6836	3.83480
6702	3.82620	6747	3.82911	6792	3.83200	6837	3.83487
6703	3.82627	6748	3.82918	6793	3.83206	6838	3.83493
6704	3.82633	6749	3.82924	6794	3.83213	6839	3.83499
6705	3.82640	6750	3.82930	6795	3.83219	6840	3.83506

*A Table of Logarithms.*

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
6841	3.83512	6886	3.83797	6931	3.84080	6976	3.84361
6842	3.83518	6887	3.83803	6932	3.84086	6977	3.84367
6843	3.83525	6888	3.83809	6933	3.84092	6978	3.84373
6844	3.83531	6889	3.83816	6934	3.84098	6979	3.84379
6845	3.83537	6890	3.83822	6935	3.84105	6980	3.84386
6846	3.83544	6891	3.83828	6936	3.84111	6981	3.84392
6847	3.83550	6892	3.83835	6937	3.84117	6982	3.84398
6848	3.83556	6893	3.83841	6938	3.84123	6983	3.84404
6849	3.83563	6894	3.83847	6939	3.84130	6984	3.84410
6850	3.83569	6895	3.83853	6940	3.84136	6985	3.84417
6851	3.83575	6896	3.83860	6941	3.84142	6986	3.84423
6852	3.83582	6897	3.83866	6942	3.84148	6987	3.84429
6853	3.83588	6898	3.83872	6943	3.84155	6988	3.84435
6854	3.83594	6899	3.83879	6944	3.84161	6989	3.84442
6855	3.83601	6900	3.83885	6945	3.84167	6990	3.84448
6856	3.83607	6901	3.83891	6946	3.84173	6991	3.84454
6857	3.83613	6902	3.83898	6947	3.84180	6992	3.84460
6858	3.83620	6903	3.83904	6948	3.84186	6993	3.84466
6859	3.83626	6904	3.83912	6949	3.84192	6994	3.84473
6860	3.83632	6905	3.83916	6950	3.84198	6995	3.84479
6861	3.83639	6906	3.83923	6951	3.84205	6996	3.84485
6862	3.83645	6907	3.83929	6952	3.84211	6997	3.84491
6863	3.83651	6908	3.83935	6953	3.84217	6998	3.84497
6864	3.83658	6909	3.83942	6954	3.84223	6999	3.84504
6865	3.83664	6910	3.83948	6955	3.84230	7000	3.84510
6866	3.83670	6911	3.83954	6956	3.84236	7001	3.84516
6867	3.83677	6912	3.83960	6957	3.84242	7002	3.84522
6868	3.83683	6913	3.83967	6958	3.84248	7003	3.84528
6869	3.83689	6914	3.83973	6959	3.84255	7004	3.84535
6870	3.83696	6915	3.83979	6960	3.84261	7005	3.84541
6871	3.83702	6916	3.83986	6961	3.84267	7006	3.84547
6872	3.83708	6917	3.83992	6962	3.84273	7007	3.84553
6873	3.83715	6918	3.83998	6963	3.84280	7008	3.84559
6874	3.83721	6919	3.84004	6964	3.84286	7009	3.84566
6875	3.83727	6920	3.84011	6965	3.84292	7010	3.84572
6876	3.83734	6921	3.84017	6966	3.84298	7011	3.84578
6877	3.83740	6922	3.84023	6967	3.84305	7012	3.84584
6878	3.83746	6923	3.84029	6968	3.84311	7013	3.84590
6879	3.83753	6924	3.84036	6969	3.84317	7014	3.84597
6880	3.83759	6925	3.84042	6970	3.84323	7015	3.84603
6881	3.83765	6926	3.84048	6971	3.84330	7016	3.84609
6882	3.83771	6927	3.84055	6972	3.84336	7017	3.84615
6883	3.83778	6928	3.84061	6973	3.84342	7018	3.84621
6884	3.83784	6929	3.84067	6974	3.84348	7019	3.84628
6885	3.83790	6930	3.84073	6975	3.84354	7020	3.84634

*A Table of Logarithms.*

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<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>
7021	3.84640	7066	3.84917	7111	3.85193	7156	3.85467
7022	3.84646	7067	3.84924	7112	3.85199	7157	3.85473
7023	3.84652	7068	3.84930	7113	3.85205	7158	3.85479
7024	3.84658	7069	3.84936	7114	3.85211	7159	3.85485
7025	3.84665	7070	3.84942	7115	3.85217	7160	3.85491
7026	3.84671	7071	3.84948	7116	3.85224	7161	3.85497
7027	3.84677	7072	3.84954	7117	3.85230	7162	3.85503
7028	3.84683	7073	3.84960	7118	3.85236	7163	3.85509
7029	3.84689	7074	3.84967	7119	3.85242	7164	3.85516
7030	3.84696	7075	3.84973	7120	3.85248	7165	3.85522
7031	3.84702	7076	3.84979	7121	3.85254	7166	3.85528
7032	3.84708	7077	3.84985	7122	3.85260	7167	3.85534
7033	3.84714	7078	3.84991	7123	3.85266	7168	3.85540
7034	3.84720	7079	3.84997	7124	3.85272	7169	3.85546
7035	3.84726	7080	3.85003	7125	3.85278	7170	3.85552
7036	3.84733	7081	3.85009	7126	3.85285	7171	3.85558
7037	3.84739	7082	3.85016	7127	3.85291	7172	3.85564
7038	3.84745	7083	3.85022	7128	3.85297	7173	3.85570
7039	3.84751	7084	3.85028	7129	3.85303	7174	3.85576
7040	3.84757	7085	3.85034	7130	3.85309	7175	3.85582
7041	3.84763	7086	3.85040	7131	3.85315	7176	3.85588
7042	3.84770	7087	3.85046	7132	3.85321	7177	3.85594
7043	3.84776	7088	3.85052	7133	3.85327	7178	3.85600
7044	3.84782	7089	3.85058	7134	3.85333	7179	3.85606
7045	3.84788	7090	3.85065	7135	3.85339	7180	3.85612
7046	3.84794	7091	3.85071	7136	3.85345	7181	3.85618
7047	3.84800	7092	3.85077	7137	3.85352	7182	3.85625
7048	3.84807	7093	3.85083	7138	3.85358	7183	3.85631
7049	3.84813	7094	3.85089	7139	3.85364	7184	3.85637
7050	3.84819	7095	3.85095	7140	3.85370	7185	3.85643
7051	3.84825	7096	3.85101	7141	3.85376	7186	3.85649
7052	3.84831	7097	3.85107	7142	3.85382	7187	3.85655
7053	3.84837	7098	3.85114	7143	3.85388	7188	3.85661
7054	3.84844	7099	3.85120	7144	3.85394	7189	3.85667
7055	3.84850	7100	3.85126	7145	3.85400	7190	3.85673
7056	3.84856	7101	3.85132	7146	3.85406	7191	3.85679
7057	3.84862	7102	3.85138	7147	3.85412	7192	3.85685
7058	3.84868	7103	3.85144	7148	3.85418	7193	3.85691
7059	3.84874	7104	3.85150	7149	3.85425	7194	3.85697
7060	3.84880	7105	3.85156	7150	3.85431	7195	3.85703
7061	3.84887	7106	3.85163	7151	3.85437	7196	3.85709
7062	3.84893	7107	3.85169	7152	3.85443	7197	3.85715
7063	3.84899	7108	3.85175	7153	3.85449	7198	3.85721
7064	3.84905	7109	3.85181	7154	3.85455	7199	3.85727
7065	3.84911	7110	3.85187	7155	3.85461	7200	3.85733

## A Table of Logarithms.

<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>
7201	3.85739	7246	3.86010	7291	3.86279	7336	3.86546
7202	3.85745	7247	3.86016	7292	3.86285	7337	3.86552
7203	3.85751	7248	3.86022	7293	3.86291	7338	3.86558
7204	3.85757	7249	3.86028	7294	3.86297	7339	3.86564
7205	3.85763	7250	3.86034	7295	3.86303	7340	3.86570
7206	3.85769	7251	3.86040	7296	3.86308	7341	3.86576
7207	3.85775	7252	3.86046	7297	3.86314	7342	3.86581
7208	3.85781	7253	3.86052	7298	3.86320	7343	3.86587
7209	3.85788	7254	3.86058	7299	3.86326	7344	3.86593
7210	3.85794	7255	3.86064	7300	3.86332	7345	3.86599
7211	3.85800	7256	3.86070	7301	3.86338	7346	3.86605
7212	3.85806	7257	3.86076	7302	3.86344	7347	3.86611
7213	3.85812	7258	3.86082	7303	3.86350	7348	3.86617
7214	3.85818	7259	3.86088	7304	3.86356	7349	3.86623
7215	3.85824	7260	3.86094	7305	3.86362	7350	3.86629
7216	3.85830	7261	3.86100	7306	3.86368	7351	3.86635
7217	3.85836	7262	3.86106	7307	3.86374	7352	3.86641
7218	3.85842	7263	3.86112	7308	3.86380	7353	3.86646
7219	3.85848	7264	3.86118	7309	3.86386	7354	3.86652
7220	3.85854	7265	3.86124	7310	3.86392	7355	3.86658
7221	3.85860	7266	3.86130	7311	3.86398	7356	3.86664
7222	3.85866	7267	3.86136	7312	3.86404	7357	3.86670
7223	3.85872	7268	3.86141	7313	3.86410	7358	3.86676
7224	3.85878	7269	3.86147	7314	3.86416	7359	3.86682
7225	3.85884	7270	3.86153	7315	3.86421	7360	3.86688
7226	3.85890	7271	3.86159	7316	3.86427	7361	3.86694
7227	3.85896	7272	3.86165	7317	3.86433	7362	3.86700
7228	3.85902	7273	3.86171	7318	3.86439	7363	3.86705
7229	3.85908	7274	3.86177	7319	3.86445	7364	3.86711
7230	3.85914	7275	3.86183	7320	3.86451	7365	3.86717
7231	3.85920	7276	3.86189	7321	3.86457	7366	3.86723
7232	3.85926	7277	3.86195	7322	3.86463	7367	3.86729
7233	3.85932	7278	3.86201	7323	3.86469	7368	3.86735
7234	3.85938	7279	3.86207	7324	3.86475	7369	3.86741
7235	3.85944	7280	3.86213	7325	3.86481	7370	3.86747
7236	3.85950	7281	3.86219	7326	3.86487	7371	3.86753
7237	3.85956	7282	3.86225	7327	3.86493	7372	3.86759
7238	3.85962	7283	3.86231	7328	3.86499	7373	3.86764
7239	3.85968	7284	3.86237	7329	3.86504	7374	3.86770
7240	3.85974	7285	3.86243	7330	3.86510	7375	3.86776
7241	3.85980	7286	3.86249	7331	3.86516	7376	3.86782
7242	3.85986	7287	3.86255	7332	3.86522	7377	3.86788
7243	3.85992	7288	3.86261	7333	3.86528	7378	3.86794
7244	3.85998	7289	3.86267	7334	3.86534	7379	3.86800
7245	3.86004	7290	3.86273	7335	3.86540	7380	3.86806

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
7381	3.86812	7426	3.87075	7471	3.87338	7516	3.87799
7382	3.86817	7427	3.87081	7472	3.87344	7517	3.87804
7383	3.86823	7428	3.87087	7473	3.87350	7518	3.87810
7384	3.86829	7429	3.87093	7474	3.87355	7519	3.87816
7385	3.86835	7430	3.87099	7475	3.87361	7520	3.87822
7386	3.86841	7431	3.87105	7476	3.87367	7521	3.87828
7387	3.86847	7432	3.87111	7477	3.87373	7522	3.87833
7388	3.86853	7433	3.87116	7478	3.87379	7523	3.87839
7389	3.86859	7434	3.87122	7479	3.87384	7524	3.87845
7390	3.86864	7435	3.87128	7480	3.87390	7525	3.87851
7391	3.86870	7436	3.87134	7481	3.87396	7526	3.87856
7392	3.86876	7437	3.87140	7482	3.87402	7527	3.87862
7393	3.86882	7438	3.87146	7483	3.87408	7528	3.87868
7394	3.86888	7439	3.87151	7484	3.87413	7529	3.87874
7395	3.86894	7440	3.87157	7485	3.87419	7530	3.87880
7396	3.86900	7441	3.87163	7486	3.87425	7531	3.87885
7397	3.86906	7442	3.87169	7487	3.87431	7532	3.87891
7398	3.86911	7443	3.87175	7488	3.87437	7533	3.87897
7399	3.86917	7444	3.87181	7489	3.87442	7534	3.87903
7400	3.86923	7445	3.87186	7490	3.87448	7535	3.87908
7401	3.86929	7446	3.87192	7491	3.87454	7536	3.87914
7402	3.86935	7447	3.87198	7492	3.87460	7537	3.87920
7403	3.86941	7448	3.87204	7493	3.87466	7538	3.87926
7404	3.86947	7449	3.87210	7494	3.87471	7539	3.87931
7405	3.86953	7450	3.87216	7495	3.87477	7540	3.87937
7406	3.86958	7451	3.87221	7496	3.87483	7541	3.87943
7407	3.86964	7452	3.87227	7497	3.87489	7542	3.87949
7408	3.86970	7453	3.87233	7498	3.87495	7543	3.87954
7409	3.86976	7454	3.87239	7499	3.87500	7544	3.87960
7410	3.86982	7455	3.87245	7500	3.87506	7545	3.87966
7411	3.86988	7456	3.87251	7501	3.87512	7546	3.87972
7412	3.86994	7457	3.87256	7502	3.87518	7547	3.87977
7413	3.86999	7458	3.87262	7503	3.87523	7548	3.87983
7414	3.87005	7459	3.87268	7504	3.87529	7549	3.87989
7415	3.87011	7460	3.87274	7505	3.87535	7550	3.87995
7416	3.87017	7461	3.87280	7506	3.87541	7551	3.87900
7417	3.87023	7462	3.87286	7507	3.87547	7552	3.87906
7418	3.87029	7463	3.87291	7508	3.87552	7553	3.87912
7419	3.87035	7464	3.87297	7509	3.87558	7554	3.87918
7420	3.87040	7465	3.87303	7510	3.87564	7555	3.87923
7421	3.87046	7466	3.87309	7511	3.87570	7556	3.87929
7422	3.87052	7467	3.87315	7512	3.87576	7557	3.87935
7423	3.87058	7468	3.87320	7513	3.87581	7558	3.87941
7424	3.87064	7469	3.87326	7514	3.87587	7559	3.87946
7425	3.87070	7470	3.87332	7515	3.87593	7560	3.87952

## A Table of Logarithms.

<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>
7561	3.87858	7606	3.88116	7651	3.88372	7696	3.88627
7562	3.87864	7607	3.88121	7652	3.88378	7697	3.88632
7563	3.87869	7608	3.88127	7653	3.88383	7698	3.88638
7564	3.87875	7609	3.88133	7654	3.88389	7699	3.88643
7565	3.87881	7610	3.88138	7655	3.88395	7700	3.88649
7566	3.87887	7611	3.88144	7656	3.88400	7701	3.88655
7567	3.87892	7612	3.88150	7657	3.88406	7702	3.88660
7568	3.87898	7613	3.88156	7658	3.88412	7703	3.88666
7569	3.87904	7614	3.88161	7659	3.88417	7704	3.88672
7570	3.87910	7615	3.88167	7660	3.88423	7705	3.88677
7571	3.87915	7616	3.88173	7661	3.88429	7706	3.88683
7572	3.87921	7617	3.88178	7662	3.88434	7707	3.88689
7573	3.87927	7618	3.88184	7663	3.88440	7708	3.88694
7574	3.87933	7619	3.88190	7664	3.88446	7709	3.88700
7575	3.87938	7620	3.88196	7665	3.88451	7710	3.88705
7576	3.87944	7621	3.88201	7666	3.88457	7711	3.88711
7577	3.87950	7622	3.88207	7667	3.88463	7712	3.88717
7578	3.87955	7623	3.88213	7668	3.88468	7713	3.88722
7579	3.87961	7624	3.88218	7669	3.88474	7714	3.88728
7580	3.87967	7625	3.88224	7670	3.88480	7715	3.88734
7581	3.87973	7626	3.88230	7671	3.88485	7716	3.88739
7582	3.87978	7627	3.88235	7672	3.88491	7717	3.88745
7583	3.87984	7628	3.88241	7673	3.88497	7718	3.88750
7584	3.87990	7629	3.88247	7674	3.88502	7719	3.88756
7585	3.87996	7630	3.88252	7675	3.88508	7720	3.88762
7586	3.88001	7631	3.88258	7676	3.88514	7721	3.88767
7587	3.88007	7632	3.88264	7677	3.88519	7722	3.88773
7588	3.88013	7633	3.88270	7678	3.88525	7723	3.88779
7589	3.88018	7634	3.88275	7679	3.88530	7724	3.88784
7590	3.88024	7635	3.88281	7680	3.88536	7725	3.88790
7591	3.88030	7636	3.88287	7681	3.88542	7726	3.88795
7592	3.88036	7637	3.88292	7682	3.88547	7727	3.88801
7593	3.88041	7638	3.88298	7683	3.88553	7728	3.88807
7594	3.88047	7639	3.88304	7684	3.88559	7729	3.88812
7595	3.88053	7640	3.88309	7685	3.88564	7730	3.88818
7596	3.88059	7641	3.88315	7686	3.88570	7731	3.88824
7597	3.88064	7642	3.88321	7687	3.88576	7732	3.88829
7598	3.88070	7643	3.88326	7688	3.88581	7733	3.88835
7599	3.88076	7644	3.88332	7689	3.88587	7734	3.88840
7600	3.88081	7645	3.88338	7690	3.88593	7735	3.88846
7601	3.88087	7646	3.88343	7691	3.88598	7736	3.88852
7602	3.88093	7647	3.88349	7692	3.88604	7737	3.88857
7603	3.88099	7648	3.88355	7693	3.88610	7738	3.88863
7604	3.88104	7649	3.88360	7694	3.88615	7739	3.88868
7605	3.88110	7650	3.88366	7695	3.88621	7740	3.88874

A Table of Logarithms.

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<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>	<i>N.</i>	<i>Logar.</i>
7741	3.88880	7786	3.89131	7831	3.89382	7876	3.89631
7742	3.88885	7787	3.89137	7832	3.89387	7877	3.89636
7743	3.88891	7788	3.89143	7833	3.89393	7878	3.89642
7744	3.88897	7789	3.89148	7834	3.89398	7879	3.89647
7745	3.88902	7790	3.89154	7835	3.89404	7880	3.89653
7746	3.88908	7791	3.89159	7836	3.89409	7881	3.89658
7747	3.88913	7792	3.89165	7837	3.89415	7882	3.89664
7748	3.88919	7793	3.89170	7838	3.89421	7883	3.89669
7749	3.88925	7794	3.89176	7839	3.89426	7884	3.89675
7750	3.88931	7795	3.89182	7840	3.89432	7885	3.89680
7751	3.88936	7796	3.89187	7841	3.89437	7886	3.89686
7752	3.88941	7797	3.89193	7842	3.89443	7887	3.89691
7753	3.88947	7798	3.89198	7843	3.89448	7888	3.89697
7754	3.88953	7799	3.89204	7844	3.89454	7889	3.89702
7755	3.88958	7800	3.89209	7845	3.89459	7890	3.89708
7756	3.88964	7801	3.89215	7846	3.89465	7891	3.89713
7757	3.88969	7802	3.89221	7847	3.89470	7892	3.89719
7758	3.88975	7803	3.89226	7848	3.89476	7893	3.89714
7759	3.88981	7804	3.89232	7849	3.89481	7894	3.89730
7760	3.88986	7805	3.89237	7850	3.89487	7895	3.89735
7761	3.88992	7806	3.89243	7851	3.89493	7896	3.89741
7762	3.88997	7807	3.89248	7852	3.89498	7897	3.89746
7763	3.89003	7808	3.89254	7853	3.89504	7898	3.89752
7764	3.89009	7809	3.89260	7854	3.89509	7899	3.89757
7765	3.89014	7810	3.89265	7855	3.89515	7900	3.89763
7766	3.89020	7811	3.89271	7856	3.89520	7901	3.89768
7767	3.89025	7812	3.89276	7857	3.89526	7902	3.89774
7768	3.89031	7813	3.89282	7858	3.89531	7903	3.89779
7769	3.89037	7814	3.89287	7859	3.89537	7904	3.89785
7770	3.89042	7815	3.89293	7860	3.89542	7905	3.89790
7771	3.89048	7816	3.89298	7861	3.89548	7906	3.89796
7772	3.89053	7817	3.89304	7862	3.89553	7907	3.89801
7773	3.89059	7818	3.89310	7863	3.89559	7908	3.89807
7774	3.89064	7819	3.89315	7864	3.89564	7909	3.89812
7775	3.89070	7820	3.89321	7865	3.89570	7910	3.89818
7776	3.89076	7821	3.89326	7866	3.89575	7911	3.89823
7777	3.89081	7822	3.89332	7867	3.89581	7912	3.89829
7778	3.89087	7823	3.89337	7868	3.89586	7913	3.89834
7779	3.89092	7824	3.89343	7869	3.89592	7914	3.89840
7780	3.89098	7825	3.89348	7870	3.89597	7915	3.89845
7781	3.89104	7826	3.89354	7871	3.89603	7916	3.89851
7782	3.89109	7827	3.89360	7872	3.89609	7917	3.89856
7783	3.89115	7828	3.89365	7873	3.89614	7918	3.89862
7784	3.89120	7829	3.89371	7874	3.89620	7919	3.89867
7785	3.89126	7830	3.89376	7875	3.89625	7920	3.89873

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
7921	3.89878	7966	3.90124	8011	3.90369	8056	3.90612
7922	3.89883	7967	3.90129	8012	3.90374	8057	3.90617
7923	3.89889	7968	3.90135	8013	3.90380	8058	3.90623
7924	3.89894	7969	3.90140	8014	3.90385	8059	3.90628
7925	3.89900	7970	3.90146	8015	3.90390	8060	3.90634
7926	3.89905	7971	3.90151	8016	3.90396	8061	3.90639
7927	3.89911	7972	3.90157	8017	3.90401	8062	3.90644
7928	3.89916	7973	3.90162	8018	3.90407	8063	3.90650
7929	3.89922	7974	3.90168	8019	3.90412	8064	3.90655
7930	3.89927	7975	3.90173	8020	3.90417	8065	3.90660
7931	3.89933	7976	3.90179	8021	3.90422	8066	3.90666
7932	3.89938	7977	3.90184	8022	3.90428	8067	3.90671
7933	3.89943	7978	3.90189	8023	3.90434	8068	3.90677
7934	3.89949	7979	3.90195	8024	3.90439	8069	3.90682
7935	3.89955	7980	3.90200	8025	3.90445	8070	3.90687
7936	3.89960	7981	3.90206	8026	3.90450	8071	3.90693
7937	3.89966	7982	3.90211	8027	3.90455	8072	3.90698
7938	3.89971	7983	3.90217	8028	3.90461	8073	3.90704
7939	3.89977	7984	3.90222	8029	3.90466	8074	3.90709
7940	3.89982	7985	3.90227	8030	3.90472	8075	3.90714
7941	3.89988	7986	3.90233	8031	3.90477	8076	3.90720
7942	3.89993	7987	3.90238	8032	3.90482	8077	3.90725
7943	3.89998	7988	3.90244	8033	3.90488	8078	3.90730
7944	3.90004	7989	3.90249	8034	3.90493	8079	3.90736
7945	3.90009	7990	3.90255	8035	3.90499	8080	3.90741
7946	3.90015	7991	3.90260	8036	3.90504	8081	3.90747
7947	3.90020	7992	3.90266	8037	3.90509	8082	3.90752
7948	3.90026	7993	3.90271	8038	3.90515	8083	3.90757
7949	3.90031	7994	3.90276	8039	3.90520	8084	3.90763
7950	3.90037	7995	3.90282	8040	3.90526	8085	3.90768
7951	3.90042	7996	3.90287	8041	3.90531	8086	3.90773
7952	3.90048	7997	3.90293	8042	3.90536	8087	3.90779
7953	3.90053	7998	3.90298	8043	3.90542	8088	3.90784
7954	3.90059	7999	3.90304	8044	3.90547	8089	3.90789
7955	3.90064	8000	3.90309	8045	3.90553	8090	3.90795
7956	3.90069	8001	3.90314	8046	3.90558	8091	3.90800
7957	3.90075	8002	3.90320	8047	3.90563	8092	3.90806
7958	3.90080	8003	3.90325	8048	3.90569	8093	3.90811
7959	3.90086	8004	3.90331	8049	3.90574	8094	3.90816
7960	3.90091	8005	3.90336	8050	3.90580	8095	3.90822
7961	3.90097	8006	3.90342	8051	3.90585	8096	3.90827
7962	3.90102	8007	3.90347	8052	3.90590	8097	3.90832
7963	3.90108	8008	3.90352	8053	3.90596	8098	3.90838
7964	3.91113	8009	3.90358	8054	3.90601	8099	3.90843
7965	3.90119	8010	3.90365	8055	3.90607	8100	3.90849

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
8101	3.90854	8146	3.91094	8191	3.91334	8236	3.91572
8102	3.90859	8147	3.91100	8192	3.91339	8237	3.91577
8103	3.90865	8148	3.91105	8193	3.91344	8238	3.91582
8104	3.90870	8149	3.91110	8194	3.91350	8239	3.91587
8105	3.90875	8150	3.91116	8195	3.91355	8240	3.91593
8106	3.90881	8151	3.91121	8196	3.91360	8241	3.91598
8107	3.90886	8152	3.91126	8197	3.91365	8242	3.91603
8108	3.90891	8153	3.91132	8198	3.91371	8243	3.91609
8109	3.90897	8154	3.91137	8199	3.91376	8244	3.91614
8110	3.90903	8155	3.91142	8200	3.91381	8245	3.91619
8111	3.90907	8156	3.91148	8201	3.91387	8246	3.91624
8112	3.90913	8157	3.91153	8202	3.91392	8247	3.91630
8113	3.90918	8158	3.91158	8203	3.91397	8248	3.91635
8114	3.90924	8159	3.91164	8204	3.91403	8249	3.91640
8115	3.90929	8160	3.91169	8205	3.91408	8250	3.91645
8116	3.90934	8161	3.91174	8206	3.91413	8251	3.91651
8117	3.90940	8162	3.91180	8207	3.91418	8252	3.91656
8118	3.90945	8163	3.91185	8208	3.91424	8253	3.91661
8119	3.90950	8164	3.91190	8209	3.91429	8254	3.91666
8120	3.90956	8165	3.91196	8210	3.91434	8255	3.91672
8121	3.90961	8166	3.91201	8211	3.91440	8256	3.91677
8122	3.90966	8167	3.91206	8212	3.91445	8257	3.91682
8123	3.90972	8168	3.91212	8213	3.91450	8258	3.91687
8124	3.90977	8169	3.91217	8214	3.91455	8259	3.91692
8125	3.90982	8170	3.91222	8215	3.91461	8260	3.91698
8126	3.90988	8171	3.91227	8216	3.91466	8261	3.91703
8127	3.90993	8172	3.91232	8217	3.91471	8262	3.91709
8128	3.90998	8173	3.91238	8218	3.91477	8263	3.91714
8129	3.91004	8174	3.91243	819	3.91482	8264	3.91719
8130	3.91009	8175	3.91249	8220	3.91487	8265	3.91724
8131	3.91014	8176	3.91254	821	3.91492	8266	3.91730
8132	3.91020	8177	3.91259	8222	3.91498	8267	3.91735
8133	3.91025	8178	3.91265	8223	3.91503	8268	3.91740
8134	3.91030	8179	3.91270	8224	3.91508	8269	3.91745
8135	3.91036	8180	3.91275	8225	3.91514	8270	3.91751
8136	3.91041	8181	3.91281	8226	3.91519	8271	3.91756
8137	3.91046	8182	3.91286	8227	3.91524	8272	3.91761
8138	3.91052	8183	3.91291	8228	3.91529	8273	3.91766
8139	3.91057	8184	3.91297	8229	3.91535	8274	3.91772
8140	3.91062	8185	3.91302	8230	3.91540	875	3.91777
8141	3.91068	8186	3.91307	8231	3.91545	8276	3.91782
8142	3.91073	8187	3.91312	8232	3.91551	8277	3.91787
8143	3.91078	8188	3.91318	8233	3.91556	8278	3.91793
8144	3.91084	8189	3.91325	8234	3.91561	8279	3.91798
8145	3.91089	8190	3.91328	8235	3.91566	8280	3.91803

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
8281	3.91808	8326	3.92044	8371	3.92278	8416	3.92511
8282	3.91814	8327	3.92049	8372	3.92283	8417	3.92516
8283	3.91819	8328	3.92054	8373	3.92288	8418	3.92521
8284	3.91824	8329	3.92059	8374	3.92293	8419	3.92526
8285	3.91829	8330	3.92065	8375	3.92298	8420	3.92531
8286	3.91834	8331	3.92070	8376	3.92304	8421	3.92536
8287	3.91840	8332	3.92075	8377	3.92309	8422	3.92542
8288	3.91845	8333	3.92080	8378	3.92314	8423	3.92547
8289	3.91850	8334	3.92085	8379	3.92319	8424	3.92552
8290	3.91855	8335	3.92091	8380	3.92324	8425	3.92557
8291	3.91861	8336	3.92096	8381	3.92330	8426	3.92562
8292	3.91866	8337	3.92101	8382	3.92335	8427	3.92567
8293	3.91871	8338	3.92106	8383	3.92340	8428	3.92572
8294	3.91876	8339	3.92111	8384	3.92345	8429	3.92578
8295	3.91882	8340	3.92117	8385	3.92350	8430	3.92583
8296	3.91887	8341	3.92122	8386	3.92355	8431	3.92588
8297	3.91892	8342	3.92127	8387	3.92361	8432	3.92593
8298	3.91897	8343	3.92132	8388	3.92366	8433	3.92598
8299	3.91903	8344	3.92137	8389	3.92371	8434	3.92603
8300	3.91908	8345	3.92143	8390	3.92376	8435	3.92609
8301	3.91913	8346	3.92148	8391	3.92381	8436	3.92614
8302	3.91918	8347	3.92153	8392	3.92387	8437	3.92619
8303	3.91924	8348	3.92158	8393	3.92392	8438	3.92624
8304	3.91929	8349	3.92163	8394	3.92397	8439	3.92629
8305	3.91934	8350	3.92169	8395	3.92402	8440	3.92634
8306	3.91939	8351	3.92174	8396	3.92407	8441	3.92639
8307	3.91944	8352	3.92179	8397	3.92412	8442	3.92645
8308	3.91950	8353	3.92184	8398	3.92418	8443	3.92650
8309	3.91955	8354	3.92189	8399	3.92423	8444	3.92655
8310	3.91960	8355	3.92195	8400	3.92428	8445	3.92660
8311	3.91965	8356	3.92200	8401	3.92433	8446	3.92665
8312	3.91971	8357	3.92205	8402	3.92438	8447	3.92670
8313	3.91976	8358	3.92210	8403	3.92443	8448	3.92675
8314	3.91981	8359	3.92215	8404	3.92449	8449	3.92681
8315	3.91986	8360	3.92221	8405	3.92454	8450	3.92686
8316	3.91991	8361	3.92226	8406	3.92459	8451	3.92691
8317	3.91997	8362	3.92231	8407	3.92464	8452	3.92696
8318	3.92002	8363	3.92236	8408	3.92469	8453	3.92701
8319	3.92007	8364	3.92241	8409	3.92474	8454	3.92706
8320	3.92012	8365	3.92247	8410	3.92480	8455	3.92711
8321	3.92018	8366	3.92252	8411	3.92485	8456	3.92717
8322	3.92023	8367	3.92257	8412	3.92490	8457	3.92722
8323	3.92028	8368	3.92262	8413	3.92495	8458	3.92727
8324	3.92033	8369	3.92267	8414	3.92500	8459	3.92732
8325	3.92038	8370	3.92273	8415	3.92505	8460	3.92737

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
8461	3.92742	8506	3.92973	8551	3.93201	8596	3.93439
8462	3.92747	8507	3.92978	8552	3.93207	8597	3.93435
8463	3.92752	8508	3.92983	8553	3.93212	8598	3.93440
8464	3.92758	8509	3.92988	8554	3.93217	8599	3.93445
8465	3.92763	8510	3.92993	8555	3.93222	8600	3.93450
8466	3.92768	8511	3.92998	8556	3.93227	8601	3.93455
8467	3.92773	8512	3.93003	8557	3.93232	8602	3.93460
8468	3.92778	8513	3.93008	8558	3.93237	8603	3.93465
8469	3.92783	8514	3.93013	8559	3.93242	8604	3.93470
8470	3.92788	8515	3.93018	8560	3.93247	8605	3.93475
8471	3.92793	8516	3.93024	8561	3.93252	8606	3.93480
8472	3.92799	8517	3.93029	8562	3.93258	8607	3.93485
8473	3.92804	8518	3.93034	8563	3.93263	8608	3.93490
8474	3.92809	8519	3.93039	8564	3.93268	8609	3.93495
8475	3.92814	8520	3.93044	8565	3.93273	8610	3.93500
8476	3.92819	8521	3.93049	8566	3.93278	8611	3.93505
8477	3.92824	8522	3.93054	8567	3.93283	8612	3.93510
8478	3.92829	8523	3.93059	8568	3.93288	8613	3.93515
8479	3.92834	8524	3.93064	8569	3.93293	8614	3.93520
8480	3.92840	8525	3.93069	8570	3.93298	8615	3.93525
8481	3.92845	8526	3.93075	8571	3.93303	8616	3.93531
8482	3.92850	8527	3.93080	8572	3.93308	8617	3.93536
8483	3.92855	8528	3.93085	8573	3.93313	8618	3.93541
8484	3.92860	8529	3.93090	8574	3.93318	8619	3.93546
8485	3.92865	8530	3.93095	8575	3.93323	8620	3.93551
8486	3.92870	8531	3.93100	8576	3.93328	8621	3.93556
8487	3.92875	8532	3.93105	8577	3.93334	8622	3.93561
8488	3.92881	8533	3.93111	8578	3.93339	8623	3.93566
8489	3.92886	8534	3.93115	8579	3.93344	8624	3.93571
8490	3.92891	8535	3.93120	8580	3.93349	8625	3.93576
8491	3.92896	8536	3.93125	8581	3.93354	8626	3.93581
8492	3.92901	8537	3.93131	8582	3.93359	8627	3.93586
8493	3.92906	8538	3.93136	8583	3.93364	8628	3.93591
8494	3.92911	8539	3.93141	8584	3.93369	8629	3.93596
8495	3.92916	8540	3.93146	8585	3.93374	8630	3.93601
8496	3.92921	8541	3.93151	8586	3.93379	8631	3.93606
8497	3.92927	8542	3.93156	8587	3.93384	8632	3.93611
8498	3.92932	8543	3.93161	8588	3.93389	8633	3.93616
8499	3.92937	8544	3.93166	8589	3.93394	8634	3.93621
8500	3.92942	8545	3.93171	8590	3.93399	8635	3.93626
8501	3.92947	8546	3.93176	8591	3.93404	8636	3.93631
8502	3.92952	8547	3.93181	8592	3.93409	8637	3.93636
8503	3.92957	8548	3.93186	8593	3.93414	8638	3.93641
8504	3.92962	8549	3.93191	8594	3.93420	8639	3.93646
8505	3.92967	8550	3.93197	8595	3.93425	8640	3.93651

## A Table of Logarithms.

<i>N</i>	<i>Logar.</i>	<i>N</i>	<i>Logar.</i>	<i>N</i>	<i>Logar.</i>	<i>N</i>	<i>Logar.</i>
8641	3.93656	8686	3.93882	8731	3.94106	8776	3.94330
8642	3.93661	8687	3.93887	8732	3.94111	8777	3.94335
8643	3.93666	8688	3.93892	8733	3.94116	8778	3.94340
8644	3.93671	8689	3.93897	8734	3.94121	8779	3.94345
8645	3.93677	8690	3.93802	8735	3.94126	8780	3.94349
8646	3.93682	8691	3.93807	8736	3.94131	8781	3.94354
8647	3.93687	8692	3.93812	8737	3.94136	8782	3.94359
8648	3.93692	8693	3.93817	8738	3.94141	8783	3.94364
8649	3.93697	8694	3.93822	8739	3.94146	8784	3.94369
8650	3.93702	8695	3.93827	8740	3.94151	8785	3.94374
8651	3.93707	8696	3.93832	8741	3.94156	8786	3.94379
8652	3.93712	8697	3.93837	8742	3.94161	8787	3.94384
8653	3.93717	8698	3.93842	8743	3.94166	8788	3.94389
8654	3.93722	8699	3.93847	8744	3.94171	8789	3.94394
8655	3.93727	8700	3.93852	8745	3.94176	8790	3.94399
8656	3.93732	8701	3.93857	8746	3.94181	8791	3.94404
8657	3.93737	8702	3.93862	8747	3.94186	8792	3.94409
8658	3.93742	8703	3.93867	8748	3.94191	8793	3.94414
8659	3.93747	8704	3.93872	8749	3.94196	8794	3.94419
8660	3.93752	8705	3.93877	8750	3.94201	8795	3.94424
8661	3.93757	8706	3.93882	8751	3.94206	8796	3.94429
8662	3.93762	8707	3.93887	8752	3.94211	8797	3.94433
8663	3.93767	8708	3.93892	8753	3.94216	8798	3.94438
8664	3.93772	8709	3.93897	8754	3.94221	8799	3.94443
8665	3.93777	8710	3.94002	8755	3.94226	8800	3.94448
8666	3.93782	8711	3.94007	8756	3.94231	8801	3.94453
8667	3.93787	8712	3.94012	8757	3.94236	8802	3.94458
8668	3.93792	8713	3.94017	8758	3.94240	8803	3.94463
8669	3.93797	8714	3.94022	8759	3.94245	8804	3.94468
8670	3.93802	8715	3.94027	8760	3.94250	8805	3.94473
8671	3.93807	8716	3.94032	8761	3.94255	8806	3.94478
8672	3.93812	8717	3.94037	8762	3.94260	8807	3.94483
8673	3.93817	8718	3.94042	8763	3.94265	8808	3.94488
8674	3.93822	8719	3.94047	8764	3.94270	8809	3.94493
8675	3.93827	8720	3.94052	8765	3.94275	8810	3.94498
8676	3.93832	8721	3.94057	8766	3.94280	8811	3.94503
8677	3.93837	8722	3.94062	8767	3.94285	8812	3.94507
8678	3.93842	8723	3.94067	8768	3.94290	8813	3.94512
8679	3.93847	8724	3.94072	8769	3.94295	8814	3.94517
8680	3.93852	8725	3.94077	8770	3.94300	8815	3.94522
8681	3.93857	8726	3.94082	8771	3.94305	8816	3.94527
8682	3.93862	8727	3.94087	8772	3.94310	8817	3.94532
8683	3.93867	8728	3.94091	8773	3.94315	8818	3.94537
8684	3.93872	8729	3.94096	8774	3.94320	8819	3.94542
8685	3.93877	8730	3.94101	8775	3.94325	8820	3.94547

*A Table of Logarithms.*

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
8821	3.94552	8866	3.94773	8911	3.94993	8956	3.95211
8822	3.94557	8867	3.94778	8912	3.94998	8957	3.95211
8823	3.94562	8868	3.94783	8913	3.95002	8958	3.95226
8824	3.94567	8869	3.94787	8914	3.95007	8959	3.95226
8825	3.94571	8870	3.94792	8915	3.95012	8960	3.95231
8826	3.94576	8871	3.94797	8916	3.95017	8961	3.95236
8827	3.94581	8872	3.94802	8917	3.95022	8962	3.95240
8828	3.94586	8873	3.94807	8918	3.95027	8963	3.95245
8829	3.94591	8874	3.94812	8919	3.95032	8964	3.95250
8830	3.94596	8875	3.94817	8920	3.95036	8965	3.95255
8831	3.94600	8876	3.94822	8921	3.95041	8966	3.95260
8832	3.94606	8877	3.94827	8922	3.95046	8967	3.95265
8833	3.94611	8878	3.94832	8923	3.95051	8968	3.95270
8834	3.94616	8879	3.94836	8924	3.95056	8969	3.95274
8835	3.94621	8880	3.94841	8925	3.95061	8970	3.95279
8836	3.94626	8881	3.94846	8926	3.95066	8971	3.95284
8837	3.94630	8882	3.94851	8927	3.95071	8972	3.95289
8838	3.94635	8883	3.94856	8928	3.95075	8973	3.95294
8839	3.94640	8884	3.94861	8929	3.95080	8974	3.95299
8840	3.94645	8885	3.94866	8930	3.95085	8975	3.95303
8841	3.94650	8886	3.94871	8931	3.95090	8976	3.95308
8842	3.94655	8887	3.94876	8932	3.95095	8977	3.95313
8843	3.94660	8888	3.94880	8933	3.95100	8978	3.95318
8844	3.94665	8889	3.94885	8934	3.95105	8979	3.95323
8845	3.94670	8890	3.94890	8935	3.95109	8980	3.95328
8846	3.94675	8891	3.94895	8936	3.95114	8981	3.95332
8847	3.94680	8892	3.94900	8937	3.95119	8982	3.95337
8848	3.94685	8893	3.94905	8938	3.95124	8983	3.95342
8849	3.94689	8894	3.94910	8939	3.95129	8984	3.95347
8850	3.94694	8895	3.94915	8940	3.95134	8985	3.95352
8851	3.94699	8896	3.94919	8941	3.95139	8986	3.95357
8852	3.94704	8897	3.94924	8942	3.95143	8987	3.95361
8853	3.94709	8898	3.94929	8943	3.95148	8988	3.95366
8854	3.94714	8899	3.94934	8944	3.95153	8989	3.95371
8855	3.94719	8900	3.94939	8945	3.95158	8990	3.95376
8856	3.94724	8901	3.94944	8946	3.95163	8991	3.95381
8857	3.94729	8902	3.94949	8947	3.95168	8992	3.95386
8858	3.94734	8903	3.94954	8948	3.95173	8993	3.95390
8859	3.94738	8904	3.94959	8949	3.95177	8994	3.95395
8860	3.94743	8905	3.94963	8950	3.95182	8995	3.95400
8861	3.94748	8906	3.94968	8951	3.95187	8996	3.95405
8862	3.94753	8907	3.94973	8952	3.95192	8997	3.95410
8863	3.94758	8908	3.94978	8953	3.95197	8998	3.95415
8864	3.94763	8909	3.94983	8954	3.95202	8999	3.95419
8865	3.94768	8910	3.94988	8955	3.95207	9000	3.95424

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
9000	3.95429	9046	3.95646	9091	3.95861	9136	3.96076
9002	3.95434	9047	3.95650	9092	3.95866	9137	3.96080
9003	3.95439	9048	3.95655	9093	3.95871	9138	3.96085
9004	3.95444	9049	3.95660	9094	3.95875	9139	3.96090
9005	3.95448	9050	3.95665	9095	3.95880	9140	3.96095
9006	3.95453	9051	3.95670	9096	3.95885	9141	3.96099
9007	3.95458	9052	3.95675	9097	3.95890	9142	3.96104
9008	3.95463	9053	3.95679	9098	3.95895	9143	3.96109
9009	3.95468	9054	3.95684	9099	3.95899	9144	3.96114
9010	3.95472	9055	3.95689	9100	3.95904	9145	3.96118
9011	3.95477	9056	3.95694	9101	3.95909	9146	3.96123
9012	3.95482	9057	3.95698	9102	3.95914	9147	3.96128
9013	3.95487	9058	3.95703	9103	3.95918	9148	3.96133
9014	3.95492	9059	3.95708	9104	3.95923	9149	3.96137
9015	3.95497	9060	3.95713	9105	3.95928	9150	3.96142
9016	3.95501	9061	3.95718	9106	3.95933	9151	3.96147
9017	3.95506	9062	3.95722	9107	3.95938	9152	3.96152
9018	3.95511	9063	3.95727	9108	3.95942	9153	3.96156
9019	3.95516	9064	3.95732	9109	3.95947	9154	3.96161
9020	3.95521	9065	3.95737	9110	3.95952	9155	3.96166
9021	3.95525	9066	3.95742	9111	3.95957	9156	3.96171
9022	3.95530	9067	3.95746	9112	3.95961	9157	3.96175
9023	3.95535	9068	3.95751	9113	3.95966	9158	3.96180
9024	3.95540	9069	3.95756	9114	3.95971	9159	3.96185
9025	3.95545	9070	3.95761	9115	3.95976	9160	3.96190
9026	3.95550	9071	3.95766	9116	3.95980	9161	3.96194
9027	3.95554	9072	3.95770	9117	3.95985	9162	3.96199
9028	3.95559	9073	3.95775	9118	3.95990	9163	3.96204
9029	3.95564	9074	3.95780	9119	3.95995	9164	3.96209
9030	3.95569	9075	3.95785	9120	3.95999	9165	3.96213
9031	3.95574	9076	3.95789	9121	3.96004	9166	3.96218
9032	3.95578	9077	3.95794	9122	3.96009	9167	3.96223
9033	3.95583	9078	3.95799	9123	3.96014	9168	3.96227
9034	3.95588	9079	3.95804	9124	3.96019	9169	3.96232
9035	3.95593	9080	3.95809	9125	3.96023	9170	3.96237
9036	3.95598	9081	3.95813	9126	3.96028	9171	3.96242
9037	3.95602	9082	3.95818	9127	3.96033	9172	3.96246
9038	3.95607	9083	3.95823	9128	3.96038	9173	3.96251
9039	3.95611	9084	3.95828	9129	3.96042	9174	3.96256
9040	3.95617	9085	3.95832	9130	3.96047	9175	3.96261
9041	3.95622	9086	3.95837	9131	3.96052	9176	3.96265
9042	3.95626	9087	3.95842	9132	3.96057	9177	3.96270
9043	3.95631	9088	3.95847	9133	3.96061	9178	3.96275
9044	3.95636	9089	3.95852	9134	3.96066	9179	3.96280
9045	3.95641	9090	3.95856	9135	3.96071	9180	3.96284

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
9181	3.96289	9226	3.96501	9271	3.96713	9315	3.96923
9182	3.96294	9227	3.96506	9272	3.96717	9317	3.96928
9183	3.96298	9228	3.96511	9273	3.96722	9318	3.96932
9184	3.96303	9229	3.96515	9274	3.96727	9319	3.96937
9185	3.96308	9230	3.96520	9275	3.96731	9320	3.96942
9186	3.96313	9231	3.96525	9276	3.96736	9321	3.96946
9187	3.96317	9232	3.96530	9277	3.96741	9322	3.96951
9188	3.96322	9233	3.96534	9278	3.96745	9323	3.96956
9189	3.96327	9234	3.96539	9279	3.96750	9324	3.96960
9190	3.96331	9235	3.96544	9280	3.96755	9325	3.96965
9191	3.96336	9236	3.96548	9281	3.96759	9326	3.96970
9192	3.96341	9237	3.96553	9282	3.96764	9327	3.96974
9193	3.96346	9238	3.96558	9283	3.96769	9328	3.96979
9194	3.96350	9239	3.96563	9284	3.96774	9329	3.96984
9195	3.96355	9240	3.96567	9285	3.96778	9330	3.96988
9196	3.96360	9241	3.96572	9286	3.96783	9331	3.96993
9197	3.96365	9242	3.96577	9287	3.96788	9332	3.96997
9198	3.96369	9243	3.96581	9288	3.96792	9333	3.97002
9199	3.96374	9244	3.96586	9289	3.96797	9334	3.97007
9200	3.96379	9245	3.96591	9290	3.96802	9335	3.97011
9201	3.96384	9246	3.96595	9291	3.96806	9336	3.97016
9202	3.96388	9247	3.96600	9292	3.96811	9337	3.97021
9203	3.96393	9248	3.96605	9293	3.96816	9338	3.97025
9204	3.96398	9249	3.96609	9294	3.96820	9339	3.97030
9205	3.96402	9250	3.96614	9295	3.96825	9340	3.97035
9206	3.96407	9251	3.96619	9296	3.96830	9341	3.97039
9207	3.96412	9252	3.96624	9297	3.96834	9342	3.97044
9208	3.96417	9253	3.96628	9298	3.96839	9343	3.97049
9209	3.96421	9254	3.96633	9299	3.96844	9344	3.97053
9210	3.96426	9255	3.96638	9300	3.96848	9345	3.97058
9211	3.96431	9256	3.96642	9301	3.96853	9346	3.97063
9212	3.96435	9257	3.96647	9302	3.96858	9347	3.97067
9213	3.96440	9258	3.96652	9303	3.96862	9348	3.97072
9214	3.96445	9259	3.96656	9304	3.96867	9349	3.97077
9215	3.96450	9260	3.96661	9305	3.96872	9350	3.97081
9216	3.96454	9261	3.96666	9306	3.96876	9351	3.97086
9217	3.96459	9262	3.96670	9307	3.96881	9352	3.97090
9218	3.96464	9263	3.96675	9308	3.96886	9353	3.97095
9219	3.96468	9264	3.96680	9309	3.96890	9354	3.97100
9220	3.96473	9265	3.96685	9310	3.96895	9355	3.97104
9221	3.96478	9266	3.96689	9311	3.96900	9356	3.97109
9222	3.96483	9267	3.96694	9312	3.96904	9357	3.97114
9223	3.96487	9268	3.96699	9313	3.96909	9358	3.97118
9224	3.96492	9269	3.96703	9314	3.96914	9359	3.97123
9225	3.96497	9270	3.96708	9315	3.96918	9360	3.97128

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
9361	3.97132	9406	3.97341	9451	3.97548	9496	3.97754
9362	3.97137	9407	3.97345	9452	3.97552	9497	3.97759
9363	3.97142	9408	3.97350	9453	3.97557	9498	3.97763
9364	3.97146	9409	3.97354	9454	3.97562	9499	3.97768
9365	3.97151	9410	3.97359	9455	3.97566	9500	3.97772
9366	3.97155	9411	3.97364	9456	3.97571	9501	3.97777
9367	3.97160	9412	3.97368	9457	3.97575	9502	3.97782
9368	3.97165	9413	3.97373	9458	3.97580	9503	3.97786
9369	3.97169	9414	3.97377	9459	3.97585	9504	3.97791
9370	3.97174	9415	3.97382	9460	3.97589	9505	3.97795
9371	3.97179	9416	3.97387	9461	3.97594		3.97800
9372	3.97183	9417	3.97391	9462	3.97598	9507	3.97804
9373	3.97188	9418	3.97396	9463	3.97602	9508	3.97809
9374	3.97192	9419	3.97400	9464	3.97607	9509	3.97813
9375	3.97197	9420	3.97405	9465	3.97612	9510	3.97818
9376	3.97202	9421	3.97410	9466	3.97617	9511	3.97823
9377	3.97206	9422	3.97414	9467	3.97621	9512	3.97827
9378	3.97211	9423	3.97419	9468	3.97626	9513	3.97832
9379	3.97216	9424	3.97424	9469	3.97630	9514	3.97836
9380	3.97220	9425	3.97428	9470	3.97635	9515	3.97841
9381	3.97225	9426	3.97433	9471	3.97640	9516	3.97845
9382	3.97230	9427	3.97437	9472	3.97644	9517	3.97850
9383	3.97234	9428	3.97442	9473	3.97649	9518	3.97855
9384	3.97239	9429	3.97447	9474	3.97653	9519	3.97859
9385	3.97243	9430	3.97451	9475	3.97658	9520	3.97864
9386	3.97248	9431	3.97456	9476	3.97663	9521	3.97868
9387	3.97253	9432	3.97460	9477	3.97667	9522	3.97875
9388	3.97257	9433	3.97465	9478	3.97672	9523	3.97877
9389	3.97262	9434	3.97470	9479	3.97676	9524	3.97882
9390	3.97267	9435	3.97474	9480	3.97681	9525	3.97887
9391	3.97271	9436	3.97479	9481	3.97685	9526	3.97891
9392	3.97276	9437	3.97483	9482	3.97690	9527	3.97896
9393	3.97280	9438	3.97488	9483	3.97695	9528	3.97900
9394	3.97285	9439	3.97493	9484	3.97699	9529	3.97905
9395	3.97290	9440	3.97497	9485	3.97704	9530	3.97909
9396	3.97294	9441	3.97502	9486	3.97708	9531	3.97914
9397	3.97299	9442	3.97506	9487	3.97713	9532	3.97918
9398	3.97304	9443	3.97511	9488	3.97717	9533	3.97923
9399	3.97308	9444	3.97516	9489	3.97722	9534	3.97928
9400	3.97313	9445	3.97520	9490	3.97727	9535	3.97932
9401	3.97317	9446	3.97525	9491	3.97731	9536	3.97937
9402	3.97322	9447	3.97529	9492	3.97736	9537	3.97941
9403	3.97327	9448	3.97534	9493	3.97740	9538	3.97946
9404	3.97331	9449	3.97539	9494	3.97745	9539	3.97950
9405	3.97336	9450	3.97543	9495	3.97750	9540	3.97955

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
9541	3.97959	9586	3.98164	9631	3.98291	9676	3.98570
9542	3.97964	9587	3.98168	9632	3.98372	9677	3.98574
9543	3.97968	9588	3.98173	9633	3.98376	9678	3.98579
9544	3.97973	9589	3.98177	9634	3.98381	9679	3.98583
9545	3.97978	9590	3.98182	9635	3.98385	9680	3.98588
9546	3.97982	9591	3.98186	9636	3.98390	9681	3.98592
9547	3.97987	9592	3.98191	9637	3.98394	9682	3.98597
9548	3.97991	9593	3.98195	9638	3.98399	9683	3.98601
9549	3.97996	9594	3.98200	9639	3.98403	9684	3.98605
9550	3.98000	9595	3.98205	9640	3.98408	9685	3.98610
9551	3.98005	9596	3.98209	9641	3.98412	9686	3.98614
9552	3.98009	9597	3.98214	9642	3.98417	9687	3.98619
9553	3.98014	9598	3.98218	9643	3.98421	9688	3.98623
9554	3.98019	9599	3.98223	9644	3.98426	9689	3.98628
9555	3.98023	9600	3.98227	9645	3.98430	9690	3.98632
9556	3.98028	9601	3.98232	9646	3.98435	9691	3.98637
9557	3.98032	9602	3.98236	9647	3.98439	9692	3.98641
9558	3.98037	9603	3.98241	9648	3.98444	9693	3.98646
9559	3.98041	9604	3.98245	9649	3.98448	9694	3.98650
9560	3.98046	9605	3.98250	9650	3.98453	9695	3.98655
9561	3.98050	9606	3.98254	9651	3.98457	9696	3.98659
9562	3.98055	9607	3.98259	9652	3.98462	9697	3.98664
9563	3.98059	9608	3.98263	9653	3.98466	9698	3.98668
9564	3.98064	9609	3.98268	9654	3.98471	9699	3.98673
9565	3.98069	9610	3.98272	9655	3.98475	9700	3.98677
9566	3.98073	9611	3.98277	9656	3.98480	9701	3.98682
9567	3.98078	9612	3.98281	9657	3.98484	9702	3.98686
9568	3.98082	9613	3.98286	9658	3.98489	9703	3.98691
9569	3.98087	9614	3.98290	9659	3.98493	9704	3.98695
9570	3.98091	9615	3.98295	9660	3.98498	9705	3.98700
9571	3.98096	9616	3.98299	9661	3.98502	9706	3.98704
9572	3.98100	9617	3.98304	9662	3.98507	9707	3.98709
9573	3.98105	9618	3.98308	9663	3.98511	9708	3.98713
9574	3.98109	9619	3.98313	9664	3.98516	9709	3.98717
9575	3.98114	9620	3.98318	9665	3.98520	9710	3.98722
9576	3.98118	9621	3.98322	9666	3.98525	9711	3.98726
9577	3.98123	9622	3.98327	9667	3.98529	9712	3.98731
9578	3.98127	9623	3.98331	9668	3.98534	9713	3.98735
9579	3.98132	9624	3.98336	9669	3.98538	9714	3.98740
9580	3.98137	9625	3.98340	9670	3.98543	9715	3.98744
9581	3.98141	9626	3.98345	9671	3.98547	9716	3.98749
9582	3.98146	9627	3.98349	9672	3.98552	9717	3.98753
9583	3.98150	9628	3.98354	9673	3.98556	9718	3.98758
9584	3.98155	9629	3.98358	9674	3.98561	9719	3.98762
9585	3.98159	9630	3.98363	9675	3.98565	9720	3.98767

## A Table of Logarithms.

N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
9721	3.98771	9722	3.98776	9723	3.98780	9724	3.98784
9725	3.98789	9726	3.98793	9727	3.98798	9728	3.98802
9729	3.98807	9730	3.98811	9731	3.98816	9732	3.98820
9733	3.98825	9734	3.98829	9735	3.98834	9736	3.98838
9737	3.98843	9738	3.98847	9739	3.98851	9740	3.98856
9741	3.98860	9742	3.98865	9743	3.98869	9744	3.98874
9745	3.98878	9746	3.98883	9747	3.98887	9748	3.98892
9749	3.98896	9750	3.98900	9751	3.98905	9752	3.98909
9753	3.98914	9754	3.98918	9755	3.98922	9756	3.98927
9757	3.98932	9758	3.98936	9759	3.98941	9760	3.98945
9761	3.98949	9762	3.98954	9763	3.98958	9764	3.98963
9765	3.98967	9800	3.99105	9797	3.99109	9798	3.99114
9799	3.99118	9800	3.99123	9801	3.99127	9802	3.99131
9803	3.99136	9804	3.99140	9805	3.99145	9806	3.99149
9807	3.99154	9808	3.99158	9809	3.99162	9810	3.99167
9811	3.99171	9812	3.99176	9813	3.99180	9814	3.99185
9815	3.99189	9816	3.99193	9817	3.99198	9818	3.99202
9819	3.99207	9820	3.99211	9821	3.99216	9822	3.99221
9823	3.99224	9824	3.99229	9825	3.99233	9826	3.99238
9827	3.99242	9828	3.99247	9829	3.99251	9830	3.99255
9831	3.99260	9832	3.99264	9833	3.99269	9834	3.99273
9835	3.99277	9836	3.99282	9837	3.99286	9838	3.99291
9839	3.99295	9840	3.99300	9841	3.99304	9842	3.99308
9843	3.99313	9844	3.99317	9845	3.99322	9846	3.99326
9847	3.99330	9848	3.99335	9849	3.99339	9850	3.99344
9851	3.99348	9852	3.99352	9853	3.99357	9854	3.99361
9855	3.99366	9856	3.99370	9857	3.99374	9858	3.99379
9859	3.99383	9860	3.99388	9861	3.99392	9862	3.99397
9863	3.99401	9864	3.99405	9865	3.99410	9866	3.99414
9867	3.99419	9868	3.99423	9869	3.99427	9870	3.99432
9871	3.99436	9872	3.99441	9873	3.99445	9874	3.99449
9875	3.99454	9876	3.99458	9877	3.99463	9878	3.99467
9879	3.99471	9880	3.99476	9881	3.99480	9882	3.99484
9883	3.99489	9884	3.99493	9885	3.99498	9886	3.99502
9887	3.99506	9888	3.99511	9889	3.99515	9890	3.99520
9891	3.99524	9892	3.99528	9893	3.99533	9894	3.99537
9895	3.99542	9896	3.99546	9897	3.99550	9898	3.99555
9899	3.99559	9900	3.99564				

A Table of Logarithms.

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N.	Logar.	N.	Logar.	N.	Logar.	N.	Logar.
9905	3.9968	9926	3.99677	9951	3.99787	9976	3.99896
9906	3.99672	9927	3.99682	9952	3.99791	9977	3.99900
9903	3.99577	9928	3.99686	9953	3.99795	9978	3.99904
9904	3.99581	9929	3.99691	9954	3.99800	9979	3.99909
9905	3.99585	9930	3.99695	9955	3.99804	9980	3.99913
9906	3.99590	9931	3.99699	9956	3.99808	9981	3.99917
9907	3.99594	9932	3.99704	9957	3.99813	9982	3.99922
9908	3.99597	9933	3.99708	9958	3.99817	9983	3.99926
9909	3.99603	9934	3.99712	9959	3.99822	9984	3.99930
9910	3.99607	9935	3.99717	9960	3.99826	9985	3.99935
9911	3.99612	9936	3.99721	9961	3.99830	9986	3.99939
9912	3.99616	9937	3.99726	9962	3.99835	9987	3.99944
9913	3.99621	9938	3.99730	9963	3.99839	9988	3.99948
9914	3.99625	9939	3.99734	9964	3.99843	9989	3.99952
9915	3.99629	9940	3.99739	9965	3.99848	9990	3.99957
9916	3.99634	9941	3.99743	9966	3.99852	9991	3.99961
9917	3.99638	9942	3.99747	9967	3.99856	9992	3.99965
9918	3.99642	9943	3.99752	9968	3.99861	9993	3.99970
9919	3.99647	9944	3.99756	9969	3.99865	9994	3.99974
9920	3.99651	9945	3.99760	9970	3.99870	9995	3.99978
9921	3.99656	9946	3.99765	9971	3.99874	9996	3.99982
9922	3.99660	9947	3.99769	9972	3.99878	9997	3.99987
9923	3.99664	9948	3.99774	9973	3.99883	9998	3.99991
9924	3.99669	9949	3.99778	9974	3.99887	9999	3.99996
9925	3.99673	9950	3.99782	9975	3.99891	10000	4.00000

b

A T A.

The Logarithm of a Fraction, being a Decimal, is the same with an integer; only the Index is negative, and is so much less than 0, as of the Decimal is removed from Unity, and these Indices may be diff'd from the Absolute ones, by setting a Negative Sign over them.

As for Exam-

Indices	3	3	7	6	5
Numbers	7	6	7	6	2

Place  
with

Here the first Place of Decimal has for its Index 9, of the second 7, of the third 7.

4568	8.65973
4563	2.65973
45.68	1.65973
4.568	0.65973
.4568	9.65973
.04568	8.65973
.004568	7.65973

Another Example.

N.B. The Logarithm is the same, only the Index differs according to the Value of the left Hand Figure or the given Number.

To find the Logarithm of a Vulgar Fraction, Subtract the Logarithm of the Denominator out of the Logarithm of the Numerator, the Remainder is the Logarithm of a Decimal equivalent to the Vulgar-Fraction.

Example 2.

3   0.47712
4   0.60106
75 : 9.87506

The Operation of Decimal Fractions is the same as of whole Numbers, both in Natural and Logarithmical Arithmetic, remembering these 3 Cautions. 1. If we are to subtract a greater Logarithm out of a less, we add 10 to the Index of the less, and 2. If the Logarithm which answers the Question (whether be Sum, Remainder, Half, Third, &c.) if the Index be Ten, Twenty, &c. neglect or cancel the said Figure in the Place of Tens in the Characteristic. Lastly, In extracting the Square Root of a Decimal, add 10 to its Index, and then halve it, and in extracting the Cube Root add 20 to its Index, and then take its third and in finding a mean between two Numbers, (if one be a Decimal and the Sum of the Indices be 10) reject 10, and halve the rest, but if it be not 10, add 10 to it, and then halve it.

In Arithmetical Operations of Cases of Trigonometry, where Radius is not concerned, the Work may be abbreviated by taking the Arithmetical Complement of the Logarithm of the first term) which is found by taking the Remainder of each Figure to 9, only that on the right hand to 10) and adding it to the Logarithms of the second and third Terms, the Sum abating Radius is the fourth Term required.

To find 2 or more Proportionals between 2 Numbers: Subtract the Logarithm of the less Number out of the Logarithm of the greater, the Remainder divide by a Number greater by one, than the Number of Means sought as here by 4 for three Means.

Example 12. and 15.

73	1.07918
.25	9.39794
	1.68124
	42031
	9.39794
1st. Mean .658	9.81815
	42031
ad. Mean 1.732	10.23856
	42031
ad. Mean 4.556	9.65887

The Quotient added to the Logarithm of the lesser Number, the Sum is the Logarithm of the first Mean, to which adding again the said Quotient the Sum is the Logarithm of the second Mean, and so forward for as many Means as the Quotient was at first order'd for.

A  
**T A B L E**  
O F

Artificial SINES, TANGENTS  
and SECANTS, the Radius  
10.00000; and to every Degree  
and Minute of the *Quadrant.*

# A Table of Artificial Sines;

o Degree.

Min.	Sine.	Tang.	Secant.	Min.
00.00000	0.00000	0.00000	Infinite.	10.00000
16.46373	9.99999	6.46373	13.53627	10.00001
26.76476	9.99995	6.76476	13.23524	10.00001
36.94085	9.99999	6.94085	13.05915	10.00001
47.00579	9.99999	7.00579	12.93421	10.00001
57.16270	9.99999	7.16270	12.83730	10.00001
67.24188	9.99999	7.24188	12.75812	10.00001
77.30882	9.99999	7.30882	12.69118	10.00001
87.36682	9.99999	7.36682	12.63318	10.00001
97.41797	9.99999	7.41797	12.58203	10.00001
107.46373	9.99999	7.46373	12.53627	10.00001
117.50512	9.99999	7.50512	12.49488	10.00001
127.54291	9.99999	7.54291	12.45709	10.00001
137.57767	9.99999	7.57767	12.42233	10.00001
147.60985	9.99999	7.60985	12.39014	10.00001
157.63982	9.99999	7.63982	12.36018	10.00001
167.66784	9.99999	7.66784	12.33215	10.00001
177.69417	9.99999	7.69417	12.30582	10.00001
187.71900	9.99999	7.71900	12.28100	10.00001
197.74248	9.99999	7.74248	12.25752	10.00001
207.76475	9.99999	7.76475	12.23524	10.00001
217.78594	9.99999	7.78594	12.21405	10.00001
227.80615	9.99999	7.80616	12.19385	10.00001
237.82545	9.99999	7.82545	12.17454	10.00001
247.84393	9.99999	7.84393	12.15606	10.00001
257.86166	9.99999	7.86167	12.13833	10.00001
267.87870	9.99999	7.87871	12.12129	10.00001
277.89509	9.99999	7.89510	12.10490	10.00001
287.91088	9.99999	7.91089	12.08911	10.00001
297.92612	9.99998	7.92613	12.07387	10.00002
307.94084	9.99998	7.94086	12.05917	10.00002
	Sine.	Tang.	Secant.	Min.

# Tangents and Secants.

Degree.

M	Sin.	Tang.	Secant.	
30	7.94084	9.99998	7.94086	12.05914
31	7.95508	9.99998	7.95510	12.04490
32	7.96887	9.99998	7.96889	12.03111
33	7.98225	9.99998	7.98225	12.01775
34	7.99520	9.99998	7.99522	12.00478
35	8.00779	9.99998	8.00781	11.99219
36	8.02002	9.99998	8.02004	11.97996
37	8.03192	9.99998	8.03195	11.96806
38	8.04350	9.99997	8.04353	11.95647
39	8.05478	9.99997	8.05481	11.94519
40	8.06578	9.99997	8.06581	11.93419
41	8.07650	9.99997	8.07653	11.92347
42	8.08697	9.99997	8.08700	11.91300
43	8.09718	9.99997	8.09722	11.90278
44	8.10717	9.99996	8.10720	11.89280
45	8.11693	9.99996	8.11696	11.88304
46	8.12647	9.99996	8.12651	11.87349
47	8.13581	9.99996	8.13585	11.86415
48	8.14495	9.99996	8.14500	11.85500
49	8.15391	9.99996	8.15395	11.84605
50	8.16268	9.99995	8.16273	11.83727
51	8.17128	9.99995	8.17133	11.82867
52	8.17971	9.99995	8.17976	11.82024
53	8.18799	9.99995	8.18804	11.81196
54	8.19610	9.99995	8.19616	11.80384
55	8.20407	9.99994	8.20413	11.79587
56	8.21190	9.99994	8.21195	11.78805
57	8.21958	9.99994	8.21964	11.78036
58	8.22713	9.99994	8.22720	11.77281
59	8.23456	9.99994	8.23462	11.76538
60	8.24186	9.99993	8.24192	11.75808
		Sine.	Tang.	Secant.

# A Table of Artificial Sines

I Degree.

Min.	Sine.	Tang.	Secant.	Min.			
0	8.24186	9.99993	8.24192	11.75808	10.00007	11.75315	60
1	8.24903	9.99993	8.24910	11.75090	10.00007	11.75097	59
2	8.25609	9.99993	8.25617	11.74384	10.00007	11.74391	58
3	8.26304	9.99993	8.26312	11.73689	10.00007	11.73695	57
4	8.26988	9.99993	8.26996	11.73004	10.00007	11.73012	56
5	8.27661	9.99992	8.27669	11.72331	10.00008	11.72339	55
6	8.28324	9.99992	8.28332	11.71668	10.00008	11.71676	54
7	8.28977	9.99992	8.28986	11.71014	10.00008	11.71023	53
8	8.29621	9.99992	8.29629	11.70371	10.00008	11.70379	52
9	8.30255	9.99991	8.30263	11.69737	10.00009	11.69745	51
10	8.30879	9.99991	8.30888	11.69112	10.00009	11.69121	50
11	8.31495	9.99991	8.31505	11.68495	10.00009	11.68505	49
12	8.32103	9.99991	8.32112	11.67888	10.00009	11.67897	48
13	8.32702	9.99990	8.32711	11.67289	10.00010	11.67298	47
14	8.33292	9.99990	8.33303	11.66698	10.00010	11.66708	46
15	8.33875	9.99990	8.33886	11.66114	10.00010	11.66125	45
16	8.34450	9.99989	8.34461	11.65539	10.00011	11.65550	44
17	8.35018	9.99989	8.35029	11.64971	10.00011	11.64982	43
18	8.35578	9.99989	8.35590	11.64411	10.00011	11.64422	42
19	8.36132	9.99989	8.36143	11.63857	10.00011	11.63869	41
20	8.36678	9.99988	8.36689	11.63311	10.00012	11.63322	40
21	8.37217	9.99988	8.37229	11.62771	10.00012	11.62783	39
22	8.37750	9.99988	8.37762	11.62238	10.00012	11.62250	38
23	8.38276	9.99987	8.38289	11.61711	10.00013	11.61724	37
24	8.38796	9.99987	8.38809	11.61191	10.00013	11.61204	36
25	8.39310	9.99987	8.39323	11.60677	10.00013	11.60690	35
26	8.39818	9.99986	8.39832	11.60169	10.00014	11.60182	34
27	8.40320	9.99986	8.40334	11.59666	10.00014	11.59680	33
28	8.40816	9.99986	8.40830	11.59170	10.00014	11.59184	32
29	8.41307	9.99985	8.41321	11.58679	10.00015	11.58693	31
30	8.41792	9.99985	8.41807	11.58193	10.00015	11.58208	30
	Sine.	Tang.	Secant.	Min.			

# Tangents and Secants.

**I Degrees.**

M.		Tang.		Secant.	
30	8.41792	9.99985	8.41807	11.58193	10.00015
31	8.42272	9.99985	8.42287	11.57713	10.00015
32	8.42746	9.99984	8.42762	11.57258	10.00016
33	8.43216	9.99984	8.43232	11.56769	10.00016
34	8.43680	9.99984	8.43696	11.56304	10.00016
35	8.44139	9.99983	8.44156	11.55844	10.00017
36	8.44594	9.99983	8.44611	11.55389	10.00017
37	8.45044	9.99983	8.45061	11.54939	10.00017
38	8.45489	9.99982	8.45507	11.54493	10.00018
39	8.45930	9.99982	8.45948	11.54052	10.00018
40	8.46360	9.99982	8.46385	11.53615	10.00018
41	8.46799	9.99981	8.46817	11.53183	10.00019
42	8.47226	9.99981	8.47245	11.52755	10.00019
43	8.47650	9.99981	8.47669	11.52331	10.00019
44	8.48069	9.99980	8.48089	11.51911	10.00020
45	8.48485	9.99980	8.48505	11.51495	10.00020
46	8.48896	9.99979	8.48917	11.51083	10.00021
47	8.49304	9.99979	8.49325	11.50675	10.00021
48	8.49708	9.99979	8.49729	11.50271	10.00021
49	8.50108	9.99978	8.50130	11.49870	10.00022
50	8.50505	9.99978	8.50527	11.49473	10.00022
51	8.50897	9.99977	8.50920	11.49080	10.00023
52	8.51287	9.99977	8.51310	11.48690	10.00023
53	8.51673	9.99977	8.51696	11.48304	10.00023
54	8.52055	9.99976	8.52079	11.47921	10.00024
55	8.52434	9.99976	8.52459	11.47541	10.00024
56	8.52810	9.99975	8.52833	11.47165	10.00025
57	8.53183	9.99975	8.53208	11.46792	10.00025
58	8.53552	9.99974	8.53576	11.46422	10.00026
59	8.53919	9.99974	8.53945	11.46055	10.00026
60	8.54282	9.99974	8.54308	11.45692	10.00026
		Sine.	Tang.	Secant.	Min.

# A Table of Artificial Sines.

2 Degrees.

Min.	Sine.		Tang.		Secant.
0	8.54282	9.99974	8.54308	11.45692	10.00026
1	8.54642	9.99973	8.54669	11.45331	10.00027
2	8.55000	9.99973	8.55027	11.44973	10.00027
3	8.55354	9.99972	8.55382	11.44618	10.00028
4	8.55705	9.99972	8.55734	11.44266	10.00028
5	8.56054	9.99971	8.56083	11.43917	10.00029
6	8.56400	9.99970	8.56429	11.43571	10.00030
7	8.56743	9.99970	8.56713	11.43227	10.00030
8	8.57084	9.99970	8.57114	11.42886	10.00030
9	8.57421	9.99970	8.57452	11.42548	10.00031
10	8.57757	9.99969	8.57788	11.42212	10.00031
11	8.58089	9.99968	8.58121	11.41879	10.00032
12	8.58419	9.99968	8.58451	11.41549	10.00032
13	8.58747	9.99968	8.58779	11.41221	10.00032
14	8.59072	9.99967	8.59105	11.40895	10.00033
15	8.59395	9.99967	8.59428	11.40572	10.00033
16	8.59715	9.99966	8.59749	11.40251	10.00034
17	8.60033	9.99966	8.60068	11.39932	10.00034
18	8.60349	9.99965	8.60384	11.39616	10.00035
19	8.60662	9.99965	8.60698	11.39302	10.00035
20	8.60973	9.99964	8.61009	11.38991	10.00036
21	8.61282	9.99964	8.61319	11.38681	10.00036
22	8.61589	9.99963	8.61626	11.38374	10.00037
23	8.61894	9.99962	8.61931	11.38069	10.00038
24	8.62196	9.99962	8.62234	11.37766	10.00038
25	8.62497	9.99961	8.62535	11.37465	10.00039
26	8.62795	9.99960	8.62834	11.37166	10.00040
27	8.63091	9.99960	8.63131	11.36869	10.00040
28	8.63385	9.99960	8.63426	11.36574	10.00040
29	8.63678	9.99960	8.63718	11.36282	10.00040
30	8.63968	9.99959	8.64009	11.35991	10.00041
		Sine.	Tang.	Secant.	

87 Degrees.

# Tangents and Secants.

$\pi$  Degrees.

$\pi$	Sine.	Tang.	Secant.	Min.		
30	8.63268	9.99959	8.64009	11.35991	10.00041	11.3603230
31	8.64256	9.99958	8.64298	11.35702	10.00042	11.3574429
32	8.64543	9.99958	8.64585	11.35415	10.00043	11.3545728
33	8.64827	9.99957	8.64870	11.35130	10.00043	11.3517327
34	8.65110	9.99956	8.65154	11.34846	10.00044	11.3489026
35	8.65391	9.99956	8.65435	11.34565	10.00044	11.3460925
36	8.65670	9.99955	8.65715	11.34285	10.00045	11.3433024
37	8.65948	9.99955	8.65993	11.34007	10.00045	11.3405323
38	8.66223	9.99954	8.66269	11.33731	10.00046	11.3377722
39	8.66497	9.99954	8.66543	11.33457	10.00047	11.3350321
40	8.66769	9.99953	8.66816	11.33184	10.00047	11.3323120
41	8.67039	9.99952	8.67087	11.32913	10.00048	11.3296119
42	8.67308	9.99952	8.67356	11.32644	10.00048	11.3269218
43	8.67575	9.99951	8.67624	11.32376	10.00049	11.3242517
44	8.67841	9.99951	8.67890	11.32110	10.00049	11.3216016
45	8.68104	9.99950	8.68154	11.31846	10.00050	11.3189615
46	8.68367	9.99949	8.68417	11.31583	10.00051	11.3163414
47	8.68627	9.99949	8.68678	11.31322	10.00051	11.3137313
48	8.68886	9.99948	8.68938	11.31062	10.00052	11.3111412
49	8.69144	9.99948	8.69169	11.30804	10.00053	11.3085711
50	8.69400	9.99947	8.69453	11.30547	10.00053	11.3060010
51	8.69654	9.99946	8.69708	11.30292	10.00054	11.303469
52	8.69907	9.99946	8.69962	11.30038	10.00054	11.300938
53	8.70159	9.99945	8.70214	11.29786	10.00055	11.298417
54	8.70409	9.99944	8.70465	11.29535	10.00056	11.295916
55	8.70658	9.99944	8.70714	11.29286	10.00056	11.293425
56	8.70905	9.99943	8.70962	11.29038	10.00057	11.290954
57	8.71151	9.99942	8.71208	11.28792	10.00058	11.288493
58	8.71395	9.99942	8.71453	11.28547	10.00058	11.286052
59	8.71638	9.99941	8.71697	11.28303	10.00059	11.283621
60	8.71880	9.99940	8.71940	11.28060	10.00060	11.281200

$\pi$  Degrees.

Min.

# A Table of Artificial Sines,

3 Degrees.

M.	Sine.		Tang.		Secant.	
0	8.71880	9.99940	8.71940	11.28060	10.00060	11.25120 60
1	8.72120	9.99940	8.72181	11.27819	10.00060	11.27380 59
2	8.72360	9.99939	8.72420	11.27580	10.00061	11.27641 58
3	8.72597	9.99938	8.72659	11.27341	10.00061	11.27403 57
4	8.72834	9.99938	8.72896	11.27104	10.00061	11.27166 56
5	8.73069	9.99937	8.73132	11.26868	10.00063	11.26931 55
6	8.73303	9.99936	8.73366	11.26634	10.00064	11.26697 54
7	8.73535	9.99936	8.73600	11.26400	10.00064	11.26465 53
8	8.73767	9.99935	8.73832	11.26163	10.00065	11.26233 52
9	8.73997	9.99934	8.74063	11.25937	10.00066	11.26003 51
10	8.74226	9.99934	8.74292	11.25708	10.00066	11.25774 50
11	8.74454	9.99933	8.74523	11.25479	10.00067	11.25546 49
12	8.74680	9.99932	8.74748	11.25252	10.00068	11.25320 48
13	8.74906	9.99932	8.74974	11.25026	10.00069	11.25095 47
14	8.75130	9.99931	8.75199	11.24801	10.00069	11.24870 46
15	8.75353	9.99930	8.75423	11.24577	10.00070	11.24647 45
16	8.75575	9.99929	8.75645	11.24355	10.00071	11.24425 44
17	8.75796	9.99929	8.75867	11.24133	10.00071	11.24205 43
18	8.76015	9.99928	8.76087	11.23913	10.00072	11.23985 42
19	8.76234	9.99927	8.76307	11.23694	10.00073	11.23766 41
20	8.76451	9.99927	8.76525	11.23475	10.00074	11.23549 40
21	8.76668	9.99926	8.76742	11.23258	10.00074	11.23333 39
22	8.76883	9.99925	8.76958	11.23042	10.00075	11.23117 38
23	8.77097	9.99924	8.77173	11.22827	10.00076	11.22903 37
24	8.77310	9.99924	8.77387	11.22613	10.00077	11.22690 36
25	8.77522	9.99923	8.77600	11.22403	10.00077	11.22478 35
26	8.77733	9.99922	8.77811	11.22189	10.00078	11.22267 34
27	8.77943	9.99921	8.78022	11.21978	10.00079	11.22057 33
28	8.78152	9.99921	8.78232	11.21768	10.00080	11.21878 32
29	8.78361	9.99920	8.78441	11.21559	10.00080	11.21640 31
30	8.78568	9.99919	8.78649	11.21351	10.00081	11.21433 30
	Sine.		Tang.		Secant.	

86 Degrees.

# Tangents and Secants.

3 Degrees.

N	Sin.	Tang.	Secant.	
30	8.75489.99919	8.78649	11.21351	10.00081 11.21433 30
31	8.787749.99918	8.78855	11.21145	10.00082 11.21226 29
32	8.789799.99917	8.79061	11.20939	10.00083 11.21021 28
33	8.791839.99917	8.79266	11.20734	10.00083 11.20817 27
34	8.793869.99916	8.79470	11.20530	10.00084 11.20614 26
35	8.795889.99915	8.79673	11.20327	10.00085 11.20412 25
36	8.797899.99914	8.79875	11.20125	10.00086 11.20211 24
37	8.79999.99913	8.80076	11.19924	10.00087 11.20010 23
38	8.801899.99913	8.80277	11.19724	10.00087 11.19811 22
39	8.803889.99912	8.80476	11.19524	10.00088 11.19612 21
40	8.805859.99911	8.80674	11.19326	10.00089 11.19415 20
41	8.807829.99910	8.80872	11.19128	10.00090 11.19218 19
42	8.809789.99909	8.81068	11.18932	10.00091 11.19022 18
43	8.811739.99909	8.81264	11.18736	10.00091 11.18827 17
44	8.813679.99908	8.81459	11.18541	10.00092 11.18633 16
45	8.815609.99907	8.81653	11.18347	10.00094 11.18440 15
46	8.817529.99906	8.81846	11.18154	10.00094 11.18248 14
47	8.819449.99905	8.82038	11.17962	10.00095 11.18056 13
48	8.821349.99904	8.82230	11.17770	10.00096 11.17866 12
49	8.823249.99904	8.82421	11.17580	10.00096 11.17676 11
50	8.825139.99903	8.82610	11.17390	10.00097 11.17487 10
51	8.827019.99902	8.82799	11.17201	10.00098 11.17299 9
52	8.828889.99901	8.82987	11.17013	10.00099 11.17112 8
53	8.830759.99900	8.83175	11.16825	10.00100 11.16925 7
54	8.832619.99900	8.83361	11.16630	10.00101 11.16739 6
55	8.834469.99898	8.83547	11.16453	10.00102 11.16554 5
56	8.836309.99898	8.83732	11.16268	10.00102 11.16370 4
57	8.838139.99897	8.83916	11.16084	10.00103 11.16187 3
58	8.839969.99896	8.84100	11.15900	10.00104 11.16004 2
59	8.841779.99895	8.84282	11.15718	10.00105 11.15823 1
60	8.843589.99894	8.84464	11.15536	10.00106 11.15642 0
	Sine.	Tang.	Secant.	Min.

86 Degrees.

# A Table of Artificial Sines,

4 Degrees.

Min.	Sine.	Tang.	Secant.	Min.
0	8.84358	9.99894	8.84464	11.15536
1	8.84539	9.99893	8.84646	11.15355
2	8.84718	9.99892	8.84826	11.15174
3	8.84897	9.99893	8.85006	11.14994
4	8.85075	9.99891	8.85185	11.14815
5	8.85252	9.99890	8.85363	11.14637
6	8.85429	9.99889	8.85540	11.14460
7	8.85605	9.99888	8.85717	11.14283
8	8.85780	9.99887	8.85893	11.14107
9	8.85955	9.99886	8.86069	11.13931
10	8.86128	9.99885	8.86241	11.13757
11	8.86301	9.99884	8.86417	11.13583
12	8.86474	9.99883	8.86591	11.13409
13	8.86645	9.99882	8.86763	11.13237
14	8.86815	9.99881	8.86935	11.13065
15	8.86987	9.99880	8.87106	11.12894
16	8.87157	9.99880	8.87277	11.12723
17	8.87326	9.99879	8.87447	11.12553
18	8.87494	9.99878	8.87616	11.12384
19	8.87662	9.99877	8.87785	11.12215
20	8.87829	9.99876	8.87953	11.12047
21	8.87995	9.99875	8.88120	11.11880
22	8.88161	9.99874	8.88287	11.11713
23	8.88326	9.99873	8.88453	11.11547
24	8.88490	9.99872	8.88619	11.11382
25	8.88654	9.99871	8.88783	11.11217
26	8.88817	9.99870	8.88948	11.11052
27	8.88980	9.99869	8.89111	11.10889
28	8.89142	9.99868	8.89274	11.10726
29	8.89304	9.99867	8.89437	11.10563
30	8.89464	9.99866	8.89598	11.10402
		Sine.	Tang.	Secant.

85 Degrees.

Min.

# Tangents and Secants.

4 Degrees.

Min.	Sin.		Tang.		Secant.	
30	8.8564	9.99866	8.89598	11.10402	10.00134	11.1053630
31	8.89625	9.99865	8.89760	11.10240	10.00135	11.1037529
32	8.89784	9.99864	8.89920	11.10080	10.00136	11.1021628
33	8.89943	9.99863	8.90080	11.09920	10.00137	11.1005727
34	8.90102	9.99862	8.90240	11.09760	10.00138	11.0989826
35	8.90260	9.99861	8.90399	11.09601	10.00139	11.0974025
36	8.90417	9.99860	8.90557	11.09443	10.00140	11.0958324
37	8.90574	9.99859	8.90715	11.09285	10.00141	11.0941623
38	8.90730	9.99858	8.90872	11.09128	10.00142	11.0927022
39	8.90885	9.99857	8.91029	11.08972	10.00143	11.0911521
40	8.91040	9.99856	8.91185	11.08815	10.00144	11.0896020
41	8.91195	9.99855	8.91340	11.08660	10.00145	11.0880519
42	8.91349	9.99854	8.91495	11.08505	10.00146	11.0865118
43	8.91502	9.99853	8.91650	11.08351	10.00147	11.0849817
44	8.91655	9.99852	8.91803	11.08197	10.00148	11.0834516
45	8.91807	9.99851	8.91957	11.08043	10.00149	11.0819315
46	8.91959	9.99850	8.92110	11.07890	10.00151	11.0804114
47	8.92110	9.99849	8.92262	11.07738	10.00152	11.0789013
48	8.92261	9.99847	8.92414	11.07586	10.00153	11.0773912
49	8.92411	9.99846	8.92565	11.07435	10.00154	11.0758911
50	8.92561	9.99845	8.92716	11.07285	10.00155	11.0743910
51	8.92710	9.99844	8.92866	11.07134	10.00156	11.072909
52	8.92859	9.99843	8.93016	11.06985	10.00157	11.071418
53	8.93007	9.99842	8.93165	11.06835	10.00158	11.069937
54	8.93154	9.99841	8.93313	11.06687	10.00159	11.068466
55	8.93302	9.99840	8.93462	11.06538	10.00160	11.066995
56	8.93448	9.99839	8.93609	11.06391	10.00161	11.065524
57	8.93594	9.99838	8.93757	11.06244	10.00162	11.064063
58	8.93740	9.99837	8.93903	11.06097	10.00163	11.062602
59	8.93885	9.99836	8.94049	11.05951	10.00165	11.061151
60	8.94030	9.99834	8.94195	11.05805	10.00166	11.059700
			Sine.	Tang.	Secant.	

85 Degrees.

M

# A Table of Artificial Sines

*5 Degrees.*

Min.	Sine	Tang.	Secant.	Min.			
0	8.94030	9.99834	8.94195	11.05805	10.00166	11.05970	60
1	8.94174	9.99833	8.94340	11.05660	10.00167	11.05826	59
2	8.94317	9.99832	8.94485	11.05515	10.00168	11.05683	58
3	8.94461	9.99831	8.94630	11.05370	10.00169	11.05539	57
4	8.94603	9.99830	8.94773	11.05227	10.00170	11.05397	56
5	8.94746	9.99829	8.94917	11.05083	10.00171	11.05254	55
6	8.94887	9.99828	8.95060	11.04940	10.00172	11.05113	54
7	8.95029	9.99827	8.95202	11.04798	10.00173	11.04971	53
8	8.95170	9.99826	8.95344	11.04656	10.00175	11.04830	52
9	8.95310	9.99824	8.95486	11.04514	10.00176	11.04690	51
10	8.95450	9.99823	8.95627	11.04373	10.00177	11.04550	50
11	8.95590	9.99822	8.95767	11.04233	10.00178	11.04411	49
12	8.95728	9.99821	8.95908	11.04093	10.00179	11.04272	48
13	8.95867	9.99820	8.96047	11.03953	10.00180	11.04133	47
14	8.96005	9.99819	8.96186	11.03863	10.00181	11.03995	46
15	8.96143	9.99817	8.96325	11.03675	10.00183	11.03857	45
16	8.96280	9.99816	8.96464	11.03536	10.00184	11.03720	44
17	8.96417	9.99815	8.96602	11.03398	10.00185	11.03583	43
18	8.96553	9.99814	8.96739	11.03261	10.00186	11.03447	42
19	8.96689	9.99813	8.96877	11.03123	10.00187	11.03311	41
20	8.96825	9.99812	8.97013	11.02987	10.00188	11.03175	40
21	8.96960	9.99810	8.97150	11.02850	10.00190	11.03040	39
22	8.97095	9.99809	8.97286	11.02715	10.00191	11.02905	38
23	8.97220	9.99808	8.97421	11.02579	10.00192	11.02771	37
24	8.97363	9.99807	8.97556	11.02444	10.00193	11.02637	36
25	8.97490	9.99806	8.97691	11.02309	10.00194	11.02504	35
26	8.97629	9.99804	8.97825	11.02175	10.00196	11.02371	34
27	8.97762	9.99803	8.97959	11.02041	10.00197	11.02238	33
28	8.97894	9.99802	8.98092	11.01908	10.00198	11.02106	32
29	8.98026	9.99801	8.98225	11.01775	10.00199	11.01974	31
30	8.98157	9.99800	8.98358	11.01642	10.00200	11.01843	30
	Sine.	Tang.	Secant.				Min.

*84 Degrees,*

# Tangents and Secants.

**5 Degrees.**

Min.	Sine.		Tang.		Secant.	
30	8.98157	9.99800	8.98358	11.01642	10.00200	11.01843 30
31	8.98283	9.99798	8.98490	11.01510	10.00202	11.01712 29
32	8.98419	9.99797	8.98622	11.01378	10.00203	11.01581 28
33	8.98549	9.99796	8.98753	11.01247	10.00204	11.01451 27
34	8.98679	9.99795	8.98884	11.01116	10.00205	11.01321 26
35	8.98808	9.99794	8.99015	11.00985	10.00207	11.01192 25
36	8.98937	9.99792	8.99145	11.00855	10.00208	11.01063 24
37	8.99066	9.99791	8.99275	11.00725	10.00209	11.00934 23
38	8.99194	9.99790	8.99405	11.00596	10.00210	11.00806 22
39	8.99322	9.99789	8.99534	11.00466	10.00211	11.00678 21
40	8.99450	9.99787	8.99662	11.00338	10.00213	11.00550 20
41	8.99577	9.99786	8.99791	11.00209	10.00214	11.00423 19
42	8.99704	9.99785	8.99919	11.00081	10.00215	11.00296 18
43	8.99830	9.99784	9.00047	10.99954	10.00217	11.00170 17
44	8.99956	9.99782	9.00174	10.99826	10.00218	11.00046 16
45	9.00082	9.99781	9.00307	10.99699	10.00220	10.99918 15
46	9.00207	9.99780	9.00427	10.99573	10.00220	10.99793 14
47	9.00332	9.99778	9.00553	10.99447	10.00222	10.99668 13
48	9.00456	9.99777	9.00679	10.99321	10.00223	10.99544 12
49	9.00581	9.99776	9.00805	10.99195	10.00224	10.99420 11
50	9.00704	9.99775	9.00930	10.99070	10.00226	10.99296 10
51	9.00828	9.99773	9.01055	10.98945	10.00227	10.99172 9
52	9.00951	9.99772	9.01179	10.98821	10.00228	10.99049 8
53	9.01074	9.99771	9.01303	10.98697	10.00229	10.98926 7
54	9.01196	9.99769	9.01427	10.98573	10.00231	10.98804 6
55	9.01318	9.99768	9.01550	10.98450	10.00232	10.98682 5
56	9.01440	9.99767	9.01673	10.98327	10.00233	10.98560 4
57	9.01561	9.99765	9.01796	10.98204	10.00235	10.98439 3
58	9.01682	9.99764	9.01918	10.98082	10.00236	10.98318 2
59	9.01803	9.99763	9.02040	10.97960	10.00237	10.98197 1
60	9.01923	9.99761	9.02162	10.97838	10.00239	10.98077 0
		Sine.		Tang.		Secant.

**84 Degrees.**

# A Table of Artificial Sines,

*6 Degrees.*

Min.	Sine.	Tang.		Secant.	
0	9.01924	9.99761	9.02162	10.97838	10.00239
1	9.02044	9.99760	9.02283	10.97717	10.00240
2	9.02163	9.99759	9.02404	10.97596	10.00241
3	9.02283	9.99757	9.02525	10.97475	10.00243
4	9.02402	9.99756	9.02646	10.97355	10.00244
5	9.02520	9.99755	9.02766	10.97235	10.00245
6	9.02636	9.99753	9.02885	10.97115	10.00247
7	9.02757	9.99752	9.03005	10.96995	10.00248
8	9.02874	9.99751	9.03124	10.96876	10.00249
9	9.02992	9.99749	9.03243	10.96758	10.00251
10	9.03109	9.99748	9.03361	10.96639	10.00252
11	9.03226	9.99747	9.03479	10.96521	10.00253
12	9.03342	9.99745	9.03597	10.96403	10.00255
13	9.03458	9.99744	9.03714	10.96286	10.00256
14	9.03574	9.99743	9.03832	10.96168	10.00258
15	9.03690	9.99741	9.03949	10.96052	10.00259
16	9.03805	9.99740	9.04065	10.95935	10.00260
17	9.03920	9.99738	9.04181	10.95819	10.00262
18	9.04034	9.99737	9.04297	10.95703	10.00263
19	9.04149	9.99736	9.04413	10.95587	10.00265
20	9.04263	9.99734	9.04528	10.95472	10.00266
21	9.04376	9.99733	9.04643	10.95357	10.00267
22	9.04490	9.99731	9.04758	10.95242	10.00269
23	9.04603	9.99730	9.04873	10.95127	10.00270
24	9.04715	9.99729	9.04987	10.95013	10.00272
25	9.04828	9.99727	9.05101	10.94899	10.00273
26	9.04940	9.99726	9.05214	10.94786	10.00274
27	9.05052	9.99724	9.05328	10.94672	10.00276
28	9.05164	9.99723	9.05441	10.94559	10.00277
29	9.05275	9.99721	9.05554	10.94447	10.00279
30	9.05386	9.99720	9.05666	10.94334	10.00280
	Sine.	Tang.		Secant.	

*83 Degrees.*

Min.

# Tangents and Secants.

*6 Degrees:*

Sine.	Tang.	Secant.
30 9.05326	9.99720	9.05666
31 9.05497	9.99719	9.05778
32 9.05667	9.99717	9.05890
33 9.05717	9.99716	9.06002
34 9.05827	9.99714	9.06113
35 9.05937	9.99713	9.06224
36 9.06046	9.99711	9.06335
37 9.06155	9.99710	9.06445
38 9.06264	9.99708	9.06556
39 9.06372	9.99707	9.06666
40 9.06481	9.99705	9.06775
41 9.06589	9.99704	9.06885
42 9.06696	9.99702	9.06994
43 9.06804	9.99701	9.07103
44 9.06911	9.99699	9.07211
45 9.07018	9.99698	9.07320
46 9.07124	9.99696	9.07428
47 9.07231	9.99695	9.07536
48 9.07337	9.99693	9.07643
49 9.07442	9.99692	9.07751
50 9.07548	9.99690	9.07858
51 9.07653	9.99689	9.07964
52 9.07758	9.99687	9.08071
53 9.07863	9.99686	9.08177
54 9.07968	9.99684	9.08283
55 9.08072	9.99683	9.08389
56 9.08176	9.99681	9.08495
57 9.08280	9.99680	9.08600
58 9.08383	9.99678	9.08705
59 9.08486	9.99677	9.08810
60 9.08589	9.99675	9.08914
Sine.	Tang.	Secant.

*8; Degrees.*

# A Table of Artificial Sines,

7 Degrees.

Mil.	Sine.		Tang.		Secant.	
0	9.08589	9.99675	9.08914	10.91086	10.0032	10.91411 60
1	9.08692	9.99674	9.09019	10.90981	10.00327	10.91308 59
2	9.08795	9.99671	9.09123	10.90877	10.00328	10.91205 58
3	9.08897	9.99670	9.09227	10.90773	10.00329	10.91103 57
4	9.08999	9.99669	9.09330	10.90670	10.00331	10.91001 56
5	9.09101	9.99667	9.09434	10.90566	10.00333	10.90899 55
6	9.09202	9.99666	9.09537	10.90463	10.00334	10.90798 54
7	9.09304	9.99664	9.09640	10.90360	10.00336	10.90696 53
8	9.09405	9.99663	9.09740	10.90258	10.00338	10.90595 52
9	9.09506	9.99661	9.09845	10.90155	10.00339	10.90494 51
10	9.09606	9.99659	9.09947	10.90053	10.00341	10.90394 50
11	9.09707	9.99658	9.10049	10.89951	10.00342	10.90294 49
12	9.09807	9.99656	9.10150	10.89850	10.00344	10.90193 48
13	9.09907	9.99655	9.10252	10.89748	10.00345	10.90094 47
14	9.10006	9.99653	9.10353	10.89647	10.00347	10.89994 46
15	9.10106	9.99651	9.10454	10.89546	10.00349	10.89894 45
16	9.10205	9.99650	9.10555	10.89445	10.00350	10.89795 44
17	9.10304	9.99648	9.10656	10.89344	10.00352	10.89696 43
18	9.10403	9.99647	9.10756	10.89244	10.00353	10.89598 42
19	9.10501	9.99644	9.10856	10.89144	10.00355	10.89499 41
20	9.10599	9.99643	9.10956	10.89044	10.00357	10.89401 40
21	9.10697	9.99642	9.11056	10.88944	10.00358	10.89303 39
22	9.10795	9.99640	9.11155	10.88845	10.00360	10.89205 38
23	9.10893	9.99638	9.11254	10.88746	10.00362	10.89107 37
24	9.10990	9.99637	9.11353	10.88647	10.00363	10.89003 36
25	9.11087	9.99635	9.11452	10.88548	10.00365	10.88913 35
26	9.11184	9.99634	9.11551	10.88449	10.00367	10.88816 34
27	9.11281	9.99632	9.11649	10.88351	10.00368	10.88719 33
28	9.11377	9.99630	9.11747	10.88253	10.00370	10.88623 32
29	9.11474	9.99629	9.11845	10.88155	10.00372	10.88526 31
30	9.11570	9.99627	9.11943	10.88057	10.00373	10.88430 30
	Sine.		Tang.		Secant.	

82 Degrees.

# Tangents and Secants.

7 Degrees.

Mn.	Sine		Tang.		Secant.	
30	9.11570	9.99627	9.11943	10.88057	10.00373	10.88430
31	9.11666	9.99625	9.12040	10.87960	10.00375	10.88334
32	9.11761	9.99624	9.12138	10.87862	10.00377	10.88239
33	9.11857	9.99622	9.12235	10.87765	10.00378	10.88143
34	9.11952	9.99620	9.12332	10.87668	10.00380	10.88048
35	9.12047	9.99619	9.12428	10.87572	10.00382	10.87953
36	9.12142	9.99617	9.12525	10.87475	10.00383	10.87858
37	9.12236	9.99615	9.12620	10.87379	10.00385	10.87764
38	9.12331	9.99613	9.12717	10.87283	10.00387	10.87669
39	9.12425	9.99612	9.12813	10.87187	10.00388	10.87575
40	9.12519	9.99610	9.12909	10.87091	10.00390	10.87481
41	9.12613	9.99608	9.13004	10.86996	10.00392	10.87388
42	9.12706	9.99607	9.13099	10.86901	10.00393	10.87295
43	9.12799	9.99605	9.13194	10.86806	10.00395	10.87217
44	9.12893	9.99603	9.13289	10.86711	10.00397	10.87108
45	9.12985	9.99602	9.13384	10.86616	10.00399	10.87015
46	9.13078	9.99600	9.13478	10.86522	10.00400	10.86922
47	9.13171	9.99598	9.13573	10.86427	10.00402	10.86829
48	9.13263	9.99596	9.13667	10.86333	10.00404	10.86737
49	9.13355	9.99595	9.13761	10.86240	10.00405	10.86645
50	9.13447	9.99593	9.13854	10.86146	10.00407	10.86553
51	9.13539	9.99591	9.13948	10.86052	10.00409	10.86461
52	9.13630	9.99589	9.14041	10.85959	10.00411	10.86370
53	9.13722	9.99588	9.14134	10.85866	10.00412	10.86278
54	9.13813	9.99586	9.14227	10.85773	10.00414	10.86187
55	9.13904	9.99584	9.14320	10.85680	10.00416	10.86096
56	9.13994	9.99582	9.14412	10.85588	10.00418	10.86006
57	9.14085	9.99581	9.14504	10.85496	10.00419	10.85915
58	9.14175	9.99579	9.14597	10.85403	10.00421	10.85825
59	9.14266	9.99577	9.14689	10.85312	10.00423	10.85734
60	9.14356	9.99575	9.14780	10.85220	10.00425	10.85645
	Sine.		Tang.		Secant.	

82 Degrees.

# A Table of Artificial Sines,

8 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.14356	9.99575	9.14780	10.85220
1	9.14445	9.99574	9.14872	10.85128
2	9.14535	9.99570	9.14963	10.85037
3	9.14624	9.99570	9.15054	10.84946
4	9.14714	9.99568	9.15145	10.84855
5	9.14803	9.99566	9.15236	10.84764
6	9.14892	9.99565	9.15327	10.84673
7	9.14980	9.99563	9.15417	10.84583
8	9.15069	9.99561	9.15508	10.84492
9	9.15157	9.99559	9.15598	10.84402
10	9.15245	9.99557	9.15689	10.84312
11	9.15333	9.99556	9.15778	10.84223
12	9.15421	9.99554	9.15867	10.84133
13	9.15508	9.99552	9.15957	10.84044
14	9.15596	9.99550	9.16046	10.83954
15	9.15683	9.99548	9.16135	10.83865
16	9.15770	9.99546	9.16224	10.83776
17	9.15857	9.99545	9.16312	10.83688
18	9.15944	9.99543	9.16401	10.83599
19	9.16030	9.99541	9.16489	10.83511
20	9.16116	9.99539	9.16517	10.83423
21	9.16203	9.99537	9.16605	10.83335
22	9.16289	9.99535	9.16753	10.83247
23	9.16374	9.99533	9.16850	10.83159
24	9.16460	9.99532	9.16928	10.83072
25	9.16545	9.99530	9.17016	10.82984
26	9.16631	9.99528	9.17103	10.82897
27	9.16716	9.99526	9.17190	10.82810
28	9.16801	9.99524	9.17277	10.82723
29	9.16886	9.99522	9.17363	10.82637
30	9.16970	9.99520	9.17450	10.82550
	Sine.	Tang.	Secant.	Min.

81 Degrees.

# Tangents and Secants.

8 Degrees.

Min.	Sine.		Tang.		Secant.	
30	9.16970	9.99520	9.17450	10.82550	10.00480	10.83030 30
31	9.17055	9.99518	9.17530	10.82464	10.00482	10.82945 29
32	9.17139	9.99517	9.17622	10.82378	10.00484	10.82861 28
33	9.17223	9.99515	9.17708	10.82292	10.00485	10.82777 27
34	9.17307	9.99513	9.17794	10.82206	10.00487	10.82693 26
35	9.17391	9.99511	9.17880	10.82120	10.00489	10.82609 25
36	9.17474	9.99509	9.17966	10.82035	10.00491	10.82526 24
37	9.17558	9.99507	9.18051	10.81949	10.00493	10.82442 23
38	9.17641	9.99505	9.18136	10.81864	10.00495	10.82359 22
39	9.17724	9.99503	9.18221	10.81779	10.00497	10.82270 21
40	9.17807	9.99501	9.18306	10.81694	10.00499	10.82193 20
41	9.17890	9.99499	9.18391	10.81609	10.00501	10.82111 19
42	9.17973	9.99497	9.18475	10.81525	10.00503	10.82027 18
43	9.18055	9.99496	9.18560	10.81440	10.00505	10.81949 17
44	9.18137	9.99494	9.18644	10.81356	10.00507	10.81863 16
45	9.18220	9.99492	9.18738	10.81272	10.00508	10.81780 15
46	9.18302	9.99490	9.18822	10.81188	10.00510	10.81698 14
47	9.18383	9.99488	9.18896	10.81104	10.00512	10.81617 13
48	9.18465	9.99486	9.18979	10.81021	10.00514	10.81535 12
49	9.18547	9.99484	9.19063	10.80937	10.00516	10.81453 11
50	9.18628	9.99482	9.19146	10.80854	10.00518	10.81372 10
51	9.18709	9.99480	9.19229	10.80771	10.00520	10.81291 9
52	9.18790	9.99478	9.19312	10.80688	10.00522	10.81210 8
53	9.18871	9.99476	9.19395	10.80605	10.00524	10.81129 7
54	9.18952	9.99474	9.19478	10.80522	10.00526	10.81048 6
55	9.19033	9.99473	9.19561	10.80439	10.00528	10.80968 5
56	9.19113	9.99470	9.19643	10.80357	10.00530	10.80887 4
57	9.19193	9.99468	9.19725	10.80275	10.00532	10.80807 3
58	9.19273	9.99466	9.19807	10.80193	10.00534	10.80727 2
59	9.19353	9.99464	9.19889	10.80111	10.00536	10.80647 1
60	9.19433	9.99462	9.19971	10.80029	10.00538	10.80567 0

Sine                    Tang.                    Secant

81 Degrees.

# A Table of Artificial Sines,

*9 Degrees.*

Min.	Sine.	Tang.	Secant.
0 9.19433	9.99462	9.19971	10.80029 10.00538 10.80567 60
1 9.19513	9.99460	9.20053	10.79947 10.00540 10.80488 59
2 9.19593	9.99458	9.20135	10.79866 10.00542 10.80408 58
3 9.19672	9.99456	9.20216	10.79784 10.00544 10.80328 57
4 9.19751	9.99454	9.20297	10.79703 10.00546 10.80249 56
5 9.19830	9.99452	9.20378	10.79622 10.00548 10.80170 55
6 9.19909	9.99450	9.20459	10.79541 10.00550 10.80091 54
7 9.19988	9.99448	9.20540	10.79460 10.00552 10.80012 53
8 9.20067	9.99446	9.20621	10.79379 10.00554 10.79933 52
9 9.20145	9.99444	9.20701	10.79299 10.00556 10.79855 51
10 9.20223	9.99442	9.20782	10.79218 10.00558 10.79777 50
11 9.20302	9.99440	9.20862	10.79138 10.00560 10.79698 49
12 9.20380	9.99438	9.20942	10.79058 10.00562 10.79620 48
13 9.20458	9.99436	9.21022	10.78978 10.00564 10.79542 47
14 9.20535	9.99434	9.21102	10.78898 10.00566 10.79465 46
15 9.20613	9.99432	9.21182	10.78819 10.00568 10.79387 45
16 9.20691	9.99430	9.21261	10.78739 10.00570 10.79309 44
17 9.20768	9.99427	9.21341	10.78660 10.00572 10.79232 43
18 9.20845	9.99425	9.21420	10.78580 10.00575 10.79155 42
19 9.20922	9.99423	9.21499	10.78501 10.00577 10.79078 41
20 9.20999	9.99421	9.21578	10.78422 10.00579 10.79001 40
21 9.21076	9.99419	9.21657	10.78343 10.00581 10.78924 39
22 9.21153	9.99417	9.21736	10.78264 10.00583 10.78847 38
23 9.21229	9.99415	9.21814	10.78186 10.00585 10.78771 37
24 9.21306	9.99413	9.21893	10.78107 10.00587 10.78695 36
25 9.21382	9.99411	9.21971	10.78029 10.00589 10.78618 35
26 9.21458	9.99409	9.22049	10.77951 10.00591 10.78542 34
27 9.21534	9.99407	9.22127	10.77873 10.00593 10.78466 33
28 9.21610	9.99405	9.22205	10.77795 10.00596 10.78390 32
29 9.21685	9.99402	9.22283	10.77717 10.00598 10.78315 31
30 9.21761	9.99400	9.22361	10.77639 10.00600 10.78239 30
	Sine.	Tang.	Secant.

80 Degrees.

Tangents and Secants.

9 Degrees.

N. o.	Sine.	Tang.	Secant.
30	9.21761 9.99400	9.22361 10.77639	10.00600 10.78239
31	9.21869 9.99398	9.22438 10.77562	10.00602 10.78164
32	9.21912 9.99395	9.22516 10.77484	10.00604 10.78088
33	9.21987 9.99394	9.22593 10.77407	10.00606 10.78013
34	9.22062 9.99392	9.22670 10.77330	10.00608 10.77938
35	9.22137 9.99390	9.22747 10.77253	10.00610 10.77863
36	9.22212 9.99388	9.22824 10.77176	10.00613 10.77789
37	9.22286 9.99385	9.22901 10.77099	10.00615 10.77714
38	9.22361 9.99383	9.22977 10.77023	10.00617 10.77639
39	9.22435 9.99381	9.23054 10.76946	10.00619 10.77565
40	9.22509 9.99379	9.23131 10.7687	10.00621 10.77491
41	9.22583 9.99377	9.23207 10.76794	10.00623 10.77417
42	9.22657 9.99375	9.23283 10.76717	10.00625 10.77343
43	9.22731 9.99373	9.23359 10.76641	10.00628 10.77269
44	9.22805 9.99370	9.23435 10.76566	10.00630 10.77195
45	9.22878 9.99368	9.23510 10.76490	10.00632 10.77122
46	9.22952 9.99366	9.23586 10.76414	10.00634 10.77048
47	9.23025 9.99364	9.23661 10.76339	10.00636 10.76975
48	9.23098 9.99362	9.23737 10.76263	10.00638 10.76902
49	9.23171 9.99359	9.23812 10.76188	10.00641 10.76829
50	9.23244 9.99357	9.23887 10.76113	10.00643 10.76756
51	9.23317 9.99355	9.23962 10.76038	10.00645 10.76683
52	9.23390 9.99353	9.24037 10.75963	10.00647 10.76610
53	9.23463 9.99351	9.24112 10.75888	10.00649 10.76538
54	9.23535 9.99348	9.24187 10.75814	10.00652 10.76465
55	9.23607 9.99346	9.24261 10.75739	10.00654 10.76393
56	9.23680 9.99344	9.24335 10.75665	10.00656 10.76321
57	9.23753 9.99342	9.24410 10.75590	10.00658 10.76249
58	9.23824 9.99340	9.24484 10.75516	10.00660 10.76177
59	9.23895 9.99337	9.24558 10.75442	10.00663 10.76105
60	9.23967 9.99335	9.24632 10.75368	10.00665 10.76033
	Sine.	Tang.	Secant.
			Min.

80 Degrees,

# A Table of Artificial Sines,

10 Degrees.

Min.	Sine,	Tang.	Secant.	
09.23967	9.99335	9.24632	10.75368	10.00665 10.76336
19.24039	9.99333	9.24706	10.75294	10.00667 10.76159
29.24110	9.99331	9.24779	10.75221	10.00669 10.75890
39.24181	9.99328	9.24853	10.75147	10.00672 10.75819
49.24253	9.99326	9.24926	10.75074	10.00674 10.75747
59.24324	9.99324	9.25000	10.75000	10.00676 10.75676
69.24395	9.99322	9.25073	10.74927	10.00678 10.75605
79.24466	9.99320	9.25146	10.74854	10.00681 10.75534
89.24536	9.99317	9.25219	10.74781	10.00683 10.75464
99.24607	9.99315	9.25292	10.74708	10.00685 10.75393
109.24678	9.99313	9.25365	10.74635	10.00687 10.75323
119.24748	9.99310	9.25437	10.74563	10.00690 10.75252
129.24818	9.99308	9.25510	10.74490	10.00692 10.75182
139.24888	9.99306	9.25582	10.74418	10.00694 10.75112
149.24958	9.99304	9.25655	10.74345	10.00696 10.75042
159.25028	9.99301	9.25727	10.74273	10.00699 10.74972
169.25098	9.99299	9.25799	10.74201	10.00701 10.74902
179.25168	9.99297	9.25871	10.74129	10.00703 10.74832
189.25237	9.99294	9.25943	10.74057	10.00706 10.74763
199.25307	9.99292	9.26015	10.73985	10.00708 10.74693
209.25376	9.99290	9.26086	10.73914	10.00710 10.74624
219.25445	9.99288	9.26158	10.73842	10.00713 10.74555
229.25514	9.99285	9.26229	10.73771	10.00715 10.74486
239.25583	9.99283	9.26301	10.73700	10.00717 10.74417
249.25652	9.99281	9.26372	10.73628	10.00719 10.74348
259.25721	9.99278	9.26443	10.73557	10.00722 10.74279
269.25790	9.99276	9.26514	10.73486	10.00724 10.74210
279.25858	9.99274	9.26585	10.73415	10.00726 10.74142
289.25927	9.99271	9.26656	10.73345	10.00729 10.74073
299.25995	9.99270	9.26726	10.73274	10.00731 10.74005
309.26063	9.99267	9.2679	10.73203	10.00733 10.73937
	Sine.	Tang.	Secant.	

79 Degrees.

# Fangents and Secante

10 Degrees.

Min.	Sine.	Tang.	Secant.	
30	9.260	9.99267	9.26797	10.73203
31	9.26131	9.99264	9.26867	10.73133
32	9.26199	9.99262	9.26938	10.73063
33	9.26267	9.99260	9.27008	10.72992
34	9.26335	9.99257	9.27078	10.72922
35	9.26403	9.99255	9.27148	10.72852
36	9.26470	9.99253	9.27218	10.72782
37	9.26538	9.99250	9.27288	10.72712
38	9.26605	9.99248	9.27357	10.72643
39	9.26672	9.99245	9.27427	10.72573
40	9.26739	9.99243	9.27496	10.72504
41	9.26807	9.99241	9.27566	10.72434
42	9.26873	9.99238	9.27635	10.72365
43	9.26940	9.99236	9.27704	10.72296
44	9.27007	9.99234	9.27773	10.72227
45	9.27074	9.99231	9.27842	10.72158
46	9.27140	9.99229	9.27911	10.72089
47	9.27206	9.99226	9.27980	10.72020
48	9.27273	9.99224	9.28049	10.71951
49	9.27339	9.99221	9.28117	10.71883
50	9.27405	9.99219	9.28186	10.71814
51	9.27471	9.99217	9.28254	10.71746
52	9.27537	9.99214	9.28323	10.71678
53	9.27602	9.99212	9.28391	10.71609
54	9.27668	9.99209	9.28459	10.71541
55	9.27734	9.99207	9.28527	10.71473
56	9.27799	9.99204	9.28595	10.71405
57	9.27864	9.99202	9.28662	10.71338
58	9.27930	9.99200	9.28730	10.71270
59	9.27995	9.99197	9.28798	10.71202
60	9.28060	9.99195	9.28865	10.71135
	Sine.	Tang.	Secant.	Min.

79 Degrees.

Table of Artificial Sines,

Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.28060	9.99195	9.2886	10.71135
1	9.28125	9.99192	9.28924	10.71067
2	9.28190	9.99190	9.29000	10.71000
3	9.28254	9.99187	9.29067	10.70933
4	9.28319	9.99185	9.29134	10.70866
5	9.28384	9.99182	9.29201	10.70799
6	9.28448	9.99180	9.29268	10.70732
7	9.28512	9.99177	9.29335	10.70665
8	9.28577	9.99175	9.29402	10.70598
9	9.28641	9.99172	9.29468	10.70532
10	9.28705	9.99170	9.29535	10.70465
11	9.28769	9.99167	9.29601	10.70399
12	9.28833	9.99165	9.29668	10.70332
13	9.28896	9.99162	9.29734	10.70266
14	9.28960	9.99160	9.29800	10.70200
15	9.29024	9.99157	9.29866	10.70134
16	9.29087	9.99155	9.29932	10.70068
17	9.29150	9.99152	9.29998	10.70002
18	9.29214	9.99150	9.30064	10.69936
19	9.29277	9.99147	9.30130	10.69871
20	9.29340	9.99145	9.30195	10.69805
21	9.29403	9.99142	9.30261	10.69739
22	9.29466	9.99140	9.30326	10.69674
23	9.29529	9.99137	9.30391	10.69609
24	9.29591	9.99135	9.30457	10.69543
25	9.29654	9.99132	9.30522	10.69478
26	9.29716	9.99130	9.30587	10.69413
27	9.29779	9.99127	9.30652	10.69348
28	9.29841	9.99124	9.30717	10.69283
29	9.29903	9.99122	9.30782	10.69218
30	9.29966	9.99119	9.30846	10.69154
	Sine.	Tang.	Secant.	Min.

# Tangents and Secants.

II Degrees.

M.	Sine.	Tang.	Secant.
30	9.30266	9.991199	10.69154
31	9.30000	9.991179	10.69089
32	9.30090	9.991149	10.69025
33	9.30151	9.991129	10.68960
34	9.30213	9.991099	10.68896
35	9.30275	9.991069	10.68832
36	9.30336	9.991049	10.68767
37	9.30398	9.991019	10.68702
38	9.30459	9.990999	10.68639
39	9.30521	9.990969	10.68575
40	9.30582	9.990939	10.68512
41	9.30643	9.990919	10.68448
42	9.30704	9.990889	10.68384
43	9.30765	9.990869	10.68321
44	9.30826	9.990839	10.68257
45	9.30887	9.990809	10.68194
46	9.30947	9.990778	10.68130
47	9.31008	9.990759	10.68067
48	9.31069	9.990729	10.68004
49	9.31129	9.990709	10.67941
50	9.31189	9.990679	10.67878
51	9.31250	9.990649	10.67815
52	9.31311	9.990629	10.67752
53	9.31370	9.990599	10.67689
54	9.31430	9.990579	10.67627
55	9.31490	9.990549	10.67564
56	9.31550	9.990519	10.67502
57	9.31600	9.990499	10.67439
58	9.31660	9.990469	10.67377
59	9.31728	9.990439	10.67315
60	9.31788	9.990409	10.67253
	Sine.	Tang.	Secant.

78 Degrees.

# A Table of Artificial Sines,

12. Degrees.

Min.	Sine.	Tang.		Secant.	
0	9.31788	9.99046	9.32747	10.67253	10.00960
1	9.31847	9.99038	9.32810	10.67191	10.00962
2	9.31907	9.99035	9.32872	10.67129	10.00965
3	9.31966	9.99032	9.32933	10.67067	10.00968
4	9.32025	9.99030	9.32995	10.67005	10.00970
5	9.32084	9.99027	9.33057	10.66994	10.00973
6	9.32143	9.99024	9.33119	10.66881	10.00976
7	9.32202	9.99022	9.33180	10.66820	10.00978
8	9.32261	9.99019	9.33242	10.66758	10.00981
9	9.32319	9.99016	9.33303	10.66697	10.00984
10	9.32378	9.99013	9.33365	10.66635	10.00987
11	9.32437	9.99011	9.33426	10.66574	10.00989
12	9.32495	9.99008	9.33487	10.66513	10.00992
13	9.32553	9.99005	9.33548	10.66452	10.00995
14	9.32612	9.99003	9.33609	10.66391	10.00998
15	9.32670	9.99000	9.33670	10.66330	10.01000
16	9.32728	9.98997	9.33731	10.66269	10.01003
17	9.32786	9.98994	9.33792	10.66208	10.01006
18	9.32844	9.98992	9.33853	10.66147	10.01009
19	9.32902	9.98989	9.33913	10.66087	10.01011
20	9.32960	9.98986	9.33974	10.66026	10.01014
21	9.33018	9.98983	9.34034	10.65966	10.01017
22	9.33075	9.98980	9.34095	10.65905	10.01020
23	9.33133	9.98978	9.34155	10.65845	10.01022
24	9.33190	9.98975	9.34216	10.65785	10.01025
25	9.33248	9.98972	9.34276	10.65724	10.01028
26	9.33305	9.98969	9.34336	10.65664	10.01031
27	9.33362	9.98967	9.34396	10.65604	10.01034
28	9.33420	9.98964	9.34456	10.65544	10.01036
29	9.33477	9.98961	9.34516	10.65484	10.01039
30	9.33534	9.98958	9.34576	10.65425	10.01042
	Sine.		Tang.		Secant.

77 Degrees,

# Tangents and Secants.

12 Degrees.

M.	Sine.	Tang.	Secant.	Min.			
30	9.34534	9.98958	9.34576	10.65425	10.01045	10.66466	30
31	9.33919	9.98955	9.34635	10.65365	10.01045	10.66409	29
32	9.33648	9.98953	9.34695	10.65305	10.01046	10.66353	28
33	9.33704	9.98950	9.34755	10.65246	10.01050	10.66296	27
34	9.33761	9.98947	9.34814	10.65186	10.01053	10.66239	26
35	9.33818	9.98944	9.34874	10.65127	10.01056	10.66183	25
36	9.33874	9.98941	9.34933	10.65067	10.01059	10.66126	24
37	9.33931	9.98938	9.34992	10.65008	10.01062	10.66069	23
38	9.33987	9.98936	9.35051	10.64949	10.01064	10.66013	22
39	9.34043	9.98933	9.35111	10.64889	10.01067	10.65957	21
40	9.34100	9.98930	9.35170	10.64830	10.01070	10.65900	20
41	9.34156	9.98927	9.35229	10.64771	10.01073	10.65844	19
42	9.34212	9.98924	9.35288	10.64712	10.01076	10.65788	18
43	9.34268	9.98921	9.35347	10.64654	10.01079	10.65732	17
44	9.34324	9.98919	9.35405	10.64595	10.01081	10.65676	16
45	9.34380	9.98916	9.35464	10.64536	10.01084	10.65620	15
46	9.34436	9.98913	9.35525	10.64478	10.01087	10.65565	14
47	9.34491	9.98910	9.35581	10.64419	10.01090	10.65509	13
48	9.34547	9.98907	9.35640	10.64360	10.01093	10.65453	12
49	9.34602	9.98904	9.35698	10.64302	10.01096	10.65398	11
50	9.34658	9.98901	9.35757	10.64243	10.01099	10.65342	10
51	9.34713	9.98899	9.35815	10.64185	10.01102	10.65287	9
52	9.34769	9.98896	9.35873	10.64127	10.01104	10.65231	8
53	9.34824	9.98893	9.35931	10.64069	10.01107	10.65176	7
54	9.34879	9.98890	9.35989	10.64011	10.01110	10.65121	6
55	9.34934	9.98887	9.36047	10.63953	10.01113	10.65066	5
56	9.34939	9.98884	9.36105	10.63895	10.01116	10.65011	4
57	9.35044	9.98881	9.36163	10.63837	10.01119	10.64956	3
58	9.35099	9.98878	9.36221	10.63779	10.01122	10.64901	2
59	9.35154	9.98875	9.36279	10.63721	10.01125	10.64846	1
60	9.35209	9.98872	9.36336	10.63664	10.01128	10.64791	0

Sine

Tang.

Secant.

77 Degrees.

# A Table of Artificial Sines,

12 Degrees.

No.	Sine.	Tang.	Secant.	
0	9.35209	9.98872	9.36336	10.63664
1	9.35264	9.98869	9.36394	10.63606
2	9.35318	9.98867	9.36452	10.63548
3	9.35373	9.98864	9.36509	10.63491
4	9.35427	9.98861	9.36566	10.63434
5	9.35482	9.98858	9.36624	10.63376
6	9.35536	9.98855	9.36681	10.63319
7	9.35590	9.98852	9.36728	10.63262
8	9.35644	9.98849	9.36795	10.63205
9	9.35698	9.98846	9.36852	10.63148
10	9.35752	9.98843	9.36929	10.63091
11	9.35806	9.98840	9.36966	10.63034
12	9.35860	9.98837	9.37023	10.62977
13	9.35914	9.98834	9.37080	10.62920
14	9.35968	9.98831	9.37137	10.62863
15	9.36022	9.98828	9.37193	10.62807
16	9.36075	9.98825	9.37250	10.62750
17	9.36129	9.98822	9.37306	10.62694
18	9.36182	9.98819	9.37363	10.62637
19	9.36236	9.98816	9.37419	10.62581
20	9.36289	9.98813	9.37476	10.62524
21	9.36342	9.98810	9.37532	10.62468
22	9.36395	9.98807	9.37588	10.62412
23	9.36449	9.98804	9.37644	10.62356
24	9.36502	9.98801	9.37700	10.62300
25	9.36555	9.98798	9.37756	10.62244
26	9.36608	9.98795	9.37812	10.62188
27	9.36660	9.98792	9.37868	10.62132
28	9.36713	9.98789	9.37924	10.62076
29	9.36766	9.98786	9.37980	10.62020
30	9.36819	9.98783	9.38035	10.61965
	Sine.	Tang.	Secant.	No.

76 Degrees.

# Tangents and Secants

13 Degrees

Min.	Sine.	Tang.	Secant.
305.6819	9.98783	9.38035	10.61965 10.01207 10.63182 30
319.3819	9.98780	9.38091	10.61909 10.01220 10.63129 29
329.36924	9.98777	9.38147	10.61853 10.01223 10.63076 28
339.36976	9.98774	9.38202	10.61798 10.01226 10.63024 27
349.37029	9.98771	9.38258	10.61743 10.01229 10.62972 26
359.37081	9.98768	9.38313	10.61687 10.01232 10.62919 25
369.37133	9.98765	9.38368	10.61632 10.01235 10.62867 24
379.37185	9.98762	9.38423	10.61577 10.01238 10.62815 23
389.37237	9.98759	9.38479	10.61521 10.01241 10.62763 22
399.37289	9.98756	9.38534	10.61465 10.01244 10.62711 21
409.37341	9.98753	9.38589	10.61411 10.01247 10.62659 20
419.37393	9.98750	9.38644	10.61356 10.01250 10.62607 19
429.37445	9.98747	9.38699	10.61301 10.01254 10.62555 18
439.37497	9.98743	9.38754	10.61246 10.01257 10.62503 17
449.37549	9.98740	9.38808	10.61192 10.01260 10.62451 16
459.37500	9.98737	9.38863	10.61137 10.01263 10.62400 15
469.37552	9.98734	9.38918	10.61082 10.01266 10.62348 14
479.37704	9.98731	9.38972	10.61028 10.01269 10.62297 13
489.37755	9.98728	9.39027	10.60973 10.01272 10.62245 12
499.37806	9.98725	9.39082	10.60919 10.01275 10.62194 11
509.37858	9.98722	9.39136	10.60864 10.01278 10.62144 10
519.37909	9.98719	9.39190	10.60810 10.01281 10.62091 9
529.37960	9.98716	9.39243	10.60755 10.01285 10.62040 8
539.38011	9.98712	9.39299	10.60701 10.01288 10.61989 7
549.38062	9.98709	9.39353	10.60645 10.01291 10.61938 6
559.38113	9.98706	9.39407	10.60593 10.01294 10.61887 5
569.38164	9.98703	9.39461	10.60539 10.01297 10.61836 4
579.38216	9.98700	9.39515	10.60485 10.01300 10.61785 3
589.38266	9.98697	9.39569	10.60431 10.01303 10.61734 2
599.38317	9.98694	9.39623	10.60377 10.01306 10.61683 1
609.38368	9.98690	9.39677	10.60323 10.01310 10.61633 0
	Sine.	Tang.	Secant.

# A Table of Artificial Sines,

Degrees.

Min.	Sine.	Tang.	Secant.
0	9.38368	9.98690	9.39677 10.60323 10.01310 10.616 60
1	9.38418	9.98687	9.36731 10.60269 10.01313 10.61582 59
2	9.38469	9.98684	9.39785 10.60215 10.01316 10.61531 58
3	9.38519	9.98681	9.39838 10.60162 10.01319 10.61481 57
4	9.38570	9.98678	9.39892 10.60108 10.01322 10.61430 56
5	9.38620	9.98675	9.39946 10.60055 10.01325 10.61380 55
6	9.38670	9.98671	9.39999 10.60001 10.01329 10.61330 54
7	9.38721	9.98668	9.40052 10.59948 10.01332 10.61279 53
8	9.38771	9.98666	9.40106 10.59894 10.01335 10.61229 52
9	9.38821	9.98662	9.40159 10.59841 10.01338 10.61179 51
10	9.38871	9.98659	9.40212 10.59788 10.01341 10.61129 50
11	9.38921	9.98656	9.40266 10.59734 10.01345 10.61079 49
12	9.38971	9.98652	9.40319 10.59681 10.01348 10.61029 48
13	9.39021	9.98649	9.40372 10.59628 10.01351 10.60979 47
14	9.39071	9.98646	9.40425 10.59575 10.01354 10.60929 46
15	9.39121	9.98643	9.40478 10.59522 10.01357 10.60876 45
16	9.39170	9.98640	9.40531 10.59469 10.01361 10.60830 44
17	9.39220	9.98636	9.40584 10.59416 10.01364 10.60780 43
18	9.39270	9.98633	9.40636 10.59364 10.01367 10.60731 42
19	9.39319	9.98630	9.40689 10.59311 10.01370 10.60681 41
20	9.39369	9.98627	9.40742 10.59258 10.01373 10.60632 40
21	9.39418	9.98623	9.40795 10.59206 10.01377 10.60582 39
22	9.39467	9.98620	9.40847 10.59153 10.01380 10.60533 38
23	9.39517	9.98617	9.40900 10.59100 10.01383 10.60483 37
24	9.39566	9.98614	9.40952 10.59048 10.01386 10.60434 36
25	9.39615	9.98610	9.41005 10.58996 10.01390 10.60385 35
26	9.39664	9.98607	9.41057 10.58943 10.01393 10.60336 34
27	9.39713	9.98604	9.41109 10.58891 10.01396 10.60287 33
28	9.39762	9.98601	9.41162 10.58839 10.01399 10.60239 32
29	9.39811	9.98597	9.41214 10.58786 10.01403 10.60189 31
30	9.39860	9.98594	9.41266 10.58734 10.01406 10.60140 30
	Sine.	Tang.	Secant.

75 Degrees.

# Tangents and Secants

14 Degrees.

No.	Sine.	Tang.	Secant.	
30	9.31260	9.98594	9.41266	10.58734
31	9.3399	9.98591	9.41318	10.58682
32	9.339958	9.98588	9.41370	10.58630
33	9.40006	9.98584	9.41422	10.58578
34	9.40055	9.98581	9.41474	10.58526
35	9.40104	9.98578	9.41526	10.58474
36	9.40152	9.98575	9.41578	10.58423
37	9.40201	9.98571	9.41629	10.58371
38	9.40249	9.98568	9.41681	10.58319
39	9.40297	9.98565	9.41733	10.58267
40	9.40346	9.98561	9.41784	10.58216
41	9.40394	9.98558	9.41836	10.58164
42	9.40442	9.98555	9.41887	10.58113
43	9.40490	9.98551	9.41939	10.58061
44	9.40538	9.98548	9.41990	10.58010
45	9.40586	9.98545	9.42042	10.57959
46	9.40634	9.98541	9.42093	10.57907
47	9.40682	9.98538	9.42144	10.57856
48	9.40730	9.98535	9.42195	10.57805
49	9.40778	9.98531	9.42246	10.57754
50	9.40825	9.98528	9.42297	10.57703
51	9.40873	9.98525	9.42348	10.57652
52	9.40921	9.98521	9.42399	10.57601
53	9.40968	9.98518	9.42450	10.57550
54	9.41016	9.98515	9.42501	10.57499
55	9.41063	9.98511	9.42552	10.57448
56	9.41111	9.98508	9.42603	10.57397
57	9.41158	9.98505	9.42653	10.57347
58	9.41205	9.98501	9.42704	10.57296
59	9.41252	9.98498	9.42755	10.57245
60	9.41300	9.98494	9.42800	10.57195
	Sine.	Tang.	Secant.	

75 Degrees.

# A Table of Artificial Sines,

Degrees.

Min.	Sine.	Tang.	Secant.	Min.	
0	9.41300	9.98494	9.42805	10.57195	10.01506
1	9.41347	9.98491	9.42856	10.57144	10.01509
2	9.41394	9.98488	9.42906	10.57094	10.01512
3	9.41441	9.98484	9.42957	10.57043	10.01516
4	9.41488	9.98481	9.43007	10.56993	10.01519
5	9.41525	9.98477	9.43057	10.56943	10.01523
6	9.41582	9.98474	9.43108	10.56893	10.01526
7	9.41628	9.98471	9.43158	10.56842	10.01529
8	9.41675	9.98467	9.43208	10.56792	10.01533
9	9.41722	9.98464	9.43258	10.56742	10.01530
10	9.41768	9.98460	9.43308	10.56692	10.01540
11	9.41815	9.98457	9.43358	10.56642	10.01543
12	9.41862	9.98454	9.43408	10.56592	10.01547
13	9.41908	9.98450	9.43458	10.56542	10.01550
14	9.41954	9.98447	9.43508	10.56492	10.01553
15	9.42001	9.98443	9.43558	10.56442	10.01557
16	9.42047	9.98440	9.43607	10.56393	10.01560
17	9.42093	9.98436	9.43657	10.56343	10.01564
18	9.42140	9.98433	9.43707	10.56293	10.01567
19	9.42186	9.98429	9.43756	10.56244	10.01571
20	9.42232	9.98426	9.43806	10.56194	10.01574
21	9.42278	9.98422	9.43855	10.56145	10.01578
22	9.42324	9.98419	9.43905	10.56095	10.01581
23	9.42370	9.98416	9.43954	10.56046	10.01584
24	9.42416	9.98412	9.44004	10.55996	10.01588
25	9.42462	9.98409	9.44053	10.55947	10.01592
26	9.42507	9.98405	9.44102	10.55898	10.01595
27	9.42553	9.98402	9.44151	10.55849	10.01599
28	9.42599	9.98398	9.44201	10.55799	10.01602
29	9.42644	9.98395	9.44250	10.55750	10.01605
30	9.42690	9.98391	9.44299	10.55701	10.01609
	Sine.	Tang.	Secant.	Min.	

# Tangents and Secants

15 Degrees.

M.	Sine.		Tang.		Secant.		
30	9.42690	9.98391	9.44299	10.55201	10.01600	10.57310	30
31	9.4275	9.98388	9.44348	10.55652	10.01612	10.57265	29
32	9.42781	9.98384	9.44397	10.55603	10.01616	10.57219	28
33	9.42816	9.98381	9.44446	10.55554	10.01620	10.57174	27
34	9.42872	9.98377	9.44495	10.55505	10.01623	10.57128	26
35	9.42917	9.9834	9.44544	10.55457	10.01627	10.57083	25
36	9.42962	9.98370	9.44592	10.55408	10.01630	10.57038	24
37	9.43008	9.98366	9.44541	10.55359	10.01634	10.56992	23
38	9.43053	9.98363	9.44690	10.55310	10.01637	10.56947	22
39	9.43098	9.98359	9.44738	10.55262	10.01641	10.56902	21
40	9.43143	9.98356	9.44787	10.55215	10.01644	10.56857	20
41	9.43188	9.98352	9.44836	10.55164	10.01648	10.56812	19
42	9.43231	9.98349	9.44884	10.55116	10.01651	10.56767	18
43	9.43278	9.98345	9.44833	10.55067	10.01655	10.56722	17
44	9.43323	9.98342	9.44981	10.55019	10.01658	10.56677	16
45	9.43368	9.98338	9.45029	10.54971	10.01662	10.56633	15
46	9.43412	9.98335	9.45078	10.54922	10.01666	10.56588	14
47	9.43457	9.98331	9.45126	10.54874	10.01669	10.56543	13
48	9.43502	9.98327	9.45174	10.54826	10.01672	10.56498	12
49	9.43546	9.98324	9.45223	10.54778	10.01676	10.56454	11
50	9.43591	9.98320	9.45271	10.54729	10.01680	10.56404	10
51	9.43635	9.98317	9.45319	10.54681	10.01683	10.56365	9
52	9.43680	9.98314	9.45367	10.54633	10.01687	10.56320	8
53	9.43724	9.98309	9.45415	10.54585	10.01691	10.56276	7
54	9.43769	9.98306	9.45463	10.54537	10.01694	10.56231	6
55	9.43813	9.98302	9.45511	10.54489	10.01698	10.56187	5
56	9.43857	9.98299	9.45559	10.54441	10.01701	10.56143	4
57	9.43901	9.98295	9.45606	10.54394	10.01705	10.56099	3
58	9.43946	9.98291	9.45654	10.54346	10.01709	10.56054	2
59	9.43990	9.98288	9.45702	10.54298	10.01712	10.56010	1
60	9.44034	9.98284	9.45750	10.54250	10.01716	10.56966	0
		Sine.	Tang.		Secant.		

74 Degrees.

A Table of Artificial Sines,

6 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.44034 9.98284	9.45750	10.54250	10.01716 10.551660
1	9.44078 9.98281	9.45797	10.54203	10.01720 10.55192259
2	9.44122 9.98277	9.45845	10.54155	10.01723 10.55187858
3	9.44166 9.98273	9.45893	10.54108	10.01727 10.55183457
4	9.44210 9.98270	9.45940	10.54060	10.01730 10.55179056
5	9.44254 9.98266	9.45988	10.54013	10.01734 10.55174755
6	9.44297 9.98262	9.46035	10.53965	10.01738 10.55170354
7	9.44341 9.98259	9.46082	10.53918	10.01741 10.55169953
8	9.44385 9.98255	9.46130	10.53870	10.01745 10.55161552
9	9.44428 9.98251	9.46177	10.53823	10.01749 10.55157351
10	9.44472 9.98248	9.46224	10.53776	10.01752 10.55152850
11	9.44516 9.98244	9.46271	10.53729	10.01756 10.55148949
12	9.44559 9.98240	9.46319	10.53681	10.01760 10.55144148
13	9.44603 9.98237	9.46366	10.53634	10.01763 10.55139847
14	9.44646 9.98233	9.46413	10.53587	10.01767 10.55135446
15	9.44689 9.98229	9.46460	10.53540	10.01771 10.55131145
16	9.44733 9.98226	9.46507	10.53493	10.01774 10.55126744
17	9.44776 9.98222	9.46554	10.53446	10.01778 10.55122443
18	9.44819 9.98218	9.46601	10.53399	10.01782 10.55118142
19	9.44862 9.98215	9.46648	10.53352	10.01785 10.55113841
20	9.44905 9.98211	9.46695	10.53306	10.01789 10.5509540
21	9.44949 9.98207	9.46741	10.53259	10.01793 10.5505239
22	9.44992 9.98204	9.46788	10.53212	10.01797 10.5500938
23	9.45035 9.98200	9.46835	10.53165	10.01800 10.5496637
24	9.45078 9.98196	9.46881	10.53119	10.01804 10.5492336
25	9.45120 9.98193	9.46928	10.53072	10.01808 10.5488035
26	9.45163 9.98189	9.46975	10.53025	10.01811 10.5483734
27	9.45206 9.98185	9.47021	10.52979	10.01815 10.5479433
28	9.45249 9.98181	9.47068	10.52932	10.01819 10.5475132
29	9.45292 9.98177	9.47114	10.52886	10.01823 10.5470931
30	9.45334 9.98174	9.47161	10.52840	10.01826 10.5466630
	Sine.	Tang.	Secant.	Min.

Tangents and Secants.

16

N	Sine.	Tang.	Secant.
30	9.455349.98174	9.47161	10.52840
31	9.455779.98170	9.47207	10.52793
32	9.454199.98166	9.47253	10.52747
33	9.454629.98162	9.47300	10.52701
34	9.455049.98159	9.47346	10.52654
35	9.455479.98155	9.47392	10.52608
36	9.455899.98151	9.47438	10.52562
37	9.456329.98147	9.47484	10.52516
38	9.456749.98144	9.47530	10.52470
39	9.457169.98140	9.47576	10.52424
40	9.457589.98136	9.47622	10.52378
41	9.457919.98132	9.47668	10.52332
42	9.458439.98129	9.47714	10.52286
43	9.458859.98125	9.47760	10.52240
44	9.459279.98121	9.47806	10.52194
45	9.459699.98117	9.47850	10.52148
46	9.460119.98113	9.47898	10.52103
47	9.460539.98109	9.47943	10.52057
48	9.460959.98106	9.47989	10.52011
49	9.461369.98102	9.48035	10.51966
50	9.461789.98098	9.48080	10.51920
51	9.462209.98094	9.48126	10.51874
52	9.462669.98090	9.48171	10.51829
53	9.463039.98087	9.48217	10.51783
54	9.463459.98083	9.48262	10.51738
55	9.463869.98079	9.48308	10.51693
56	9.464289.98075	9.48353	10.51647
57	9.464699.98071	9.48398	10.51602
58	9.465119.98067	9.48444	10.51557
59	9.465559.98064	9.48489	10.51511
60	9.465949.98060	9.48534	10.51466
	Sine	Tang.	Secant.

73 Degrees.

A Table of Artificial Sines,

7 Degrees.

M	Sine.		Tang.		Secant.	N
0	9.46594	9.98060	9.48534	10.51466	10.01940	10.53407 60
1	9.46635	9.98056	9.48579	10.51424	10.01944	10.53365 59
2	9.46676	9.98052	9.48624	10.51376	10.01948	10.53324 58
3	9.46717	9.98048	9.48669	10.51331	10.01952	10.53283 57
4	9.46759	9.98044	9.48714	10.51286	10.01956	10.53242 56
5	9.46800	9.9804	9.48759	10.51241	10.01960	10.53200 55
6	9.46841	9.98036	9.48804	10.51196	10.01964	10.53159 54
7	9.46882	9.98033	9.48849	10.51151	10.01968	10.53118 53
8	9.46923	9.98029	9.48894	10.51106	10.01971	10.53077 52
9	9.46964	9.98025	9.48939	10.51061	10.01975	10.53030 53
10	9.47004	9.98021	9.48984	10.51016	10.01979	10.52995 50
11	9.47046	9.98017	9.49029	10.50971	10.01983	10.52955 49
12	9.47086	9.98013	9.49073	10.50927	10.01987	10.52914 48
13	9.47127	9.98009	9.49118	10.50882	10.01991	10.52873 47
14	9.47168	9.98005	9.49163	10.50837	10.01995	10.52823 46
15	9.47209	9.98001	9.49207	10.50793	10.01999	10.52781 45
16	9.47249	9.97997	9.49252	10.50748	10.02003	10.52751 44
17	9.47290	9.97993	9.49297	10.50704	10.02007	10.52710 43
18	9.47330	9.97990	9.49341	10.50659	10.02011	10.52670 42
19	9.47371	9.97986	9.49385	10.50614	10.02015	10.52629 41
20	9.47412	9.97982	9.49430	10.50570	10.02019	10.52589 40
21	9.47452	9.97978	9.49474	10.50526	10.02023	10.52543 39
22	9.47492	9.97974	9.49519	10.50481	10.02026	10.52508 38
23	9.47533	9.97970	9.49563	10.50437	10.02030	10.52467 37
24	9.47573	9.97966	9.49607	10.50393	10.02034	10.52427 36
25	9.47613	9.97962	9.49652	10.50349	10.02038	10.52387 35
26	9.47654	9.97958	9.49696	10.50304	10.02042	10.52346 34
27	9.47694	9.97954	9.49740	10.50260	10.02046	10.52306 33
28	9.47734	9.97950	9.49784	10.50216	10.02050	10.52266 32
29	9.47774	9.97946	9.49828	10.50172	10.02054	10.52226 31
30	9.47814	9.97942	9.49872	10.50128	10.02058	10.52186 30
	Sine.		Tang.		Secant.	M

72 Degrees.

# Tangents and Secants.

17 Degrees.

$\frac{\pi}{5}$	Sine.	Tang.	Secant.	
30 9.47814	9.97942	9.49872	10.50128	10.02058
31 9.47854	9.97938	9.49816	10.50084	10.02062
32 9.47894	9.97934	9.49960	10.50040	10.02066
33 9.47934	9.97930	9.50004	10.49996	10.02070
34 9.47974	9.97926	9.50048	10.49952	10.02074
35 9.48014	9.97922	9.50092	10.49908	10.02078
36 9.48054	9.97918	9.50136	10.49864	10.02082
37 9.48094	9.97914	9.50180	10.49820	10.02086
38 9.48133	9.97910	9.50224	10.49777	10.02090
39 9.48173	9.97906	9.50267	10.49733	10.02094
40 9.48213	9.97902	9.50311	10.49689	10.02098
41 9.48253	9.97898	9.50355	10.49645	10.02102
42 9.48292	9.97894	9.50398	10.49602	10.02106
43 9.48332	9.97890	9.50442	10.49558	10.02110
44 9.48371	9.97886	9.50485	10.49515	10.02114
45 9.48411	9.97882	9.50529	10.49471	10.02118
46 9.48450	9.97878	9.50572	10.49428	10.02122
47 9.48490	9.97874	9.50616	10.49384	10.02126
48 9.48529	9.97870	9.50659	10.49341	10.02130
49 9.48568	9.97866	9.50703	10.49297	10.02135
50 9.48608	9.97862	9.50746	10.49254	10.02139
51 9.48647	9.97857	9.50789	10.49211	10.02143
52 9.48686	9.97853	9.50833	10.49167	10.02147
53 9.48725	9.97849	9.50876	10.49124	10.02151
54 9.48764	9.97844	9.50919	10.49081	10.02155
55 9.48803	9.97841	9.50962	10.49038	10.02159
56 9.48842	9.97837	9.51005	10.48995	10.02163
57 9.48881	9.97833	9.51049	10.48952	10.02167
58 9.48920	9.97829	9.51092	10.48908	10.02171
59 9.48959	9.97825	9.51135	10.48865	10.02175
60 9.48998	9.97821	9.51178	10.48822	10.02179
	Sine.	Tang.	Secant.	Min.

72 Degrees.

# A Table of Artificial Sines,

78 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.48998	9.97821	9.52178	10.48822
1	9.49037	9.97817	9.51221	10.4879
2	9.49076	9.97814	9.51264	10.48737
3	9.49115	9.97808	9.51306	10.48690
4	9.49153	9.97804	9.51349	10.48551
5	9.49192	9.97800	9.51392	10.48608
6	9.49231	9.97796	9.51435	10.48565
7	9.49270	9.97792	9.51478	10.48522
8	9.49308	9.97788	9.51520	10.48480
9	9.49347	9.97784	9.51563	10.48437
10	9.49385	9.97779	9.51606	10.48394
11	9.49424	9.97775	9.51648	10.48352
12	9.49462	9.97771	9.51691	10.48309
13	9.49501	9.97767	9.51734	10.48267
14	9.49539	9.97763	9.51779	10.48224
15	9.49577	9.97759	9.51819	10.48181
16	9.49615	9.97754	9.51861	10.48139
17	9.49654	9.97750	9.51903	10.48097
18	9.49692	9.97746	9.51946	10.48054
19	9.49730	9.97742	9.51988	10.48012
20	9.49768	9.97738	9.52031	10.47970
21	9.49806	9.97734	9.52073	10.47927
22	9.49844	9.97729	9.52115	10.47885
23	9.49882	9.97725	9.52157	10.47843
24	9.49920	9.97721	9.52200	10.47801
25	9.49958	9.97717	9.52242	10.47758
26	9.49996	9.97713	9.52284	10.47716
27	9.50034	9.97708	9.52326	10.47674
28	9.50072	9.97704	9.52368	10.47632
29	9.50110	9.97700	9.52410	10.47590
30	9.50148	9.97696	9.52452	10.47548
	Sine.	Tang.	Secant.	

71 Degrees.

# Tangents and Secants.

18 Degrees.

N	Sine.	Tang.	Secant.	
30	9.50148	9.97696	9.51452	10.4754
31	9.50185	9.97691	9.512194	10.47506
32	9.50223	9.97687	9.512516	10.47464
33	9.50261	9.97683	9.512571	10.47422
34	9.50298	9.97679	9.512610	10.47380
35	9.50336	9.97675	9.512662	10.47335
36	9.50374	9.97670	9.512703	10.47297
37	9.50411	9.97666	9.512745	10.47256
38	9.50449	9.97662	9.512787	10.47213
39	9.50486	9.97657	9.512829	10.47172
40	9.50523	9.97653	9.51287	10.47130
41	9.50561	9.97649	9.512912	10.47088
42	9.50598	9.97645	9.512954	10.47047
43	9.50635	9.97640	9.512996	10.47005
44	9.50673	9.97636	9.513037	10.46963
45	9.50710	9.97632	9.513078	10.46922
46	9.50747	9.97628	9.513120	10.46880
47	9.50784	9.97623	9.513161	10.46839
48	9.50821	9.97619	9.513203	10.46798
49	9.50859	9.97615	9.513244	10.46756
50	9.50896	9.97610	9.513285	10.46715
51	9.50933	9.97606	9.513327	10.46673
52	9.50970	9.97602	9.513368	10.46632
53	9.51007	9.97597	9.513409	10.46591
54	9.51043	9.97593	9.513450	10.46550
55	9.51080	9.97589	9.513492	10.46508
56	9.51117	9.97584	9.513535	10.46467
57	9.51154	9.97580	9.513574	10.46426
58	9.51191	9.97576	9.513615	10.46385
59	9.51228	9.97571	9.513656	10.46344
60	9.51264	9.97567	9.513695	10.46303
	Sine.	Tang.	Secant.	

71 Degrees.

# A Table of Artificial Sines,

19 Degrees.

M.	Sine.		Tang.		Secant.	
0	9.51264	9.97567	9.53697	10.46302	10.02433	10.4873660
1	9.51301	9.97563	9.53738	10.46222	10.02437	10.4869959
2	9.51338	9.97559	9.53779	10.46121	10.02442	10.4866358
3	9.51374	9.97554	9.53820	10.46080	10.02446	10.4862657
4	9.51411	9.97550	9.53861	10.46139	10.02450	10.4858956
5	9.51447	9.97545	9.53902	10.46098	10.02455	10.4855355
6	9.51484	9.97541	9.53943	10.46057	10.02459	10.4851654
7	9.51520	9.97537	9.53984	10.46016	10.02464	10.4848053
8	9.51557	9.97532	9.54025	10.45976	10.02468	10.4844352
9	9.51593	9.97528	9.54065	10.45935	10.02472	10.4840751
10	9.51629	9.97523	9.54106	10.45894	10.02477	10.4837150
11	9.51666	9.97519	9.54147	10.45853	10.02481	10.4833449
12	9.51702	9.97515	9.54188	10.45813	10.02486	10.4829848
13	9.51738	9.97510	9.54228	10.45772	10.02490	10.4826247
14	9.51775	9.97506	9.54269	10.45731	10.02494	10.4822646
15	9.51811	9.97501	9.54309	10.45691	10.02499	10.4818945
16	9.51847	9.97497	9.54350	10.45650	10.02503	10.4815344
17	9.51883	9.97493	9.54391	10.45610	10.02508	10.4811743
18	9.51919	9.97488	9.54431	10.45569	10.02512	10.4808142
19	9.51955	9.97484	9.54472	10.45528	10.02516	10.4804541
20	9.51991	9.97479	9.54512	10.45488	10.02521	10.4800940
21	9.52027	9.97475	9.54552	10.45448	10.02525	10.4797339
22	9.52063	9.97471	9.54593	10.45407	10.02530	10.4793738
23	9.52099	9.97466	9.54633	10.45367	10.02534	10.4790137
24	9.52135	9.97461	9.54673	10.45327	10.02539	10.4786536
25	9.52171	9.97457	9.54714	10.45286	10.02543	10.4782935
26	9.52207	9.9745	9.54754	10.45246	10.02548	10.4779334
27	9.52242	9.97448	9.54794	10.45206	10.02551	10.4775833
28	9.52278	9.97444	9.54835	10.45166	10.02556	10.4772232
29	9.52314	9.97439	9.54875	10.45125	10.02561	10.4768631
30	9.52350	9.97435	9.54915	10.45085	10.02565	10.4765130

Sine.                    Tang.                    Secant.

70 Degrees.

Min.

# Tangents and Secants.

19° Degrees.

M	Sine.	Tang.	Secant.	M	
30	9.52350	9.974359	10.45085	10.02565	10.4765130
31	9.52385	9.974309	10.45045	10.02570	10.4761529
32	9.52421	9.974269	10.45005	10.02574	10.4757928
33	9.52456	9.974219	10.44965	10.02579	10.4754427
34	9.52492	9.974179	10.44925	10.02583	10.4750826
35	9.52528	9.974129	10.44885	10.02587	10.4747325
36	9.52563	9.974089	10.44845	10.02592	10.4743724
37	9.52598	9.974039	10.44805	10.02597	10.4740223
38	9.52634	9.973999	10.44765	10.02601	10.4736622
39	9.52669	9.973949	10.44725	10.02606	10.4733121
40	9.52705	9.973909	10.44685	10.02610	10.4729520
41	9.52740	9.973859	10.44645	10.02615	10.4726019
42	9.52775	9.973819	10.44605	10.02619	10.4722518
43	9.52811	9.973769	10.44566	10.02624	10.4719017
44	9.52846	9.973729	10.44526	10.02628	10.4715416
45	9.52881	9.973679	10.44486	10.02633	10.4711915
46	9.52916	9.973639	10.44446	10.02637	10.4708414
47	9.52951	9.973599	10.44407	10.02642	10.4704913
48	9.52986	9.973549	10.44367	10.02647	10.4701412
49	9.53022	9.973499	10.44327	10.02651	10.4697911
50	9.53057	9.973449	10.44288	10.02656	10.4694410
51	9.53092	9.973409	10.44248	10.02660	10.469099
52	9.53127	9.973359	10.44209	10.02665	10.468748
53	9.53161	9.973319	10.44169	10.02669	10.468397
54	9.53196	9.973269	10.44130	10.02674	10.468046
55	9.53231	9.973229	10.44090	10.02679	10.467695
56	9.53266	9.973179	10.44051	10.02683	10.467344
57	9.53301	9.973129	10.44012	10.02688	10.466993
58	9.53336	9.973089	10.43972	10.02692	10.466642
59	9.53370	9.973049	10.43933	10.02697	10.466301
60	9.53405	9.972999	10.43893	10.02701	10.465950
	Sine.	Tang.	Secant.	M	

70° Degrees.

# A Table of Artificial Sines,

20 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.53405	9.97299	9.56107	10.4380 10.02701
1	9.53440	9.97294	9.56146	10.43804 10.02706
2	9.53475	9.97289	9.56185	10.43818 10.02711
3	9.53510	9.97285	9.56224	10.43826 10.02715
4	9.53544	9.97280	9.56264	10.43836 10.02720
5	9.53578	9.97276	9.56303	10.43839 10.02725
6	9.53613	9.97271	9.56342	10.43858 10.02729
7	9.53647	9.97266	9.56381	10.43869 10.02734
8	9.53682	9.97261	9.56420	10.43880 10.02738
9	9.53716	9.97257	9.56459	10.43841 10.02743
10	9.53751	9.97252	9.56498	10.43802 10.02748
11	9.53785	9.97248	9.56537	10.43463 10.02752
12	9.53819	9.97243	9.56576	10.43424 10.02757
13	9.53854	9.97238	9.56615	10.43385 10.02762
14	9.53888	9.97234	9.56654	10.43346 10.02766
15	9.53922	9.97229	9.56693	10.43307 10.02771
16	9.53957	9.97225	9.56732	10.43268 10.02776
17	9.53991	9.97220	9.56771	10.43229 10.02780
18	9.54025	9.97215	9.56810	10.43190 10.02785
19	9.54059	9.97211	9.56849	10.43151 10.02790
20	9.54093	9.97206	9.56887	10.43113 10.02794
21	9.54127	9.97201	9.56925	10.43074 10.02799
22	9.54161	9.97196	9.56965	10.43035 10.02804
23	9.54195	9.97192	9.57004	10.42996 10.02808
24	9.54229	9.97187	9.57042	10.42958 10.02813
25	9.54263	9.97182	9.57081	10.42919 10.02818
26	9.54297	9.97178	9.57120	10.42881 10.02822
27	9.54331	9.97173	9.57158	10.42842 10.02827
28	9.54365	9.97168	9.57197	10.42803 10.02832
29	9.54399	9.97164	9.57235	10.42765 10.02837
30	9.54433	9.97159	9.57274	10.42726 10.02841
	Sine.	Tang.	Secant.	Min.

69 Degrees.

# Tangents and Secants.

20 Degrees.

Zig.	Sine.	Tang.	Secant.	
30	9.54433	9.97159	9.574	10.42726
31	9.54466	9.97154	9.571	10.42688
32	9.54500	9.97149	9.571	10.42649
33	9.54534	9.97145	9.571	10.42611
34	9.54567	9.97140	9.571	10.42572
35	9.54601	9.97135	9.571	10.42534
36	9.54635	9.97130	9.571	10.42496
37	9.54668	9.97126	9.571	10.42457
38	9.54702	9.97121	9.571	10.42419
39	9.54735	9.97116	9.571	10.42381
40	9.54769	9.97111	9.571	10.42342
41	9.54802	9.97107	9.571	10.42304
42	9.54836	9.97102	9.571	10.42266
43	9.54869	9.97097	9.571	10.42228
44	9.54903	9.97092	9.571	10.42190
45	9.54936	9.97087	9.571	10.42151
46	9.54969	9.97083	9.571	10.42113
47	9.55003	9.97078	9.571	10.42075
48	9.55036	9.97073	9.571	10.42037
49	9.55069	9.97068	9.571	10.41999
50	9.55102	9.97064	9.571	10.41961
51	9.55136	9.97059	9.571	10.41923
52	9.55169	9.97054	9.571	10.41885
53	9.55202	9.97049	9.571	10.41847
54	9.55235	9.97044	9.571	10.41809
55	9.55268	9.97039	9.571	10.41771
56	9.55301	9.97035	9.571	10.41734
57	9.55334	9.97030	9.571	10.41696
58	9.55367	9.97025	9.571	10.41658
59	9.55400	9.97020	9.571	10.41620
60	9.55433	9.97015	9.571	10.41582
	Sine	Tang.	Secant.	Min.

69 Degrees.

# A Table of Artificial Sines,

21 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.55433	9.97015	9.58418	10.4154
1	9.55469	9.97010	9.58456	10.41445
2	9.55499	9.97006	9.58493	10.41357
3	9.55532	9.97001	9.58531	10.41269
4	9.55564	9.96996	9.58569	10.41181
5	9.55597	9.96991	9.58606	10.41104
6	9.55630	9.96986	9.58644	10.41056
7	9.55663	9.96981	9.58682	10.41019
8	9.55695	9.96976	9.58719	10.41081
9	9.55728	9.96971	9.58757	10.41243
10	9.55761	9.96967	9.58794	10.41206
11	9.55793	9.96962	9.58832	10.41168
12	9.55826	9.96957	9.58869	10.41131
13	9.55858	9.96952	9.58907	10.41093
14	9.55891	9.96947	9.58944	10.41056
15	9.55923	9.96942	9.58981	10.41019
16	9.55956	9.96937	9.59016	10.40981
17	9.55988	9.96932	9.59056	10.40944
18	9.56021	9.96927	9.59094	10.40907
19	9.56053	9.96922	9.59131	10.40869
20	9.56086	9.96917	9.59168	10.40832
21	9.56118	9.96912	9.59205	10.40795
22	9.56150	9.96908	9.59243	10.40757
23	9.56182	9.96903	9.59280	10.40720
24	9.56215	9.96898	9.59317	10.40683
25	9.56247	9.96893	9.59354	10.40646
26	9.56280	9.96888	9.59391	10.40609
27	9.56311	9.96883	9.59429	10.40572
28	9.56343	9.96878	9.59466	10.40534
29	9.56376	9.96873	9.59503	10.40497
30	9.56408	9.96868	9.59540	10.40460
	Sine.	Tang.	Secant.	

68 Degrees.

# Tangents and Secants.

21 Degrees.

M.	Sine.		Tang.		Secant.	
30	9.56408	9.96868	9.59140	10.40460	10.03132	10.43193 30
31	9.56440	9.96863	9.59177	10.40423	10.03137	10.43561 29
32	9.56472	9.96858	9.5924	10.40386	10.03142	10.43528 28
33	9.56504	9.96853	9.5961	10.40349	10.03147	10.43496 27
34	9.56536	9.96848	9.5968	10.40312	10.03152	10.43464 26
35	9.56568	9.96843	9.5975	10.40275	10.03157	10.43432 25
36	9.56600	9.96838	9.59752	10.40238	10.03162	10.43401 24
37	9.56631	9.96833	9.59799	10.40202	10.03167	10.43369 23
38	9.56663	9.96828	9.5985	10.40165	10.03172	10.43337 22
39	9.56695	9.96823	9.5987	10.40128	10.03177	10.43305 21
40	9.56727	9.96818	9.59909	10.40091	10.03182	10.43273 20
41	9.56759	9.96813	9.59946	10.40054	10.03187	10.43241 19
42	9.56790	9.96808	9.59983	10.40017	10.03192	10.43210 18
43	9.56822	9.96803	9.60019	10.39981	10.03197	10.43178 17
44	9.56854	9.96798	9.60056	10.39944	10.03202	10.43146 16
45	9.56884	9.96793	9.60093	10.39907	10.03207	10.43114 15
46	9.56917	9.96788	9.60130	10.39870	10.03212	10.43083 14
47	9.56949	9.96783	9.60160	10.39834	10.03217	10.43051 13
48	9.56980	9.96778	9.60203	10.39797	10.03223	10.43020 12
49	9.57012	9.96773	9.60240	10.39761	10.03228	10.42988 11
50	9.57044	9.96767	9.60276	10.39724	10.03233	10.42956 10
51	9.57075	9.96762	9.60313	10.39687	10.03238	10.42925 9
52	9.57107	9.96757	9.60349	10.39651	10.03243	10.42893 8
53	9.57138	9.96752	9.60386	10.39614	10.03248	10.42862 7
54	9.57170	9.96747	9.60422	10.39578	10.03253	10.42831 6
55	9.57201	9.96742	9.60459	10.39541	10.03258	10.42799 5
56	9.57232	9.96737	9.60495	10.39505	10.03263	10.42768 4
57	9.57264	9.96732	9.60532	10.39468	10.03268	10.42736 3
58	9.57295	9.96727	9.60568	10.39432	10.03273	10.42709 2
59	9.57326	9.96722	9.60605	10.39395	10.03278	10.42674 1
60	9.57358	9.96717	9.60641	10.39359	10.03283	10.42643 0

Sine.

Tang.

Secant.

68 Degrees.

# A Table of Artificial Sines,

22 Degrees.

M	Sine.		Tang.		Secant.	
0	9.57358	9.96717	9.60641	10.39355	10.03283	10.42643
1	9.57389	9.96712	9.60677	10.39233	10.03289	10.42611
2	9.57420	9.96706	9.60714	10.39186	10.03294	10.42580
3	9.57451	9.96701	9.60750	10.39150	10.03299	10.42549
4	9.57482	9.96696	9.60786	10.39114	10.03304	10.42518
5	9.57514	9.96691	9.60823	10.39178	10.03309	10.42487
6	9.57545	9.96686	9.60859	10.39113	10.03314	10.42455
7	9.57576	9.96681	9.60895	10.39155	10.03319	10.42424
8	9.57607	9.96676	9.60931	10.39059	10.03324	10.42393
9	9.57638	9.96671	9.60967	10.39033	10.03330	10.42362
10	9.57669	9.96665	9.61004	10.38996	10.03335	10.42331
11	9.57700	9.96660	9.61040	10.38960	10.03340	10.42300
12	9.57731	9.96655	9.61076	10.38924	10.03345	10.42269
13	9.57762	9.96650	9.61112	10.38888	10.03350	10.42238
14	9.57793	9.96645	9.61148	10.38852	10.03355	10.42207
15	9.57824	9.96640	9.61184	10.38816	10.03361	10.42176
16	9.57855	9.96634	9.61200	10.38780	10.03366	10.42146
17	9.57885	9.96629	9.61256	10.38744	10.03371	10.42115
18	9.57916	9.96624	9.61292	10.38708	10.03376	10.42084
19	9.57947	9.96619	9.61328	10.38672	10.03381	10.42053
20	9.57978	9.96614	9.61364	10.38636	10.03386	10.42023
21	9.58008	9.96609	9.61400	10.38600	10.03392	10.41992
22	9.58039	9.96603	9.61436	10.38564	10.03397	10.41961
23	9.58070	9.96598	9.61472	10.38528	10.03402	10.41930
24	9.58101	9.96593	9.61508	10.38492	10.03407	10.41900
25	9.58131	9.96588	9.61544	10.38457	10.03412	10.41869
26	9.58162	9.96582	9.61579	10.38421	10.03418	10.41838
27	9.58192	9.96577	9.61615	10.38385	10.03423	10.41808
28	9.58223	9.96572	9.61651	10.38349	10.03428	10.41777
29	9.58253	9.96567	9.61687	10.38313	10.03433	10.41747
30	9.58284	9.96562	9.61722	10.38278	10.03439	10.41716
	Sine.		Tang.		Secant.	

67 Degrees.

# Tangents and Secants.

22 Degrees.

M <sup>o</sup>	Sine.	Tang.	Secant.	
30	9.58284	9.96562	9.61722	10.38276
31	9.58314	9.96550	9.6158	10.38242
32	9.58345	9.96551	9.6141	10.38200
33	9.58375	9.96546	9.6118	10.38171
34	9.58406	9.96541	9.6118	10.38139
35	9.58436	9.96535	9.6119	10.38099
36	9.58467	9.96530	9.61136	10.38064
37	9.58497	9.96525	9.61172	10.38028
38	9.58527	9.96520	9.61089	10.37992
39	9.58557	9.96514	9.62043	10.37957
40	9.58588	9.96509	9.62079	10.37921
41	9.58618	9.96504	9.62114	10.37886
42	9.58648	9.96498	9.62150	10.37850
43	9.58678	9.96493	9.62185	10.37815
44	9.58709	9.96488	9.62221	10.37779
45	9.58739	9.96483	9.62256	10.37744
46	9.58769	9.96477	9.62292	10.37709
47	9.58799	9.96472	9.62327	10.37673
48	9.58829	9.96467	9.62362	10.37638
49	9.58859	9.96461	9.62398	10.37603
50	9.58889	9.96456	9.62433	10.37567
51	9.58919	9.96451	9.62468	10.37532
52	9.58949	9.96445	9.62504	10.37490
53	9.58979	9.96440	9.62539	10.37461
54	9.59009	9.96435	9.62574	10.37426
55	9.59039	9.96429	9.62609	10.37391
56	9.59069	9.96424	9.62645	10.37356
57	9.59098	9.96419	9.62680	10.37320
58	9.59128	9.96413	9.62715	10.37285
59	9.59158	9.96408	9.62750	10.37250
60	9.59188	9.96403	9.62785	10.37215
	Sine.	Tang.	Secant.	

67 Degrees.

# A Table of Artificial Sines,

23 Degrees.

N.	Sine.	Tang.	Secant.	
0	9.59188	9.96403	9.62185	10.371510.0359710.4081260
1	9.59218	9.96397	9.62220	10.3718010.0360310.4078259
2	9.59247	9.96392	9.62255	10.3714510.0360810.4075358
3	9.59278	9.96387	9.62291	10.3711010.0361410.4072357
4	9.59307	9.96381	9.622926	10.3707510.0361910.4069356
5	9.59336	9.96376	9.62961	10.3703910.0362410.4066455
6	9.59366	9.96370	9.62996	10.3700410.0363010.4063454
7	9.59396	9.96365	9.63031	10.3706910.0363510.4060453
8	9.59425	9.96360	9.63066	10.37093410.0364010.4057552
9	9.59455	9.96354	9.63101	10.3690010.0364610.4054551
10	9.59484	9.96349	9.63135	10.3686510.0365110.4051650
11	9.59514	9.96343	9.63170	10.3683010.0365710.4048649
12	9.59543	9.96338	9.63215	10.3679510.0366210.4045748
13	9.59573	9.96333	9.63250	10.3676010.0366810.4042747
14	9.59602	9.96327	9.63275	10.3672510.0367310.4039846
15	9.59632	9.96322	9.63310	10.3669010.0367810.4036945
16	9.59661	9.96316	9.63345	10.3665510.0368410.4033944
17	9.59690	9.96311	9.63380	10.3662110.0368910.4031043
18	9.59720	9.96305	9.63414	10.3658610.0369510.4028042
19	9.59749	9.96300	9.63449	10.3655110.0370010.4025141
20	9.59778	9.96295	9.63484	10.3651610.0370610.4022240
21	9.59808	9.96289	9.63519	10.3648210.0371110.4019339
22	9.59837	9.96284	9.63553	10.3644710.0371610.4016338
23	9.59866	9.96278	9.63588	10.3641210.0372210.4013437
24	9.59895	9.96273	9.63623	10.3637710.0372710.4010536
25	9.59924	9.96267	9.63657	10.3634310.0373310.4007635
26	9.59954	9.96262	9.63692	10.3630810.0373810.4004634
27	9.59983	9.96256	9.63727	10.3627410.0374410.4001733
28	9.60012	9.96251	9.63761	10.3623910.0374910.4008832
29	9.60041	9.96245	9.63796	10.3620410.0375510.4005931
30	9.60070	9.96240	9.63830	10.3617010.0376010.4003030
	Sine.	Tang.	Secant.	

66 Degrees.

Min.

# Tangents and Secants.

23 Degrees.

M.	Sine.	Tang.	Secant.	
30	9.60070	9.96240	9.63830	10.36170
31	9.60099	9.96234	9.63865	10.36135
32	9.60128	9.96229	9.63899	10.36101
33	9.60157	9.96223	9.63934	10.36066
34	9.60186	9.96218	9.63968	10.36032
35	9.60215	9.96212	9.64003	10.35997
36	9.60244	9.96207	9.64037	10.35963
37	9.60273	9.96201	9.64072	10.35928
38	9.60302	9.96196	9.64106	10.35894
39	9.60331	9.96190	9.64141	10.35860
40	9.60359	9.96185	9.64175	10.35825
41	9.60388	9.96179	9.64209	10.35791
42	9.60417	9.96174	9.64243	10.35757
43	9.60446	9.96168	9.64278	10.35722
44	9.60475	9.96162	9.64312	10.35688
45	9.60503	9.96157	9.64346	10.35654
46	9.60532	9.96151	9.64381	10.35619
47	9.60561	9.96146	9.64415	10.35585
48	9.60589	9.96140	9.64449	10.35550
49	9.60618	9.96135	9.64483	10.35517
50	9.60647	9.96129	9.64517	10.35483
51	9.60675	9.96124	9.64552	10.35448
52	9.60704	9.96118	9.64586	10.35414
53	9.60732	9.96112	9.64620	10.35380
54	9.60761	9.96107	9.64654	10.35346
55	9.60789	9.96101	9.64688	10.35312
56	9.60818	9.96096	9.64722	10.35278
57	9.60846	9.96090	9.64756	10.35244
58	9.60875	9.96084	9.64790	10.35210
59	9.60903	9.96079	9.64824	10.35176
60	9.60931	9.96073	9.64858	10.35142
	Sine.	Tang.	Secant.	

66 Degrees.

A Table of Artificial Sines,

24 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.60931	9.96073	9.64858	10.3512
1	9.60950	9.96067	9.64892	10.3508
2	9.60982	9.96052	9.64926	10.3574
3	9.61016	9.96056	9.64960	10.3540
4	9.61045	9.96051	9.64994	10.3506
5	9.61073	9.96045	9.65028	10.3472
6	9.61101	9.96039	9.65062	10.3448
7	9.61129	9.96034	9.65096	10.3404
8	9.61158	9.96028	9.65130	10.3470
9	9.61186	9.96022	9.65164	10.34836
10	9.61214	9.96017	9.65197	10.34803
11	9.61242	9.96011	9.65231	10.34764
12	9.61270	9.96005	9.65265	10.34735
13	9.61298	9.96000	9.65299	10.34701
14	9.61326	9.95994	9.65333	10.34667
15	9.61355	9.95988	9.65367	10.34634
16	9.61383	9.95983	9.65400	10.34600
17	9.61411	9.95977	9.65434	10.34566
18	9.61439	9.95971	9.65467	10.34533
19	9.61467	9.95965	9.65501	10.34499
20	9.61494	9.95960	9.65535	10.34465
21	9.61522	9.95954	9.65568	10.34432
22	9.61550	9.95944	9.65602	10.34398
23	9.61578	9.95943	9.65636	10.34364
24	9.61606	9.95937	9.65669	10.34331
25	9.61634	9.95931	9.65702	10.34297
26	9.61662	9.95925	9.65736	10.34264
27	9.61689	9.95920	9.65770	10.34230
28	9.61717	9.95914	9.65803	10.34197
29	9.61745	9.95908	9.65837	10.34163
30	9.61773	9.95902	9.65870	10.34130
		Sine	Tang.	Secant.

# Tangents and Secants.

24 Degrees.

S. E.	Sine.	Tang.	Secant.	
30	9.61773	9.95902	9.61870	10.34130
31	9.61800	9.95897	9.61504	10.34096
32	9.61828	9.95891	9.615937	10.34063
33	9.61856	9.95885	9.615971	10.34029
34	9.61883	9.95879	9.66004	10.33996
35	9.61911	9.95872	9.66138	10.33962
36	9.61939	9.95868	9.66171	10.33929
37	9.61966	9.95862	9.66174	10.33896
38	9.61994	9.95856	9.66173	10.33862
39	9.62021	9.95850	9.66171	10.33829
40	9.62049	9.95845	9.66204	10.33796
41	9.62076	9.95839	9.66238	10.33762
42	9.62104	9.95833	9.66271	10.33729
43	9.62131	9.95827	9.66304	10.33696
44	9.62159	9.95821	9.66337	10.33663
45	9.62186	9.95815	9.66371	10.33629
46	9.62214	9.95810	9.66404	10.33596
47	9.62241	9.95804	9.66437	10.33563
48	9.62268	9.95798	9.66470	10.33530
49	9.62296	9.95792	9.66504	10.33497
50	9.62323	9.95786	9.66537	10.33463
51	9.62350	9.95780	9.66570	10.33430
52	9.62377	9.95774	9.66603	10.33397
53	9.62405	9.95769	9.66636	10.33364
54	9.62432	9.95761	9.66669	10.33331
55	9.62459	9.95757	9.66702	10.33298
56	9.62486	9.95751	9.66735	10.33265
57	9.62514	9.95745	9.66768	10.33232
58	9.62541	9.95739	9.66801	10.33199
59	9.62568	9.95734	9.66834	10.33166
60	9.62595	9.95728	9.66867	10.33133
	Sine	Tang.	Secant.	M.

65 Degrees.

# A Table of Artificial Sines,

25 Degrees.

Min.	Sine.	Tang.		Secant.	
0	9.625959.95728	9.66967	10.33133	10.04272	10.37409 60
1	9.626129.95722	9.66909	10.33100	10.04278	10.37378 59
2	9.626299.95716	9.66933	10.33057	10.04284	10.37353 58
3	9.626469.95710	9.66966	10.33034	10.04290	10.37324 57
4	9.6267039.95704	9.66999	10.33001	10.04296	10.37297 56
5	9.627309.95698	9.67032	10.32558	10.04302	10.37270 55
6	9.627579.95692	9.67065	10.3295	10.04308	10.37243 54
7	9.627849.95686	9.67098	10.3292	10.04314	10.37216 53
8	9.628119.95680	9.67131	10.3289	10.04320	10.37189 52
9	9.628389.95674	9.67163	10.3287	10.04326	10.37162 51
10	9.628659.95668	9.67196	10.32804	10.04332	10.37135 50
11	9.628929.95663	9.67229	10.32771	10.04338	10.37108 49
12	9.629189.95657	9.67262	10.32738	10.04343	10.37082 48
13	9.629459.95651	9.67295	10.32705	10.04349	10.37055 47
14	9.629729.95645	9.67328	10.32673	10.04355	10.37028 46
15	9.629999.95639	9.67361	10.32640	10.04361	10.37001 45
16	9.630259.95633	9.67323	10.32607	10.04367	10.36974 44
17	9.630529.95627	9.67226	10.32574	10.04373	10.36948 43
18	9.630799.95621	9.67258	10.32542	10.04379	10.36921 42
19	9.631069.95615	9.67491	10.32509	10.04385	10.36894 41
20	9.631339.95609	9.67524	10.32476	10.04391	10.36867 40
21	9.631599.95603	9.67556	10.32444	10.04397	10.36841 39
22	9.631869.95597	9.67589	10.32411	10.04403	10.36814 38
23	9.632139.95591	9.67622	10.32378	10.04409	10.36787 37
24	9.632399.95585	9.67654	10.32346	10.04415	10.36761 36
25	9.632669.95579	9.67687	10.32313	10.04421	10.36734 35
26	9.632929.95573	9.67719	10.32281	10.04427	10.36708 34
27	9.633199.95567	9.67752	10.32248	10.04433	10.36681 33
28	9.633459.95561	9.67785	10.32215	10.04439	10.36655 32
29	9.633729.95555	9.67817	10.32183	10.04445	10.36628 31
30	9.633989.95549	9.67850	10.32150	10.04451	10.36602 30
	Sine.	Tang.		Secant.	

64 Degrees.

# Tangents and Secants.

25 Degrees.

Min.	Sine.	Tang.	Secant.	
30	9.63398	9.95549	9.67850	10.32150
31	9.63425	9.95543	9.67882	10.32118
32	9.63451	9.95537	9.67915	10.32085
33	9.63478	9.95531	9.67947	10.32053
34	9.63504	9.95525	9.67980	10.32021
35	9.63531	9.95519	9.68012	10.31988
36	9.63557	9.95513	9.68044	10.31956
37	9.63583	9.95507	9.68077	10.31923
38	9.63610	9.95501	9.68110	10.31891
39	9.63636	9.95494	9.68142	10.31858
40	9.63662	9.95488	9.68174	10.31826
41	9.63689	9.95482	9.68206	10.31794
42	9.63715	9.95476	9.68239	10.31761
43	9.63741	9.95470	9.68271	10.31729
44	9.63767	9.95464	9.68303	10.31697
45	9.63794	9.95458	9.68336	10.31664
46	9.63820	9.95452	9.68368	10.31632
47	9.63846	9.95446	9.68400	10.31600
48	9.63872	9.95440	9.68432	10.31568
49	9.63898	9.95434	9.68465	10.31535
50	9.63924	9.95427	9.68497	10.31503
51	9.63950	9.95421	9.68529	10.31471
52	9.63976	9.95415	9.68561	10.31439
53	9.64002	9.95409	9.68593	10.31407
54	9.64028	9.95403	9.68626	10.31375
55	9.64054	9.95397	9.68658	10.31342
56	9.64080	9.95391	9.68690	10.31310
57	9.64106	9.95385	9.68722	10.31278
58	9.64132	9.95378	9.68754	10.31246
59	9.64158	9.95372	9.68786	10.31214
60	9.64184	9.95366	9.68818	10.31182
	Sine.	Tang.	Secant.	Min.

64 Degrees.

# A Table of Artificial Sines,

~~126~~ Degrees.

M	Sine.	Tang.	Secant.	N
0	9.64184	9.95366	9.68818	10.31182
1	9.64210	9.95360	9.68850	10.31150
2	9.64236	9.95354	9.68882	10.31118
3	9.64262	9.95348	9.68914	10.31086
4	9.64288	9.95341	9.68946	10.31054
5	9.64314	9.95335	9.68978	10.31022
6	9.64339	9.95329	9.69010	10.30990
7	9.64365	9.95323	9.69042	10.30958
8	9.64391	9.95317	9.69074	10.30926
9	9.64417	9.95310	9.69106	10.30894
10	9.64442	9.95304	9.69138	10.30862
11	9.64468	9.95298	9.69170	10.30830
12	9.64494	9.95292	9.69202	10.30798
13	9.64519	9.95286	9.69234	10.30766
14	9.64545	9.95279	9.69266	10.30734
15	9.64571	9.95273	9.69298	10.30703
16	9.64596	9.95267	9.69329	10.30671
17	9.64622	9.95261	9.69361	10.30639
18	9.64647	9.95254	9.69393	10.30607
19	9.64673	9.95248	9.69425	10.30575
20	9.64698	9.95242	9.69457	10.30543
21	9.64724	9.95236	9.69488	10.30512
22	9.64749	9.95229	9.69520	10.30480
23	9.64775	9.95223	9.69552	10.30448
24	9.64800	9.95217	9.69584	10.30416
25	9.64826	9.95211	9.69615	10.30385
26	9.64851	9.95204	9.69647	10.30353
27	9.64877	9.95198	9.69679	10.30321
28	9.64902	9.95192	9.69710	10.30290
29	9.64927	9.95185	9.69742	10.30258
30	9.64953	9.95179	9.69774	10.30226
	Sine.	Tang.	Secant.	N

63 Degrees.

# Tangents and Secants.

26 Degrees.

M.	Sine.	Tang.	Secant.	
30	9.64953	9.95179	9.69774	10.30326
31	9.64978	9.95173	9.69805	10.30195
32	9.65003	9.95167	9.69837	10.30163
33	9.65029	9.95160	9.69869	10.30132
34	9.65054	9.95154	9.69900	10.30100
35	9.65079	9.95148	9.69932	10.30068
36	9.65104	9.95141	9.69963	10.30037
37	9.65130	9.95135	9.69995	10.30005
38	9.65155	9.95129	9.70026	10.29974
39	9.65180	9.95122	9.70058	10.29942
40	9.65205	9.95116	9.70089	10.29911
41	9.65230	9.95110	9.70121	10.29879
42	9.65256	9.95103	9.70152	10.29848
43	9.65281	9.95097	9.70184	10.29816
44	9.65306	9.95091	9.70215	10.29785
45	9.65331	9.95084	9.70247	10.29753
46	9.65356	9.95078	9.70278	10.29722
47	9.65381	9.95071	9.70310	10.29791
48	9.65406	9.95065	9.70341	10.29659
49	9.65431	9.95059	9.70372	10.29628
50	9.65456	9.95052	9.70404	10.29596
51	9.65481	9.95046	9.70435	10.29565
52	9.65506	9.95039	9.70466	10.29534
53	9.65531	9.95033	9.70498	10.29502
54	9.65556	9.95027	9.70529	10.29471
55	9.65581	9.95020	9.70560	10.29440
56	9.65605	9.95014	9.70592	10.29408
57	9.65630	9.95007	9.70623	10.29377
58	9.65655	9.95000	9.70654	10.29346
59	9.65680	9.95995	9.70685	10.29315
60	9.65704	9.95988	9.70717	10.29283
		Sine.	Tang.	Secant.

63 Degrees.

# A Table of Artificial Sines,

27 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.65707	9.94988	9.70717	10.29283
1	9.65710	9.94981	9.70748	10.29252
2	9.65714	9.94971	9.70779	10.29221
3	9.65719	9.94969	9.70810	10.29190
4	9.65804	9.94962	9.70841	10.29159
5	9.65828	9.94956	9.70873	10.29127
6	9.65853	9.94949	9.70904	10.29096
7	9.65878	9.94943	9.70935	10.29065
8	9.65903	9.94936	9.70966	10.29034
9	9.65927	9.94930	9.70997	10.29003
10	9.65952	9.94924	9.71028	10.28972
11	9.65976	9.94917	9.71059	10.28941
12	9.66001	9.94911	9.71090	10.28910
13	9.66026	9.94904	9.71121	10.28879
14	9.66050	9.94898	9.71152	10.28848
15	9.66075	9.94891	9.71184	10.28816
16	9.66099	9.94885	9.71215	10.28785
17	9.66124	9.94878	9.71246	10.28754
18	9.66148	9.94872	9.71277	10.28723
19	9.66173	9.94865	9.71308	10.28692
20	9.66197	9.94858	9.71339	10.28661
21	9.66221	9.94852	9.71370	10.28630
22	9.66246	9.94845	9.71401	10.28600
23	9.66270	9.94839	9.71431	10.28569
24	9.66295	9.94832	9.71462	10.28538
25	9.66319	9.94826	9.71493	10.28507
26	9.66343	9.94819	9.71524	10.28476
27	9.66368	9.94813	9.71555	10.28445
28	9.66392	9.94806	9.71586	10.28414
29	9.66416	9.94800	9.71617	10.28383
30	9.66441	9.94793	9.71648	10.28352
	Sine.	Tang.	Secant.	Min.

62 Degrees,

# Tangents and Secants.

27 Degrees.

Z. P.	Cir.	Tang.	Secant.	
30	9.66441	9.94793	9.71648	10.28352 10.0520 10.33559 30
31	9.66465	9.94786	9.71679	10.28322 10.05214 10.33535 29
32	9.66489	9.94780	9.71709	10.28291 10.05220 10.33511 28
33	9.66513	9.94773	9.71740	10.28260 10.05227 10.33487 27
34	9.66538	9.94767	9.71771	10.28229 10.05233 10.33463 26
35	9.66562	9.94760	9.71802	10.28198 10.05240 10.33438 25
36	9.66586	9.94753	9.71833	10.28168 10.05247 10.33414 24
37	9.66610	9.94747	9.71863	10.28137 10.05253 10.33390 23
38	9.66634	9.94740	9.71894	10.28106 10.05260 10.33366 22
39	9.66658	9.94734	9.71925	10.28075 10.05267 10.33342 21
40	9.66682	9.94727	9.71956	10.28045 10.05273 10.33318 20
41	9.66707	9.94720	9.71986	10.28014 10.05280 10.33294 19
42	9.66731	9.94714	9.72017	10.27983 10.05286 10.33270 18
43	9.66755	9.94707	9.72048	10.27952 10.05293 10.33245 17
44	9.66779	9.94700	9.72078	10.27922 10.05300 10.33221 16
45	9.66803	9.94694	9.72109	10.27891 10.05306 10.33197 15
46	9.66827	9.94687	9.72139	10.27860 10.05313 10.33173 14
47	9.66851	9.94680	9.72170	10.27830 10.05320 10.33149 13
48	9.66875	9.94674	9.72201	10.27799 10.05326 10.33125 12
49	9.66899	9.94667	9.72232	10.27769 10.05333 10.33101 11
50	9.66923	9.94660	9.72262	10.27738 10.05340 10.33078 10
51	9.66946	9.94654	9.72293	10.27707 10.05346 10.33054 9
52	9.66970	9.94647	9.72323	10.27677 10.05353 10.3303 8
53	9.66994	9.94640	9.72354	10.27646 10.05360 10.33006 7
54	9.67018	9.94634	9.72384	10.27616 10.05366 10.32982 6
55	9.67042	9.94627	9.72415	10.27585 10.05373 10.32958 5
56	9.67066	9.94620	9.72445	10.27555 10.05380 10.32934 4
57	9.67090	9.94614	9.72476	10.27524 10.05386 10.32910 3
58	9.67113	9.94607	9.72507	10.27494 10.05393 10.32887 2
59	9.67137	9.94600	9.72537	10.27463 10.05400 10.32863 1
60	9.67161	9.94594	9.72567	10.27433 10.05407 10.32839 0
		Sine.	Tang.	Secant.

62 Degrees.

A Table of Artificial Sines,

28 Degrees.

Min.	Sine.	Tang.	Secant.				
0	9.67161	9.94594	9.72567	10.27433	10.05407	10.32839	60
1	9.67185	9.94587	9.72598	10.27422	10.05413	10.32815	59
2	9.67208	9.94580	9.72628	10.27372	10.05420	10.32792	58
3	9.67232	9.94573	9.72659	10.27341	10.05427	10.32768	57
4	9.67256	9.94567	9.72689	10.27311	10.05433	10.32744	56
5	9.67280	9.94560	9.72720	10.27280	10.05440	10.32711	55
6	9.67303	9.94553	9.72750	10.27250	10.05447	10.32697	54
7	9.67327	9.94546	9.72781	10.27220	10.05454	10.32673	53
8	9.67351	9.94540	9.72811	10.27189	10.05460	10.32650	52
9	9.67374	9.94533	9.72841	10.27159	10.05467	10.32626	51
10	9.67398	9.94526	9.72871	10.27128	10.05474	10.32602	50
11	9.67421	9.94519	9.72901	10.27098	10.05481	10.32579	49
12	9.67445	9.94513	9.72931	10.27068	10.05487	10.32555	48
13	9.67468	9.94506	9.72961	10.27037	10.05494	10.32532	47
14	9.67492	9.94499	9.72991	10.27007	10.05501	10.32508	46
15	9.67516	9.94492	9.73023	10.26977	10.05508	10.32485	45
16	9.67539	9.94485	9.73054	10.26947	10.05515	10.32461	44
17	9.67562	9.94479	9.73084	10.26916	10.05521	10.32438	43
18	9.67586	9.94472	9.73114	10.26886	10.05528	10.32414	42
19	9.67609	9.94465	9.73144	10.26856	10.05535	10.32391	41
20	9.67633	9.94458	9.73175	10.26825	10.05542	10.32367	40
21	9.67656	9.94451	9.73205	10.26795	10.05549	10.32344	39
22	9.67680	9.94445	9.73235	10.26765	10.05555	10.32320	38
23	9.67703	9.94438	9.73265	10.26735	10.05562	10.32297	37
24	9.67726	9.94431	9.73296	10.26705	10.05569	10.32274	36
25	9.67750	9.94424	9.73326	10.26674	10.05576	10.32250	35
26	9.67773	9.94417	9.73356	10.26644	10.05583	10.32227	34
27	9.67796	9.94410	9.73386	10.26614	10.05590	10.32204	33
28	9.67820	9.94404	9.73416	10.26584	10.05596	10.32180	32
29	9.67843	9.94397	9.73446	10.26554	10.05603	10.32157	31
30	9.67866	9.94390	9.73476	10.26524	10.05610	10.32134	30
	Sine.	Tang.	Secant.				

61 Degrees.

# Tangents and Secants.

28 Degrees.

M.	Sine.	Tang.	Secant.	
30	9.67866	9.94390	9.73476	10.26524
31	9.67890	9.94383	9.73507	10.26493
32	9.67913	9.94376	9.73537	10.26463
33	9.67936	9.94369	9.73567	10.26433
34	9.67959	9.94362	9.73597	10.26403
35	9.67982	9.94356	9.73627	10.26273
36	9.68006	9.94349	9.73657	10.26343
37	9.68029	9.94342	9.73687	10.26313
38	9.68052	9.94335	9.73717	10.26283
39	9.68075	9.94328	9.73747	10.26253
40	9.68098	9.94321	9.73777	10.26223
41	9.68121	9.94314	9.73807	10.26193
42	9.68144	9.94307	9.73837	10.26163
43	9.68167	9.94300	9.73867	10.26133
44	9.68191	9.94293	9.73897	10.26103
45	9.68214	9.94286	9.73927	10.26073
46	9.68237	9.94280	9.73957	10.26043
47	9.68260	9.94273	9.73987	10.26012
48	9.68283	9.94266	9.74017	10.25983
49	9.68306	9.94259	9.74047	10.25953
50	9.68328	9.94252	9.74077	10.25923
51	9.68351	9.94245	9.74107	10.25893
52	9.68374	9.94238	9.74137	10.25864
53	9.68397	9.94231	9.74166	10.25834
54	9.68420	9.94224	9.74196	10.25804
55	9.68443	9.94217	9.74226	10.25774
56	9.68466	9.94210	9.74256	10.25744
57	9.68489	9.94203	9.74286	10.25714
58	9.68512	9.94196	9.74316	10.25684
59	9.68534	9.94189	9.74345	10.25655
60	9.68557	9.94182	9.74375	10.25625
	Sine	Tang.	Secant.	

61 Degrees.

# A Table of Artificial Sines,

29 Degrees.

M.	Sine.	Tang.	Secant.	
0	9.625576	9.41829	9.74375	10.25625
1	9.68580	9.94175	9.74405	10.25595
2	9.68523	9.94168	9.74435	10.25565
3	9.68625	9.94161	9.74465	10.25536
4	9.68648	9.94154	9.74494	10.25506
5	9.68671	9.94147	9.74524	10.25476
6	9.68694	9.94140	9.74554	10.25446
7	9.68716	9.94133	9.74584	10.25417
8	9.68739	9.94126	9.74613	10.25387
9	9.68762	9.94119	9.74643	10.25357
10	9.68784	9.94112	9.74673	10.25327
11	9.68807	9.94105	9.74702	10.25298
12	9.68830	9.94098	9.74732	10.25268
13	9.68852	9.94091	9.74762	10.25238
14	9.68875	9.94083	9.74791	10.25209
15	9.68897	9.94076	9.74821	10.25179
16	9.68920	9.94069	9.74851	10.25150
17	9.68942	9.94062	9.74880	10.25120
18	9.68965	9.94055	9.74910	10.25090
19	9.68987	9.94048	9.74939	10.25061
20	9.69010	9.94041	9.74969	10.25031
21	9.69032	9.94034	9.74997	10.25002
22	9.69055	9.94027	9.75028	10.24972
23	9.69077	9.94020	9.75058	10.24942
24	9.69100	9.94013	9.75087	10.24913
25	9.69122	9.94005	9.75117	10.24883
26	9.69144	9.93998	9.75146	10.24854
27	9.69167	9.93991	9.75176	10.24824
28	9.69190	9.93984	9.75205	10.24795
29	9.69212	9.93977	9.75235	10.24765
30	9.69234	9.93970	9.75264	10.24736
	Sine.	Tang.	Secant.	
	60 Degrees.			
				M.

# Tangents and Secants.

29 Degrees.

No.	Sine.	Tang.	Secant.	
30	9.69234	9.93970	9.75264	10.24756
31	9.69250	9.93963	9.75294	10.24706
32	9.69279	9.93955	9.75323	10.24677
33	9.69301	9.93948	9.75353	10.24647
34	9.69323	9.93941	9.75382	10.24618
35	9.69345	9.93934	9.75412	10.24589
36	9.69368	9.93927	9.75441	10.24559
37	9.69390	9.93919	9.75470	10.24530
38	9.69412	9.93912	9.75500	10.24500
39	9.69434	9.93905	9.75529	10.24471
40	9.69456	9.93898	9.75559	10.24442
41	9.69479	9.93891	9.75588	10.24412
42	9.69501	9.93884	9.75617	10.24383
43	9.69523	9.93876	9.75647	10.24354
44	9.69545	9.93869	9.75676	10.24324
45	9.69567	9.93862	9.75705	10.24295
46	9.69589	9.93855	9.75735	10.24266
47	9.69611	9.93848	9.75764	10.24236
48	9.69633	9.93840	9.75793	10.24207
49	9.69655	9.93833	9.75822	10.24178
50	9.69677	9.93826	9.75852	10.24148
51	9.69700	9.93819	9.75881	10.24119
52	9.69722	9.93811	9.75901	10.24090
53	9.69744	9.93804	9.75940	10.24061
54	9.69765	9.93797	9.75969	10.24032
55	9.69787	9.93790	9.75998	10.24002
56	9.69809	9.93782	9.76027	10.23973
57	9.69831	9.93775	9.76056	10.23944
58	9.69853	9.93768	9.76086	10.23914
59	9.69873	9.93760	9.76115	10.23885
60	9.69897	9.93753	9.76144	10.23856
	Sine.	Tang.	Secant.	Min.

60 Degrees.

# A Table of Artificial Sines,

30 Degrees.

M	Sine.	Tang.	Secant.	
0	9.69197	9.93753	9.7144	10.23856
1	9.69199	9.93746	9.76173	10.23827
2	9.69194	9.93739	9.76202	10.23798
3	9.69963	9.93731	9.76231	10.23769
4	9.69984	9.93724	9.76261	10.23739
5	9.70006	9.93717	9.76290	10.23710
6	9.70028	9.93709	9.76319	10.23681
7	9.70050	9.93702	9.76348	10.23652
8	9.70072	9.93695	9.76377	10.23623
9	9.70093	9.93687	9.76406	10.23594
10	9.70115	9.93680	9.76435	10.23565
11	9.70137	9.93673	9.76464	10.23536
12	9.70159	9.93665	9.76493	10.23507
13	9.70180	9.93658	9.76522	10.23478
14	9.70202	9.93651	9.76551	10.23449
15	9.70224	9.93643	9.76581	10.23420
16	9.70245	9.93636	9.76610	10.23391
17	9.70267	9.93628	9.76639	10.23362
18	9.70289	9.93621	9.76668	10.23333
19	9.70310	9.93614	9.76697	10.23304
20	9.70332	9.93606	9.76726	10.23275
21	9.70353	9.93599	9.76755	10.23246
22	9.70375	9.93591	9.76783	10.23217
23	9.70396	9.93584	9.76812	10.23188
24	9.70418	9.93577	9.76841	10.23159
25	9.70440	9.93569	9.76870	10.23130
26	9.70461	9.93562	9.76899	10.23101
27	9.70483	9.93554	9.76928	10.23072
28	9.70504	9.93547	9.76957	10.23043
29	9.70525	9.93540	9.76986	10.23014
30	9.70547	9.93532	9.77015	10.22985
	Sine.	Tang.	Secant.	

59 Degrees.

# Tangents and Secants.

30 Degrees.

$\frac{X}{S}$	$S$		Tang.		Secant.	
30	9.70547	9.93532	9.77015	10.22905	10.06468	10.945330
31	9.70568	9.93525	9.77044	10.22956	10.06475	10.943229
32	9.70599	9.93517	9.77073	10.22927	10.06483	10.941028
33	9.70611	9.93510	9.77102	10.22899	10.06490	10.2938927
34	9.70633	9.93502	9.77130	10.22870	10.06498	10.2936726
35	9.70654	9.93495	9.77159	10.22841	10.06505	10.2934625
36	9.70675	9.93487	9.77188	10.22812	10.06513	10.2932524
37	9.70697	9.93480	9.77217	10.22783	10.06520	10.2930323
38	9.70718	9.93472	9.77246	10.22754	10.06528	10.2928222
39	9.70739	9.93465	9.77275	10.22726	10.06535	10.2926121
40	9.70761	9.93457	9.77303	10.22697	10.06543	10.2923920
41	9.70782	9.93450	9.77332	10.22668	10.06550	10.2921819
42	9.70803	9.93442	9.77361	10.22639	10.06558	10.2919718
43	9.70825	9.93435	9.77390	10.22610	10.06565	10.2917617
44	9.70846	9.93427	9.77418	10.22582	10.06573	10.2915516
45	9.70867	9.93420	9.77447	10.22553	10.06580	10.2913315
46	9.70888	9.93412	9.77476	10.22524	10.06588	10.2911214
47	9.70909	9.93405	9.77505	10.22495	10.06595	10.2909313
48	9.70931	9.93397	9.77533	10.22467	10.06603	10.2906912
49	9.70952	9.93390	9.77562	10.22438	10.06610	10.2904811
50	9.70973	9.93382	9.77591	10.22409	10.06618	10.2902710
51	9.70994	9.93375	9.77620	10.22381	10.06625	10.290069
52	9.71015	9.93367	9.77648	10.22352	10.06633	10.289858
53	9.71036	9.93360	9.77677	10.22323	10.06640	10.289647
54	9.71058	9.93352	9.77706	10.22295	10.06648	10.289436
55	9.71079	9.93344	9.77734	10.22266	10.06656	10.289215
56	9.71100	9.93337	9.77763	10.22237	10.06663	10.289004
57	9.71121	9.93329	9.77792	10.22209	10.06671	10.288793
58	9.71142	9.93322	9.77820	10.22180	10.06678	10.288582
59	9.71163	9.93314	9.77849	10.22151	10.06686	10.288371
60	9.71184	9.93307	9.77877	10.22122	10.06693	10.288160
		Sine.	Tang.		Secant.	

59 Degrees.

A Table of Artificial Sines,

31 Degrees.

M.	Sine.		Tang.		Secant.	
0	9.7184	9.93307	9.77877	10.22123	10.06693	10.2881660
1	9.71205	9.93299	9.77906	10.22094	10.06701	10.2879559
2	9.71226	9.93291	9.77935	10.22065	10.06709	10.2877458
3	9.71247	9.93284	9.77963	10.22037	10.06716	10.2875357
4	9.71268	9.93276	9.77992	10.22008	10.06727	10.2873256
5	9.71289	9.93269	9.78020	10.21980	10.06732	10.2871155
6	9.71310	9.93261	9.78049	10.21951	10.06739	10.2869054
7	9.71331	9.93253	9.78078	10.21923	10.06747	10.2866953
8	9.71352	9.93246	9.78106	10.21894	10.06754	10.2864852
9	9.71373	9.93238	9.78135	10.21865	10.06762	10.2862751
10	9.71394	9.93230	9.78163	10.21837	10.06770	10.2860750
11	9.71414	9.93223	9.78192	10.21808	10.06777	10.2858649
12	9.71435	9.93215	9.78220	10.21780	10.06785	10.2856548
13	9.71456	9.93208	9.78249	10.21751	10.06793	10.2854447
14	9.71477	9.93200	9.78277	10.21723	10.06800	10.2852346
15	9.71498	9.93192	9.78306	10.21695	10.06808	10.2850245
16	9.71519	9.93185	9.78334	10.21666	10.06816	10.2848144
17	9.71539	9.93177	9.78363	10.21637	10.06823	10.2846143
18	9.71560	9.93169	9.78391	10.21609	10.06831	10.2844042
19	9.71581	9.93161	9.78419	10.21581	10.06839	10.2841941
20	9.71602	9.93154	9.78448	10.21552	10.06846	10.2839840
21	9.71622	9.93146	9.78479	10.21524	10.06854	10.2837839
22	9.7164	9.93138	9.78508	10.21495	10.06862	10.2835738
23	9.7166	9.93130	9.78536	10.21467	10.06869	10.2833637
24	9.71685	9.93123	9.78562	10.21438	10.06877	10.2831536
25	9.71705	9.93115	9.78590	10.21410	10.06885	10.2829535
26	9.71726	9.93108	9.78618	10.21382	10.06893	10.2827434
27	9.71747	9.93100	9.78647	10.21353	10.06900	10.2825333
28	9.71767	9.93092	9.78675	10.21325	10.06908	10.2823332
29	9.71788	9.93084	9.78704	10.21296	10.06916	10.2821231
30	9.71809	9.93077	9.78732	10.21268	10.06923	10.2819230
	Sine		Tang.		Secant.	

58 Degrees.

# Tangents or Secants.

31 Degrees.

Mil°	Sine.	Tang.	Secant.	
30	9.71809	9.93017	9.78732	10.2123 10.06923 10.28192 30
31	9.71829	9.93069	9.78760	10.21240 10.0693 10.28171 29
32	9.71850	9.93061	9.78789	10.21211 10.06939 10.28150 28
33	9.71870	9.93053	9.78817	10.21183 10.06947 10.28130 27
34	9.71891	9.93046	9.78845	10.21155 10.06954 10.28109 26
35	9.71911	9.93038	9.78874	10.21126 10.06961 10.28089 25
36	9.71932	9.93030	9.78902	10.21098 10.06970 10.28068 24
37	9.71953	9.93022	9.78930	10.21070 10.06978 10.28048 23
38	9.71973	9.93015	9.78959	10.21042 10.06986 10.28027 22
39	9.71994	9.93007	9.78987	10.21013 10.06993 10.28007 21
40	9.72014	9.92999	9.79015	10.20985 10.07001 10.27986 20
41	9.72035	9.92991	9.79043	10.20957 10.07009 10.27966 19
42	9.72055	9.92983	9.79072	10.20928 10.07017 10.27945 18
43	9.72075	9.92976	9.79100	10.20900 10.07025 10.27925 17
44	9.72096	9.92968	9.79128	10.20872 10.0703 10.27904 16
45	9.72116	9.92960	9.79156	10.20844 10.07040 10.27884 15
46	9.72137	9.92952	9.79185	10.20815 10.07048 10.27863 14
47	9.72157	9.92944	9.79213	10.20787 10.07056 10.27845 13
48	9.72177	9.92936	9.79241	10.20759 10.07064 10.27823 12
49	9.72196	9.92929	9.79269	10.20731 10.07071 10.27802 11
50	9.72218	9.92921	9.79297	10.20703 10.07079 10.27782 10
51	9.72239	9.92913	9.79326	10.20674 10.07087 10.27762 9
52	9.72259	9.92905	9.79354	10.20646 10.07095 10.27741 8
53	9.72279	9.92897	9.79382	10.20618 10.07103 10.27721 7
54	9.72299	9.92889	9.79410	10.20590 10.07111 10.27701 6
55	9.72320	9.92881	9.79438	10.20562 10.07118 10.27681 5
56	9.72340	9.92874	9.79466	10.20534 10.07126 10.27660 4
57	9.72360	9.92866	9.79495	10.20505 10.07134 10.27640 3
58	9.72381	9.92858	9.79523	10.20477 10.07142 10.27620 2
59	9.72401	9.92850	9.79551	10.20449 10.07150 10.27599 1
60	9.72421	9.92842	9.79579	10.20421 10.07158 10.27579 0
	Sine.	Tang.	Secant.	

58 Degrees.

A Table of Artificial Sines.

32 Degrees.

Mil.	Sine.	Tang.	Sec. nt.	
0	9.724	9.92842	9.7979	10.20421
1	9.72	9.92834	9.79607	10.20393
2	9.72446	9.92826	9.79535	10.20365
3	9.72482	9.92818	9.79663	10.20337
4	9.72502	9.92810	9.79691	10.20309
5	9.72522	9.92803	9.79719	10.20281
6	9.72542	9.92795	9.79747	10.20253
7	9.72562	9.92787	9.79776	10.20225
8	9.72582	9.92779	9.79804	10.20196
9	9.72602	9.92770	9.79832	10.20168
10	9.72623	9.92763	9.79860	10.20140
11	9.72643	9.92755	9.79888	10.20112
12	9.72663	9.92747	9.79916	10.20084
13	9.72683	9.92739	9.79944	10.20056
14	9.72703	9.92731	9.79972	10.20028
15	9.72723	9.92723	9.80000	10.20000
16	9.72743	9.92715	9.80028	10.19972
17	9.72763	9.92707	9.80056	10.19944
18	9.72783	9.92699	9.80084	10.19916
19	9.72803	9.92691	9.80112	10.19888
20	9.72823	9.92683	9.80140	10.19860
21	9.72843	9.92675	9.80168	10.19833
22	9.72863	9.92667	9.80196	10.19805
23	9.72883	9.92659	9.80223	10.19777
24	9.72902	9.92651	9.80251	10.19749
25	9.72922	9.92643	9.80279	10.19721
26	9.72942	9.92635	9.80307	10.19693
27	9.72962	9.92627	9.80335	10.19665
28	9.72982	9.92619	9.80363	10.19637
29	9.73002	9.92611	9.80391	10.19609
30	9.73022	9.92603	9.80419	10.19581
	Sine.	Tang.	Secant.	Mil.

57 Degrees.

# Tangents and Secants.

32 Degrees.

M.	Sine	Tang.	Secant.	
30	9.73022	9.92603	9.80419	10.19581
31	9.73042	9.92595	9.80447	10.19553
32	9.73061	9.92587	9.80475	10.19526
33	9.73081	9.92579	9.80502	10.19498
34	9.73101	9.92571	9.80530	10.19470
35	9.73121	9.92563	9.80558	10.19442
36	9.73140	9.92555	9.80586	10.19414
37	9.73160	9.92547	9.80614	10.19386
38	9.73180	9.92538	9.80642	10.19359
39	9.73200	9.92530	9.80669	10.19331
40	9.73219	9.92522	9.80697	10.19303
41	9.73239	9.92514	9.80725	10.19275
42	9.73259	9.92505	9.80753	10.19247
43	9.73278	9.92498	9.80781	10.19220
44	9.73298	9.92490	9.80808	10.19192
45	9.73318	9.92482	9.80836	10.19164
46	9.73337	9.92474	9.80864	10.19136
47	9.73357	9.92465	9.80892	10.19108
48	9.73377	9.92457	9.80919	10.19081
49	9.73396	9.92449	9.80947	10.19053
50	9.73416	9.92441	9.80975	10.19025
51	9.73435	9.92433	9.80003	10.18998
52	9.73455	9.92425	9.81030	10.18970
53	9.73474	9.92416	9.81058	10.18942
54	9.73494	9.92408	9.81086	10.18914
55	9.73513	9.92401	9.81112	10.18887
56	9.73533	9.92392	9.81141	10.18859
57	9.73553	9.92384	9.81169	10.18831
58	9.73572	9.92376	9.81196	10.18804
59	9.73591	9.92367	9.81224	10.18775
60	9.73611	9.92359	9.81252	10.18748
	Sine	Tang.	Secant.	

57 Degrees.

Min.

# A Table of Artificial Sines,

33 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.73010	9.92359	9.81252	10.18748
1	9.73030	9.92355	9.81279	10.18721
2	9.73050	9.92343	9.81307	10.18693
3	9.73069	9.92335	9.81335	10.18669
4	9.73089	9.92326	9.81362	10.18638
5	9.73708	9.92318	9.81390	10.18610
6	9.73727	9.92310	9.81418	10.18582
7	9.73747	9.92302	9.81445	10.18555
8	9.73766	9.92293	9.81473	10.18527
9	9.73786	9.92285	9.81500	10.18500
10	9.73805	9.92277	9.81528	10.18472
11	9.73824	9.92269	9.81556	10.18445
12	9.73843	9.92260	9.81583	10.18417
13	9.73863	9.92252	9.81611	10.18389
14	9.73882	9.92244	9.81638	10.18362
15	9.73901	9.92236	9.81666	10.18334
16	9.73921	9.92227	9.81693	10.18307
17	9.73940	9.92219	9.81721	10.18279
18	9.73959	9.92211	9.81748	10.18252
19	9.73978	9.92202	9.81776	10.18224
20	9.73998	9.92194	9.81804	10.18197
21	9.74017	9.92186	9.81831	10.18169
22	9.74036	9.92177	9.81859	10.18142
23	9.74055	9.92169	9.81886	10.18114
24	9.74074	9.92161	9.81913	10.18087
25	9.74093	9.92152	9.81941	10.18059
26	9.74113	9.92144	9.81968	10.18031
27	9.74132	9.92136	9.81996	10.18004
28	9.74151	9.92127	9.82023	10.17977
29	9.74170	9.92119	9.82051	10.17949
30	9.74189	9.92111	9.82078	10.17922
	Sine.	Tang.	Secant.	Min.

56 Degrees.

# Tangents and Secants.

33 Degrees.

M.	Sine.		Tang.		Secant.	
30	9.74189	9.92111	9.82078	10.1792	10.07889	10.15811
31	9.74208	9.92102	9.82106	10.1789	10.07848	10.14792
32	9.74227	9.92094	9.82133	10.17867	10.07806	10.25773
33	9.74246	9.92086	9.82161	10.17839	10.07914	10.25754
34	9.74265	9.92077	9.82188	10.17812	10.07923	10.25735
35	9.74284	9.92069	9.82215	10.17785	10.07931	10.25716
36	9.74303	9.92060	9.82243	10.17757	10.07940	10.25697
37	9.74322	9.92052	9.82270	10.17730	10.07948	10.25678
38	9.74341	9.92044	9.82298	10.17702	10.07956	10.25659
39	9.74360	9.92035	9.82325	10.17675	10.07965	10.25642
40	9.74379	9.92027	9.82352	10.17648	10.07973	10.25623
41	9.74398	9.92018	9.82380	10.17620	10.07982	10.25602
42	9.74417	9.92010	9.82407	10.17593	10.07990	10.25583
43	9.74436	9.92002	9.82435	10.17565	10.07999	10.25564
44	9.74455	9.91993	9.82462	10.17538	10.08007	10.25546
45	9.74474	9.91985	9.82489	10.17511	10.08015	10.25526
46	9.74493	9.91976	9.82517	10.17483	10.08024	10.25507
47	9.74512	9.91968	9.82544	10.17456	10.08032	10.25488
48	9.74531	9.91959	9.82571	10.17429	10.08041	10.25469
49	9.74549	9.91951	9.82599	10.17401	10.08049	10.25451
50	9.74568	9.91942	9.82626	10.17374	10.08058	10.25432
51	9.74587	9.91934	9.82653	10.17347	10.08066	10.25413
52	9.74606	9.91925	9.82681	10.17320	10.08075	10.25394
53	9.74625	9.91917	9.82708	10.17292	10.08083	10.25375
54	9.74644	9.91908	9.82735	10.17265	10.08092	10.25356
55	9.74662	9.91900	9.82762	10.17238	10.08100	10.25338
56	9.74681	9.91892	9.82790	10.17210	10.08109	10.25319
57	9.74700	9.91883	9.82817	10.17183	10.08117	10.25300
58	9.74719	9.91874	9.82844	10.17156	10.08126	10.25281
59	9.74737	9.91866	9.82872	10.17129	10.08134	10.25263
60	9.74756	9.91857	9.82899	10.17102	10.08143	10.25244

Sine.

Tang.

Secant.

M.  
P.

56 Degrees.

A Table of Artificial Sines,

34 Degrees.

Min.	Sine.	Tang.	Secant.	
09.7476	9.9187	9.82899	10.17101	10.08143
19.7475	9.91349	9.82926	10.17074	10.08151
29.7474	9.91840	9.82953	10.17047	10.08160
39.7482	9.91832	9.82981	10.17020	10.08168
49.7483	9.91823	9.83008	10.16992	10.08177
59.7485	9.91815	9.83025	10.16965	10.08185
69.74868	9.91806	9.83062	10.16938	10.08194
79.74887	9.91798	9.83089	10.16911	10.08202
89.74906	9.91789	9.83117	10.16884	10.08211
99.74924	9.91781	9.83144	10.16856	10.08220
109.74943	9.91772	9.83171	10.16829	10.08228
119.74962	9.91763	9.83198	10.16802	10.08237
129.74980	9.91755	9.83215	10.16775	10.08245
139.74999	9.91746	9.83233	10.16748	10.08254
149.75017	9.91738	9.83280	10.16720	10.08262
159.75036	9.91729	9.83307	10.16693	10.08271
169.75054	9.91720	9.83334	10.16666	10.08280
179.75073	9.91712	9.83361	10.16639	10.08288
189.75091	9.91703	9.83388	10.16612	10.08297
199.75110	9.91695	9.83415	10.16585	10.08305
209.75128	9.91686	9.83443	10.16558	10.08314
219.75147	9.91677	9.83470	10.16530	10.08322
229.75165	9.91669	9.83497	10.16503	10.08331
239.75184	9.91660	9.83524	10.16476	10.08340
249.75202	9.91651	9.83551	10.16449	10.08349
259.75221	9.91643	9.83578	10.16422	10.08357
269.75239	9.91634	9.83605	10.16395	10.08366
279.75258	9.91625	9.83632	10.16368	10.08375
289.75276	9.91617	9.83659	10.16341	10.08383
299.75294	9.91608	9.83686	10.16314	10.08392
309.75313	9.91599	9.83713	10.16287	10.08401

Sine.

Tang.

Secant.

55 Degrees.

# Tangents and Secants.

34 Degrees.

<u>N.</u>	<u>Sine.</u>	<u>Tang.</u>	<u>Secant.</u>	<u>M.</u>			
30	9.75313	9.91599	9.83713	10.16207	0.08401	10.24687	30
31	9.75331	9.91591	9.83741	10.16260	0.08409	10.24669	29
32	9.75350	9.91582	9.83768	10.16232	0.08418	10.24651	28
33	9.75368	9.91573	9.83795	10.16205	0.08427	10.24632	27
34	9.75386	9.91565	9.83822	10.16178	0.08435	10.24614	26
35	9.75405	9.91556	9.83849	10.16151	0.08444	10.24595	
36	9.75423	9.91547	9.83876	10.16124	0.08453	10.24577	24
37	9.75441	9.91539	9.83903	10.16097	0.08462	10.24559	23
38	9.75460	9.91530	9.83930	10.16070	0.08470	10.24541	22
39	9.75478	9.91521	9.83957	10.16043	0.08479	10.24522	21
40	9.75496	9.91512	9.83984	10.16016	0.08488	10.24504	20
41	9.75514	9.91504	9.84011	10.15989	0.08497	10.24486	19
42	9.75533	9.91495	9.84038	10.15962	0.08505	10.24467	18
43	9.75551	9.91486	9.84065	10.15935	0.08514	10.24449	17
44	9.75569	9.91477	9.84092	10.15908	0.08523	10.24431	16
45	9.75587	9.91469	9.84119	10.15881	0.08532	10.24413	15
46	9.75605	9.91460	9.84146	10.15854	0.08540	10.24394	14
47	9.75624	9.91451	9.84173	10.15827	0.08549	10.24376	13
48	9.75642	9.91442	9.84200	10.15800	0.08558	10.24358	12
49	9.75660	9.91433	9.84227	10.15773	0.08567	10.24340	11
50	9.75678	9.91425	9.84254	10.15747	0.08575	10.24322	10
51	9.75696	9.91416	9.84281	10.15720	0.08584	10.24304	9
52	9.75714	9.91407	9.84307	10.15693	0.08593	10.24286	8
53	9.75732	9.91398	9.84334	10.15666	0.08602	10.24267	7
54	9.75751	9.91389	9.84361	10.15639	0.08611	10.24249	6
55	9.75769	9.91381	9.84388	10.15612	0.08619	10.24231	5
56	9.75787	9.91372	9.84415	10.15585	0.08628	10.24213	4
57	9.75805	9.91363	9.84442	10.15558	0.08637	10.24195	3
58	9.75823	9.91354	9.84469	10.15531	0.08646	10.24177	2
59	9.75841	9.91345	9.84496	10.15504	0.08655	10.24159	
60	9.75859	9.91336	9.84523	10.15477	0.08664	10.24141	
	<u>Sine.</u>	<u>Tang.</u>	<u>Secant.</u>				

55 Degrees.

# A Table of Artificial Sines,

35 Degrees.

S	Sine.	Tang.	Secant.	M		
0	9.75859	9.91336	10.15477	10.08665	10.2414160	
1	9.75877	9.91288	10.15450	10.08672	10.2412359	
2	9.75895	9.91261	10.15424	10.08681	10.2410558	
3	9.75913	9.91231	9.84603	10.15397	10.08690	10.2408757
4	9.75931	9.91201	9.84630	10.15370	10.08699	10.2406956
5	9.75949	9.91129	9.84657	10.15345	10.08708	10.2405155
6	9.75967	9.91123	9.84684	10.15316	10.08717	10.2403354
7	9.75985	9.91127	9.84711	10.15289	10.08726	10.2401953
8	9.76003	9.91126	9.84738	10.15262	10.08735	10.2399752
9	9.76021	9.91125	9.84764	10.15236	10.08743	10.2397951
10	9.76039	9.91124	9.84791	10.15209	10.08752	10.2396150
11	9.76057	9.91123	9.84818	10.15182	10.08761	10.2394349
12	9.76075	9.91123	9.84845	10.15155	10.08770	10.2392548
13	9.76093	9.91121	9.84872	10.15128	10.08779	10.2390747
14	9.76111	9.91121	9.84899	10.15101	10.08788	10.2388946
15	9.76129	9.91120	9.84925	10.15075	10.08797	10.2387245
16	9.76146	9.91119	9.84952	10.15048	10.08806	10.2385444
17	9.76164	9.91118	9.84979	10.15021	10.08815	10.2383643
18	9.76182	9.91117	9.85000	10.14994	10.08824	10.2381842
19	9.76200	9.91116	9.85033	10.14968	10.08833	10.2380041
20	9.76218	9.91115	9.85056	10.14941	10.08842	10.2378240
21	9.76236	9.91115	9.85080	10.14914	10.08851	10.2376439
22	9.76253	9.91114	9.85113	10.14887	10.08860	10.2374738
23	9.76271	9.91113	9.85146	10.14860	10.08868	10.2372937
24	9.76289	9.91123	9.85166	10.14834	10.08877	10.2371136
25	9.76307	9.91114	9.85193	10.14807	10.08886	10.2369335
26	9.76325	9.91105	9.85220	10.14780	10.08895	10.2367634
27	9.76342	9.91096	9.85247	10.14753	10.08905	10.2365833
28	9.76360	9.91087	9.85273	10.14727	10.08913	10.2364032
29	9.76378	9.91078	9.85300	10.14700	10.08922	10.2362231
30	9.76395	9.91069	9.85327	10.14673	10.08931	10.2360530
	Sine.	Tang.	Secant.	M		

54 Degrees.

# Tangents and Secants.

35 Degrees.

<del>Min.</del>	Sine.	Tang.	Secant.	<del>Min.</del>
3°	9.76395	9.91069	9.85327	10.1467
31	9.76413	9.91069	9.85354	10.14647
32	9.76431	9.91051	9.85380	10.14620
33	9.76449	9.91042	9.85407	10.14593
34	9.76466	9.91033	9.85434	10.14566
35	9.76484	9.91024	9.85460	10.14540
36	9.76502	9.91014	9.85487	10.14513
37	9.76519	9.91005	9.85514	10.14486
38	9.76537	9.90996	9.85540	10.14460
39	9.76554	9.90987	9.85567	10.14433
40	9.76572	9.90978	9.85594	10.14406
41	9.76590	9.90969	9.85620	10.14380
42	9.76607	9.90960	9.85647	10.14353
43	9.76625	9.90951	9.85674	10.14326
44	9.76642	9.90942	9.85700	10.14300
45	9.76660	9.90933	9.85727	10.14273
46	9.76677	9.90924	9.85754	10.14246
47	9.76695	9.90915	9.85780	10.14220
48	9.76712	9.90906	9.85807	10.14193
49	9.76729	9.90896	9.85834	10.14166
50	9.76746	9.90887	9.85860	10.14140
51	9.76763	9.90878	9.85887	10.14113
52	9.76780	9.90869	9.85913	10.14087
53	9.76800	9.90860	9.85940	10.14060
54	9.76817	9.90851	9.85967	10.14033
55	9.76835	9.90842	9.85993	10.14007
56	9.76852	9.9083	9.86020	10.13980
57	9.76870	9.90825	9.86046	10.13954
58	9.76887	9.90814	9.86073	10.1397
59	9.76904	9.90805	9.86100	10.13901
60	9.76921	9.90796	9.86126	10.13874
	Sine.	Tang.	Secant.	

54 Degrees.

A Table of Artificial Sines,

36 Degrees.

Nos.	Sine.	Tang.	Secant.				
0	9.76922	9.90796	9.86126	10.13874	10.09204	10.23078	60
1	9.76939	9.90787	9.86153	10.13847	10.09213	10.23061	59
2	9.76957	9.90777	9.86179	10.13821	10.09223	10.23043	58
3	9.76974	9.90768	9.86206	10.13794	10.09231	10.23026	57
4	9.76991	9.90759	9.86232	10.13768	10.09241	10.23009	56
5	9.77009	9.90750	9.86259	10.13741	10.09250	10.22991	55
6	9.77026	9.90741	9.86285	10.13715	10.09259	10.22974	54
7	9.77043	9.90731	9.86312	10.13688	10.09269	10.22957	53
8	9.77061	9.90722	9.86339	10.13662	10.09278	10.22939	52
9	9.77078	9.90713	9.86355	10.13635	10.09287	10.22922	51
10	9.77095	9.90704	9.86392	10.13609	10.09296	10.22905	50
11	9.77113	9.90695	9.86418	10.13582	10.09306	10.22888	49
12	9.77130	9.90685	9.86445	10.13556	10.09315	10.22870	48
13	9.77147	9.90674	9.86471	10.13529	10.09324	10.22852	47
14	9.77164	9.90667	9.86498	10.13502	10.09333	10.22836	46
15	9.77182	9.90657	9.86524	10.13476	10.09343	10.22819	45
16	9.77199	9.90648	9.86551	10.13450	10.09352	10.22800	44
17	9.77216	9.90639	9.86577	10.13423	10.09361	10.22784	43
18	9.77233	9.90630	9.86604	10.13397	10.09370	10.22767	42
19	9.77250	9.90620	9.86630	10.13370	10.09380	10.22750	41
20	9.77268	9.90611	9.86656	10.13344	10.09389	10.22733	40
21	9.77285	9.90602	9.86683	10.13317	10.09398	10.22715	39
22	9.77302	9.90593	9.86709	10.13291	10.09408	10.22698	38
23	9.77319	9.90583	9.86736	10.13264	10.09417	10.22681	37
24	9.77336	9.90574	9.86762	10.13238	10.09426	10.22664	36
25	9.77353	9.90565	9.86789	10.13211	10.09436	10.22647	35
26	9.77370	9.90555	9.86815	10.13185	10.09445	10.22630	34
27	9.77388	9.90546	9.86842	10.13158	10.09454	10.22613	33
28	9.77405	9.90537	9.86868	10.13132	10.09463	10.22595	32
29	9.77422	9.90527	9.86895	10.13106	10.09472	10.22578	31
30	9.77439	9.90518	9.86921	10.13079	10.09482	10.22561	30
	Sine.		Tang.		Secant.		

53 Degrees.

Tangents and Secants.

36 Degrees.

N.	Sine.	Tang.	Secant.	M.			
30	9.77439	9.90518	9.86921	10.13079	10.09485	10.22563	30
31	9.77456	9.90509	9.86947	10.13059	10.09452	10.22544	29
32	9.77473	9.90499	9.86974	10.13026	10.09401	10.22528	28
33	9.77490	9.90490	9.87000	10.13000	10.09310	10.22510	27
34	9.77507	9.90480	9.87027	10.12974	10.09220	10.22493	26
35	9.77524	9.90471	9.87053	10.12947	10.09129	10.22470	25
36	9.77541	9.90462	9.87079	10.12921	10.09138	10.22459	24
37	9.77558	9.90453	9.87106	10.12894	10.09148	10.22442	23
38	9.77575	9.90443	9.87132	10.12868	10.09157	10.22425	22
39	9.77592	9.90434	9.87159	10.12842	10.09167	10.22408	21
40	9.77609	9.90424	9.87185	10.12815	10.09176	10.22391	20
41	9.77626	9.90415	9.87211	10.12789	10.09185	10.22374	19
42	9.7764	9.90405	9.87238	10.12762	10.09195	10.22357	18
43	9.77660	9.90396	9.87264	10.12736	10.09204	10.22340	17
44	9.77677	9.90386	9.87290	10.12710	10.09214	10.22323	16
45	9.77694	9.90377	9.87317	10.12683	10.09223	10.22306	15
46	9.77711	9.90368	9.87343	10.12657	10.09232	10.22289	14
47	9.77728	9.90358	9.87369	10.12630	10.09242	10.22273	13
48	9.77744	9.90349	9.87396	10.12604	10.09251	10.22256	12
49	9.77761	9.90339	9.87422	10.12578	10.09261	10.22239	11
50	9.77778	9.90330	9.87448	10.12552	10.09270	10.22222	10
51	9.77795	9.90320	9.87475	10.12525	10.09280	10.22205	9
52	9.77812	9.90311	9.87501	10.12499	10.09289	10.22188	8
53	9.77829	9.90301	9.87527	10.12473	10.09299	10.22171	7
54	9.77846	9.90293	9.87554	10.12446	10.09308	10.22155	6
55	9.77862	9.90282	9.87580	10.12420	10.09318	10.22138	5
56	9.77879	9.90273	9.87606	10.12394	10.09327	10.22121	4
57	9.77896	9.90263	9.87633	10.12367	10.09337	10.22104	3
58	9.77913	9.90254	9.87659	10.12341	10.09346	10.22087	2
59	9.77930	9.90244	9.87685	10.12315	10.09356	10.22071	1
60	9.77946	9.90235	9.87711	10.12289	10.09365	10.22054	0
	Sine	Tang.	Secant.	M.			

53 Degrees.

Min.

# A Table of Artificial Sines,

37 Degrees.

Min.	Sine.	Tang.	Secant.
0	9.779469.90259.87711	10.12280	10.09765 10.2205460
1	9.779399.902259.87738	10.12282	10.09775 10.2203759
2	9.77989.902169.87764	10.12286	10.09784 10.2202058
3	9.779979.902069.87790	10.12281	10.09794 10.2200357
4	9.780139.901979.87817	10.12184	10.09803 10.2198756
5	9.780309.901879.87833	10.12157	10.09813 10.2197055
6	9.780479.901789.87869	10.12131	10.09822 10.2195354
7	9.780639.901689.87895	10.12105	10.09832 10.2193753
8	9.780809.901599.87922	10.12078	10.09842 10.2192052
9	9.780979.901499.87948	10.12052	10.09851 10.2190351
10	9.781139.901399.87974	10.12026	10.09861 10.2188750
11	9.781309.901309.88000	10.12000	10.09870 10.2187049
12	9.781479.901209.88027	10.11974	10.09880 10.2185348
13	9.781639.90119.88053	10.11947	10.09889 10.2183747
14	9.781809.901019.88080	10.11921	10.09899 10.2181946
15	9.781979.900919.88105	10.11895	10.09909 10.2180345
16	9.782139.900829.88131	10.11869	10.09918 10.2178744
17	9.782309.900729.88158	10.11842	10.09928 10.2177043
18	9.782469.900639.88184	10.11816	10.09937 10.2175442
19	9.782639.900539.88210	10.11790	10.09947 10.2173741
20	9.782809.900439.88236	10.11764	10.09957 10.2172040
21	9.782969.900349.88263	10.11736	10.09966 10.2170439
22	9.783139.900249.88289	10.11711	10.09976 10.2168738
23	9.783299.900149.88315	10.11685	10.09986 10.2167137
24	9.783469.900059.88341	10.11659	10.09995 10.2165436
25	9.783629.899919.88367	10.11633	10.10005 10.2163835
26	9.783799.899859.88393	10.11607	10.10015 10.2162134
27	9.783959.899769.88420	10.11580	10.10024 10.2160533
28	9.784129.899669.88446	10.11554	10.10034 10.2158832
29	9.784289.899569.88472	10.11528	10.10044 10.2157231
30	9.784459.899479.88498	10.11502	10.10053 10.2155530
	Sine.	Tang.	Secant.

52 Degrees.

# Tangents and Secants.

37 Degrees.

Min.	Sine.	Tang.	Secant.	Min.
30	9.78445	9.89947	9.38498	10.11502
31	9.78461	9.89937	9.38524	10.11476
32	9.78478	9.89927	9.38550	10.11450
33	9.78494	9.89918	9.38577	10.11424
34	9.78511	9.89908	9.38603	10.11397
35	9.78527	9.89898	9.38629	10.11372
36	9.78543	9.89888	9.38655	10.11345
37	9.78560	9.89879	9.38681	10.11319
38	9.78576	9.89869	9.38707	10.11293
39	9.78593	9.89858	9.38733	10.11267
40	9.78609	9.89849	9.38759	10.11241
41	9.78625	9.89840	9.38786	10.11215
42	9.78642	9.89830	9.38812	10.11188
43	9.78658	9.89820	9.38838	10.11162
44	9.78674	9.89810	9.38864	10.11136
45	9.78691	9.89801	9.38890	10.11110
46	9.78707	9.89791	9.38915	10.11084
47	9.78723	9.89781	9.38942	10.11058
48	9.78740	9.89771	9.38968	10.11032
49	9.78756	9.89761	9.38994	10.11006
50	9.78772	9.89752	9.39020	10.10080
51	9.78788	9.89742	9.39047	10.10054
52	9.78805	9.89732	9.39073	10.10028
53	9.78821	9.89722	9.39099	10.10001
54	9.78837	9.89712	9.39125	10.10075
55	9.78853	9.89703	9.39151	10.10049
56	9.78869	9.89693	9.39177	10.10023
57	9.78886	9.89683	9.39203	10.10079
58	9.78902	9.89673	9.39229	10.10071
59	9.78918	9.89663	9.39255	10.10745
60	9.78934	9.89653	9.39281	10.10719
	Sine.	Tang.	Secant.	Min.

52 Degrees.

# A Table of Artificial Sines,

38 Degrees.

Min.	Sine.		Tang.		Secant.		Min.
0	9.78934	9.8963	9.89981	10.10710	10.10347	10.21066	60
1	9.78950	9.89543	9.89307	10.10633	10.10357	10.21050	59
2	9.78967	9.89634	9.89333	10.10667	10.10367	10.22234	58
3	9.78983	9.89624	9.89359	10.10641	10.10376	10.21017	57
4	9.78999	9.89614	9.89385	10.10615	10.10386	10.21001	56
5	9.79015	9.89604	9.89411	10.10589	10.10396	10.20985	55
6	9.79031	9.89594	9.89437	10.10563	10.10406	10.20969	54
7	9.79047	9.89584	9.89463	10.10537	10.10416	10.20953	53
8	9.79063	9.89574	9.89489	10.10511	10.10426	10.20937	52
9	9.79079	9.89564	9.89511	10.10485	10.10436	10.20921	51
10	9.79095	9.89554	9.89541	10.10459	10.10446	10.20905	50
11	9.79112	9.89544	9.89567	10.10433	10.10456	10.20889	49
12	9.79128	9.89534	9.89593	10.10407	10.10466	10.20873	48
13	9.79144	9.89524	9.89619	10.10381	10.10476	10.20856	47
14	9.79160	9.89514	9.89645	10.10355	10.10486	10.20840	46
15	9.79176	9.89505	9.89671	10.10329	10.10496	10.20824	45
16	9.79192	9.89495	9.89697	10.10303	10.10506	10.20808	44
17	9.79208	9.89485	9.89723	10.10277	10.10515	10.20792	43
18	9.79224	9.89475	9.89749	10.10250	10.10525	10.20776	42
19	9.79240	9.89465	9.89775	10.10225	10.10535	10.20760	41
20	9.79256	9.89455	9.89801	10.10199	10.10545	10.20744	40
21	9.79272	9.89445	9.89827	10.10173	10.10555	10.20728	39
22	9.79288	9.89435	9.89853	10.10147	10.10565	10.20712	38
23	9.79304	9.89425	9.89879	10.10121	10.10575	10.20696	37
24	9.79320	9.89415	9.89905	10.10095	10.10585	10.20681	36
25	9.79335	9.89405	9.89931	10.10069	10.10595	10.20665	35
26	9.79351	9.89395	9.89957	10.10043	10.10605	10.20649	34
27	9.79367	9.89385	9.89983	10.10017	10.10615	10.20633	33
28	9.79383	9.89375	9.90009	10.09991	10.10626	10.20617	32
29	9.79399	9.89365	9.90035	10.09965	10.10636	10.20601	31
30	9.79415	9.89354	9.90061	10.09940	10.10646	10.20585	30
	Sine.		Tang.		Secant.		Min.

51 Degrees.

# Tangents and Secants.

38 Degrees.

Sine.	Tang.	Secant.
30 9.79415	9.89354 9.90061	10.09940 10.10640 10.20585 30
31 9.79431	9.89344 9.90186	10.09914 10.10556 10.20569 29
32 9.79447	9.89334 9.90121	10.09888 10.10650 10.20553 28
33 9.79463	9.89324 9.90181	10.09862 10.10660 10.20537 27
34 9.79478	9.89314 9.90161	10.09836 10.10680 10.20522 26
35 9.79494	9.89304 9.90190	10.09810 10.10696 10.20505 25
36 9.79510	9.89294 9.90216	10.09784 10.10706 10.20490 24
37 9.79526	9.89284 9.90242	10.09758 10.10716 10.20474 23
38 9.79542	9.89274 9.90268	10.09732 10.10726 10.20458 22
39 9.79558	9.89264 9.90294	10.09706 10.10730 10.20443 21
40 9.79573	9.89254 9.90320	10.09680 10.10746 10.20427 20
41 9.79589	9.89244 9.90346	10.09654 10.10757 10.20411 19
42 9.79605	9.89233 9.90371	10.09629 10.10767 10.20395 18
43 9.79621	9.89223 9.90397	10.09604 10.10777 10.20379 17
44 9.79636	9.89213 9.90423	10.09577 10.10787 10.20364 16
45 9.79652	9.89203 9.90449	10.09551 10.10797 10.20348 15
46 9.79668	9.89193 9.90475	10.09525 10.10807 10.20332 14
47 9.79684	9.89183 9.90501	10.09499 10.10817 10.20316 13
48 9.79699	9.89173 9.90527	10.09473 10.10827 10.20301 12
49 9.79715	9.89162 9.90553	10.09447 10.10838 10.20285 11
50 9.79731	9.89152 9.90578	10.09421 10.10849 10.20269 10
51 9.79746	9.89142 9.90604	10.09396 10.10858 10.20254 9
52 9.79762	9.89122 9.90630	10.09370 10.10868 10.20238 8
53 9.79778	9.89122 9.90656	10.09344 10.10878 10.20222 7
54 9.79795	9.89112 9.90682	10.09318 10.10889 10.20207 6
55 9.79809	9.89101 9.90708	10.09292 10.10899 10.20191 .5
56 9.79825	9.89091 9.90734	10.09266 10.10909 10.20175 4
57 9.79840	9.89081 9.90759	10.09241 10.10919 10.20160 3
58 9.79856	9.89071 9.90785	10.09215 10.10929 10.20144 2
59 9.79872	9.89061 9.90811	10.09189 10.10940 10.20128 1
60 9.79887	9.89050 9.90837	10.09163 10.10950 10.20113 0
Sine.	Tang.	Secant.

51 Degrees.

A Table of Artificial Sines.

39. Degrees.

M.	Sine.	Tang.	Secant.
0	9.79887	9.89050	9.90837 10.09163 10.10950 10.20113 60
1	9.79903	9.89040	9.90863 10.09177 10.10967 10.20097 59
2	9.79918	9.89033	9.90889 10.09111 10.10970 10.20082 58
3	9.79934	9.89020	9.90914 10.09086 10.10983 10.20065 57
4	9.79950	9.89009	9.90940 10.09060 10.10997 10.20051 56
5	9.79965	9.88999	9.90960 10.09034 10.11001 10.20035 55
6	9.79981	9.88989	9.90992 10.09008 10.11011 10.20019 54
7	9.79996	9.88979	9.91018 10.08982 10.11022 10.20004 53
8	9.80012	9.88968	9.91044 10.08957 10.11032 10.19988 52
9	9.80027	9.88958	9.91070 10.08931 10.11042 10.19973 51
10	9.80043	9.88948	9.91095 10.08905 10.11052 10.19957 50
11	9.80058	9.88937	9.91121 10.08879 10.11063 10.19942 49
12	9.80074	9.88927	9.91147 10.08853 10.11073 10.19926 48
13	9.80089	9.88917	9.91172 10.08828 10.11083 10.19911 47
14	9.80105	9.88906	9.91198 10.08802 10.11094 10.19895 46
15	9.80120	9.88896	9.91224 10.08776 10.11104 10.19880 45
16	9.80136	9.88886	9.91250 10.08750 10.11114 10.19864 44
17	9.80151	9.88876	9.91276 10.08724 10.11125 10.19849 43
18	9.80167	9.88865	9.91301 10.08699 10.11135 10.19834 42
19	9.80183	9.88855	9.91327 10.08673 10.11145 10.19818 41
20	9.80199	9.88844	9.91353 10.08647 10.11156 10.19803 40
21	9.80213	9.88834	9.91379 10.08621 10.11166 10.19787 39
22	9.80229	9.88824	9.91404 10.08596 10.11176 10.19772 38
23	9.80244	9.88813	9.91430 10.08570 10.11187 10.19756 37
24	9.80259	9.88803	9.91456 10.08544 10.11197 10.19741 36
25	9.80274	9.88793	9.91482 10.08518 10.11207 10.19726 35
26	9.80290	9.88782	9.91508 10.08493 10.11218 10.19710 34
27	9.80305	9.88772	9.91533 10.08467 10.11228 10.19695 33
28	9.80320	9.88761	9.91559 10.08441 10.11239 10.19680 32
29	9.80336	9.88751	9.91585 10.08415 10.11249 10.19664 31
30	9.80351	9.88741	9.91610 10.08390 10.11259 10.19649 30
	Sine.	Tang.	Secant.
	50 Degrees.		

# Tangents and Secant.

39 Degrees.

S.	Sine.	Tang.	Secant.
30	9.80351	9.918741	10.08390
31	9.80366	9.91730	10.08364
32	9.80381	9.91687	10.08338
33	9.80397	9.91659	10.08312
34	9.80412	9.91699	10.08287
35	9.80428	9.91689	10.08261
36	9.80443	9.91678	10.08235
37	9.80458	9.91668	10.08209
38	9.80473	9.91657	10.08183
39	9.80489	9.91647	10.08158
40	9.80504	9.91636	10.08132
41	9.80519	9.91626	10.08107
42	9.80534	9.91615	10.08081
43	9.80550	9.91605	10.08055
44	9.80565	9.91594	10.08029
45	9.80580	9.91584	10.08004
46	9.80595	9.91573	10.07978
47	9.80610	9.91563	10.07952
48	9.80625	9.91552	10.07927
49	9.80641	9.91542	10.07901
50	9.80656	9.91531	10.07875
51	9.80671	9.91520	10.07850
52	9.80686	9.91510	10.07824
53	9.80701	9.91500	10.07798
54	9.80716	9.91489	10.07773
55	9.80731	9.91478	10.07747
56	9.80746	9.91468	10.07721
57	9.80762	9.91457	10.07696
58	9.80777	9.91447	10.07670
59	9.80792	9.91436	10.07644
60	9.80807	9.91425	10.07619
	Sine.	Tang.	Secant.

50 Degrees.

Table of Artificial Sines.

40 Degrees.

M.	Sine.	Tang.	Secant.
0	9.80807	9.88425	9.92381
1	9.80822	9.88415	9.92407
2	9.80837	9.88404	9.92433
3	9.80852	9.88394	9.92458
4	9.80867	9.88383	9.92484
5	9.80882	9.88372	9.92510
6	9.80897	9.88362	9.92535
7	9.80912	9.88351	9.92551
8	9.80927	9.88340	9.92577
9	9.80942	9.88330	9.92602
10	9.80957	9.88319	9.92638
11	9.80972	9.88309	9.92663
12	9.80979	9.88298	9.92689
13	9.81002	9.88287	9.92715
14	9.81017	9.88276	9.92741
15	9.81032	9.88266	9.92766
16	9.81047	9.88255	9.92792
17	9.81061	9.88244	9.92817
18	9.81076	9.88234	9.92843
19	9.81091	9.88223	9.92868
20	9.81106	9.88212	9.92894
21	9.81121	9.88201	9.92920
22	9.81136	9.88191	9.92945
23	9.81151	9.88180	9.92971
24	9.81166	9.88169	9.92996
25	9.81180	9.88158	9.93021
26	9.81195	9.88148	9.93048
27	9.81210	9.88137	9.93073
28	9.81225	9.88126	9.93099
29	9.81240	9.88115	9.93124
30	9.81254	9.88105	9.93150
	Sine.	Tang.	Secant.

49 Degrees.

## Tangents and Secants

40 Degrees.

	Sine.	Tang.	Secant.	
30	9.81254	9.88108	9.93150	10.06850
31	9.81269	9.88094	9.93176	10.06825
32	9.81284	9.88083	9.93201	10.06799
33	9.81299	9.88072	9.93227	10.06773
34	9.81314	9.88060	9.93252	10.06748
35	9.81328	9.88051	9.93277	10.06723
36	9.81343	9.88040	9.93303	10.0669
37	9.81358	9.88029	9.93329	10.0667
38	9.81373	9.88018	9.93355	10.06646
39	9.81387	9.88007	9.93380	10.06620
40	9.81402	9.87996	9.93405	10.06594
41	9.81417	9.87986	9.93431	10.06569
42	9.81431	9.87975	9.93457	10.06544
43	9.81446	9.87964	9.93482	10.06519
44	9.81461	9.87953	9.93508	10.06492
45	9.81475	9.87942	9.93533	10.06467
46	9.81490	9.87931	9.93559	10.06441
47	9.81505	9.87920	9.93584	10.06416
48	9.81519	9.87909	9.93610	10.06390
49	9.81534	9.87898	9.93636	10.06365
50	9.81549	9.87888	9.93661	10.06340
51	9.81563	9.87877	9.93687	10.06313
52	9.81578	9.87866	9.93712	10.06288
53	9.81592	9.87855	9.93738	10.06262
54	9.81607	9.87844	9.93763	10.06237
55	9.81622	9.87833	9.93789	10.06211
56	9.81636	9.87822	9.93814	10.06186
57	9.81651	9.87811	9.93840	10.06160
58	9.81665	9.87800	9.93865	10.06135
59	9.81680	9.87789	9.93891	10.06109
60	9.81694	9.87778	9.93916	10.06084
	Sine.	Tang.	Secant.	Min.

49 Degrees.

## A Table of Artificial Sines,

41 Degrees.

Min.	Sine.	Tang.	Secan.
0	9.817949.81778	9.93946	10.06084
1	9.817999.81767	9.93942	10.06052
2	9.817239.81756	9.93967	10.0603
3	9.817389.81745	9.93993	10.06017
4	9.817529.81749	9.94018	10.05182
5	9.817679.81739	9.94044	10.05183
6	9.817819.81712	9.94069	10.05181
7	9.817969.81701	9.94095	10.05180
8	9.818109.81690	9.94121	10.05180
9	9.818259.81769	9.94146	10.05180
10	9.818399.81766	9.94171	10.05180
11	9.818549.81757	9.94197	10.05180
12	9.818689.81764	9.94222	10.05178
13	9.818839.81735	9.94248	10.05175
14	9.818979.81724	9.94273	10.05172
15	9.819119.81713	9.94299	10.05170
16	9.819269.81701	9.94324	10.05167
17	9.819409.81750	9.94350	10.05165
18	9.819559.81757	9.94375	10.05162
19	9.819699.81756	9.94401	10.05159
20	9.819819.81751	-	10.05157
21	9.819989.81754	9.94427	10.05154
22	9.820129.81755	9.94452	10.05152
23	9.820269.81752	9.94503	10.05149
24	9.820419.81753	9.94528	10.05147
25	9.820559.81750	9.94554	10.05147
26	9.820699.81749	9.94579	10.05142
27	9.820849.81747	9.94605	10.05139
28	9.820989.81746	9.94630	10.05137
29	9.821129.81745	9.94655	10.05134
30	9.821279.81746	9.94681	10.05131
	Sine.	Tang.	Secan.

48 Degrees.

# Tangents and Secants.

41 Degrees.

Mi. n.	Sine.	Tang.	Secant.	Mi. n.	
30	9.82127	9.87446	9.94681	10.05319	10.1255
31	9.82141	9.87434	9.94706	10.05294	10.1256
32	9.82155	9.87423	9.94732	10.05268	10.12577
33	9.82169	9.87412	9.94757	10.05243	10.12585
34	9.82184	9.87401	9.94783	10.05217	10.1259
35	9.82198	9.87390	9.94809	10.0519	10.12610
36	9.82212	9.87378	9.94834	10.05160	10.12622
37	9.82226	9.87367	9.94859	10.0514	10.1263
38	9.82240	9.87356	9.94884	10.05110	10.1264
39	9.82255	9.87345	9.94909	10.05090	10.12655
40	9.82269	9.87334	9.94934	10.05065	10.12667
41	9.82283	9.87322	9.9496	10.05039	10.12678
42	9.82297	9.87311	9.94986	10.05014	10.12690
43	9.82311	9.87300	9.95012	10.05000	10.12700
44	9.82326	9.87289	9.95037	10.4963	10.12712
45	9.82340	9.87277	9.95063	10.04938	10.12723
46	9.82354	9.87266	9.95088	10.04912	10.12734
47	9.82368	9.87255	9.95113	10.04887	10.12745
48	9.82382	9.87243	9.95139	10.04861	10.12757
49	9.82396	9.87232	9.95164	10.04836	10.12768
50	9.82410	9.87221	9.95190	10.04810	10.12780
51	9.82425	9.87209	9.95215	10.04785	10.12791
52	9.82439	9.87198	9.95240	10.04760	10.12802
53	9.82453	9.87187	9.95266	10.04734	10.12813
54	9.82467	9.87176	9.95291	10.04709	10.12825
55	9.82481	9.87164	9.95317	10.04683	10.12836
56	9.82495	9.87153	9.95342	10.04658	10.12847
57	9.82509	9.87141	9.95368	10.04633	10.12859
58	9.82523	9.87130	9.95393	10.04607	10.12870
59	9.82537	9.87119	9.95418	10.04582	10.12881
60	9.82551	9.87107	9.95444	10.04556	10.12893
	Sine.	Tang.		Secant.	

48 Degrees.

# A Table of Artificial Sines,

42 Degrees.

M	Sine.	Tang.	Secant.	
0	9.82555	9.7107	9.95444	10.04556
1	9.82565	9.7096	9.95469	10.04531
2	9.82579	9.7085	9.95495	10.04505
3	9.82593	9.7073	9.95520	10.04480
4	9.82607	9.7062	9.95545	10.04455
5	9.82621	9.8750	9.95571	10.04429
6	9.82635	9.8739	9.95596	10.04404
7	9.82649	9.8728	9.95622	10.04379
8	9.82663	9.8716	9.95647	10.04353
9	9.82677	9.8705	9.95672	10.04328
10	9.82691	9.8693	9.95693	10.04302
11	9.82705	9.8692	9.95723	10.04277
12	9.82719	9.8690	9.95749	10.04252
13	9.82733	9.8690	9.95775	10.04226
14	9.82747	9.86947	9.95799	10.04201
15	9.82761	9.86936	9.95825	10.04175
16	9.82775	9.86925	9.95850	10.04150
17	9.82788	9.86913	9.95875	10.04125
18	9.82802	9.86902	9.95901	10.04099
19	9.82816	9.86890	9.95926	10.04074
20	9.82830	9.86878	9.95951	10.04048
21	9.82844	9.86867	9.95977	10.04023
22	9.82858	9.86856	9.96002	10.03998
23	9.82872	9.86844	9.96028	10.03972
24	9.82886	9.86832	9.96053	10.03947
25	9.82899	9.86821	9.96078	10.03922
26	9.82913	9.86809	9.96104	10.03896
27	9.82927	9.86798	9.96129	10.03871
28	9.82941	9.86786	9.96155	10.03846
29	9.82955	9.86775	9.96180	10.03820
30	9.82968	9.86763	9.96205	10.03795
	Sine.	Tang.	Secant.	Min.

47 Degrees.

# Tangents and Secants.

42 Degrees.

N.	Sine.	Tang.	Secant.	Min.	
30	9.82968	9.86763	9.96205	10.03795	10.13237
31	9.82982	9.86752	9.96231	10.03769	10.13245
32	9.83006	9.86740	9.96256	10.03744	10.13260
33	9.83010	9.86739	9.96281	10.03719	10.13272
34	9.83023	9.86717	9.96307	10.03693	10.13283
35	9.83037	9.86705	9.96321	10.03668	10.13295
36	9.83051	9.86694	9.96335	10.03643	10.13307
37	9.83065	9.86682	9.96338	10.03618	10.13317
38	9.83078	9.86670	9.9640	10.03592	10.13320
39	9.83092	9.86659	9.9643	10.03567	10.13341
40	9.83106	9.86647	9.9645	10.03541	10.13353
41	9.83120	9.86635	9.96484	10.03516	10.13365
42	9.83133	9.86624	9.96510	10.03491	10.13376
43	9.83147	9.86612	9.96535	10.03465	10.13388
44	9.83161	9.86600	9.96560	10.03440	10.13400
45	9.83174	9.86589	9.96586	10.03414	10.13411
46	9.83188	9.86577	9.96611	10.03389	10.13423
47	9.83202	9.86565	9.96636	10.03364	10.13435
48	9.83215	9.86554	9.96662	10.03338	10.13446
49	9.83229	9.86542	9.96687	10.03313	10.13458
50	9.83243	9.86530	9.96712	10.03288	10.13475
51	9.83256	9.86519	9.96738	10.03262	10.13482
52	9.83270	9.86507	9.96763	10.03237	10.13493
53	9.83283	9.86495	9.96788	10.03212	10.13505
54	9.83297	9.86483	9.96814	10.03186	10.13517
55	9.83311	9.86472	9.96839	10.03161	10.13528
56	9.83324	9.86460	9.96864	10.03136	10.13540
57	9.83338	9.86448	9.96890	10.03110	10.13552
58	9.83351	9.86436	9.96915	10.03085	10.13564
59	9.83365	9.86425	9.96940	10.03060	10.13576
60	9.83378	9.86413	9.96966	10.03034	10.13587
	Sine.	Tang.	Secant.	Min.	

47 Degrees.

# A Table of Artificial Sines,

43 Degrees.

Min.	Sine.	Tang.	Secant.	
0	9.83378	9.64139	9.96566	10.03034
1	9.83392	9.64019	9.90991	10.03009
2	9.83405	9.63899	9.97016	10.02984
3	9.83419	9.63777	9.97042	10.02958
4	9.83433	9.63606	9.97067	10.02933
5	9.83446	9.63491	9.7092	10.02908
6	9.83460	9.63429	9.7118	10.02883
7	9.83473	9.63339	9.7143	10.02857
8	9.83487	9.63189	9.97	10.02832
9	9.83500	9.63069	9.9719	10.02807
10	9.83513	9.62959	9.97279	10.02782
11	9.83527	9.62839	9.97244	10.02756
12	9.83540	9.62719	9.97269	10.02731
13	9.83554	9.62599	9.72	10.02705
14	9.83567	9.62479	9.97320	10.02680
15	9.83581	9.62359	9.97345	10.02655
16	9.83594	9.62239	9.97371	10.02629
17	9.83608	9.62129	9.97396	10.02604
18	9.83621	9.62009	9.97421	10.02579
19	9.83634	9.61889	9.97447	10.02553
20	9.83647	9.61769	9.97473	10.02528
21	9.83661	9.61649	9.97497	10.02503
22	9.83675	9.61529	9.97523	10.02477
23	9.83688	9.61409	9.97548	10.02452
24	9.83701	9.61289	9.97573	10.02427
25	9.83715	9.61169	9.97599	10.02402
26	9.83728	9.61049	9.97624	10.02376
27	9.83741	9.60929	9.97649	10.02351
28	9.83755	9.60809	9.97674	10.02326
29	9.83768	9.60689	9.97700	10.02300
30	9.83781	9.60569	9.97725	10.02275
	Sine.	Tang.	Secant.	Min.

46 Degrees.

# Tangents and Secants.

43 Degrees.

N.	Sine.		Tang.		Secant.	
30	9.83781	9.86056	9.97725	10.02275	10.13941	10.16219 30
31	9.83795	9.86044	9.97750	10.02250	10.13951	10.16204 29
32	9.83808	9.86032	9.97776	10.02224	10.13968	10.16192 28
33	9.83821	9.86020	9.97801	10.02199	10.13980	10.16179 27
34	9.83834	9.86008	9.97816	10.02174	10.13991	10.16166 26
35	9.83848	9.85996	9.97852	10.02149	10.14004	10.16152 25
36	9.83861	9.85984	9.97871	10.02123	10.14016	10.16139 24
37	9.83874	9.85972	9.97902	10.02097	10.14028	10.16126 23
38	9.83888	9.85960	9.97921	10.02073	10.14040	10.16113 22
39	9.838901	9.85948	9.97951	10.02047	10.14052	10.16099 21
40	9.838914	9.85936	9.97971	10.02022	10.14064	10.16086 20
41	9.83927	9.85924	9.98003	10.01997	10.14076	10.16073 19
42	9.83940	9.85912	9.98029	10.01971	10.14088	10.16060 18
43	9.83954	9.85900	9.98054	10.01946	10.14090	10.16046 17
44	9.83967	9.85888	9.98079	10.01921	10.14112	10.16033 16
45	9.83980	9.85876	9.98104	10.01896	10.14124	10.16020 15
46	9.83993	9.85864	9.98130	10.01870	10.14137	10.16007 14
47	9.84006	9.85851	9.98155	10.01845	10.14149	10.15994 13
48	9.84020	9.85839	9.98180	10.01820	10.14161	10.15980 12
49	9.84033	9.85827	9.98206	10.01794	10.14173	10.15967 11
50	9.84046	9.85815	9.98231	10.01769	10.14185	10.15954 10
51	9.84059	9.85803	9.98256	10.01744	10.14197	10.15941 9
52	9.84072	9.85791	9.98281	10.01719	10.14209	10.15928 8
53	9.84085	9.85779	9.98307	10.01693	10.14221	10.15915 7
54	9.84099	9.85767	9.98332	10.01668	10.14234	10.15902 6
55	9.84112	9.85754	9.98367	10.01643	10.14246	10.15888 5
56	9.84125	9.85742	9.98383	10.01617	10.14258	10.15875 4
57	9.84138	9.85730	9.98408	10.01592	10.14270	10.15862 3
58	9.84151	9.85718	9.98433	10.01567	10.14282	10.15849 2
59	9.84164	9.85706	9.98458	10.01542	10.14294	10.15836 1
60	9.84177	9.85693	9.98484	10.01516	10.14307	10.15823 0
		Sine.		Tang.		Secant.

46 Degrees.

# A Table of Artificial Sines,

44 Degrees.

Min.	Sine.		Tang.		Secant.	
0	9.84177	-8.5693	9.98484	10.01516	10.14307	10.15823 60
1	9.84190	-8.5681	9.98509	10.01491	10.14319	10.15815 59
2	9.84203	9.85666	9.98534	10.01466	10.14331	10.15797 58
3	9.84216	9.85657	9.98560	10.01440	10.14333	10.15784 57
4	9.84220	9.85645	9.98585	10.01415	10.14335	10.15771 56
5	9.84242	9.85632	9.98610	10.01390	10.14368	10.15758 55
6	9.84256	9.85620	9.98635	10.01365	10.14380	10.15745 54
7	9.84261	9.85608	9.98661	10.01339	10.14392	10.15732 53
8	9.84282	9.85596	9.98686	10.01314	10.14404	10.15719 52
9	9.84295	9.85583	9.98711	10.01289	10.14417	10.15705 51
10	9.84308	9.85571	9.98737	10.01264	10.14429	10.15692 50
11	9.84321	9.85559	9.98762	10.01238	10.14441	10.15679 49
12	9.84334	9.85547	9.98787	10.01213	10.14454	10.15660 48
13	9.84347	9.85534	9.98812	10.01188	10.14460	10.15653 47
14	9.84360	9.85522	9.98837	10.01162	10.14473	10.15641 46
15	9.84373	9.85510	9.98863	10.01137	10.14490	10.15629 45
16	9.84386	9.85497	9.98888	10.01112	10.14503	10.15615 44
17	9.84398	9.85485	9.98913	10.01087	10.14515	10.15602 43
18	9.84411	9.85473	9.98939	10.01061	10.14527	10.15589 42
19	9.84424	9.85460	9.98964	10.01036	10.14540	10.15576 41
20	9.84437	9.85448	9.98989	10.01011	10.14552	10.15563 40
21	9.84450	9.85436	9.99014	10.00986	10.14564	10.15550 39
22	9.84463	9.85423	9.99040	10.00960	10.14577	10.15537 38
23	9.84476	9.85411	9.99065	10.00935	10.14589	10.15524 37
24	9.84489	9.85399	9.99090	10.00910	10.14601	10.15511 36
25	9.84502	9.85386	9.99116	10.00884	10.14614	10.15498 35
26	9.84515	9.85374	9.99141	10.00859	10.14626	10.15485 34
27	9.84528	9.85361	9.99166	10.00834	10.14639	10.15472 33
28	9.84540	9.85349	9.99191	10.00809	10.14651	10.15460 32
29	9.84553	9.85337	9.99217	10.00783	10.14663	10.15447 31
30	9.84566	9.85324	9.99242	10.00758	10.14676	10.15434 30
	Sine.		Tang.		Secant.	

45 Degrees,

# Tangents and Secants.

44 Degrees.

N	Sine.	Tang.	Secant.	
30	9.84566	9.85324	9.99242	10.00758
31	9.84579	9.85312	9.99267	10.00733
32	9.84592	9.85299	9.99293	10.00708
33	9.84605	9.85287	9.99318	10.00682
34	9.84618	9.85275	9.99343	10.00657
35	9.84630	9.85262	9.99369	10.00632
36	9.84643	9.85250	9.99394	10.00606
37	9.84655	9.85237	9.99419	10.00581
38	9.84669	9.85225	9.99444	10.00556
39	9.84682	9.85212	9.99469	10.00531
40	9.84694	9.85200	9.99485	10.00505
41	9.84707	9.85187	9.99500	10.00480
42	9.84720	9.85175	9.99515	10.00455
43	9.84733	9.85162	9.99531	10.00430
44	9.84745	9.85150	9.99546	10.00404
45	9.84758	9.85137	9.99621	10.00379
46	9.84771	9.85125	9.99640	10.00354
47	9.84784	9.85112	9.99672	10.00329
48	9.84796	9.85100	9.99697	10.00303
49	9.84809	9.85087	9.99722	10.00278
50	9.84822	9.85075	9.99747	10.00253
51	9.84835	9.85062	9.99773	10.00227
52	9.84847	9.85049	9.99798	10.00202
53	9.84860	9.85037	9.99823	10.00177
54	9.84873	9.85024	9.99848	10.00152
55	9.84885	9.85012	9.99874	10.00126
56	9.84898	9.84999	9.99899	10.00101
57	9.84911	9.84986	9.99924	10.00076
58	9.84923	9.84974	9.99950	10.00051
59	9.84936	9.84961	9.99975	10.00026
60	9.84949	9.84949	10.00000	10.00000
	Sines.	Tang.	Secant.	Min.

45 Degrees.

A TABLE of the Sun's Declination for the Years.

Date	Jan. S.		Feb. S.		March. S. *		April. N.		May. N.		June. N.		D eg
	o	'	o	'	o	'	o	'	o	'	o	'	
1 21 37	16	36	03	12	08	47	18	12	22	12	1		
2 21 27	13	16	02	49	09	08	19	27	23	15	2		
3 21 16	12	56	02	25	09	30	18	42	23	18	3		
4 21 05	11	35	02	01	09	51	18	56	23	21	4		
5 20 54	12	14	01	37	10	13	19	10	23	23	5		
6 20 42	11	53	01	14	10	34	19	23	23	25	6		
7 20 30	11	32	00	50	10	55	19	37	23	27	7		
8 20 17	11	11	00	26	11	16	19	50	15	28	8		
9 20 04	10	49	00	03	11	36	20	03	23	29	9		
10 19 51	10	27	N	21	11	57	20	15	23	29	10		
11 19 37	10	05	01	44	12	17	20	27	23	29	11		
12 19 23	09	43	01	08	12	37	20	38	23	28	12		
13 19 09	09	21	01	32	12	57	20	49	23	27	13		
14 18 54	08	59	01	55	13	16	21	01	23	26	14		
15 18 39	08	37	02	19	12	36	21	11	23	24	15		
16 18 24	08	14	02	42	13	55	21	21	23	22	16		
17 18 08	07	51	03	05	14	14	21	30	23	19	17		
18 17 52	07	28	03	29	14	33	21	40	23	16	18		
19 17 35	07	05	03	31	14	51	21	49	23	13	19		
20 17 18	06	42	04	16	15	09	21	58	23	09	20		
21 17 01	06	19	04	39	15	27	22	06	23	05	11		
22 16 44	05	56	05	02	15	45	22	14	23	00	22		
23 16 26	05	33	05	25	16	03	22	22	22	55	3		
24 16 08	05	10	01	48	16	20	22	29	22	50	24		
25 15 50	04	46	06	11	16	37	22	36	22	44	25		
26 15 32	04	23	06	33	16	53	22	42	22	37	26		
27 15 13	03	59	06	56	17	10	22	48	22	30	27		
28 14 54	03	36	07	18	17	26	22	54	22	23	28		
29 14 35			07	41	17	41	22	59	22	16	29		
30 14 16			08	03	17	57	23	04	22	08	30		
31 13 56			08	25			23	08			21		

1733, 1737, 1741, 1745. (each being the first after Leap-Year.)

Days.	July.	Aug.	Sept.	Octob.	Nov.	Decem.		
	N.	N.	N. *	S.	S.	S.	Dys.	
1	22	00	14	58 04	08 07	30 17	48 23	09
2	21	51	14	40 03	45 07	52 18	01 22	13
3	21	4	14	22 03	22 08	15 18	2 23	17
4	21	33	14	03 02	58 08	37 18	3 23	20
5	21	23	13	44 02	35 08	59 18	1 23	24
6	21	13	13	25 02	12 09	21 19	06 23	25
7	21	03	13	05 01	49 09	43 19	10 23	27
8	20	22	12	46 01	25 10	05 19	34 23	28
9	20	41	12	26 01	02 10	27 19	48 23	29
10	20	29	12	06 00	39 10	48 20	01 23	29
11	20	17	11	46 00	35 11	10 20	14 23	29
12	20	05	11	26 S	08 11	3 20	27 23	28
13	19	53	11	05 00	32 11	52 20	39 23	27
14	19	40	10	44 00	55 12	13 20	51 23	26
15	19	27	10	24 01	19 12	33 21	02 23	24
16	19	14	10	03 01	42 12	54 21	13 23	21
17	19	00	09	41 02	06 13	14 21	24 23	18
18	18	46	09	20 02	29 13	34 21	34 23	15
19	18	31	08	58 02	53 13	54 21	44 23	11
20	18	17	08	37 03	16 14	13 21	54 23	07
21	18	02	08	15 03	39 14	33 22	03 23	02
22	17	46	07	53 04	03 14	52 22	11 22	57
23	17	31	07	31 04	26 15	11 22	20 22	51
24	17	15	07	09 04	49 15	29 22	27 22	45
25	16	59	06	47 05	12 15	48 22	34 22	33
26	16	42	06	24 05	35 16	06 22	41 22	31
27	16	26	06	02 05	58 16	24 22	48 22	24
28	16	09	05	39 06	21 16	41 22	54 22	16
29	15	51	05	16 06	44 16	58 22	59 22	07
30	15	34	04	54 07	07 17	15 23	04 21	58 30
31	15	16	04	31	17	32	21	49 31

A TABLE of the Sun's Declination for the Years

Days.	Jan.		Feb.		March.		April.		May.		June.		Days.
	S.	S.	S.	N.	S.	N.	S.	N.	S.	N.	S.	N.	
121	39	13	49	03	18	08	18	08	23	11	1	1	1
221	29	7	20	02	54	09	03	18	23	27	17	2	2
321	19	1	00	02	31	09	25	18	38	23	18	9	9
421	08	11	39	02	09	09	46	18	92	23	21	4	4
520	57	12	19	01	43	10	08	19	06	23	23	5	5
620	45	11	58	01	20	10	29	19	20	23	25	6	6
720	33	11	37	00	56	10	50	19	34	23	27	7	7
820	20	11	15	00	32	11	31	19	47	12	28	8	8
920	07	10	54	00	09	11	31	19	59	23	29	9	9
1019	54	10	32	N	14	11	52	20	12	23	29	10	10
1119	41	10	10	00	38	12	12	20	24	23	29	11	11
1219	27	09	48	01	02	12	32	20	36	23	28	12	12
1319	12	09	26	01	26	12	52	20	47	23	27	13	13
1418	58	09	04	01	49	13	12	20	58	23	26	14	14
1518	43	08	42	02	13	13	31	21	08	23	24	15	15
1618	27	08	19	02	36	13	50	21	19	23	22	16	16
1718	11	07	57	03	00	14	09	21	29	23	20	17	17
1817	55	07	34	03	23	14	28	21	38	23	17	18	18
1917	39	07	11	03	47	14	47	21	47	23	13	19	19
2017	22	06	48	04	1	15	09	21	56	23	10	20	20
2117	05	06	25	04	33	15	23	22	05	23	06	21	21
2216	48	06	02	04	56	15	41	22	13	23	01	22	22
2316	31	05	39	05	19	15	58	22	20	22	56	23	23
2416	13	05	15	05	42	16	15	22	27	22	51	24	24
2515	55	04	52	06	05	16	32	22	34	22	45	25	25
2615	36	04	29	06	28	16	49	22	41	22	39	26	26
2715	18	04	05	06	90	17	05	22	47	22	32	27	27
2813	58	03	42	07	13	17	22	22	53	22	25	28	28
2914	29		07		35	17	38	22	58	22	18	29	29
3014	20		07		57	17	53	23	03	22	10	30	30
3114	00		08		19		23		07		13	11	11

1730, 1734, 1738, 1742, (each being the second after Leap-year.)

Days.	July. N.	Aug. N.	Sep. N. *	Octob. S.	Nov. S.	Decem. S.	Days. 1
	0	1	0	1	0	1	
1 22	02	15	02 04	13 07	24 17	44 23	08 1
2 25	53	14	44 03	50 07	47 18	9 25	12 2
3 1	44	14	26 03	27 08	09 18	10 25	16 3
4 21	35	14	07 03	04 08	32 18	3 23	19 4
5 21	26	13	48 02	41 08	54 18	47 23	22 5
6 21	16	13	29 02	17 09	16 19	02 23	24 6
7 21	06	13	10 01	54 09	38 19	17 23	26 7
8 20	55	12	51 01	34 10	00 19	31 23	27 8
9 20	44	12	31 01	07 10	21 19	45 23	28 9
10 20	33	12	17 00	44 10	43 19	58 23	29 10
11 20	21	11	51 00	21 11	04 20	11 23	29 11
12 20	09	11	31 S	03 11	26 20	24 23	28 12
13 19	57	11	10 00	26 11	47 20	36 23	27 13
14 19	44	10	49 00	50 12	08 20	48 23	26 14
15 19	31	10	28 01	13 12	28 21	00 23	24 15
16 19	18	10	07 01	37 12	45 21	11 23	22 16
17 19	04	09	46 02	00 13	09 21	22 23	19 17
18 18	50	09	25 02	23 13	29 21	32 23	16 18
19 18	35	09	04 02	47 13	49 21	42 23	12 19
20 18	20	08	42 03	10 14	09 21	51 23	08 20
21 18	05	08	20 03	34 14	28 22	00 23	03 21
22 17	51	07	58 03	57 14	47 22	05 22	58 22
23 17	35	07	34 04	20 15	06 22	17 22	52 23
24 17	19	07	14 04	44 15	25 22	25 22	46 24
25 17	03	06	52 05	07 15	43 22	33 22	40 25
26 16	46	06	30 05	30 16	01 22	40 22	33 26
27 16	30	06	07 05	53 16	19 22	46 22	25 27
28 16	13	05	44 06	16 16	37 22	52 22	17 28
29 15	56	05	22 06	39 16	54 22	58 22	09 29
30 15	39	04	50 27	02 17	11 23	03 22	00 30
31 15	21	04	36	17	28	21	51 31

A TABLE of the Sun's Declination for the Years

Date	Jan.		Feb.		March.		April.		May.		June.		Days.
	S.	S.	S.	S.	S.	*	N.	N.	N.	N.	N.	N.	
1 21	42	13	45	03	24	08	36	18	09	23	10	1	
2 21	30	13	25	03	00	08	58	18	20	23	14	2	
3 21	21	13	05	02	36	09	17	18	35	23	17	3	
4 21	10	13	44	02	13	09	39	13	49	23	20	4	
5 20	59	12	24	01	49	10	03	19	03	23	23	5	
6 20	48	10	03	01	25	10	24	19	15	23	25	6	
7 20	36	11	42	01	02	10	45	19	39	23	26	7	
8 20	23	11	21	00	38	11	06	19	43	23	27	8	
9 20	10	10	59	00	14	11	27	19	56	23	28	9	
10 19	57	10	38	N	09	11	47	20	09	23	29	10	
11 19	44	10	16	00	33	12	07	20	21	23	29	11	
12 19	30	09	54	00	56	12	27	20	33	23	29	12	
13 19	16	09	32	01	20	12	47	20	44	23	28	13	
14 19	01	09	10	01	44	13	07	20	55	23	27	14	
15 18	46	08	17	02	07	13	26	21	06	23	25	15	
16 18	31	08	25	02	31	13	46	21	16	23	23	16	
17 18	15	08	02	02	54	14	05	21	26	23	21	17	
17 17	59	07	39	03	18	14	24	21	36	23	18	18	
18 17	43	07	17	03	41	14	42	21	45	23	14	19	
19 17	26	06	5	04	04	14	59	21	54	23	11	20	
20 17	09	06	31	04	27	15	19	22	03	23	07	21	
21 16	52	06	08	04	51	15	37	22	11	23	02	22	
22 16	35	05	44	05	14	15	54	22	18	22	57	23	
23 16	10	05	21	05	37	16	11	22	26	22	52	24	
24 15	59	04	53	05	59	16	28	22	33	22	46	25	
25 15	41	04	3	06	22	16	45	22	39	22	40	26	
26 15	22	04	1	06	45	17	02	22	45	22	34	27	
27 15	03	03	47	07	07	17	17	22	51	22	27	28	
28 14	44		07		30	17	34	22	56	22	20	29	
29 14	25		27		52	17	50	23	01	22	12	30	
30 14	05		08		14		2		06		31		

1721, 1735, 1739, 1743, (each being the third after Leap-Year.)

Days.	July.		Aug.		Sep.		Octob.		Nov.		Decem.		Days.
	N.	S.	N.	S.	N.	S.	N.	S.	N.	S.	N.	S.	
1	22	04	15	07	07	19	07	19	11	41	23	07	1
2	21	55	14	40	03	56	07	41	17	51	23	11	2
3	21	47	14	30	03	33	08	04	18	13	23	11	3
4	21	38	14	20	03	10	08	26	18	28	23	18	4
5	21	28	13	52	02	46	08	48	18	43	23	21	5
6	21	18	13	34	02	23	09	11	18	18	23	21	6
7	21	08	12	15	02	00	09	33	19	13	23	26	7
8	20	51	12	55	01	36	09	54	19	27	23	27	8
9	20	46	12	36	01	13	10	16	19	41	23	28	9
10	20	29	12	16	00	50	10	38	19	55	23	29	10
11	20	23	11	56	00	26	10	59	20	08	23	29	11
12	20	13	11	35	00	03	11	20	20	21	23	29	12
13	20	01	11	15	S	20	11	42	20	33	23	28	13
14	19	47	10	51	00	44	12	03	20	45	23	27	14
15	19	31	10	34	01	07	12	23	20	57	23	25	15
16	19	20	10	13	01	31	12	44	21	08	23	23	16
17	19	07	09	51	01	54	13	04	21	19	23	20	17
18	18	53	09	30	02	18	13	24	21	30	23	17	18
19	18	38	09	09	02	41	13	44	21	40	23	13	19
20	18	24	08	47	03	05	14	04	21	49	23	09	20
21	18	09	08	25	03	28	14	23	21	58	23	04	21
22	17	54	08	04	03	51	14	41	22	07	22	59	22
23	17	38	07	42	04	15	15	01	22	16	22	54	23
24	17	23	07	20	04	38	15	20	22	24	22	48	24
25	17	07	06	57	05	01	15	39	22	31	22	42	25
26	16	50	06	35	05	24	15	57	22	38	22	35	
27	16	34	06	12	05	47	16	15	22	45	22	27	7
28	16	17	05	50	06	10	16	33	22	51	22	20	28
29	16	00	05	27	06	33	16	50	22	57	22	12	29
30	15	42	05	05	06	56	17	07	23	02	22	03	30
31	15	25	04	42			17	24		21	54	31	

A TABLE of the Sun's Declination for the Years

Days.	Jan. S.	Feb. S.	March. S.	April. N.	May. N.	June. N.	Days.
	o	o	o	o	o	o	
1 21	44	13	90 03	06 08	52 18	16 23	13
2 21	34	13	30 02	42 09	14 18	31 23	16
3 21	24	13	10 02	19 09	36 18	46 23	19
4 21	13	12	49 01	55 09	57 19	00 23	22
5 21	02	12	29 01	31 10	19 19	14 23	24
6 20	51	12	08 01	08 10	40 19	27 23	26
7 20	39	11	47 00	44 11	01 19	40 23	27
8 20	27	11	26 00	20 11	21 19	53 23	28
9 20	14	11	04 N	03 11	42 20	06 23	29
10 20	01	10	43 00	27 12	02 20	18 23	29
11 19	47	10	21 00	51 12	23 20	30 23	29
12 19	35	09	59 01	14 12	40 20	41 23	28
13 19	19	09	37 01	38 13	02 20	52 23	27
14 19	05	09	15 02	02 13	22 21	03 23	25
15 18	50	08	53 02	25 13	41 2	14 23	23
16 18	35	08	30 02	49 14	00 21	24 23	21
17 18	19	08	08 03	12 14	19 21	34 23	18
18 18	03	07	45 03	35 14	38 21	43 23	15
19 17	47	07	22 03	59 14	56 21	52 23	12
20 17	30	06	59 04	22 15	14 22	00 23	08
21 17	13	06	36 04	45 15	32 22	09 23	04
22 16	56	06	13 05	08 15	50 22	17 22	59
23 16	39	05	50 05	31 16	07 22	25 22	54
24 16	21	05	27 05	54 16	25 22	31 22	48
25 16	03	05	03 06	17 16	41 22	28 22	42
26 15	45	04	40 06	39 16	58 22	44 22	35
27 15	27	04	17 07	02 17	14 22	50 22	29
28 15	08	03	53 07	24 17	30 22	55 22	22
29 14	49	03	29 07	47 17	46 23	00 22	14
30 14	29		08	09 18	07 23	05 22	06
31 14	10		08	31	23	09	31

1732, 1736, 1740, 1744, (being Leap-Year.)

Days.	July.		Aug.		Sept.		Octob.		Nov.		Decem.		Days.
	N.	S.	N.	S.	N.	S.	N.	S.	N.	S.	N.	S.	
1	21	58	14	53	04	01	07	36	17	53	23	10	1
2	21	49	14	3	03	38	07	58	18	09	23	14	2
3	1	4	14	16	03	15	08	21	18	25	22	17	4
4	21	31	13	58	02	52	08	43	18	40	23	20	5
5	21	1	13	39	02	29	09	05	18	55	23	23	6
6	21	11	13	19	02	05	09	27	19	10	23	29	6
7	21	00	1	00	01	42	09	49	19	24	23	27	7
8	20	4	12	40	01	19	10	11	19	38	23	28	8
9	20	38	12	21	00	55	10	33	19	52	23	29	9
10	20	27	12	01	00	32	10	54	20	05	23	29	10
11	20	15	11	40	00	08	11	15	20	18	23	29	11
12	20	02	11	20	S	15	11	37	20	30	23	28	12
13	19	50	10	59	00	38	11	58	20	42	23	27	13
14	19	37	10	39	01	02	12	18	20	54	23	28	14
15	19	24	10	18	01	25	12	39	21	05	23	23	15
16	19	10	09	57	01	49	12	59	21	16	23	20	16
17	18	56	09	35	02	12	13	19	21	27	23	17	17
18	18	42	09	14	02	36	13	39	21	37	23	14	18
19	18	27	08	52	02	59	13	59	21	47	23	10	19
20	18	12	08	31	03	22	14	19	21	56	23	05	20
21	17	57	08	09	03	46	14	38	22	05	23	00	21
22	17	42	07	47	04	09	14	57	22	14	22	55	22
23	17	26	07	25	04	32	15	16	22	22	22	49	23
24	17	10	07	03	04	56	15	34	22	29	22	43	24
25	16	54	06	40	05	19	15	53	22	36	22	36	25
26	16	38	06	18	05	42	16	11	22	43	22	2	26
27	16	21	05	55	06	05	16	29	22	49	22	21	27
28	16	04	05	33	06	28	16	46	22	55	22	13	28
29	15	47	05	10	06	51	17	03	23	01	22	05	29
30	15	29	04	47	07	13	17	20	23	06	21	56	30
31	15	11	04	24		17		37		21	46	31	

A TABLE of the Variation of the Sun's Declination to every 15 Degrees of Longitude from the Meridian of London.

Degrees of Longitude from the Meridian of London.

Daily Variat.	D. M.	D. M.	D. M.	D. M.	D. M.	Deg. Min.						
2	00	00	00	00	00	00	01	01	01	01	01	01
3	00	00	00	00	01	01	01	01	01	01	01	01
4	00	00	00	01	01	01	01	02	02	02	02	02
5	00	00	01	01	01	01	01	02	02	02	02	02
6	00	00	01	01	01	01	02	02	02	02	03	03
7	00	01	01	01	01	02	02	03	03	03	03	03
8	00	01	01	01	02	02	02	03	03	03	04	04
9	00	01	01	01	02	02	03	03	03	04	04	04
10	00	01	01	02	02	02	03	03	04	04	05	05
11	00	01	01	02	02	03	03	04	04	05	05	05
12	00	01	01	02	02	03	03	04	04	05	05	06
13	01	01	02	02	03	03	04	04	05	05	06	06
14	01	01	02	02	03	03	04	05	05	06	06	06
15	01	01	02	02	03	04	04	05	06	06	07	07
16	01	01	02	03	03	04	05	05	06	07	07	07
17	01	01	02	02	04	04	05	06	06	07	08	08
18	01	01	02	03	04	04	05	06	07	07	08	09
19	01	02	02	03	04	05	06	06	07	08	09	09
20	01	02	02	03	04	05	06	06	07	08	09	10
21	01	02	03	03	04	05	06	07	08	09	10	10
22	01	02	03	04	05	05	06	07	08	09	10	11
23	01	02	03	04	05	06	07	08	09	10	11	11
24	01	02	03	04	05	06	07	08	09	10	11	12

# S U P P L E M E N T

T O THIS

## N E W E D I T I O N :

C O N T A I N I N G

1. The easy Construction of the Tables of Sines, Tangents and Secant.
2. Two new Methods of Sailing without Tables or Instruments, by only Vulgar Arithmetick: mentioned in Wilsons Navigation.
3. Four Ways of Laying down Traverses on Paper.
4. The Disagreement in the sundry Kinds of Sailing exemplified, in Plain, Mercator, Middle Latitude, Circle, and Sailing by Parallel Parts a Method taught by John Ward in his Posthumous-Works.
5. To find the Meridional Parts without a Table of them.
6. To estimate Distances by Sound, &c.
7. A Table of New and Full Moons, with all the visible Eclips for 21 Years to come, from 1736 to 1757.
8. A ready Method to calculate the Lunations throughout the whole Year, with a Table of Stars corrected to the Year 1716.
9. Sundry Errors and Defects in Chards, Compasses, Quadrant, Cross-Staff, Nocturnal and Nautical Tables, specified with proper Helps, &c.
10. A Synopsis of all the possible Varieties in working an Observation.

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By S A M U E L F U L L E R.

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D U B L I N :

Printed by and for S A M . F U L L E R , at the Globe  
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## SECT. I.

To make the Table of Natural Sines, Tangents and Secants easily.

Seeing the Periphery of a Circle whose Radius is 1, is 6.283185, and the Natural Sine of one Minute sensibly differs from the Length of the Arch of one Min. &c. say,

As the Periphery in Minutes - - - - 21600  
is to the Periphery in equal Parts - - 6283185  
so is one Minute - - - - -

to the Parts agreeing to that Minute 0.000290888, equal to the Natural Sine of one Minute, which agrees with the largest Table of Natural Sines I ever saw.

Next to find its COSINE.

From the Square of Radius - - - 100000000, &c.  
deduct the Sq. of Sine of one Min. 00000024612

the remains is - - - - - 0.99999915388 whose Sq. R. is 999999999  
the Cosine required or Sine of 89°. 59'

Then in a rank of Arches Equidistant say

As the Sine of any Arch in that Rank

is to the Sum of the Sines of any 2 Arches equally remote from it on each Side

so is the Sine of any other Arch in the said Rank to the Sum of the Sines of 2 Arches next it on each side having the same common Distance.

Let the Radius be made the mean or middle Term between these Extremes and the Proportion will run thus

As the Radius is to the double Cosine of one Minute :  
so is the Sine of one Minute to the Sine of 2' and 0'.

and,

So is the Sine of 2' to the Sum of 3' and 1'.

and,

So is the Sine of 3' to the Sum of the Sines of 4' and 2', and so on in a successive Order from Minute to Minute

As the Cosine of any Arch is to its Sine: So is Radius to its Tangent sought, or for the Table of Natural Secants, Say,

As the Cosine to Radius, so is Radius to the Secant sought, or divide the Square of Radius by the Natural Cosine, the Quotient is the Natural Secant

The Tables of Artificial Sines, Tangents and Secants are only the respective Logarithms of their Natural Sines, Tangents and Secants, and have this Property that

Sine and Cosecant  
the Artificial } Tangent and Cotangent } do always make up 20.00000 &c.  
Secant and Cosine } or double Radius  
wherefore one is the Complement of the other to Double Radius

And then if from the Sum of the Sines of 3' and 1' be taken, the Sine of 1', the Remainder will be the Sine of 3', and the like, if from the Sum of 4' and 2' be taken the Sine of 2', the Remainder will be the Sine of 4'.

Proceeding thus all the Natural Sines in the Quadrant may be calculated by Addition and Subtraction only.

Having made the Table of Sines to form the Table of Natural Tangents, Say,

The SUPPLEMENT.

3

SECT. II.

PLAIN-SAILING Arithmetical.

A TABLE of Given Numbers.

Points	Latitude.	Depart.	Points
0 $\frac{1}{4}$	99 : 88	24 : 88	7 $\frac{3}{4}$
0 $\frac{1}{2}$	99 : 52	09 : 76	7 $\frac{1}{2}$
0 $\frac{3}{4}$	98 : 92	14 : 66	7 $\frac{1}{4}$
I	98 : 08	19 : 51	7
I $\frac{1}{4}$	97 : 01	24 : 27	6 $\frac{3}{4}$
I $\frac{1}{2}$	95 : 71	28 : 99	6 $\frac{1}{2}$
I $\frac{3}{4}$	94 : 15	33 : 71	6 $\frac{1}{4}$
2	92 : 39	38 : 27	6
2 $\frac{1}{4}$	90 : 40	42 : 77	5 $\frac{3}{4}$
2 $\frac{1}{2}$	88 : 20	47 : 13	5 $\frac{1}{2}$
2 $\frac{3}{4}$	85 : 79	51 : 38	5 $\frac{1}{4}$
3	83 : 15	55 : 56	5
3 $\frac{1}{4}$	80 : 33	59 : 55	4 $\frac{3}{4}$
3 $\frac{1}{2}$	77 : 29	63 : 45	4 $\frac{1}{2}$
3 $\frac{3}{4}$	74 : 10	67 : 15	4 $\frac{1}{4}$
4	70 : 71	70 : 71	4
Points	Depart.	Latitude.	Points

The Use of this Table is for working the six Cases of Plain Sailing; in which observe, that in the first and last Column, you have the Rumbs or Points of the Compass, with the Points, and quarter Points, number'd from the Meridian or North and South Line, either East or West, according as they stand in order; thus S. S. W. is two Points, because South is upon the Meridian, then S. by W. is one Point, and S. S. W. two Points, &c. So likewise N. N. E. and N. N. W. is two Points from the North Again, suppose a Ship sails S. W.  $\frac{1}{2}$  S. that is, three Points and an half, and N. N. E.  $\frac{1}{2}$  E. is two Points and a Quarter; which being a Thing so commonly known, I shall not need to add any more Examples.

The Number of Points thus found, observe on which Side of the Table it is found, for if you find the Course at the left Hand, then find the Denomination of Latitude and Departure at the Top: But if the Course be on the right Hand, find the Denomi-

nation of Latitude and Departure at the Bottom; for the left Hand Column contains all the Points under four Points, and the right Hand Column contains all the rest of the Points to 8. Now if the Course be found in the first Column, (viz. less than four Points) then in the second Column is the given Numbers for Difference of Latitude, and in the third Column is the given Numbers to find Departure: But if the Course be in the last Column, (viz. above four Points) then in the third Column is the given Numbers to find Difference of Latitude, and the second is for the Departure, &c. And the Use of the Table being thus known for the first Case, the rest is easily found by Consequence, as we have hinted and shall make it evident and intelligible to the meanest Capacity, by the following Examples.

Note, If you have a given Number, with a Cypher on the left hand, (as in  $7 \frac{1}{2}$  and  $7 \frac{3}{4}$  Points) although a Cypher adds nothing to the Product (being on the left Hand) yet it causeth a Figure more to be cut off for the Decimal Fraction; and having cut off as many Figures towards the right Hand as you multiply by, the rest is the Latitude or Departure sought, and those cut off are a Numerator of a Decimal Fraction to a Denominator consisting of as many Cyphers as you cut off Figures, with a 1 at the left Hand; so if you cut off 97, it is  $\frac{97}{100}$ , or if you cut off 342, it is  $\frac{342}{1000}$ . and so of the rest.

# The SUPPLEMENT.

Note, When you have found the given Number in the Table, you need not always use all the 4 Figures, especially, if the third or fourth be a small Digit, as 1 or 2, as suppose your given Number be 8315, here the third Figure being a 1, you may cut off the two last Figures, and use only 83, to work with. Again, if the third Figure be one of the highest Digits, as 8 or 9, you may cut off the two last, only add one to the second Figure, and so work as before; as suppose your Number be 189, you may add 1 to the second Figure, *viz.* 8, and then cut off the two last, and then your Number to work will be 18, the Reason of all which is very evident to any that understands the Nature of Decimals, and will by a little Practise become easy to the meanest Capacity.

## PLAIN SAILING.

**CASE I.** Course and Distance given, to find the Difference of Latitude and Departure.

### The Rule.

Multiply the Distance by the given Numbers for the Course, and from the Product cut off as many Figures as you multiply by, and the rest is the Difference of Latitude and Departure required.

**Question.** A Ship sails N. W. by N. 123 Miles; I demand her Diff. of Latitude and Departure.

The given Number for Diff. Latitude being 8315, we shall only use 83, and cut off the other two Figures (towards the right hand) and multiplying the Distance 123, by the given Number 83, and from the Product cut off two Figures, (because you multiply by two Figures) you have the Difference of Latitude; but for Departure the given Number is 5556, the third Figure being a 5, we shall for more Exactness use three Figures, *viz.* 555, and work as before. The Operation for the Difference of Latitude and Departure will stand thus:

For Difference of Latitude.

$$\begin{array}{r} 123 \\ \times 83 \\ \hline 269 \\ 984 \\ \hline 102109 \end{array}$$

For Departure.

$$\begin{array}{r} 123 \\ \times 555 \\ \hline 615 \\ 615 \\ \hline 615 \\ \hline 681265 \end{array}$$

The Difference of Latitude is 102  $\frac{2}{10}$  the Departure is 68  $\frac{265}{1000}$ ; but you need not regard the Fractions, only if a Fraction be considerably above half of one Mile, or Minute, you may add 1 to the whole Number; as suppose your Fraction be  $\frac{7}{8}$ , *viz.*  $\frac{7}{100}$  you may add 1 to the whole Number, and reject the Fraction, &c.

*Another Example in Case I.*

A Ship sails N N.W.  $\frac{1}{2}$  W. 165 Miles; I demand the Difference of Latitude and Departure.

N. N. W.  $\frac{1}{2}$  W. is  $2\frac{1}{2}$  Points.

# The SUPPLEMENT.

5

For Difference of Latitude.

$$\begin{array}{r} 165 \\ - 88 \\ \hline \end{array}$$

$$\begin{array}{r} 1320 \\ - 320 \\ \hline \end{array}$$

$$145 \mid 10 \text{ Diff. of Latitude } 145.$$

For Departure.

$$\begin{array}{r} 165 \\ - 47 \\ \hline \end{array}$$

$$\begin{array}{r} 1159 \\ - 660 \\ \hline \end{array}$$

$$77 \mid 11$$

Dep. 77, or rather 78, because the Fraction is  $\frac{5}{10}$ .

CASE II. Course and Difference of Latitude given, to find Distance and Departure.

## The RULE.

For the Distance, add as many Cyphers to the Difference of Latitude as the Number of Figures you think to make use of in the given Number, and then divide it by the given Number, and the Quotient is the Distance which being found, find the Departure as in Case I.

Question. A Ship sails S. W. by S. till her Difference of Latitude be 174; I demand the Distance and Departure.

The Course is 3 Points, the given Numbers 8315 and 5556.

For the Distance.

$$\begin{array}{r} 83) 17400(209 \text{ Diff.} \\ . . 800 \\ \hline \end{array}$$

$$53$$

For Departure.

$$\begin{array}{r} 209 \\ - 555 \\ \hline 1045 \\ - 1045 \\ \hline 115 \mid 995 \end{array}$$

The Distance 209, and Departure 115, or rather 116, because the Fraction is so great, viz. above  $\frac{5}{10}$ .

CASE III. Course and Departure given, to find Distance and Difference of Latitude.

## The RULE.

Add so many Cyphers to the Departure as you think to use Figures in the given Number; and then divide by the given Number answering to Departure, and the Quotient is the Distance, which being found, find the Difference of Latitude, as in Case I.

Question. A Ship sails N. by E.  $\frac{3}{4}$  E. till her Departure be 72; her Distance and Difference of Latitude is required.

For the Distance.

$$\begin{array}{r} 337) 72000(213 \\ . . 460 \\ 1230 \\ \hline \end{array}$$

$$219$$

For Diff. Lat.

$$\begin{array}{r} 214 \\ - 49 \\ \hline 856 \\ - 1926 \\ \hline 201 \mid 16 \end{array}$$

The

# The SUPPLEMENT.

The Distance is  $2\frac{1}{4}$ , (being so large a Fraction) the Difference of Latitude is  $201$ .

**CASE IV.** Distance and Difference of Latitude given to find the Course and Departure.

## The RULE.

Square the Distance (that is multiply it by it self) and likewise the Difference of Latitude, and subtract the lesser Number from the greater, the square Root of the Remainder is the Departure required, and then for the Course, add two or three Cyphers to the Difference of Latitude, and divide that Sum by the Distance, the Quotient is the given Number & the Course, which being found in the Table, you have again the Course required.

*Note.* If you cannot find exactly the same Numbers (which seldom happens) find the nearest to it, which is sufficient, and finds the Course to the nearest Quarter Point.

*Question.* A Ship sails between the North and East  $110$  Miles; and then finds by Observation, that she hath rais'd the Pole  $1$  Degree, or  $60$  Min. or Miles; I demand the Course and Departure.

### For the Course.

$100)60000(545$	$110$	$60$
.50	$110$	$60$
.600	$\underline{\quad}$	$\underline{\quad}$
.50	$1100$	$3600$
$\underline{110}$	$\underline{\quad}$	$\underline{\quad}$
$12100$	$\underline{\quad}$	$\underline{\quad}$

### For the Departure

Sq. of Dist.	12100	Sq. of Diff. Lat.	3600	Diff. of Sq.	8500	82	36

The Quotient  $545$  sought in the Table, the nearest given Number is  $555$ , and against that, for the Course, you have five Points, which is N. E. by E. because the Course is between North and East, and the Departure is  $92$ , for you need not regard the Fraction in the Square Root, it being but a small Part of a Mile or Minute in the Departure.

**CASE V.** Distance and Departure given, to find Course and Difference of Latitude.

## The RULE.

Subtract the Square of the Departure from the Square of the Distance, the Square Root of the Remainder is the Difference of Latitude; and then find the Course as in Case IV; only mind to find the Quotient in the Departure Column.

*Question.* A Ship sails in the S. W. Quarter  $1\frac{1}{4}$  Miles, her Departure  $95$ ? I demand the Course and Difference of Latitude.

# The SUPPLEMENT.

For the Course.

$$124 \quad 863(766)$$

$$\cdot 82$$

$$\cdot 760$$

$$\overline{16}$$

$$124 \quad 91$$

$$124 \quad 95$$

$$496 \quad 475$$

$$248 \quad 355$$

$$124 \quad \overline{525}$$

$$15376 \quad \overline{525}$$

For the Diff. of Lat.

$$\text{Square of Dist.} \quad 15376$$

$$\text{Sq. of Diff. Lat.} \quad 9025$$

$$\text{Diff. of Squares} \quad 6351$$

$$6351(79)$$

$$\cdot 49$$

$$449)1458$$

$$\cdot 348$$

$$\overline{110}$$

The Course is S. W.  $\frac{1}{2}$  W. nearest; for the nearest given Number to the Quotient 766 is 772, which is the Number for four  $\frac{1}{2}$  Points, or S. W.  $\frac{1}{2}$  W. and the Difference of Latitude is 79, or rather 80, because the Remainder of the square Root is so great: And here observe for a general Rule, that because the last Remainder in the Extraction is a Numerator to twice the Root for a Denominator? therefore if the last Remainder be more than the Root, add one to the Root, and that will be the Root exact enough in this Case; but if the Remainder be less than the Root found, the Root is nearest whole Number that answers the Question, and you need not regard the Fraction at all; Thus in the Example, Case IV. the Root is 92, and the Remainder is but 36, and therefore I keep 92 for the Departure, and reject the Fraction. But in the Example in Case V, the Root is 79, and the Remainder is more than the Root, viz. 110; and therefore I add 1 to 79, and the Sum 80 is the Difference of Latitude required, and so in others.

CASE VI. Difference of Latitude and Departure given, to find the Course and Distance.

## The RULE.

Square the Difference of Latitude, and also the Departure, and add the two Squares together; the Square Root of the Sum is the Distance required; and then find the Course, as in Case IV, or Case V.

*Question.* A Ship sails in the N. W. Quarter, till her Difference of Latitude be 120, and her Departure 108; I demand the Course and Distance.

For the Distance.

$$220$$

$$108 \quad \text{Square of Diff. Lat.} \quad 48400$$

$$220$$

$$108 \quad \text{Square of Departure.} \quad 11664$$

$$\overline{44}$$

$$864 \quad \text{Sum of the Squares} \quad 60064$$

$$44$$

$$1080 \quad \overline{60064}$$

$$60064(245)$$

$$48400$$

$$11664 \quad \overline{4}$$

$$60064(245)$$

$$\overline{44}$$

$$44)100$$

$$\overline{176}$$

For the Course.

$$245)220000(897$$

$$2400$$

$$1950$$

$$485)2464$$

$$\overline{2425}$$

$$\overline{59}$$

The Course is 2 Points and a Quarter, or N. N. W.  $\frac{1}{4}$  W. the Distance 2 Miles.

Although the Operation in this Case seems the most tedious of all the rest, because we have assumed greater Numbers for the Data of the Question, yet even in the greatest Number this Way is much more expeditious than working by a Canon; as a little Practice will make manifest.

## *NAVIGATION New Model'd;*

O R,

*The Whole Art Perform'd by a NEW METHOD.*

### PART II.

*Rules and Grounds of this Method.*

**I**N Order to the right Understanding of this new Method of *Trigonometry*, I shall proceed, according to the usual Method, and shall, for the Help of Memory, lay down some fundamental Rules or Axioms, upon which the whole Operation depends, and by which all the Cases in *Plain Trigonometry*, both Right and Oblique, may be solved, without any Book, Table or Instrument whatsoever. But before I come to the Axioms, I shall premise, that whenever a Side and an Angle is given, to find another Side, (which is the first and most useful Case in Navigation) there must first be a Number found, which I call the Natural Radius, not only because it is the Original, from whence the Solutions are deduced, but also because being found, it produces the same Answer in Natural Numbers, that the Radius, or Sine of 90, produces in a Sinical Proportion; and this Natural Radius is thus found:

#### *METHOD the First.*

Take the Angle whose opposite Side is either given or sought, and divide four times the Square of its Complement to 90 Degrees by 300 added to three times the said Complement, and then the Quotient added to the said Angle is the Natural Radius required; and this Rule is universally true in all Angles from 0 to 90.

*METHOD*

# THE SUPPLEMENT.

## Method the Second.

But because in Angles under 45, the Complements are above 45, and their Squares amount to greater Numbers than the Squares of the Complements of the Angles above 45; therefore to render the Work as easy, and the Contrivance as useful as possible, I shall shew another Way to find the Natural Radius for all Angles under 45, and the Rule is,

D. side  $\times$  3 times the Square of the Angle (whose opposite Side is given or sought by 1000, the Quotient added to 57 + 3, that is 57 + 3, the Sum is the Natural Radius required.

This being premised, the Rules are these.

## R U L E the First. In Right-angled Triangles.

### An Angle and a Side given, to find another Side.

The Natural Radius bears always the same Proportion to the Hypotenuse that the Angle (by which the Natural Radius was found) bears to its opposite Side.

Therefore if the Angles and Hypotenuse, be given, it is; As Natural Radius to Hypotenuse, so the Angle to its opposite Side. But if the Angles and a Leg be given, then it is, As the Angle to its opposite Side, so is the Natural Radius to the Hypotenuse.

## R U L E the Second. In Right-angled Triangles.

### Two Sides given, to find a Third.

The Hypotenuse is equal in Power to the two Legs: that is, the Square of the Hypotenuse is equal to the Square of both Legs added together; of which see more in p. 6. 7.

## R U L E the Third. In Right-angled Triangles.

### (The Hypotenuse and a Leg given, to find the other Leg.)

Multiply the Sum of the Hypotenuse, and given Leg, by their Difference: The Square Root of the Product is the other Leg required.

## R U L E the Fourth. In Right-angled Triangles.

### Three Sides given, to find an Angle.

Add half the longer Leg to the Hypotenuse: Then, As that Sum to 16; so is the shorter Leg to its opposite Angle.

## R U L E the Fifth. In Oblique Triangles.

### Three Sides given, to find where the Perpendicular must fall.

Multiply the Sum of the two shortest Sides by their Difference, and divide the Product by the third Side, which is the greatest, and upon which the Perpendicular is to fall: The Quotient added to the greatest Side, or subtracted from it, shall be double the greater or lesser Segment, on each Side, of the Perpendicular.

*Another Way.*

Add the Squares of the biggest and least Sides together, and from their Sum subtract the Square of the middlemost; Half the Remainder, divide by the biggest Side, the Quotient is the lesser Segment, which subtracted from the whole Base, leaves the bigger Segment.

---

*Plain Sailing by a New Method.*

I shall now proceed to some Examples in Right-angled Triangles, applied to Plain-Sailing; and here note, That to avoid Fractions, I shall propose the given Angle always in whole Degrees, that being sufficiently exact in all Uses in Navigation; yea, and a far more exact Way, than reckoning by Points; one Degree being a much smaller Part of a great Circle than a Quarter Point of the Compass. And I shall make use of Degrees rather than Quarter Points, not only for its Exactness, but also because it is a Method much in Use aboard of the Men of War, to reckon the Course in Degrees, and not in Points and Quarter-Points.

**CASE I.** Course and Distance given, to find the Difference of Latitude and Departure.

A Ship sails South 25 Degrees Easterly 96 Miles; I demand as above.

*The Operation at large.*

Note, Where both Legs are required, choose always to find the lesser first, because the Natural Radius is more easily found, and then find the longer Leg by Rule the Third.

*For the Departure.**The RULE I.*

The Angle - - - - -	25
Multipled by it self - - - - -	25
-----	
125	
50	
-----	

As Natural Rad. 59. 2.  
to the Distance 96 : So  
the lesser Angle 25, to its  
opposite Side the Depart-  
ture.

Square of the Angle - - -	625
Multipled by - - - - -	3
-----	
The Product - - - - -	1875
1875 divided by 1000 is 1.875	
To which add - - - - -	57.3
-----	
Sum is Natural Rad.	59.175
Or rather briefest - - -	59.2
Which is exact enough.	

96 59.2)2400(40 $\frac{1}{2}$   
25 320  
-----  
480 320  
192 Nearest which 40 $\frac{1}{2}$   
----- is the Departure  
2400 req.

# The SUPPLEMENT.

II

Then for the Difference of Longitude by RULE III.

Hypothenuse or Distance	96.0	
The Dep. in Decimals	40.5	
Sum	136.5	7575 (5)
Difference	55.5	64
		-----
	6845	167) 1175
	6825	1169
	6825	(6)
		-----
The Product	7575.75	

The Depart. is  $40\frac{1}{2}$  (or in Decimals 40.5.) The Diff. of Lat. 87.

CASE II. Course and Difference of Latitude given, to find the rest.

A Ship sails North 38 Degrees West, her Difference of Latitude 120; her Distance and Departure is required.

Here the Side opposite to the bigger Angle is given, therefore we must make Use of Method I. to find the Natural Radius, because Method II. serves only to Degrees under 45.

$$\begin{array}{r}
 38 \quad 38 \quad 414) 5776(13^3 \frac{1}{2} \\
 38 \quad 3 \quad 1636 \\
 \hline
 304 \quad 14 \\
 174 \quad 300 \\
 \hline
 1444 \quad 434 \\
 \hline
 4 \\
 \hline
 5776
 \end{array}$$

Because the Fraction is so great, I shall call the Quotient 14, which added to the bigger Angle 52,  $52 + 14 = 66$  is the Natural Radius.

Then by RULE I.

As 52, the greater Angle to 120 its opposite Side: so is Natural Radius 66, to the Distance required.

Then for Departure, by RULE III.

120	Distance	152	
66	Diff. Latit.	120	.8704 (93) Departure
	Sum	272	81
	Difference	32	183) 604
		544	549
		816	(55)
7920	Product	8704	
			52) 7920 (152
			272
			120
			16

The Distance 152. The Departure 93.

CASE III. Course and Departure given, to find Distance and Difference of Latitude.

A Ship sails North 19 Degrees Easterly, her Departure 72 Miles; I demand as above.

Here the shorter Log is given; therefore I shall find the Natural Radius by Method II.

Three Times the Square of the given Angle is 1083, this divided by 1000, which is done by cutting off three Figures to the right Hand, the Quotient is 1.083; which because the second Figure in the Fraction is above 5, I add one to the first Figure, which is a Cypher, and then call the Quotient 1.1, which added to 57.3, the Sum 58.4 is the Natural Radius required.

$$\begin{array}{r} 19 \\ \times 3 \\ \hline 19 \\ 19 \\ \hline 174 \\ 19 \\ \hline 362 \\ 3 \\ \hline 1.083 \end{array}$$

Then for the Distance by RULE I.

As the Angle 19, to its opposite Side 72: So is the Natural Radius 58.4, to the Distance

$$\begin{array}{r} 58.4 & 19)4204(221 & \text{The Distance} \\ 72 & -40 & \text{required.} \\ \hline 1168 & -24 \\ 4088 & -5 \\ \hline 4204.8 & \end{array}$$

To find Difference of Latitude by RULE III.

$$\begin{array}{r} \text{Distance} \quad \dots \quad 221 \\ \text{Departure} \quad \dots \quad 72 \quad 43657(108 \\ \text{Sum} \quad \dots \quad 293 \quad 4 \\ \text{Difference} \quad \dots \quad 149 \quad 40)03657 \\ \hline 2637 \\ 1172 \\ 293 \\ \hline 43657 \end{array}$$

The Root 208, but the Fraction being so large, I rather call it 109, the Difference of Lat. required.

CASE IV. Distance and Difference of Latitude given to find the Course and Departure.

A Ship sails between the North and East 117 Miles, her Difference of Latitude 102 Miles; I demand her Course and Departure.

For the Departure, by RULE III.

$$\begin{array}{r} \text{Distance} \quad \dots \quad 117 \\ \text{Diff. of Lat.} \quad \dots \quad 103 \quad 3080(55 \\ \text{Sum} \quad \dots \quad 220 \quad 25 \\ \text{Difference} \quad \dots \quad 14 \quad 305)580 \\ \hline 880 \\ 220 \\ \hline 3080 \end{array}$$

The Departure 55 $\frac{1}{2}$ .

# The SUPPLEMENT.

13

Then for the Course, by RULE I.

Hypothenuse or Distance - 7  
Half the longest Leg - 51.5

Sum - - - - - 168.5

As 168.5 to 51.5: So shortest Leg or Departure, 55.5, to its opposite Angle, the course.

$$\begin{array}{r} 55.5 \\ \times 3 \\ \hline 168.5 ) 4773.0 ( 28 \\ \underline{- 168.5} \\ \hline 309 \\ \times 3 \\ \hline 927 \\ \underline{- 900} \\ \hline 27 \\ \times 3 \\ \hline 81 \\ \underline{- 75} \\ \hline 6 \\ \times 3 \\ \hline 18 \\ \underline{- 15} \\ \hline 3 \\ \times 3 \\ \hline 9 \\ \underline{- 9} \\ \hline 0 \end{array}$$

The Course 28  $\frac{55}{85}$  Degrees, which is almost  $\frac{1}{3}$  viz. 21 Degrees, 59 Minutes.

## CASE V. Distance and Departure given, to find the rest.

A Ship sails in the South-West Quarter, 124 Miles, her Departure 95 Miles; I demand her Course and Difference of Latitude.

For the Difference of Latitude, by RULE III.

$$\begin{array}{r} \text{Distance} - - 124 \\ \text{Departure} - - 95 \\ \hline \text{Sum} - - 219 \\ \text{Difference} - - 29 \\ \hline \\ 197 \\ 438 \\ \hline \\ \text{Product} - - 6351 \end{array} \quad \begin{array}{r} 6351(79) \\ \underline{- 49} \\ \hline 1451 \\ \underline{- 1341} \\ \hline 110 \end{array}$$

The Square Root of 6351 is 79 or rather 80 (because the Remainder 110 is more than the Root) the Difference of Latitude required.

Then for the Course, by RULE IV.

$$\begin{array}{r} \text{Hypothenuse or Distance} - - 124 \\ \text{Longest Leg, which here is Dep. 95 it half} \quad 47.5 \\ \hline \\ \text{Sum} - - 171.5 \end{array}$$

As 171.5, to 86: So the shorter Leg (which here is the Difference of Latitude) 80, to its opposite Angle, the Complement of the Course.

$$\begin{array}{r} 86 \\ \times 2 \\ \hline 171.5 ) 6880.0 ( 40 \text{ Degrees} \\ \underline{- 6880} \\ \hline 0200 \\ \hline 20.0 \end{array}$$

The Complement of the Course is 40 Degrees, and consequently the Course is 50 Degrees, from the South Westerly, and the Difference of Latitude is 80 Miles *seve*.

CASE

CASE VI. Difference of Latitude and Departure given, to find the Course and Distance.

A Ship sails in N<sup>o</sup> York-W<sup>o</sup> Quarter, till her Difference of Latitude be 220 Miles, and her Departure 108; I demand the rest.

For the Distance, by RULE II.

$$\begin{array}{r}
 220 \\
 210 \\
 \hline
 40 \\
 44 \\
 \hline
 48400
 \end{array}
 \quad
 \begin{array}{r}
 108 \text{ Square of Diff. of Lat.} - 4340 \\
 108 \text{ Square of Departure} - 1166 \\
 \hline
 864 \\
 1080 \\
 \hline
 11664
 \end{array}
 \quad
 \begin{array}{r}
 \text{Sum of the Squares} - 60064(245) \\
 4
 \end{array}$$

Then for the Course by RULE IV.

As 355, to 86: So 108 to the Angle of the Course.

$$\begin{array}{r}
 108 \\
 86 \\
 \hline
 648 \\
 864 \\
 \hline
 9288
 \end{array}
 \quad
 \begin{array}{r}
 355)9288(26 \\
 2188 \\
 \hline
 58
 \end{array}$$

$$\begin{array}{r}
 44)200 \\
 176 \\
 \hline
 485)2464 \\
 2425 \\
 \hline
 (39)
 \end{array}$$
  
 The Distance is 245, and the Course  $26\frac{5}{8}\frac{3}{4}$  Degrees, or  $26^{\circ} 9m$ , or N. N. W. somewhat more than  $\frac{1}{4}W.$

## Oblique Triangles by a New Method.

How to solve all the Cases in Oblique Plain Triangles, by this New Method, without any Canon, Book, Instrument, &c.

In the Solution of Oblique Triangles, by this New Method, it is necessary that they be first divided into two right-angled Triangles by a Perpendicular let fall, in which observe:

Let it fall from the End of a given Side, and opposite to the given Angle.

By this Means the Perpendicular will sometimes fall within, and sometimes without; when it falls within, it falls upon some intermediate Part of the Base, or longest Sides; but when it falls without, it falls upon one of the shortest Sides continued; in either Case, there are two right-angled Triangles produced, and then the Angles or Sides sought are found as if they were Parts of a right-angled Triangle.

C A S E I

Given { The Angle at  $A$   $30^{\circ}$   
 The Angle at  $B$   $45^{\circ}$  } Required the Sides  $AC$ ,  
 The Side  $BC$  290

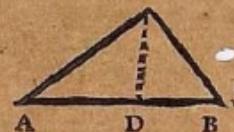
Here the Perpendicular falls from the End of the given Side  $BC$ , and opposite the given Angle at  $B$ ; then in the Triangle  $BDC$  is given the Angle at  $B$ , and the Side  $BC$ , to find the Side  $CD$ , which being found, there is given in the Triangle  $ADC$ , the Angle at  $A$  and the Side  $DC$ , to find  $AC$ , the Side required.

I shall not trouble the Reader with the Operation for finding Natural Radius, it having been often enough repeated in the foregoing Pages; but being found by Method I, the natural Radius for the Angle  $45^{\circ}$  is  $63.62$ ; therefore, As  $63.62$ , to Side  $CB$ , 290; So  $45^{\circ}$ , the Angle at  $B$ , to the Side opposite  $CD$ .

$$\begin{array}{r} 45 \\ 290 \end{array} \quad 63.62) 13050.00(205 \text{ The Side } CD 205.$$

Fig. 1.  
C

$$\begin{array}{r} 4050 \\ 90 \\ \hline 23050 \end{array} \quad \dots 7.98$$



Now in the Triangle  $ADC$ , is given the Angle at  $A$   $30^{\circ}$  o m, and the Side  $DC$  205, to find  $AC$ .

The Natural Radius therefore found by Method II, if the Angle  $30^{\circ}$  is  $60^{\circ}$ . Therefore,

As the Angle at  $A$   $30^{\circ}$ , to Side opposite  $DC$ ,  $45^{\circ}$ : So  $60^{\circ}$  to the Hypotenuse  $AC$  Required.

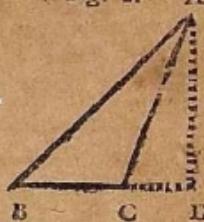
$$\begin{array}{r} 205 \\ 60 \\ \hline 2300 \end{array} \quad 80) 12300(410. \text{ The Side } AC \text{ required.}$$

C A S E II.

Given { The Side  $AB$  560  
 The Side  $AC$  410 } Required the Angle at  $C$ .  
 The Angle  $B$   $45^{\circ}$

Here the Perpendicular falls without, upon the Side  $BC$  continued, and in the Triangle  $BDA$  there is given the Angle at  $B$   $45^{\circ}$ , and the Hypotenuse  $AB$  560, to find  $AD$ , which being found you have in the Triangle  $CAD$ , the Hypotenuse  $CA$ , and the Leg  $AD$ , to find the Leg  $CD$ , and the Angle  $DAC$ , and by Subtraction, the Angle  $DCA$ , and the Angle  $BCA$ , its Supplement in their proper Case of right-angled Triangles.

Fig. 2. A



## The Operation.

The Natural Radii is for the given Angle 45, is 63.62, as found by Method I. Therefore,  $\frac{63.62}{560}$  = the Hypotenuse 560; So the Angle at B 45, to the Side  $\overline{AC}$ .

$$\begin{array}{r}
 560 & 63.62) 25100.00(396 \text{ the Side } AD \\
 45 & 6114.0 \\
 \hline
 2800 & 3882.0 \\
 2240 & \hline
 \hline
 25200 & .6480
 \end{array}$$

Then you have  $AD$  396, and  $AC$  410, to find  $CD$  by Rule III, thus:

$$\begin{array}{r}
 \text{Side } AC - - - 410 \\
 \text{Side } AD - - - 396 \\
 \hline
 \text{Sum} - - - 806 \\
 \text{Difference} - - - 14 \\
 \hline
 3224 \\
 806 \\
 \hline
 \text{Product} - - 11284
 \end{array}
 \quad
 \begin{array}{r}
 11284) 106, \text{ the Leg } CD, \\
 106 \\
 \hline
 20) 014 \\
 00 \\
 \hline
 1284 \\
 1236 \\
 \hline
 (48
 \end{array}$$

Then for the Angle  $CAD$ , by RULE IV.

$$\begin{array}{r}
 \text{Hypothenuse } AC - - 410 \\
 \text{Half the Leg } AD - - 198 \\
 \hline
 \text{Sum} - - - - - 608
 \end{array}
 \quad
 \begin{array}{r}
 \text{As } 608 \text{ to } 86, \text{ so is } 106 \text{ to} \\
 \text{the Angle } CAD. \\
 106 \\
 86 \\
 \hline
 3636
 \end{array}$$

$$\begin{array}{r}
 636 \\
 848 \\
 \hline
 9116
 \end{array}
 \quad
 \begin{array}{r}
 608) 9116(14\frac{504}{808} \\
 608 \\
 \hline
 3036 \\
 2848 \\
 \hline
 188
 \end{array}$$

The Angle  $CAD$  is  $14\frac{504}{808}$ , or rather 15 Degrees; which subtracted from 90, leaves  $ACD$ , 75 Degrees; and that subtracted from 180, leaves 105 Degrees, the Angle  $ACB$  required.

**CASE III.** Given as in CASE II, to find the Third Side  $BC$ .

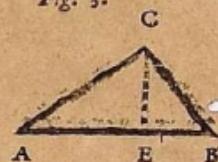
In the whole Triangle  $BDA$ , you have given the Angle  $ABD$  45, and the Hypotenuse  $BA$  560; also by Consequence, the Angle  $BAD$ , which is also 45, to find the whole Side  $BD$ ; but in this Case the acute Angles being equal, viz. 45 Degrees, the Leg  $BD$  is equal to  $AD$ , viz. 396; then having found  $CD$  106 by the second Operation in Case II, subtract it from the whole Side  $BD$  396, the Remainder 290, is the Side  $BC$  required.

CASE IV.

Given  $\begin{cases} \text{The Side } AC \ 410 \\ \text{The Side } AB \ 560 \\ \text{The Angle at } A \ 30^{\circ} \end{cases}$  Angle at B.

In the first triangle  $AEC$ , is given the Angle at  $A$   $30^{\circ}$ , and the Hypotenuse  $AC$   $410$ , to find  $CE$ , which by the first Case hereof is found to be  $205$ , and therefore I need not repeat the Operation. Then Fig. 3. in the same Triangle  $ACE$ , there is given the Sides  $AC$   $410$ , and  $CE$   $205$ , to find the Side  $AE$  by Rule III.

$$\begin{array}{rcl} AC & - & - & - & 410 & 126075(355, \text{ the Leg } AE) \\ CE & - & - & - & 205 & 9 \\ \hline & & & & & \\ \text{Sum} & - & - & - & 615 & 35360 \\ \text{Difference} & - & - & - & 205 & 325 \\ \hline & & & & & \\ & 3075 & & & 705)3575 & \\ 12300 & & & & 3525 & \\ \hline & & & & & \\ \text{Product} & - & - & - & 126075 & 50 \end{array} \quad \text{Fig. 3.}$$



The Leg  $AE$   $355$  subtracted from the whole Side  $AB$   $560$ , rests  $EB$   $205$ ; then in the Triangle  $BEC$ , you have given  $BE$   $205$ , and  $EC$   $205$ , to find  $CB$  by Rule II, and the Angle  $B$  by Rule IV, but in this Case,  $EC$  and  $EB$  being equal, the Angle at  $B$  is proved to be  $45^{\circ}$  Degrees without Calculation.

CASE V.

Given as in CASE IV, to find the third Side,  $BC$ .

Although this is the Fifth Case in the Trigonometrical Operation, yet the Side  $BC$  is necessarily found in Case IV, before the Angle at  $B$  can be found; and therefore altho' the Operation in Case IV be somewhat tedious, yet both the Fourth and Fifth Cases, are included in it.

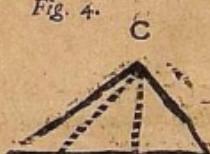
CASE VI.

Given  $\begin{cases} AB & - & - & - & 560 \\ AC & - & - & - & 410 \\ BC & - & - & - & 290 \end{cases}$  Required the Angle at A.

Find  $AE$  by the Rule laid down in Axiom IV. of Plain Triangles. As the Base  $AB$   $560$ , to the Sum of the other two Sides,  $700$ : So the Difference of the said Sides  $120$ , to the Difference of the Segments of the Base  $AD$   $150$ , as by the Operation below.

Fig. 4.

$$\begin{array}{rcl} 700 & 56.0)8400.0(150 \\ 700 & 280 \\ \hline & 84000 & .000 \end{array}$$



To the half Diff.  $75$  add the half Base  $150$ , the Sum  $355$  is the greater Base  $AE$ ; but subtracted, the Difference is the lesser Base  $EB$   $205$ .

The

Then in the Triangle  $AEC$ , there is given  $\angle C$  41°, and  $\angle E$  35°, to find  $CE$  by Rule III, and the Angle at  $A$  by Rule IV.

$$\begin{array}{rcl} \text{The Side } AC & - & 410 \\ \text{The Side } AE & - & 355 \\ \hline \end{array}$$

$$\begin{array}{r} 42075(205 \\ 405)02075 \\ \hline 2025 \end{array}$$

$$\begin{array}{rcl} \text{Their Sum} & - & 765 \\ \text{Their Difference} & - & 55 \\ \hline \end{array}$$

$$\begin{array}{r} 3925 \\ 3845 \\ \hline \end{array}$$

The square Root of 42075,  
viz. 205 is the Side  $CE$  re-  
quired.

$$\text{Product} - - - 42075$$

Then, by RULE IV, find the Angles at  $A$ .

$$\begin{array}{rcl} \text{Hypothenuse} & - & 410 \\ \text{Half the longest Leg} & - & 177.5 \\ \hline \end{array}$$

$$\text{Their Sum} - - - 587.5$$

As 587.5, to 86: So  $CE$  205, to the Angle opposite at  $A$  30°.

$$\begin{array}{rcl} 205 & 587.5)17630.2(30 & \text{The Angle at } A \\ 86 & \dots 5 & \text{Req.} \\ \hline 1230 & 50 & \\ 1640 & & \\ \hline 17630 & & \end{array}$$

Although this Method be not altogether so expeditious for oblique Triangles, as the Calculation by Logarithms, because you are obliged to divide every oblique Triangle into two right-angled ones, which sometimes requires two Operations; yet I thought fit to insert it to make the Method complete, it being of great Use when Tables are wanting, and of sufficient Exactness for most Uses in Navigation; but the right-angled Cases, as perform'd hereby, I shall recommend to the Reader, as a Thing very useful, sufficiently exact, and as expeditious as any Method commonly in Use.

To help the Memory, and shun the former Operations of finding the Natural Radius, some use the following Approximation.

If the Degrees of the Angle be between	Deg. 0° and 10°	Deg. 10° and 20°	Deg. 20° and 30°	Deg. 30° and 40°	Deg. 40° and 50°	The Natural Radius is
	57	58	59	60	61	

And for every intermediate Degree, they add  $\frac{1}{10}$  or .1 to the proper Natural Radius aforegoing, so 35° will have 60.5 for its Natural Radius.

SECT. III.

*Four Ways of laying down Traverse on Paper.*

A Traverse may be protracted four different Ways; viz.

I. By drawing new Meridians thro' the Extremity of every Course parallel to the first Meridian: then laying off the Course and Distance.

II. By laying down the Quantity of the Angle (after the first Course is protracted) between the Point next to be laid down, and the Point opposite to the Course last protracted; and so proceeding till the whole is finished.

III. Having a Circle described and divided like the *Mariner's Compass*, draw the several Courses parallel to the Rumbs in the Compass, and lay off the Distances as usual, which being done, a Line drawn from the Port left to the Place last laid down is the Distance and the Angle, which this Line makes with the Meridian, is the direct Course in all the Methods.

IV. Some have a Brass Circle cut into 32 Points of the Compass like Teeth, about the Center of which underneath a thin Brass Scale of equal Parts is made to play all round; then draw a Meridian Line on the Paper, on it set the North and South Points of the Brass Compass, and prick off the first Course and Distance by turning the Scale to the given Course, and against the Distance on the Scale make a Prick, and so draw the first Course, on which Line lay its opposite Rumb of the Brass Compass, and then turn the Scale to the second Course, and by the Scale set off its proper Distance, and so do with the rest of the Courses, all remembering to place the Compass on the last Line with that Rumb opposite to the Course last laid down.

SECT. IV.

*The Disagreement in the sundry Kinds of Sailing exemplified in Plain, Mercator, &c.*

MIDDLE Latitude Sailing is at best but an Approximation, and Approximations are to be used either when we have no direct Rule for solving the Proposition, or that by such an Approximation we save the Expence of some Trouble, neither of which is the Case before us; tis absurd to use a Multiplicity of Rules approximate, when a few direct ones will adequately and truly solve all the Cases: But some say in Voyages near the Equator, and in very short Runs, the Error is but small, which is granted; but inasmuch as its Rules are every where more or less Erroneous, it is certainly very absurd to use them, and the more so because neither Time nor Trouble is saved, the Multiplicity of Rules making more Variety of Cases than all the true ones put together, why should People burthen their Memories with such an Heap of Falsities.

Great Circle Sailing can be but of little Use in Navigation so long as Ships are steer'd by the Compass, and therefore our Author did well to omit it.

To exemplify the Disagreements of the sundry Sorts of Sailing, I shall instance the following Example: From Iceland, Lat. 66.26 to the River of

of the *Amazons* on the Equinoctial, whose Difference of Longitude suppose to be  $36^{\circ}$  W.

Sought	The Diff. of Lat. $66^{\circ}.16'$	$= 3986$ Miles.	
	The Diff. Long. $36 \dots$	$= 2160$	
According to			
	Plain Sailing	Middle Lat.	
		Mercator	
		Taral. Parts.	
Course $28^{\circ}.17'$	4.23	21.25	20.47
Dist. 4533	4376	4294	4263
By the Arch of a great Circle Distance is 4268			

Diff. in Dist.  $> 265 + 1 \quad 108 + 1 \quad 26 + 1 \quad 5 -$   
from which is

Wherefore whatsoever Method will not hold pretty near to the Truth, viz. to that by the Arch of a great Circle in long Distances, is proportionably false in short ones; and altho' the Errors are not so evident in short Voyages, yet the Aggregate or Sum of those Errors, will amount to that of a long Voyage; and therefore it is my Opinion, that neither Plain-Sailing, nor that by the Middle Latitude ought to be depended upon in any Voyage.

### SECT. V.

~~To supply the Absence of (or to form) a Table of Meridional Parts by the 3 following PROBLEMS.~~

PROB. I. To find the Meridional Parts to any given Latitude.

#### R U L E.

**T**O the given Latitude add 90, then find the Tangent of half that Sum, from which subtract the Radius, and divide the Remainder by 1263.3, the Quotient is the true Meridional Parts contain'd between the Equator and that Latitude.

*Example.* Given the Lat.  $48.30$ .

Here  $90^{\circ} + 48^{\circ}.30 = 138.30$  and the half is  $69.15$ , whose Tan. is  $10.4125142$ , deduct Radius, the Dividend is  $4125142$ , and being divided by  $1263.3$  the Quotient is  $3336.6$ , the Meridional Parts answering the Lat.  $48.30$ .

PROB. II. To find the Meridional Parts contain'd between the Latitude of any two Places in one Hemisphere

#### R U L E.

To each of the given Latitudes add 90, then find the Tangent of their half Sums as above, the Difference of these two Tangents being divided

# The SUPPLEMENT.

21

By 1263.3 the Quotient will be the true Meridional Parts contain'd between those two Latitudes.

Example. Given the Lat. 30° both N.  
And Lat. 12.14° S.

Here  $30 + 30 = 140$ , whose half is  $70^{\circ}$ , its Tangent is 10.4389341  
And  $90 + 12.14 = 102.14$  whose half is  $51^{\circ} 7'$  its Tang. is 10.0934397

Difference of the Tangents 3454944  
Which being divided by 1263.3 the Quotient is 2734.8 the Meridional Parts sought.

PROB. III. To find the Meridional Parts contain'd between the Latitudes of two Places that are in different Hemispheres.

## R U L E.

To each of the given Latitudes add 90, and find the Tangent to each of their half Sums, then add these two Tangents together and their Sum made less by twice the Radius 20.000, &c. divide the Remainder by 1263.3 the Quotient is the true Meridional Parts between the two Latitudes.

Example. Given the Lat. 14.24 N.  
And Lat. 16.3 S.

Here  $90^{\circ} + 16.3 = 106.3$  its half is  $51^{\circ} 1'. 30''$  and 3 10.1232799  
its Tangent is — — — — —  
And  $90 + 14.24 = 104.24$  its half is  $52.12$  and its 10.1103177  
Tangent is — — — — —  
Total 20 1 2335976

Which divide by 1263.3 the Quotient is 1849.1  
the meridional Parts contain'd between the 2 Latitudes.

## SECT. VI.

To Estimate the Distances of Places by Sound and Lightning.

FROM sundry Experiments it has been determin'd that Sound travels at the Rate of 1142 Feet in one Second of Time; but the Motion of Light is in a Manner instantaneous, moving 10000 Miles in a Second, wherefore, if the Difference between the Time an Explosion is first seen, and the Time that the Sound reaches the Ear be given, the Distance may easily be found.

For an English Mile contains 5280 Feet, consequently Sound requires 47.623 to travel a Mile; but a Geographical Mile according to Norwood's Experiment contains 6120 Feet. Wherefore,

As

*The SUPPLEMENT.*

As  $\{ 280 : 6120 : : 4.623 : 5.358$  Seconds Sound takes to travel a Geographical Mile. Then,

As  $\{ 4.623 \}$  So is an English Miles to the Time that Sound goes to  $\{ 5.358 \}$  even Distance in Geog. Miles quickest to travel over that Dist.

And on the Contrary,

As  $\{ 4.623 \}$  is to 1, so is the Number of Seconds between the Time a Sound is generated, and the Time it arrives at any Place to the Miles. Dist. between those two Places in Geog.

So if I counted 70 Seconds between the Sight of the Lightning and hearing the Clap of Thunder, the Distance of said Thunder was 15.14 English Miles.

The best Way of measuring Seconds is by a Watch or Clock that shews Seconds, or by the Vibration of a Plummert of 9.2 Inches betwixt the Center of the Plummert and Pin whereon it hangs; then give it a small Swing, and the Number of Vibrations equal the Number of Seconds of Time during the Experiment: if the Plummert be but 9.8 Inches, each Vibration will be but half a Second of Time.

By this may an half Minute Glass be examined

## SECT. VIII.

*By having the Time of the first New D in January, all other Aspects of the D and C may be collected throughout the whole Year by adding to.*

D. H.      "

Jan. 1, the D being New or $\sigma$ in her Age	- - - - -	00	00	00	00
For the Sextile Aspect * take		4	22	7	20
First Square □	- - - - -	7	9	11	1
Triangle Aspect Δ	- - - - -	9	20	14	41
Full D or & Opposition	- - - - -	14	18	22	2
Full D's Δ Triangle last	- - - - -	19	18	22	2
Second □ Square	- - - - -	22	3	33	2
Second * Sextile	- - - - -	24	14	26	42
Other New D or σ	- - - - -	29	12	44	3

## SECT. IX.

## SECT. IX.

*Sundry Errors and Defects in Chards, Compases,  
Quadrant, Cross-Staff, Nocturnal and Nautical  
Tables, specified with proper Helps, &c.*

TI S now above one Hundred and Fifty Years since the Errors of the plain Chard have been detected and corrected by *E. Wright*, the famous Author of what is falsely called *Mercator's Chard*, and *Mercator's Sailing*; and yet because of its Ease and Antiquity, the Plain Chard is too much in Use and Vogue among the Ignorant, tho' its very Foundation is Erroneous, supposing the Earth to be a Plane, and not a Globe, which may cause the Mariner in far northerly Voyages to err sometimes one, two, or three Points in his Course, and make his Distance double or triple the true Distance: Also by it the Proportion of the Length of Places far distant from the Equator to their Breadth is so much the more faulty, by how much the more distant they are from the Equator: the Longitude of Places on the common Sea Chard, is only true on or near the Line, because there only the Meridians and Parallels are equal; but the Parallels decrease and grow less and less towards the Poles, where all the Meridians unite and meet in a Point; wherefore, 'tis not safe to trust to these common Sea-Chards neither for Longitude, Course nor Distance of Places: much less to transfer Places from them to the Globes: All these Errors are excellently corrected by the true Chard commonly called *Mercator's*, whose Latitude, Longitude, Course and Distance of Places agree with the Globe, and ought only to be used by the expert Sailor, who desires to hit his Port and sail thither the shortest, surest and safest Way.

The Custom of drawing Rumb Lines for every Point of the Compas from several Places in the Chart, is very absurd; for these Rumbs do very much deface and obscure the Chart, so that the Places laid thereon are not so readily discern'd as otherwise they would; besides, these Rumbs are but of little or no Use, and the common Way of using them is mostly Guess-work at best; but to find the Bearing of Places without such Perplexity and Confusion of Rumb-Lines, lay the Meridian of a Protractor on the Meridian of the Chart, the Center thereof being on one Place, from which stretch a fine Thread to cut the Protractor, and the other Place; that Degree of the Protractor so cut by the Thread, gives the Bearing of said Place, in the Absence of a Bras or Horn Protractor; get one of Velom or Paitboard, having the Points of the Compas corresponding, which ought to go along with the Charts.

Tho' it can't be expected that a Chart should be more exact than the Discoveries of the Times will admit, yet it might be expected as exact and complete as those Discoveries would make it; therefore they are to blame, who let Errors pass, which they might with a little Pains have corrected; but we can expect no better, when Men that are capable decline the Task, and leave it to those to perform who know little or nothing of the Matter.

As to the Compas, the chiefest Instrument for keeping the Course; if its Variation be neglected, and no Allowance for Lee-Way be made; how many Points will the negligent Sailor miss in sundry Places? and what false Bearings and Distances of Places will he make? thus added to the false Projection

Projection of the common Sea Chart, renders it an inextricable bytinth of Error, out of which 'tis will be hard for a Man to free himself; ever, the following Cautions ought to be minded in making the Bittable or Case where the Chard is placed; great Care should be taken to make it exactly Square, or at right Angles, and so fixed that two of its Sides be exactly parallel to the true Direction of the Ship, which is generally shewn by the Crease between the two Middle Planks upon the Deck. 'Tis also a bad Custom to have two Compasses in the same Bittable, for their Attraction may make them vary half a Point from each other, which is plain if they were removed farther off, they would exactly point out the same Degree, tho' touch'd by different Magnets, provided both were good. Also to use a Slow Chard in bad Weather is absurd; for if the Chard will not Traverse, it may as well be laid aside; and consider that the apparent Motions of the Chard shews the real Motion of the Ship, and not of it self; which Motion being shewn, they have the Advantage of knowing how and when to check her, and consequently of bringing her steady much sooner. The Mariner should often examine how the Compas plays or traverses; whether if moved from its Point it will return again or stand on either Side; then examine whether the Center-Pin and Cap be free from Rust, Roughness, Bluntness, or Dirtyneſs; for the least Resistance or Friction about the Center, will very much hinder its vibration, because the attractive Power of the Magnet is small in Proportion to that of Gravity.

For the easier cleaning the Cap and Needle, 'tis no small Improvement to fasten the Glass in a Brass Ring fitted to the Head of the Box like a Surveyor's, so that at any Time it may be taken off, or lifted up with Ease, without jolting the Chard off and on, whereby the Pin is blunted and spoil'd; and besides, if the Mariner has several Chards very light fitted to the same Box, he may easily change and use which he likes best, without the Charge and Lumber of Compas-Boxes carried only for the Sake of their Chards.

Also I prefer an heavy Brass Compas to a light Wooden one: for the less the Chard is disturb'd, the nearer will it keep to its true Meridian.

As to the common Azimuth Compas, 'tis hardly practicable to observe within half a Point, notwithstanding the pretended Accuracy of some People in observing the Minutes of a Degree; for if any Observation were to be made by the common Azimuth Compas, on *Terra Firma*, (where we may have Time and Opportunity sufficient for rectifying it, which is not easily had at Sea) the said Instrument must be first of all rectified by the Help of the Chard, and this Rectification will be more or less accurate according to the Goodnes or Length of the Needle: It plainly appears then, that whatever Exactnes we pretend to by Help of the Index, is only Imaginary; since the Goodnes of the Observation entirely depends upon the Position of the Needle; for rectifying of which, the Index is of no Manner of Help to us, and consequently 'tis very absurd to pretend to make Use of it even on *Terra Firma*, but vastly more on Ship-board, where the continual Yawing of the Ship, and Motion of the Chard, render such Observations vastly uncertain, differing, and less exact than the Course pointed by the common Chard; because, when one looks downwards upon the Glass, the smalleſt Alteration in the Position of the Eye, will make an apparent Alteration in the Position of the Chard; whereas looking directly before at a Perpendicular Line drawn in the Box, we are not so lyable to err; and as the Ship and Chard are both in continual Motion, the Motion of the Chard is render'd ambiguous, and hence no Manner of Certainty, whether the Needle at the Time of Observation be in its own Meridian, or considerably to the E. or W. nor how much, we cannot judge. Again one Person continually

tinually moves the Index as the Ship yaws, and another looks through the Sight, saying, very well; as Notice he sees the Object, which Notice has given, even while the Index had moved 15 or 20 Degrees out of its former Position: And consequently the Observation must be vastly uncertain, since there is no manner of Guide, when and where to take it; nor do I like a Celestial Observation taken by two or three Hands at once, and perhaps among the Catalogue of vulgar Errors, there is not an Instance, wherein People improve more upon themselves, than in their common Notion concerning the Accuracy of Observations made by this Instrument.

### *The Description of a New Azimuth-Compass.*

**T**HIS Instrument consists of a Chard and two Boxes, and is hung in two Brass Rings after the same Manner with the common Sea-Compass, the innermost Box wherein the Chard is placed is made to turn easily in the innermost Ring without disturbing the outward Box; to the Outside of the said innermost Box are fixed two upright Sights like Surveyor's, diametrically opposite for rectifying the Instrument, by keeping the said Sights to the Object; at the Bottom of the said Box is fixed a large Piece of Lead to keep it parallel to the Horizon; within this Box are drawn two upright black Lines, exactly under the Middle of the two upright Sights, and at 90° Distance from these are drawn two other black Lines after the same Manner.

In observing look through the slit-Sight, turning till the Hair or Thread cut the Sun or Star, then hold and keep still the same Sight steady, which will stay the Instrument from being affected with the yawing of the Ship; then observe what Degree of the Chard is cut by the Perpendicular black Line under the object-Sight, for the magnet's Amplitude or Azimuth.

*Note.* 'Tis best to take the Sun's Amplitude when the lower Limb is about  $\frac{1}{4}$  above the Horizon, because the Refraction makes the Sun appear so high when his Center is really in the Horizon; but indeed for Practice, if the Place of Observation be not too far from the Equator, the Bearing of the Sun may be very well taken for an Amplitude at any Height not exceeding 2 Degrees.

This Instrument is very useful for finding the Lee-Way; and also for setting the Bearings of Head-Lands, for having directed the Index to the Wake of the Ship, the Chard will point out the true Course, the Difference of which, and the Course shewn by the Compass in the Bittacle is the Lee-Way required.

Or when the Ship is within Sight of Land, the Lee-Way may be found without setting her Wake, thus. As the Ship sails along observe carefully what Point on the Shore keeps still on the same Point of the Compass without any Alteration. I say that is the Ship's true Course, and the Difference betwixt it and the Point of the Compass the Ship capes at, is the Ship's Drift or Lee-Way.

Of Davis's ~~Sea~~<sup>Marine</sup> Quadrant, commonly called the English Quadrant.

THE common Method of fitting the Horizon-Vane slopewise, is both absurd, and leads the Observer into Error; for when the Sight-Vane and Horizon-Vane are directly in a right Line passing through the Center near the Middle of the Quadrant, the Opening in the Horizon-Vane appears so contracted, that the Horizon is not distinctly discern'd, and the said Opening will appear wider, or narrower, according as the Sight-Vane is nearer to, or farther from the Beginning of the Graduation; Whereas, the upper Edge thereof on the Foreside of the Horizon-Vane, should be made the fiducial Edge, (because the Sky is quicker discern'd than the Water) and so that it may be exactly perpendicular to the Center of the Instrument. Or let said Vane have a wide Opening, and in the Middle a String, Wire, &c. to cut the Horizon, above it, the Sky, and under it, the Water. When the Sun's Altitude exceed 12 or 15° use the Sea Quadrant, if less, use the Fore- or Cross-Staff.

Note, When Observation is made by the upper Edge of the shade-Vane, add 16' to the Zenith-Distance; for the true Zenith-Distance, if by the lower Edge of the shade-Vane, subtract 16' from the Zenith-Distance for the true; because in the first Case the Shadow is terminated by a Ray proceeding from the upper Part of the Sun's Disk, and not from its Center: In the last Case 'tis the lower Part of the Sun that determines the Shadow.

To help this, there is another Vane call'd the Glass-Vane, having a double convex Convexity in it, which contracts the Sun's Rays, and casts them in a small bright Spot upon a little Circle made upon the Horizon-Vane; this Spot being made by all the solar Rays contracted together corresponds to the Center of the Sun, and is so clear and conspicuous that even in hazy Weather the Sun's Altitude may be taken, and in clear Weather the Spot is more conspicuous than the Shadow, which at best is hardly defin'd.

### The Cross-Staff.

Whereby the Altitude of Sun, Moon and Stars is taken, and the Latitude found; and by which the dead Reckoning is corrected, both as to Course and Distance, may lead the Mariner astray, if he neglect the proper Abatement for the Eccentricity of the Eye by 20, 30, or 60 Minutes, if the Height be much, the Staff small, and the Eccentricity of the Eye great. To this may be added other proper Allowances for the Height of the Eye above the Level, for the Parallax and Refraction of the Sun: Tables of which follow:

Height of the Eye. Feet.	Allowances. Minutes.
3	2
6	3
12	4
20	5
30	6
40	7
50	8

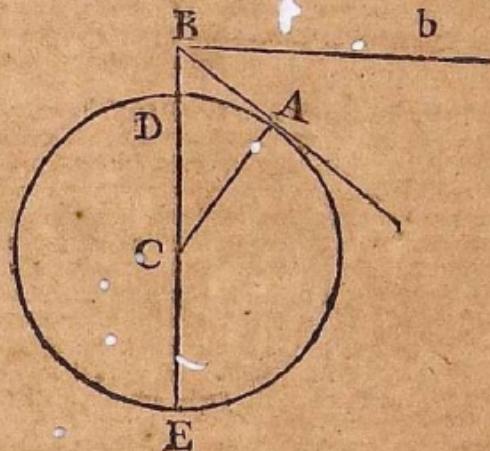
Because the Eye of the Observer is always above the Surface of the Sea, the apparent Horizon must be lower than the true Horizon (passing thro' the Eye) and consequently the Altitude must be made more than it really is, and the Zenith-Distance so much less, and this Error will be greater or less according to the Height of

of the Eye above the Water, which being known, the Dip may be found from the foregoing Table. Thus, if the Height of the Eye above the Surface be 20 Feet, the Dip of the Horizon will be 5 Minutes, and so much added to the Zenith-Distance.

*The Calculation of the above TABLE.*

Let  $DE$  = Dia. of the Earth,  
 $CD = CA$  its Semidiameter,  
and  $BD$  = Height of the Eye  
above the Surface of the Water, then will  $A$  be the Point where the Sky and Water seem to meet. Let  $Bb$  be parallel to  $DA$  (which because of the Smallness of the Arch may in this Case be taken for a right Line) then is the Angle  $ABb$  the Dip of the Horizon, to find which by Calculation, in the right-angled Triangle  $CAB$  right-angled at  $A$ , are given  $CA$  = Semidiameter of the Earth, and  $CB = (CD + DB)$  equal to the Semidiameter of the Earth together, with the Height of the Eye above its Surface; where to find the Angle  $B$  say as  $CB$  to  $CA$  so is Radius to Sine of  $B$  the Complement, whereof is  $ABb$ , the Dip required; after the same Manner  $BA$  the Semidiameter of the apparent Horizon may be found. *Euclid 3. 36.*

$BE + BD = BAq$  or  $BCq - CAq = BAq$ .



Zenith Distance. Degrees.	Add Refraction Minutes.	Dip at Parallax, Minutes.
90	33	3
89	23 $\frac{1}{3}$	3
88	17 $\frac{1}{3}$	3
87	13 $\frac{1}{2}$	3
86	10 $\frac{2}{3}$	3 $\frac{11}{12}$
85	9	2.59
84	7 $\frac{3}{4}$	2.58
83	6 $\frac{3}{4}$	2.58
82	6	2.57
81	5 $\frac{1}{3}$	2.57
80	5	2.57
79	4 $\frac{1}{3}$	2.56
77	3 $\frac{2}{3}$	2.55
75	3 $\frac{1}{4}$	2.54
70	2 $\frac{1}{3}$	2.48
60	1 $\frac{1}{2}$	2.36
50	1	2.18
30	$\frac{1}{2}$	1.30
20	$\frac{1}{3}$	1.

The Refraction of all the venly Bodies (occasion'd by the Deasity of the Atmosphere or thick Vapours of the Air) makes them appear wh they really are, especilly when they are near the Horizon, add thereto the Zenith Distance, add thereto the Refraction, subtract it from the Altitude which according to Flamsteed's Observation, is in our Latitude as in the foregoing Table. Supposing the Observor's Eye to be 20 Foot above the Surface of the Sea, and the Zenith Distance observed by the Quadrant or Cross-Staff, to be 75° the true Zenith Distance (allowing for Refraction and Dip of the Horizon) will be 75° 8'

The common Fore or Cross-Staff, is very incommodious, and also liable to Error, For, 1. Because the Vanes are made to slide towards or from the Eye, the Radius is continually alter'd from about 30 Inches, to about 8 or 9 Inches, which is a very great Defect and Inconveniencie. 2. The Manner we are obliged to hold the Instrument being Sideways from the Eye, and then look as it were slanting over the Crosses, is very awkward and unnatural; for certainly in all Observations, the Instrument which carries the Sight ought to be so contriv'd as to be held directly bewixt the Eye and the Object. Lastly 'tis difficult to place the Staff so that the Eye may exactly answer to the Center; also the Number of Crosses and so many Sets of Divisions on the Staff, and to make the Crosses keep always perpendicular to the Place of the Staff, are no small Inconveniencies.

To help all which Defects, &c. some contrive a new Sort with a flat Staff, and one transum Cross, having at the End of the Staff a Sight Vane on the transum Cross slide two Object Vanes like the Sight of a Circumferentor, one for the Stars, and the other for the Horizon, having Degrees graduated on both Sides from the End of the Staff, which Degrees in Time of Observatio be added to form the Altitude.

These Instruments can do but little Service: tho' never so well contriv'd and used, if the Declination of the Sun and Stars be not also known; wherefore new and correct Tables agreeing with Celestial Observations should not only be made for such as make the greatest Declination of the Sun, but 23° 29' not 23° 31' 30" or more, as formerly; but the proportionnal Parts agreeing to the daily Difference of Declination, and Difference of Longitude the Ship is in at Sea, should be also properly applied as the Declination either increaseth or decreases, else by such Neglect, an Error of 24' in the Latitude may happen. Moreover, the Declination of Stars in some Tables have been out in whole Degrees, and the Mariners beloved Pole Star has been made 40' farther from the Pole than it ought; wherefore Flamsteed's new Table of the Stars Rectified to the present Year, ought to be prefer'd above all other extant.

The Nocturnal is design'd for finding the Hour of the Night, and Altitude of the Pole Star; but it happens to be so imperfect as not to answer either of these Particulars. 1. For holding the Instrument in the Plane of the Equinoctial, there is no other Guide than to look through the Hole in the Middle of a thin Plane; in this Case 'tis easy to err even half a Score Degrees, both in Direction towards the North, and in the Elevation above the Horizon. Some are of Opinion a better Guess may be made with the Instrument than with it; moreover, the Pole-Star's Distance from the Pole is 20' more than it ought, and is variable both in the same and Different Latitudes.

The SUPPLEMENT

A TABLE of the Variation of the  
Ecliptic for 100 Years to E.

D.	M.	4		8		12		16		20		29		60		72		
		I	II	I	II	I	II	I	II	I	II	I	II	I	II	I	II	
Jan.	10	S	23	S	46	1S	08	1S	31	1S	54	3S	48	5S	42	7S	37	
	20	0	29	0	57	1	26	1	55	2	24	4	48	7	12	9	36	
	30	0	34	1	09	1	43	2	18	2	49	5	38	8	27	11	15	
Feb.	9	0	38	1	15	1	53	2	31	3	08	6	17	9	25	12	34	
	19	0	41	1	21	2	02	2	42	3	23	6	46	10	09	13	32	
	29	0	42	1	25	2	07	2	49	3	32	7	04	10	36	14	08	
March	10	A	43	1A	26	2A	09	2A	52	3A	35	7A	11	10A	46	14A	21	
	20	0	43	1	25	2	08	2	50	3	33	7	06	10	39	14	13	
	30	0	41	1	22	2	03	2	45	3	26	6	51	10	18	13	43	
April	9	0	39	1	17	1	56	2	34	3	13	6	26	9	39	12	51	
	19	0	35	1	09	1	44	2	19	1	54	5	48	8	42	11	37	
	29	0	30	1	00	1	30	2	00	2	29	4	59	7	28	9	58	
May	9	0	24	0	48	1	12	1	36	1	59	3	59	5	58	7	58	
	19	0	17	0	34	0	51	1	08	1	25	2	50	4	15	5	39	
	29	0	09	0	19	0	28	0	37	0	46	1	33	2	19	3	52	
June	8	0	01	0	02	0	03	0	05	0	05	0	11	0	16	0	28	
	18	S	07	S	14	S	21	S	28	0S	35	1S	10	1S	4	0	2S55	
	28	0	15	0	30	0	45	1	00	1	14	2	28	4	57	6	11	
July	8	0	22	0	44	1	06	1	28	1	50	4	44	5	27	7	21	
	18	0	28	0	57	1	25	1	54	2	22	4	45	6	07	9	29	
	28	0	34	1	07	1	41	2	15	2	49	5	8	8	27	11	16	
Aug.	7	0	38	1	16	1	54	2	32	3	10	7	20	9	30	12	39	
	17	0	41	1	22	1	03	2	44	3	25	7	50	10	15	13	39	
	27	0	43	1	26	2	09	2	52	3	37	7	10	10	45	11	55	
Sept.	6	0	44	1	27	2	18	2	55	3	38	7	17	10	55	14	53	
	16	A	43	1A	27	2A	10	2A	53	3A	37	7A	14	10A	51	14A	27	
	26	0	42	1	24	2	06	2	48	3	30	7	00	10	30	13	59	
Oct.	6	0	39	1	19	1	58	2	38	3	17	6	34	9	51	13	09	
	16	0	36	1	12	1	48	2	24	2	59	5	59	8	58	11	58	
	26	0	31	1	02	1	33	2	05	2	36	5	13	7	49	10	25	
Nov.	5	0	26	0	51	1	17	1	42	2	08	4	16	6	14	8	32	
	15	0	19	0	38	0	57	1	16	1	35	3	10	4	45	6	19	
	25	0	12	0	23	0	35	0	46	0	58	1	56	2	54	3	52	
Dec.	5	0	04	0	08	0	12	0	15	0	18	0	37	0	55	1	14	
	15	S	04	S	09	S	13	S	17	0S	21	0S	44	1S	6	1S	27	
	25	0	12	0	24	0	36	0	48	1	00	2	01	3	01	4	01	
	31	0	16	0	33	0	49	1	06	1	22	2	45	4	07	5	30	
																	6	53

SECT.

# SUPPLEMENT.

SYNOPSIS of all the possible Cases open in working an Observation at Sea.

ati- on.	Sun's Sha- dow.		R U L E .	What Lat- itude.
S°	S° d.	N° d.	Add the Declination and Zenith Distance, the Sum is the Latitude.	N°
	N° d.	S° d.		S°
N°	N° d.	S° d.	The Difference of them is the Latitude, when the Zenith Distance is greater.	S°
S°	S° d.	N° d.		N°
N°	N° d.	S° d.	But when the Zenith Distance is less than the Declination, the Difference is the Latitude.	N°
S°	S° d.	N° d.		S°
None at all.	N° d.	S° d. No Shadow.	The Zenith-Distance is the Latitude.	S° O N°
	S° d.	N° d.		
N°	On the Zenith	No Sha- dow.	The Declination is the Latitude.	N°
S°				S°

Note, { N° } stands for { North }      { S° } stands for { South }      { N.d. } stands for { Northward }      { S.d. } stands for { Southward }

O in the Latitude is nothing, consequently under the Equator.

Bewixt the 10th of March and the 12th of September, the Declination of the Sun is North, and bewixt the 12th of September and 10th of March the Declination is South.

But if the Sun or Star do not Rise or Set in 24 Hours, observe this general Rule.

If the Object ob- { under } the Pole { Sum } of the Meridian-  
serv'd be { above } { Difference }

Altitude and Complement of Declination, is the Latitude of the same Name with the Declination.

Or without the Declination, observe the Meridian-Altitude when above the Pole, and when below: Half their Sum is the Latitude.

## the Longitude by Pendulum-Watches.

1. Take at least two Watches, that if one should stop by any Misfortune or Neglect, the other may keep going.
2. Keep them close, free from Moisture or Dust.
3. Let them be well adjusted by an Equation-Table, before they be taken to Sea, and kept going while at Sea.
4. Set them to the exact Moment of Time observed by the Sun in the Place left, regarding the Equation-Number.
5. Then arriving at the Place whose Longitude is sought, observe exactly the Time by the Sun in that Place, and also by the Watch, allowing for the Equation; if they both agree exactly, there is no Difference of Longitude. But if the Time of the Day there, be greater than that shewn by the Watches, then the Difference of Longitude is Easterly: but if less Westerly.
6. Convert the Difference of Time into Degrees, which will be the Difference of Longitude in Degrees with greater Exactness than those Ways that depend upon Tables, so various among themselves, such as Calculations of Lunar-Eclipses, &c. which are as laborious as uncertain, and their true Beginning or Ending are scarce to be distinguished for some Minutes, by Reason of the Penumbra: tho' four Minutes in Time will alter the Longitude a whole Degree.
7. To convert Time into Degrees, or Degrees into Time.

	Time.				Measure.	
	Hour.	Min.	Sec.		Min.	
Remember	1	0	0		0	
	0	4	0	{	1	0
	0	1	0		0	15
	0	0	4		0	1
				is equal to		
Thus	3	42	32	=	55	38
For	3	0	0	=	45	0
	40	0	0	=	10	0
	2	0	0	=	0	30
	0	32	0	=	0	8

8. Wherefore, considering the vast Improvement in Watch-work by the Learned Dr. Hook, the Ingenious Huyghens, &c. whose very first Work, being try'd by Major Holm's, prov'd both Satisfactory and Useful, in a great Streight, and met with Commendation, and the Approbation of the States of Holland; Insomuch that he obtain'd a Patent for them; this seems for its Readiness, and because done by one alone, no despisable Way, tho' not infallible.

*To learn the Names of the most noted Stars by*

Rectify the Globe to the Latitude, Day, and Hour of the Day, then in every Star on the Circle Tread a Hole, and the Eye was placed in the very Center of the Globe, and looking thro' each Hole, a direct Ray from the Eye thro' the Center of the Star if extended to the Firmament, would cut the same Star in the Heavens, which that Star on the' Globe represented: if the Globe was duly rectified and set exactly level, and the Meridian due North, then would the Stars that be,

Rising	{	Rising	{
On the Meridian		On the Meridian	
On the Zenith		On the Zenith	
Setting		Setting	
On any Azimuth		On the same Azimuth	
On any Almicanter		On the same Almicanter	

Wherefore, take the Azimuth or Amplitude by a Compass, or Altitude by a Quadrant of any Star whose Name is desired, and find what Star hath the same Altitude or Azimuth by it is either its Name, or what Part of the Constellation it possesses, as also its Magnitude, &c. It may be objected, that the Planets  $\text{\texttt{V}}$ ,  $\text{\texttt{J}}$ , and  $\text{\texttt{S}}$  especially, may cause the young Beginner to mistake, wherefore this shall be the next Problem.

*To distinguish the Planets from the fixed Stars.*

1. Planets don't twinkle commonly.
2. They are bigger than ordinary.
3.  $\text{\texttt{V}}$  and  $\text{\texttt{S}}$  especially. They are of differing Colors,  $\text{\texttt{V}}$  of a leaden Color, and of the 3<sup>d</sup> Magnitude,  $\text{\texttt{V}}$  bigger than the first, of a Silver-Color,  $\text{\texttt{J}}$  of the second Magnitude, of a Copper-Color,  $\text{\texttt{S}}$  bigger than  $\text{\texttt{V}}$  of a Glittering Color like new-coin'd Silver,  $\text{\texttt{S}}$  of the third Size, Pale-White, like Quick-silver, never above thirty Degrees from the Sun, seldom seen but when he rises before the Sun, or sets just after the Sun,
4. They shew their Places in a Week or two observably from some known fixed Star.
5. Consult an Ephemeris to see in what Sign the Planets are, and if they are not in the Sign observed, know it is a fixed Star.

*To steer in the Night by the fixed Stars.*

1. Rectify the Globe to the Latitude and Hour of the Day.
2. Then turn the Globe till the Difference of Longitude has passed thro' the Meridian, that is betwixt the Place left and the Place sail'd to.
3. If any Star in the Latitude and Longitude aim'd at, come to or near the Meridian, that Star is then in or near the Zenith of the Port desired. Then direct the Ship towards the same Star in the Heavens without Fear, still observing what Star is in or near the Zenith of the Place sail'd to.